**LASERS**

# **Multiwavelength Generation of Stokes Radiation Components with a Small Wavelength Spacing under Stimulated Raman Scattering in a SrMoO<sub>4</sub> Crystal**

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**Abstract**—Theoretical and experimental studies were conducted on providing conditions for the generation of multiple radiation components with a small wavelength spacing in a crystalline synchronously pumped SRS laser with combined frequency shift on high-frequency and low-frequency vibrational modes of an SRS-active crystal. A theoretical analysis has shown an important role of four-wave parametric Raman interactions on the low-frequency vibrational mode of the crystal provided the conditions of coherence and of nonlinear phase capture of such interactions are satisfied. For the first time, SRS generation was carried out at five closely spaced wavelengths of 1194, 1242, 1294, 1336, and 1396 nm in a SrMoO<sub>4</sub> crystal under synchronous pumping by a high intensity picosecond YAlO<sub>3</sub>:Nd<sup>3+</sup> laser at a wavelength of 1079 nm satisfying the condition of nonlinear phase capture.

**Keywords:** stimulated Raman scattering, first and second crystal vibrational modes, spectrally multiplexed multiwavelength generation

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# 1. INTRODUCTION

Multiwavelength radiation sources with a small wavelength spacing are becoming increasingly popular nowadays due to the advancement of microelectronics, optical communications, physics, chemistry, and biomedicine. Their main application today is spectrum multiplexing of optical communication channels. The key areas of research worldwide are the creation of such emitters based on semiconductor [1] and fiber-optic [2] quantum electronics. However, we have to use solid-state laser sources in laser impact tasks to overcome the problem of optical breakdown of the active medium. Multiwavelength generation can be carried out in solid-state quantum electronics by stimulated Raman scattering (SRS) in crystals (see, e.g., [3]), but the SRS-based laser frequency conversion is usually accompanied by a large frequency shift on the most intense high-frequency vibrational mode of a crystal. The participation of second low-frequency vibrational modes can reduce the wavelength spacing between generated SRS radiation components. This multiwavelength generation with a small wavelength spacing was carried out for the first time in a  $BaWO_4$ crystal based on nanosecond SRS with combined frequency shift simultaneously on the high-frequency and low-frequency vibrational modes [4]. The generation was achieved at four wavelengths (554, 564, 575, and 583 nm) in the visible spectral range using second-harmonic pumping of a neodymium laser with a wavelength of 527 nm. Similar operations were performed later using SRS on two vibrational modes of KGd(WO<sub>4</sub>)<sub>2</sub> [5], GdVO<sub>4</sub> [6], and YVO<sub>4</sub> [7] crystals. A series of operations has been performed recently with synchronously pumped SRS on combined vibrational modes in various crystals under pumping with a wavelength of 1063 nm [8–10] to achieve multiwavelength generation in the near-infrared range, which is more relevant for telecommunication applications. The use of transient SRS regime under synchronous picosecond pumping was shown to increase the efficiency of multiwavelength SRS generation on combined vibrational modes. For instance, SRS generation was implemented in  $[8]$  using a SrWO<sub>4</sub> crystal at four closely spaced wavelengths of 1178, 1227, 1279, and 1321 nm for different combinations of highfrequency and low-frequency shifts. This was due to the fact that the generation efficiency under the transient SRS regime depends on the integral Raman cross section, which has close values for the first (symmetric stretching) and second (symmetric bending) vibrational modes in tetragonal crystals because the second (less intense) mode is spectrally broad.

This paper is devoted to the search for conditions of the efficient SRS generation of a large number of spectrally multiplexed Stokes radiation components on combined vibrational modes. A theoretical study indicating the important role of four-wave parametric Raman interactions on the low-frequency vibrational mode of an SRS-active crystal has been carried out. SRS generation at five closely spaced wavelengths (1194, 1242, 1294, 1336, and 1396 nm) in a  $SrMoO<sub>4</sub>$  crystal under high-intensity synchronous pumping by a picosecond YAlO<sub>3</sub>:Nd<sup>3+</sup> laser with a wavelength of 1079 nm has been experimentally realized for the first time.

### 2. THEORY

The interaction of radiation with two vibrational modes of an SRS-active crystal can be described as follows:

$$
\frac{\partial^2 E}{\partial z^2} - \frac{1}{c^2} \frac{\partial^2 (\varepsilon E)}{\partial t^2} = \frac{4\pi}{c^2} N_1 \frac{\partial \alpha}{\partial Q_1} \frac{\partial^2 (Q_1 E)}{\partial t^2} + \frac{4\pi}{c^2} N_2 \frac{\partial \alpha}{\partial Q_2} \frac{\partial^2 (Q_2 E)}{\partial t^2},\tag{1}
$$

$$
\frac{\partial^2 Q_1}{\partial t^2} + \frac{2}{\tau_1} \frac{\partial Q_1}{\partial t} + \Omega_1^2 Q_1 = \frac{1}{2m_1} \frac{\partial \alpha}{\partial Q_1} E^2,
$$
\n(2)

$$
\frac{\partial^2 Q_2}{\partial t^2} + \frac{2}{\tau_2} \frac{\partial Q_2}{\partial t} + \Omega_2^2 Q_2 = \frac{1}{2m_2} \frac{\partial \alpha}{\partial Q_2} E^2,
$$
\n(3)

where  $Q_1$  and  $Q_2$  are the amplitudes of the first and second vibrations, respectively (e.g., the first vibration is the symmetric stretching mode of internal vibrations of the anionic group of a scheelite-like crystal and the second vibration is the symmetric bending mode of internal vibrations of the same anionic group);  $\Omega_{1,2} = 2\pi v_{1,2}c$  is the central cyclic frequency of the first and second vibrational modes ( $\Omega_1 > \Omega_2$ );  $v_{1,2}$  and  $\tau_{1,2}$  is the wave number and dephasing time of the first and second vibrational modes;  $m_{1,2}$  and  $N_{1,2}$  is the effective mass and concentration of vibrating particles participating in the first and second vibrations;  $\partial\alpha/\partial\c O_{1,2}$  is the medium polarizability variation under the action of the first and second vibrations; *c* is the light speed in vacuum. The model (1)–(3) differs from the classical SRS model [11] by the presence of an additional constitutive equation (3) for the forced vibration of the crystal on the second vibrational mode and of an additional (last) summand in the wave equation (1) to account for this additional vibration.

We assume that the SRS-active crystal is placed in an optical resonator with a high quality factor for the spectral region containing not only the first Stokes component of SRS radiation with high-frequency shift  $(\Omega_1)$ , but also the next two (second and third) Stokes components with an additional low-frequency shift ( $\Omega_2$ ). Let the index *p* denote the pump wave with frequency  $\omega_p$  and wavelength  $\lambda_p$ ; index S denote the first SRS radiation Stokes component with high-frequency shift (the frequency  $\omega_s = \omega_p - \Omega_1$ , wavelength  $\lambda_S = (\lambda_P^{-1} - v_1)^{-1}$ ); index Ss denote the second Stokes component with an additional low-frequency shift (the frequency  $\omega_{Ss} = \omega_S - \Omega_2$ , wavelength  $\lambda_{Ss} = (\lambda_S^{-1} - v_2)^{-1}$ ); index Sss denote the third Stokes component with another additional low-frequency shift (the frequency  $\omega_{\rm Sss}=\omega_{\rm Ss}-\Omega_2$ , wavelength  $\lambda_{\rm Sss}=(\lambda_{\rm Ss}^{-1}-\nu_2)^{-1}$ ). Then the light field and the amplitudes of medium vibrations in the approximation of slowly varying amplitudes can be written as

$$
E = \frac{1}{2} E_{\rm p} \exp(i\omega_{\rm p}t - i k_{\rm p}z) + \frac{1}{2} E_{\rm s} \exp(i\omega_{\rm s}t - i k_{\rm s}z)
$$
  
+ 
$$
\frac{1}{2} E_{\rm ss} \exp(i\omega_{\rm ss}t - i k_{\rm ss}z) + \frac{1}{2} E_{\rm Sss} \exp(i\omega_{\rm Sss}t - i k_{\rm Sss}z) + \text{c.c.},
$$
 (4)

$$
Q_1 = \frac{1}{2}q_1 \exp[i\Omega_1 t - i(k_P - k_S)z] + c.c.,
$$
 (5)

$$
Q_2 = \frac{1}{2} q_2 \exp[i\Omega_2 t - i(k_s - k_{ss})z] + \text{c.c.},
$$
\n(6)

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where  $E_j$ ,  $\omega_j$ , and  $k_j$  are a slowly varying amplitude, frequency, and the wave number for each radiation component  $(j = p, S, Ss, Sss)$ ;  $q_1$  and  $q_2$  are the slowly varying amplitudes of the first and second medium vibration. The substitution of the expressions (4) to (6) into the wave equation (1) yields the following system of shortened wave equations for each presented radiation component:

$$
\frac{\partial E_{\rm p}}{\partial z} + \frac{1}{u_{\rm p}} \frac{\partial E_{\rm p}}{\partial t} = -i \frac{\pi \omega_{\rm p}}{n_{\rm p}c} N_1 \frac{\partial \alpha}{\partial Q_1} E_{\rm s} q_1 - \frac{\beta}{2} E_{\rm p},
$$
\n
$$
\frac{\partial E_{\rm S}}{\partial z} + \frac{1}{u_{\rm s}} \frac{\partial E_{\rm S}}{\partial t} = -i \frac{\pi \omega_{\rm S}}{n_{\rm s}c} N_1 \frac{\partial \alpha}{\partial Q_1} E_{\rm p} q_1^* - i \frac{\pi \omega_{\rm S}}{n_{\rm s}c} N_2 \frac{\partial \alpha}{\partial Q_2} E_{\rm s} q_2 - \frac{\beta}{2} E_{\rm s},
$$
\n
$$
\frac{\partial E_{\rm S}}{\partial z} + \frac{1}{u_{\rm S}} \frac{\partial E_{\rm S}}{\partial t} = -i \frac{\pi \omega_{\rm S}}{n_{\rm s}c} N_2 \frac{\partial \alpha}{\partial Q_2} E_{\rm s} q_2^* - i \frac{\pi \omega_{\rm S}}{n_{\rm s}c} N_2 \frac{\partial \alpha}{\partial Q_2} E_{\rm s} q_2 \exp(-i\Delta k_2 z) - \frac{\beta}{2} E_{\rm s},
$$
\n(7)\n
$$
\frac{\partial E_{\rm Sss}}{\partial z} + \frac{1}{u_{\rm Sss}} \frac{\partial E_{\rm Sss}}{\partial t} = -i \frac{\pi \omega_{\rm Sss}}{n_{\rm s}c} N_2 \frac{\partial \alpha}{\partial Q_2} E_{\rm s} q_2^* \exp(i\Delta k_2 z) - \frac{\beta}{2} E_{\rm Sss},
$$
\n(7)

where *uj* is the group velocity of the *j*th radiation component; *nj* is the refractive index of the *j*th radiation component;  $\Delta k_2 = k_s + k_{Sss} - 2k_{Ss}$  is the wave mismatch of the parametric four-wave coupling of the SRS radiation components with a low-frequency relative shift. The last summand describing linear losses in the medium with the harmful loss factor  $\beta$  was formally introduced into the equations of (7). The substitution of (4) to (6) into the material equations (2) and (3) yields shortened material equations of the first and second vibrations of the SRS-active crystal:

$$
\frac{\partial q_1}{\partial t} + \frac{1}{\tau_1} q_1 = -i \frac{1}{4m_1 \Omega_1} \frac{\partial \alpha}{\partial Q_1} E_p E_s^*,
$$
\n
$$
\frac{\partial q_2}{\partial t} + \frac{1}{\tau_2} q_2 = -i \frac{1}{4m_2 \Omega_2} \frac{\partial \alpha}{\partial Q_2} [E_S E_{SS}^* + E_{SS} E_{SS}^* \exp(i \Delta k_2 z)].
$$
\n(8)

We find the following expressions in steady-state approximation ( $\partial q_{1,2}/\partial t = 0$ ) for the steady-state SRS gain of SRS radiation Stokes components on the first and second vibrational modes (in terms of radiation intensity):

$$
g_1 = \frac{4\pi^2 \omega_s N_1 \tau_1}{m_1 \Omega_1 c^2 n_s n_p} \left(\frac{\partial \alpha}{\partial \Omega_1}\right)^2,
$$
  
\n
$$
g_2 = \frac{4\pi^2 \omega_{ss} N_2 \tau_2}{m_2 \Omega_2 c^2 n_{ss} n_s} \left(\frac{\partial \alpha}{\partial \Omega_2}\right)^2,
$$
\n(9)

which are experimentally measurable characteristics.

We write the system of equations (7), (8) through the experimentally measured characteristics. For this purpose, we introduce modified vibration amplitudes similarly as it was done in [12]:

$$
\overline{q}_1 = q_1 \frac{m_1 \Omega_1 c^2 n_p n_s}{4 \omega_s \partial \alpha / \partial Q_1},
$$
\n
$$
\overline{q}_2 = q_2 \frac{m_2 \Omega_2 c^2 n_s n_{ss} n_{ss}}{4 \omega_{ss} \partial \alpha / \partial Q_2}.
$$
\n(10)

Then we get the final model. The system of wave equations:

$$
\frac{\partial E_{\rm p}}{\partial z} + \frac{1}{u_{\rm p}} \frac{\partial E_{\rm p}}{\partial t} = -ig_1 \Delta v_1 \frac{\omega_{\rm p}}{n_{\rm p}} E_{\rm s} \overline{q}_1 - \frac{\beta}{2} E_{\rm p},
$$
\n
$$
\frac{\partial E_{\rm s}}{\partial z} + \frac{1}{u_{\rm s}} \frac{\partial E_{\rm s}}{\partial t} = -ig_1 \Delta v_1 \frac{\omega_{\rm s}}{n_{\rm s}} E_{\rm p} \overline{q}_1^* - ig_2 \Delta v_2 \frac{\omega_{\rm s}}{n_{\rm s} n_{\rm sss}} E_{\rm s} \overline{q}_2 - \frac{\beta}{2} E_{\rm s},
$$
\n
$$
\frac{\partial E_{\rm ss}}{\partial z} + \frac{1}{u_{\rm ss}} \frac{\partial E_{\rm ss}}{\partial t} = -ig_2 \Delta v_2 \frac{\omega_{\rm ss}}{n_{\rm ss} n_{\rm sss}} E_{\rm s} \overline{q}_2^* - ig_2 \Delta v_2 \frac{\omega_{\rm ss}}{n_{\rm ss} n_{\rm sss}} E_{\rm sss} \overline{q}_2 \exp(-i \Delta k_2 z) - \frac{\beta}{2} E_{\rm ss},
$$
\n
$$
\frac{\partial E_{\rm ss}}{\partial z} + \frac{1}{u_{\rm ss}} \frac{\partial E_{\rm sss}}{\partial t} = -ig_2 \Delta v_2 \frac{\omega_{\rm sss}}{n_{\rm ssss}^2} E_{\rm sss} \overline{q}_2^* \exp(i \Delta k_2 z) - \frac{\beta}{2} E_{\rm sss},
$$
\n(11)

$$
\frac{\partial \overline{q}_1}{\partial t} + \frac{1}{\tau_1} \overline{q}_1 = -i \frac{c^2 n_p n_s}{16 \omega_s} E_p E_s^*,
$$
\n
$$
\frac{\partial \overline{q}_2}{\partial t} + \frac{1}{\tau_2} \overline{q}_2 = -i \frac{c^2 n_s n_{ss} n_{ss} s s_s}{16 \omega_{ss}} [E_s E_s^* + E_{ss} E_s^* \exp(i \Delta k_2 z)].
$$
\n(12)

An analysis of the system of equations (11), (12) has shown that according to (9) the SRS gain is determined by the coefficient  $g_{1,2}$ ; therefore, the second vibrational mode loses competition to the first mode because  $g_2 < g_1$ . In the essentially transient mode, when the second summand on the left side of the equations (12) can be neglected, the SRS gain on both vibrational modes depends on the characteristic parameter  $g_{1,2}\Delta v_{1,2}$ , so it is necessary to select a crystal for SRS on combined vibrational modes, for which  $g_2\Delta v_2$ is close to  $g_1 \Delta v_1$  (in other words, the integral cross sections for the first and second vibrational modes are about equal).

Tetragonal crystals, in particular scheelite-like crystals for which  $g_2\Delta v_2 \approx g_1\Delta v_1$  due to  $\Delta v_2 > \Delta v_1$ , are suitable for this problem [8, 13]. We chose the  $SrMoO<sub>4</sub>$  crystal as the test object because it has the broadest line of the second vibrational mode with a relatively high SRS gain coefficient among scheelite-like crystals [8]. We have the following characteristics for  $SrMoO<sub>4</sub>$  under the action of pumping by radiation polarized perpendicular to the crystal's optical axis:  $v_1 = 888 \text{ cm}^{-1}$ ,  $\Delta v_1 = 2.6 \text{ cm}^{-1}$  and  $g_1 = 5.6 \text{ cm/GW}$  for  $\lambda_p \approx 1.06$  µm [14];  $v_2 = 327$  cm<sup>-1</sup>,  $\Delta v_2 = 10.5$  cm<sup>-1</sup>, and  $g_2 \approx g_1 J_2 / J_1 = 1.17$  cm/GW ( $J_{1,2}$  are the intensities of the first and second vibrational modes in the Raman spectrum) for  $\lambda_p \approx 1.06$  µm [8]. The values of the characteristic parameters for the first and second vibrational modes are close:  $g_1 \Delta v_1 = 14$  GW<sup>-1</sup> and  $= 12.3$  GW<sup>-1</sup>. This should provide the transient SRS with combined frequency shift. Another reason for the crystal selection is the well-known data on the refractive index dispersion of the  $SrMoO<sub>4</sub>$  crystal throughout its region of transparency [15]. This made it possible to calculate the wave mismatch of the partially degenerate four-wave parametric interaction processes on the first and second vibrational modes [11]:  $v_2$  = 327 cm<sup>-1</sup>,  $\Delta v_2$  $g_2 \Delta v_2$ 

$$
\Delta k_{1,2} = k_{p,S} + k_{Ss,Sss} - 2k_{S,Ss} = (n_{p,S} + n_{Ss,Sss} - 2n_{S,Ss})2\pi\lambda_{S,Ss}^{-1} + (n_{p,S} - n_{Ss,Sss})2\pi\nu_{1,2}.
$$
 (13)

For  $\lambda_p = 1079$  nm, it has a relatively low  $\Delta k_2 = 4.4$  cm<sup>-1</sup> on the second vibrational mode compared to  $\Delta k_1 = 34.9 \text{ cm}^{-1}$  on the first vibrational mode owing to  $v_2 < v_1$ . That is why the four-wave interaction of the SRS radiation components with the low-frequency relative shift is accounted for in model (11), (12), but the high-frequency relative shift is disregarded.

# 3. NUMERICAL MODELING

We assumed in numerical modeling that the SRS-active crystal was placed in a ring resonator whose length is equal to the pump pulse repetition period in order to carry out synchronous single-pass pumping by a series of ultrashort pulses. Therefore, the numerical calculation of the system of equations (11), (12) describing the single-pass SRS was made repeatedly so that corresponding output parameters of the previous calculation of the amplitudes of the SRS radiation component were taken as input values of the amplitudes in each subsequent calculation of single-pass SRS. The dephasing time ( $\tau_{1,2}$ ) was believed to be significantly shorter than the pump pulse repetition period and thus the vibrational amplitudes were supposed to be equal to zero at the start of each calculation that followed. So, the pump pulse repetition period had no effect in the calculations on the simulated SRS process. In order to save computational time, the pump pulse repetition period was chosen as short as possible being equal to three times the duration of the Gaussian pump pulse. The duration of Gaussian pump pulses was set to be 43 ps at level 1/*e* (36 ps at half-maximum). The output parameters of each calculation also took into account useful loss of the resonator having an output mirror with reflection coefficients  $R_S = 99\%$ ,  $R_{SS} = 96\%$ , and  $R_{SS} = 92\%$ at wavelengths  $\lambda_s = 1194$  nm,  $\lambda_{Ss} = 1242$  nm, and  $\lambda_{Sss} = 1294$  nm under pumping at a wavelength  $\lambda_p$  = 1079 nm. The harmful loss factor β was set to be 0.005 cm<sup>-1</sup>. The resonator was chosen to be highly adequate for the first Stokes component ( $\lambda_S$ ) in the interest of stimulating the SRS stage with an additional low-frequency shift. The model does not take into account the generation of the second Stokes compo-



**Fig. 1.** The results of calculating SRS processes for a 3 cm long SrMoO<sub>4</sub> crystal under synchronous pumping by a series of pulses with peak intensities of 0.15 (a), 0.9 (b), and 4.9 GW/cm<sup>2</sup> (c) (the blue curves indicate pump radiation  $(I_p)$ , the green curves indicate the first Stokes component  $(I_S)$ , the orange curves indicate the second Stokes component  $(I_S)$ , and the red curves indicate the third Stokes component  $(I_{SSS})$ ; the green, orange and red arrows indicating the generation thresholds of the first, second and third Stokes components, respectively).

nent with high-frequency shift under the assumption of low quality factor of the resonator at its wavelength  $(\lambda_{ss} = (\lambda_s^{-1} - v_1)^{-1} = 1335 \text{ nm})$ . The intensity of the radiation components was defined as  $I_j = |E_j|^2 c n_j / 8\pi$ . |

Figure 1 shows the results of calculating SRS processes for a  $SrMoO<sub>4</sub>$  crystal 3 cm long under synchronous pumping by a series of picosecond pulses with peak intensities of 0.15 (Fig. 1a), 0.9 (Fig. 1b), and 4.9 GW/cm2 (Fig. 1c).

It can be seen from Fig. 1 that with a low pump intensity of 0.15 GW/cm<sup>2</sup> (Fig. 1a) the generation threshold of the first SRS radiation Stokes component with high-frequency shift (green line) can be reached at a pump pulse number of 33. The generation thresholds of the second and third SRS radiation Stokes components with additional low-frequency shifts (orange and red lines) are reached at pump pulse numbers of 54 and 57, respectively. This is a cascade mode of SRS conversion with suppressed Ramanparametric coupling due to violation of its coherence condition ( $\Delta k_2 L \leq \pi$ ).

Higher pump intensity up to  $0.9 \text{ GW/cm}^2$  (Fig. 1b) reduces the threshold values of the pump pulse number to 6, 12, and 13 for the first, second, and third Stokes components of SRS radiation, respectively. It is important that the generation threshold of the third Stokes component approaches the generation threshold of the second Stokes component. Consequently, the influence of parametric Raman four-wave coupling is enhanced, which can be explained by nonlinear phase capture of interacting waves [16].

A further increase in the pump intensity up to 4.9  $GW/cm^2$  (Fig. 1c) at which the generation threshold of the first Stokes component is reached already under the action of the first pulse leads not only to a decrease in the generation thresholds, but also to their equalization for higher (second and third) Stokes components of SRS radiation, which ensures simultaneous generation of several Stokes components with a low-frequency relative shift.

In terms of theory [16–18], the effect of nonlinear phase capture of the parametric Raman interaction occurs when the following condition is satisfied:

$$
\frac{\Delta k}{gI_{\rm p}} < 1,\tag{14}
$$

where Δ*k* is the wave mismatch of the parametric four-wave interaction; *g* is the SRS gain coefficient;  $I_p$  is the pump radiation intensity of the parametric Raman interaction. Then it is possible to introduce a critical pump intensity of the parametric Raman interaction which, if exceeded, ensures nonlinear capture of the phases of this interaction on the first or second vibrational mode:

$$
I_{\text{cr1,2}} = \frac{\Delta k_{1,2}}{g_{1,2}}.\tag{15}
$$

So the interaction on the first vibrational mode of the SrMoO<sub>4</sub> crystal ( $\Delta k_1 = 34.9$  cm<sup>-1</sup>,  $g_1 = 5.6$  cm/GW) requires a very high pump intensity,  $I_p > I_{cr1} = 6.2$  GW/cm<sup>2</sup>; however, for the parametric Raman interaction on the second vibrational mode of SrMoO<sub>4</sub> ( $\Delta k$ <sub>2</sub> = 4.4 cm<sup>-1</sup>, *g*<sub>2</sub> = 1.17 cm/GW), the critical intensity decreases to  $I_{cr2} = 3.7$  GW/cm<sup>2</sup>.

Our process of synchronously pumped SRS with combined frequency shift can be represented as the first stage of conversion by means of SRS with high-frequency shift and the second stage of parametric Raman conversion with low-frequency shift. Then the role of the pump radiation of the four-wave interaction is played at a separate second conversion stage by the first Stokes component with wavelength  $\lambda_s$ that has a parametric Raman coupling with the second ( $\lambda_{ss}$ ) and third ( $\lambda_{ss}$ ) components. The condition of nonlinear phase capture of such parametric Raman interaction is written as  $I_{\text{Stokes}} > I_{\text{cr2}}$  where  $I_{\text{Stokes}} =$  $I_{S}/(1 - R_{S})$  is the intraresonator intensity of the first Stokes component and  $I_{S}$  is its output intensity.

The calculation showed (see Fig. 1) that the output intensity of the first Stokes component at the generation threshold of this component was  $I_s = 0.02, 0.05$ , and 0.13 GW/cm<sup>2</sup> for pump intensities  $I_p = 0.15$ , 0.9, and 4.9 GW/cm<sup>2</sup>, respectively. And the intraresonator intensity of the first Stokes component was  $I_{\text{Stokes}} = 0.5I_{\text{cr2}}$ , 1.3*I*<sub>cr2</sub>, and 3.5*I*<sub>cr2</sub>, respectively ( $\Delta k = 4.4$  cm<sup>-1</sup>, *g*<sub>2</sub> = 1.17 cm/GW, and *R*<sub>S</sub> = 0. 99).

Thus, in the first case with  $I_p = 0.15$  GW/cm<sup>2</sup> (Fig. 1a), the condition  $I_{\text{Stokes}} > I_{\text{cr2}}$  is not fulfilled, the intermediate case  $I_p = 0.9$  GW/cm<sup>2</sup> (Fig. 1b) is approximately at the limit of fulfillment of this condition, and the higher pump intensity  $I_p = 4.9 \text{ GW/cm}^2$  (Fig. 1c) fully supports the fulfillment of this condition. Therefore, it can be assumed that we can be guided by a simpler condition  $I_p > I_{cr2} = 3.7$  GW/cm<sup>2</sup> in order to ensure completely the effect of nonlinear phase capture.

Figure 2 displays calculated dependences of the output pulse intensity of the third Stokes component  $(I_{\text{Sss}})$  normalized to the input pump intensity  $(I_{\text{p}})$  on the length of the SRS-active crystal (*L*) for the pump pulse with the indicated number at  $I_pL = 0.45$  GW/cm (Fig. 2a) and  $I_pL = 5.7$  GW/cm (Fig. 2b).

Figure 2a demonstrates the case of low-intensity pumping whereby the condition of nonlinear phase capture  $I_{\text{Stokes}} > I_{\text{cr2}}$  is not satisfied except for the shortest crystal length ( $L = 0.5$  cm,  $I_p = 0.9$  GW/cm<sup>2</sup>) for which  $I_{\text{Stokes}} = 1.3 I_{\text{cr2}}$ . The generation of the third Stokes component is shown for three numbers (56, 57, and 58) of the pump pulse which overcome the generation threshold of the second Stokes component. It should be noted that Fig. 1a corresponds to Fig. 2a for *L* = 3 cm. The generation threshold of the second Stokes component is reached at the 54th pump pulse (see the orange arrow in Fig. 1a), and the same is observed irrespective of the crystal length for a constant value of  $I<sub>p</sub>L$ .

In Fig. 2a, there is a characteristic dependence of the generation intensity reduction when the condition of nonlinear interaction coherence is violated [19],  $\Delta k<sub>2</sub>L<\pi$  being the effective generation of the third Stokes component at  $L \leq 1.5$  cm. It can be concluded that in the case of low-intensity pumping where the condition of nonlinear phase capture  $I_{\text{Stokes}} > I_{\text{cr2}}$  is violated it is necessary to reduce the length of the SRS-active crystal for multiwavelength generation of Stokes components with low-frequency shift. It agrees with earlier experiments on SRS generation in an SrWO<sub>4</sub> crystal under synchronous picosecond pumping with low intensity up to 0.4 GW/cm<sup>2</sup> [8, 20]. The long SrWO<sub>4</sub> crystal ( $L = 3.6$  cm) [20] produced the generation of only the first ( $\lambda_s$ ) and second ( $\lambda_{ss}$ ) Stokes components while in a short SrWO<sub>4</sub> crystal ( $L = 1.4$  cm) under similar experimental conditions [8], an additional third ( $\lambda_{\rm sss}$ ) Stokes component with combined frequency shift was generated due to the maintenance of the coherence condition.

Figure 2b shows the case of high-intensity pumping that fulfills the condition of nonlinear phase capture  $I_{\text{Stokes}} > I_{\text{cr2}}$  except for the longest crystals ( $L > 5.5$  cm,  $I_{\text{p}} < 1$  GW/cm<sup>2</sup>). The generation of the third Stokes component is shown for three numbers  $(8, 9, \text{ and } 10)$  of the pump pulse where the generation threshold of the second Stokes component is overcome. It can be seen that the reduction of generation efficiency with crystal length is observed only at the 8th pump pulse, but at the next (9th and 10th) pump pulses the dependence even starts to increase slowly, which demonstrates the nonlinear phase capture of the parametric Raman interaction. It can be concluded that it is advantageous to increase the crystal length for the multiwavelength generation of the SRS radiation Stokes components with low-frequency shift under high-intensity pumping that supports the fulfillment of the condition of nonlinear phase capture.



**Fig. 2.** The calculated dependences of the output pulse intensity of the third Stokes component  $(I_{SS})$  normalized to the input pump intensity  $(I_p)$  on the SrMoO<sub>4</sub> crystal length for a pump pulse with the indicated number at  $I_pL = 0.45$  (a) and 5.7 GW/cm (b).

## 4. AN EXPERIMENTAL STUDY AT HIGH-INTENSITY PUMPING

We have performed an experiment on SRS in a long (7 cm)  $SrMoO<sub>4</sub>$  crystal under the action of highintensity synchronous picosecond pumping that satisfied the condition that nonlinear phase capture  $(I_p$  $I_{\text{cr2}}$  = 3.7 GW/cm<sup>2</sup>) should be fully achieved. The optical scheme of the experiment is presented in Fig. 3.

The radiation from the YA1O<sub>3</sub>: Nd<sup>3+</sup>pump laser was focused by the concave mirror *1* into the SRSactive element *2* placed in an external zigzag optical resonator consisting of two concave (*3* and *4*) and two flat (*5* and *6*) mirrors. The output SRS radiation was decomposed into a spectrum using a diffraction grating (600/mm) and sent to a recording system.

A high-power oscillator-amplifier laser system based on YAlO<sub>3</sub>:Nd<sup>3+</sup> crystals with a wavelength  $\lambda_p$  = 1079 nm was used as a pump laser generating in the passive mode locking regime trains of 56 laser pulses with a duration of individual pulses  $\tau_p = 64$  ps and their repetition period of 8 ns. The energy of the laser pulse train was 18 mJ, which corresponded to the energy of individual pulses  $E_p = 320 \,\mu\text{J}$  [21]. The pump laser was isolated from the SRS laser by means of a Faraday isolator (not shown in Fig. 3). The use of a concave mirror *1* with a radius of curvature of 240 cm made it possible to focus the pump radiation beam into a focal spot with the minimum beam radius  $r_p = 290 \mu m$  (at level  $1/e^2$ ) and Gaussian transverse distribution of radiation intensity, which yielded a high pump radiation intensity  $I_p = 2W_p/(\tau_p \pi r_p^2)$ 3.8 GW/cm<sup>2</sup> exceeding  $I_{cr2}$ .

An SrMoO<sub>4</sub> crystal of length  $L = 7$  cm with antireflection coatings on plane-parallel end faces was used as the active element of the SRS laser. The crystal was grown by the Czochralski method at the Research Center for Laser Materials and Technologies, General Physics Institute of the Russian Academy of Sciences. The optical axis of the crystal was directed perpendicular to the direction of laser radiation propagation and oriented along the polarization direction of the pump radiation in order to excite not only the first ( $v_1 = 888$  cm<sup>-1</sup>) but also the second ( $v_2 = 327$  cm<sup>-1</sup>) vibrational mode of the SrMoO<sub>4</sub> crystal [8].



**Fig. 3.** The optical scheme of the laser system and the photograph (bottom) of the spatial distribution of Stokes SRS components after the decomposition of the output SRS radiation into spectrum by a diffraction grating: (*1*) focusing mirror; (*2*) SRS active element; (*3–6*) resonator mirrors.

The length of the SRS laser resonator was precisely adjusted (the mirror *6* was installed on a micrometer table) to synchronize the resonator round trip time with the pump pulse repetition period (8 ns). The end plane mirror 5 was highly reflective at SRS radiation wavelengths from 1194 to 1396 nm  $(R<sub>1192-1396</sub> > 99%)$ . Concave mirrors 3 and 4 (radius of curvature 100 cm) were transparent at the pump wavelength (transmittance  $T_{1079} = 97.1\%$ ) and had the following of reflection coefficient distribution over wavelengths of SRS radiation:  $R_{1194} = 99.3\%$ ,  $R_{1242} = 99.2\%$ ,  $R_{1294} = 92.9\%$ ,  $R_{1336} = 7.0\%$ , and  $R_{1396} =$ 15.3%. The output plane mirror *6* had the following distribution of reflection coefficients over the SRS radiation wavelengths:  $R_{1194} = 99.2\%, R_{1242} = 98.5\%, R_{1294} = 86.6\%, R_{1336} = 24.2\%, \text{ and } R_{1396} = 48.0\%.$  The resonator configuration was calculated in the ReZonator software tool [22] to match the size of the fundamental transverse mode of the first Stokes component of the SRS radiation with the pump beam focal radius  $(r_p = 290 \,\mu m)$  at the resonator round trip time synchronized with the pump pulse repetition period (8 ns).

It should be noted that we observed in the experiment a larger number of generated components of SRS radiation than in the theory discussed above: not only the calculated wavelengths  $\lambda_s = 1194$  nm,  $\lambda_{ss} =$ 1242 nm, and  $\lambda_{SS} = 1294$  nm, but also  $\lambda_{SS} = (\lambda_S^{-1} - v_1)^{-1} = 1336$  nm and  $\lambda_{SSs} = (\lambda_{SS}^{-1} - v_2)^{-1} = 1396$  nm. The wavelengths of all five generated SRS radiation components recorded by OceanOptics HR2000 spectrometer (200–1100 nm, resolution 2 nm) after frequency doubling with lithium iodate crystal corresponded to the above calculated values. The radiation linewidths did not exceed the resolution of the spectrometer. Figure 4 demonstrates this measurement result.

The beam profiles of each of the five separated SRS radiation components were also recorded (see Fig. 3, photo below). The beam profiles were close to Gaussian, which indicates high spatial quality of the generated SRS radiation owing to matching the size of the fundamental transverse mode of SRS radiation with the pump beam radius.

Figure 5 shows the dependence of the pulse train energy of the total output SRS radiation on the SRS laser resonator length detuning for the energy of the laser pulse train equal to 18 mJ. It can be seen that the detuning curve is relatively wide  $(\Delta L_{1/2} = 16 \text{ mm}$  at half-maximum) and symmetric, which is characteristic of the case of high-intensity synchronous picosecond pumping [21, 23] in contrast to the narrow  $(\Delta L_{1/2}$  < 1 mm) and asymmetric detuning curves obtained with low-intensity synchronous picosecond pumping [8–10, 24]. The maximum train energy of the total output SRS radiation at the best pump synchronization was 1.3  $\pm$  0.1 mJ (output energy instability of 8%) at a pump pulse train energy of 18  $\pm$  1 mJ (input energy instability 5%), which corresponded to an SRS conversion efficiency of about 7%. The output



**Fig. 4.** Spectrum of the generated SRS radiation.



**Fig. 5.** The dependency of the total output SRS pulse train energy on the SRS laser resonator length detuning.

energy was distributed over the SRS components as follows: 9% to  $\lambda_s$  = 1194 nm, 62% to  $\lambda_{ss}$  = 1242 nm, 17% to  $\lambda_{SS}$  = 1294 nm, 8% to  $\lambda_{SS}$  = 1336 nm, and 4% to  $\lambda_{SSs}$  = 1396 nm.

Figure 6 shows oscillograms of all components of the generated radiation. The oscillograms were obtained using four LFD-2F avalanche photodiodes connected to a four-channel Tektronix TDS7404B (4 GHz) oscilloscope with two consecutive measurements first for the components with wavelengths  $\lambda_n$ ,  $\lambda_s$ ,  $\lambda_{\rm Sss}$ , and  $\lambda_{\rm SSS}$  and then for the components with wavelengths  $\lambda_p$ ,  $\lambda_{\rm SS}$ , and  $\lambda_{\rm SS}$  to be further combined. It can be seen from Fig. 6 that the generation of the first Stokes component ( $\lambda_s$  = 1194 nm) with highfrequency shift  $v_1$  occurred without a time delay relative to the pump pulse train ( $\lambda_p = 1079$  nm), i.e., it was carried out practically in one pass of the SRS crystal due to high-intensity pumping. The second Stokes component ( $\lambda_{SS}$  = 1336 nm) with a doubled high-frequency shift  $2v_1$  was also generated without delay. The resonator mirrors for this component had low reflection coefficients ( $R_{1336} = 7.0\%$  for concave mirrors *3* and *4* and 24.2% for output mirror *6*), so its generation was also done in one pass.

However, the generation of the second Stokes component with combined frequency shift  $(v_1 + v_2)$  at the wavelength  $\lambda_{\rm{Ss}} = 1242$  nm occurred with a noticeable delay, which is explained by its development in a high-quality resonator ( $R_{1242} = 99.2\%$  for concave mirrors *3* and *4* and  $R_{1242} = 98.5\%$  for output mirror *6*). At the same time, the train of the next (third) Stokes component with combined frequency shift  $(v_1 + v_2 + v_2)$  at the wavelength  $\lambda_{\rm Sss} = 1294$  nm had no appreciable delay relative to the pulse train of the previous Stokes component with the wavelength  $\lambda_{\rm{SS}} = 1242$  nm, which can be explained by the parametric Raman interaction on the low-frequency vibrational mode due to the fulfillment of the nonlinear phase



**Fig. 6.** Oscillograms of frequency components of the generated radiation.

capture condition. The pulse train of the third Stokes component  $(\lambda_{ss})$  was relatively short, i.e., it ended prematurely compared to the pulse train of the previous second Stokes component ( $\lambda_{\rm{SS}}$ ) repeating the pattern of depletion of the pulse train of the first Stokes component  $(\lambda_s)$  during its conversion at the second SRS stage. This proves the participation of the first Stokes component not only in the process of SRS conversion into the second Stokes components ( $\lambda_{ss}$  and  $\lambda_{ss}$ ), but also in the process of parametric Raman interaction with the next two SRS components having low-frequency relative shifts ( $\lambda_{SS}$  and  $\lambda_{SS}$ ).

The biggest question is the generation mechanism of the last Stokes component with the wavelength  $\lambda_{SSs}$  = 1396 nm. A simple explanation consisting in the third stage of the SRS conversion with low-frequency shift  $(v_2)$  from the previous component  $(\lambda_{SS})$  (the blue arrow in Fig. 4 for the last frequency shift) does not stand up to scrutiny because there is a generation delay although the resonator mirrors for  $\lambda_{SS}$ have low reflection coefficients ( $R_{1396} = 15.3\%$  for concave mirrors 3 and 4 and  $R_{1396} = 48.0\%$  for output mirror *6*) as is the case for the  $\lambda_{SS}$ . Besides, the relative proportion of the output SRS energy attributable to the  $\lambda_{SS}$  wavelength component is small (8%). The largest share of energy was attributable to the component with the wavelength  $\lambda_{SS}$  (62%), so it can be assumed that the SRS generation of the last component ( $\lambda_{SS}$ ) originated from it with an additional high-frequency shift ( $v_1$ ) (the red arrow for the last frequency shift corresponds to it in Fig. 4). This is also indicated by the same generation delay for the components with wavelengths  $\lambda_{SS}$  and  $\lambda_{SSs}$  (Fig. 6). However, the generation of the pulse train of the last component  $(\lambda_{SSs})$  ended prematurely compared to the component at wavelength  $\lambda_{SSs}$  repeating the pattern of depletion of the pulse train of the first Stokes component  $(\lambda_s)$ . This indicates the participation of the first Stokes component ( $\lambda_s$ ) in the generation of the last Stokes component ( $\lambda_{SSs}$ ), which could occur in four-wave parametric Raman interactions. First, it could be a four-wave interaction on the low-frequency vibrational mode  $(v_2)$  involving components with wavelengths  $\lambda_s$ ,  $\lambda_{ss}$ ,  $\lambda_{ss}$ , and  $\lambda_{SSs}$ . This process should be more efficient under high-intensity pumping (the condition of nonlinear phase capture is fulfilled). Second, there could be a four-wave interaction on the high-frequency vibrational mode  $(v_1)$  that involves components with wavelengths  $\lambda_p$ ,  $\lambda_s$ ,  $\lambda_{ss}$ , and  $\lambda_{SS}$  (without participation of the  $\lambda_{SS}$  wavelength component). But the condition of nonlinear phase capture is not satisfied for this interaction. Thus, the most likely explanation for the generation of the last component ( $\lambda_{SS}$ ) is a combination of the four-wave interaction ( $\lambda_s$ ,  $\lambda_{ss}$ ,  $\lambda_{SSs}$ , and  $\lambda_{SSs}$ ) on the low-frequency vibrational mode ( $v_2$ ) and of the SRS conversion  $\lambda_{SS} \to \lambda_{SS}$  on the high-frequency vibrational mode  $(v_1)$ . The latter occurs without the component  $(\lambda_{SS})$ , which is confirmed experimentally because Fig. 6 shows that the generation at the  $\lambda_{SSs}$  wavelength continued despite the fact that the generation at the  $\lambda_{SS}$  wavelength had stopped.

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We also used a PS-1/S1-type streak camera [25] (developed by the Prokhorov General Physics Institute, Russian Academy of Sciences) to measure the duration of the generated pulses of the output SRS radiation. For the first Stokes component with a high-frequency shift ( $\lambda_s$ ), the pulse duration  $\lambda_s$  was 20  $\pm$  5 ps. A shortened pulse duration  $\tau_{\rm ss}$  = 8  $\pm$  2 ps was recorded for the second Stokes component with combined frequency shift ( $\lambda_{\rm{SS}}$ ). These values are close to the theoretical estimate [26]  $\tau_{\rm{S}}\approx\sqrt{\tau_{\rm{p}}\tau_{\rm{l}}}$  and  $\tau_{\rm{SS}}\approx$  $\tau_p \tau_2$ , respectively.

# 5. CONCLUSIONS

Theoretical and experimental studies were carried out on conditions for the generation of multiple radiation components with a small wavelength spacing in a crystal SRS laser under synchronous pumping with combined frequency shift. A  $SrMoO<sub>4</sub>$  crystal possessing the first (high-frequency) and second (lowfrequency) vibrational modes similar in Raman integral cross section values was used as an active medium. A theoretical analysis indicated an important role of four-wave parametric Raman interactions on the low-frequency vibrational mode of the SRS-active crystal when the conditions of coherence and nonlinear phase capture of such interactions are satisfied. The generation of a crystalline SRS laser in the nearinfrared range for five closely spaced wavelengths with combined frequency shift was achieved for the first time. The use of high-intensity synchronous picosecond pumping with a wavelength of 1079 nm satisfying the condition of nonlinear phase capture of parametric Raman interaction on the second vibrational mode made possible efficient generation at wavelengths of 1194, 1242, 1294, 1336, and 1396 nm with various combinations of frequency shifts (888  $\mu$  327 cm<sup>-1</sup>).

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## CONFLICT OF INTEREST

The authors of this work declare that they have no conflicts of interest.

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