Solution Combustion Synthesis for Preparation of Structured Catalysts: A Mini-Review on Process Intensification for Energy Applications and Pollution Control1

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Abstract—Solution combustion synthesis (SCS) is a preparation technique that can be used to synthesize a variety of inorganic nanomaterials and structured catalysts. It is based on a self-propagating exothermic redox reaction between organic salts and a fuel mixed together in an aqueous solution, which results in the formation of nanocrystalline and highly pure solid nanomaterials. SCS can be considered as an attractive synthesis method for catalysts due to the simple nature of the synthetic route and short reaction times. The process is easily scaled up to any kind of application which makes it economically attractive. This mini-review provides a short overview on the synthesis of structured catalysts by SCS and their recent utilization for energy applications and pollution control.

Keywords: SHS, solution combustion synthesis (SCS), nanomaterials, in situ deposition, monoliths, open cell foams

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INTRODUCTION

In the recent years, solution combustion synthesis (SCS), also known as self-propagating high-temperature synthesis (SHS), has attracted the interest of many scientists as an intriguing technique to prepare catalysts for many different applications in a simple and easy way. Proof of this can be found in numerous review articles $(1-30)$ among the most famous) that have been published from the end of the 1960's. Starting in 1967, Russian scientists Merzhanov, Skhiro, and Borovinskaya first described this technique for the preparation of ceramic and intermetallic compounds, via solid flame combustion [31, 32]. In October 2007, after 40 years from this discovery, a dedicated international conference was held in Russia, with the presence of Merzhanov [33], to celebrate the anniversary of this methodology. Since then, this method also found extensive practical applications at the industrial level.

SCS is considered to be attractive for catalysts preparation due to the simple nature of the synthetic route, short reaction times, and relatively low cost [18, 28, 34, 35]. Furthermore, the composition, homogeneity, morphology, and stoichiometry can be finely tuned to obtain the desired products that are highly crystalline and pure. Moreover, SCS allows the preparation of not only of nanomaterials and nanopowders but also, structured catalysts which carry on a thin film of catalytic material. This material can be easily coated in situ over any kind of ceramic or metallic surface for many different applications [36–46].

Figure 1 shows an overview of different supports that are normally used to prepare structured catalysts, where both the geometry (different shapes and porosity: monoliths, foams, tissues, corrugated plates, etc.) and the nature of the support (different materials: cordierite, alumina, zirconia, carborundum, metal alloys such as FeCrAlloy®, etc.) can vary greatly. The process can be easily scaled up and industrialized, which makes it economically attractive [18, 28].

THEORETICAL BASIS OF SCS

SCS is based on a self-propagating, exothermic, redox reaction between organic salts mixed with a fuel in either an aqueous solution or solid state [1, 6]. The precursors are gently heated to start the ignition of the reaction. The combination of an organic fuel, an oxygen source (oxidizer) and heat (ignition mode) results ¹ The article is published in the original. $\frac{1}{2}$ in a self-propagating combustion reaction which can

Fig. 1. Examples of different ceramic and metallic supports that can be used to prepare structured catalysts by SCS (courtesy of Bekaert SA, Chauger Honeycomb Ceramics, Lanik s.r.o., Schwank GmbH, Worgas Bruciatori s.r.l.).

Fig. 2. SCS used to prepare structured catalysts: in situ deposition of a thin layer of catalyst over monoliths and foams (by immersion or spraying).

be described using propellant chemistry [9, 47]. The intimate mixing, at a molecular level, of the precursors allows for uniform formation of the desired products. The initial combustion reaction self-propagates as a chemical reaction wave, starting with the reactive molecules which then involve the entire solution, via a front-layer heat transfer, to the final product. The reaction temperature, which reaches high values for a very short time, allows for the high degree of crystallinity and purity. Due to the combustion reaction, a large amount of gases are generated (mainly $CO₂$, H_2O , and N_2 , with traces of CO and NO_x) within the short reaction time, favoring the formation of nanosized powder with relatively high specific surface area. These gases inhibit crystallites growth and limit agglomerates, favoring the formation of a rather porous structure [28, 48, 49]. The synthesis is easily adaptable to any size of structured supports with any

shape and many starting materials for preparation of structured catalysts, as briefly illustrated in Fig. 2. To deposit in situ the catalyst, immersion, deep-coating, or spray-coating can be used indifferently, depending on the best operative conditions according to the final application [16, 43, 44, 50–52].

Any kind of solution containing an organic fuel and a metal precursor can, in principle, be used for SCS. The first pre-industrial preparation can be considered the one reached by Kingsley and Patil in 1998 [6]. They placed a mixture of aluminum nitrate and urea, dissolved in distilled water, in a muffle furnace at 500°C. The mixture boiled, foamed, and ignited with an incandescent flame at a temperature of approximately 1350°C. They produced a fluffy, fine, highly crystallized, nanosized α -alumina in less than 5 min, with a specific surface area of approximately 8 m^2 g^{-1} . Figure 3 shows the fine powder obtained by Kingsley and Patil, together with the physicochemical characterization: the XRD spectrum is typical of α-alumina and the lattice constant parameters they calculated were in agreement with literature data [6]. SEM and TEM investigations enlightened the typical shape of the surface, characterized by a series of cracks and pores due to the formation of gases during the combustion reaction [6]. Despite the explosive nature of uncontrolled exothermic redox reactions, the combustion of the aluminum nitrate–urea mixtures is selfpropagating and non-explosive [6, 7]. The advantage of the self-propagating combustion reaction lies in the large amount of gases that are generated within a short period of time.

Basically, SCS is a reaction of combustion between one or more metal nitrates (which acts as an oxidizer) and an organic fuel. Reagents can be mixed in an aqueous solution to favor intimate mixing at a molecular level, assuring a high degree of purity in the final product. Depending on the valence of the metal in the nitrate, the fuel-to-oxidizer ratio ϕ (the so-called elemental stoichiometric coefficient) represents the ratio between the total valences of the fuel and the total valences of the oxidizer. When ϕ is equal to 1, the reaction proceeds according to stoichiometric conditions and the initial mixture does not require atmospheric oxygen for completing the oxidation of fuel [18]. When ϕ > 1 there are fuel-rich conditions (that is, oxygen is a product of the reaction), whereas when $\phi \leq 1$ this means there are fuel-lean conditions (that is, oxygen is a reagent of the reaction). Thus, a variation of ϕ means a variation of the amount of heat released during the reaction, and in turn a variation of the crystalline structure of the final product. In addition to this, ϕ also strongly influences the heat of reaction [47]. Numerous scientists have demonstrated that, for an ideal reaction (no heat losses), the heat of reaction becomes more exothermic while $\phi > 1$, whereas when $\phi \ll 1$ the reaction becomes endothermic [47, 23].

The low temperature decomposition of the organic fuel favors the ignition of the reaction. The ignition can be obtained either with a hot metal wire, or by placing the solution into an oven at a relatively low temperature, or into a microwave oven. This proceeds in a self-sustained fashion due to its exothermic and autocatalytic features [1, 28, 53]. Figure 4A shows a typical example of the effect of ϕ while synthesizing $Co₃O₄$ spinel by SCS (synthetic conditions: cobalt nitrate and urea as precursors, vigorously mixed in aqueous solution at different ϕ values, then placed in an oven for 20 min at 250°C [54]). While maintaining constant temperature of the oven, the ignition temperature of the reaction is anticipated and the maximum temperature recorded during self-propagation increases with φ. This is because of the increase of the exothermic level of the combustion reaction (appreciable by calculating the temperature of adiabatic flame, reported in Fig. 4b). The higher temperature

Fig. 3. α-Alumina synthesized by Kingsley and Patil in 1988: as-prepared foamy powder (a), TEM images (b, c), and XRD spectrum (d). Data rearranged from [6].

reached during the synthesis allows for a faster process and in turn, smaller average crystallite size. A variation of the ignition source temperature affects the whole SCS process. In particular, an increase of the temperature at which the reagents are exposed, boosts self-ignition by accelerating the reaction, thus allowing higher flame temperatures to easily be reached. Surely, the parameter which most affects the whole process is φ, which must be optimized case by case depending on the desired application of the final products.

The choice of the organic fuel plays another important role in the SCS process. Fuels fulfill various purposes: they help to homogeneously mix the organic precursors of the desired final products by favoring the formation of metal ion complexes [4, 9]. They decompose fast forming various compounds, aiding the combustion reaction, such as combustible gases $HNO₃$ and $NH₃$, which provide the necessary heat to complete the reaction [23, 49, 55]. The fuel allows for propellant chemistry, being a source of C and H atoms, it favors the formation of $CO₂$ and $H₂O$ gaseous products which inhibit particle growth and form a porous structure [6, 7, 28, 48, 49]). Thus, fuels must possess at least the following properties: (*i*) being soluble in water and compatible with metal nitrates; (*ii*) having low ignition

Fig. 4. Effect of the fuel-to-oxidizer ratio φ on the measured reaction temperature with the oven set at 250°C (a), adiabatic temperature of reaction (b), and crystallite dimensions during the synthesis of $Co₃O₄$ (b). Insets: FESEM images of $Co₃O₄$. Data partially rearranged from [53].

temperature (preferably below 500°C) and not explosive combustion reaction; (*iii*) developing a large amount of gases during combustion, possibly harmless; and (*iv*) being available, and preferably, cheap.

Simple compounds such as urea, glycine, alanine, glycerol, etc. are recognized as potential fuels [9, 55]. Compounds containing N–N bonds are well-known to better assist the combustion reaction, even if they act a drawback with the release of NO*x* emissions during combustion [53]. In some cases, the use of highly viscous fuels, such as glycerol, helps obtain a better distribution of the final desired product on the structured catalyst support [53]. Table 1 lists the most common organic fuels typically employed in SCS, along with their main features.

Thus, SCS is a viable technique to produce useful materials such as advanced ceramics, catalysts, phosphors, pigments, composites, intermetallic, and nanomaterials [9, 18, 21–24, 28, 34, 35, 56–62].

SCS FOR PROCESS INTENSIFICATION

Structured catalysts are widely used in energyrelated and environmental applications, such as fuels production (syngas, hydrogen, biodiesel, etc.) [40– 43, 64, 87, 96, 102–107], electrochemical processes and fuel cells [62, 95, 100, 108–116], stationary and automotive emission control systems [45, 46, 71, 77, 117–125], and catalytic redox processes [36, 37, 65, 72, 76, 126–130]. The preparation of highly active, well dispersed metal particles that are uniformly distributed over structured supports, plays a crucial role at an industrial level. SCS allows for the preparation of adhesive coatings on structures such as ceramic or metallic tissues, spheres, monoliths, foams, etc. Compared to other preparation techniques, SCS provides many advantages. The most common technique at an industrial level, the wash-coating, first requires a detailed optimization of the various operative parameters, such as the concentration of the slurry, pH, viscosity, the speed of dipping, etc., to assure an adequate adhesive layer of catalyst on the surface of the structures [42, 52, 131, 132].

The World Energy Outlook 2016 [133], released by the International Energy Agency on November 2016, predicts a 30% increase of primary energy demand by 2040, due to growing population. To meet these needs, it is essential to respect the quality of air, water, and soil in order to take care of the environment and reduce local pollution, with regards to the recent Paris Agreement [134]. This agreement implies, on one hand, to increase energy production, on the other hand, to manage the continuous requirement of new products all while taking care of the environment. From this perspective, process intensification (PI) allows for a cleaner, safer, smaller, and more energyefficient process design approach for any kind of technological application [135–137]. More specifically, SCS is seen as a manufacturing technique which allows for PI because of its intrinsic energy saving (low energy requirements only during the initial ignition step) [22, 30] and production of highly pure products. The high temperature, reached during the self-propagating exothermic reaction, does not require any additional energy source which allows for complete conversion of reactants into pure, high-quality products. In fact, any impurities present in the starting materials can easily volatilize during heating [22]. Moreover, SCS requires relatively cheap reactants, simple equipment, and low-cost facilities, leading to a reduction in production costs when compared to conventional manufacturing processes. Thus, SCS is an attractive, innovative, and intriguing technique to produce structured catalysts by PI [18, 20].

Precisely, structured catalysts based on monoliths and foams can provide many advantages with respect

Fuel	Structure	$\Delta H_{\text{comb}}^{\circ}$, kJ mol ⁻¹	Synthesized products [refs]
Urea, CH_4N_2O	NH ₂ H_2N	-633	$Pt/CeO2; Ni/CeO2; Rh/Al2O3;$ $Ni/Al2O3; Pd/Co3O4; CeO2/ZrO2;$ $Bi_x Mo_yO_z$; CaCu ₃ Ti ₄ O ₁₂ ; LaCr _{0.9} O ₃ $[41, 43, 63 - 71]$
Glycine, $C_2H_5NO_2$	H_2	-974	$Ni/CeO2; Co3O4; Mn3O4; LaMnO3;$ $La_{1-x}Sr_xM_xO_3$ (M = Fe, Co, Ni) $[41, 67, 72 - 77]$
β -Alanine, C ₃ H ₇ NO ₂	OН H_2N	-1329	Pt/CeO ₂ ; LaMO ₃ (M = Mn, Cr, Sr); CoWO ₄ ; La _{1 - x} Sr _x M _x O ₃ (M = Fe, Co, Ni); Ca ₃ Al ₂ O ₆ ; CaAl _{12 – 2x} Ni _x Ti _x O ₁₉ $[72, 78 - 82]$
Glycerol, $C_3H_8O_3$	OН HO OH	-1654	LaMnO ₃ ; NiFe ₂ O ₄ ; LiMn ₂ O ₄ ; Co_3O_4/γ -Al ₂ O ₃ ; CuCo ₂ O ₄ ; CuCr ₂ O ₄ $[53, 72, 83 - 86]$
Oxalyl dihydrazide, $C_2H_6N_4O_2$	V_{H_2} H_2	-1218	$Pt/CeO2; Ni/CeO2; ZrO2/CuO;$ CuO/CeO ₂ ; [41, 74, 87-91]
Citric acid, $C_6H_8O_7$	OН Ω OH H _O OН	-1961	$SrFeO3, Sr0.85Ce0.15FeO3-x; Fe2O3;$ Fe_3O_4 ; Mn ₂ O ₃ Ni/Y ₂ O ₃ /ZrO ₂ ; $Co/SiO2$; Al-Mn-Mg-O [61, 92-98]
Hydrazine, N_2H_4	H H	-622	BaTiO ₃ ; Fe ₂ O ₃ ; Fe ₃ O ₄ ; MgCr ₂ O ₄ ; α -CaCr ₂ O ₄ ; La _{0 7} Ba ₀ 3MnO ₃ ; Fe ₂ O ₃ ; $Fe3O4[9, 99-101]$

Table 1. Fuels most commonly employed for SCS and some examples of synthesized products

to packed beds. In fact, they can operate at higher space velocity with reduced pressure drop due to their higher surface-to-volume ratio [138, 139]. Recently, open cell foams have been used as an attractive alternative for many different applications due to their high mechanical strength and enhanced heat transfer properties [140–142]. The characteristics of open cell foams as structured supports for catalysts, including their high porosity and tortuosity, provide better catalytic performance which allows for a reduced catalyst loading with good distribution on the surface of the structure, lower pressure drops, and enhanced heat transfer properties with high thermal stability [138, 139, 143–145]. These characteristics make these structured catalysts very attractive for highly exothermic or endothermic reactions (combustion or reforming processes), and also for low contact time reactions (partial oxidation processes) [138, 139, 143, 144]. Until now, very few publications are available in the literature on structured catalysts prepared by SCS : these few include articles that are most focused on the

uniformly covering structured supports plays a crucial role in many industrially important catalytic applications. This issue becomes important for three-way structured catalysts such as monoliths and foams. The

energy applications or pollution control.

metal deposition on the structures requires additional precursors to achieve a uniform distribution. In the literature, different approaches such as rotation of the impregnated monolith, freeze-drying, microwave heating, and spraying were proposed to improve the effectiveness of metal deposition on structured catalysts by SCS.

preparation and characterization of the structured catalysts [53, 146], while others are more focused on the use of monoliths [37, 40, 42, 71, 77, 123, 126] or open cell foams [45, 46, 106] as structured catalysts for

SCS FOR PREPARATION OF STRUCTURED CATALYSTS BASED ON FOAMS The preparation of highly dispersed metal particles

Fig. 5. Effect of pressure on the burning rate during the synthesis of Fe foams by SCS of Fe–bistetrazolamine complex. In the insets: SEM images of the grain size of Fe foams obtained at low (a) and high pressure (b). Data rearranged from [146].

Regarding the preparation of foams as structured supports, Tappan et al. synthesized ultra-low density nanostructured metal foams by SCS [146]. They prepared metal complexes based on Fe and bistetrazolamine, as the organic ligand, to form pellets. SCS was performed in an inert atmosphere to ignite the pellets, resulting in a vigorous burn producing sparks. In this case, the decomposition of the Fe–bistetrazolamine complex liberates gases, while Fe was reduced to an oxidation state of zero, giving rise to highly porous iron nanofoams. Varying the concentration of the Fe– bistetrazolamine complex, or the synthesis conditions (inert pressure, type of inert atmosphere, N_2 or Ar), allows for controlling the characteristics of the final nanostructured metal foams. Figure 5 shows the variation of the burning rate of Fe–bistetrazolamine complex, as a function of Ar pressure during SCS, together with the morphology obtained, enlightened via SEM. The structural size of Fe grains decreases at lower pressures, where their size was 30–50 nm attained at high pressure and 10–50 nm at low pressure. These authors demonstrated that it is possible to increase the specific surface area of these foams from 20 to 120 m^2 g^{-1} , after heat treatment at 500°C under hydrogen flow without altering the grain size. In fact, the heat treatment after SCS favors the removal of volatile elements while completing the densification process, considering the short time at which SCS occurs.

Zavyalova et al. [53] covered ceramic foams with a uniform film of Pt metal nanoparticles by microwave-assisted SCS. They dipped α -alumina foams into a solution of glycerol and Pt nitrate, pre-heated at 80°C for 2 h. After removing the excess of solution by spraying dry air, the dipped foams were placed into a microwave, set at 700 W, at a varied synthesis time of 3 to 9 min. Microwave irradiation provides rapid and selective heating of the precursors' solution. They adjusted the Pt loading from 0.6 to 2 wt % by repeating the synthesis up to 3 consecutive times. Figure 6a shows the sequence of the SCS reaction, where it is visible that the combustion front propagates very fast through the foam starting from the bottom side. The whole process is very fast coming to conclusion, being over in less than 10 min after up to 3 impregnation cycles (Fig. 6b). The physicochemical characterization enlightened a homogeneous catalytic layer covering the entire foam (Fig. 6c), with a Pt dispersion between 5 and 20% (the shorter the synthetic time, the higher the dispersion). The mean Pt crystallite size, measured by Rietveld method from XRD, and confirmed by TEM, is between 15 and 20 nm and is, thus independent from the synthesis conditions (Fig. 6d). The adhesion of the thin coating layers was verified to be excellent: by stressing the coated foams in ultrasonic bath for 1 h, less than 0.1 wt $\%$ weight loss was recorded.

SCS TO PREPARE STRUCTURED CATALYSTS FOR ENERGY APPLICATIONS

Nowadays, the challenge is to move towards zeroemission energy sources. On this perspective, hydrogen is the most attractive energy carrier to be used in fuel cells, electrical vehicles, and electrical power plants, with zero, or near-to-zero emissions of greenhouse gases and hazardous species. Hydrogen, which unfortunately is not available in nature, can be produced via reforming processes from many hydrogencontaining molecules and fuels [147], or by electrolysis of water using renewable energy [148]. Thus, the interest of scientists lies in the production of syngas (a mixture of H_2 and CO) from the reforming of commonly available hydrocarbons. Steam reforming of natural gas on noble metal catalysts is the most widely used industrial process to produce syngas. Indeed, also the use of renewable fuels, such as biogas and light alcohols (methanol and ethanol) represents an interesting and relatively low-cost renewable source of hydrogen, since these fuels can be derived from biomass [149, 150]. As an energy source, also the catalytic combustion of hydrocarbons is an attractive solution for both industrial and domestic applications. The use of a catalyst for a combustion reaction promotes the full and efficient oxidation of hydrocarbons at temperatures far lower than those established in typical flame combustors, with high combustion efficiency. Thus, reaching the complete conversion of hydrocarbons at lower temperature, emissions of CO, unburned, and NO*^x* are drastically reduced.

Fig. 6. Microwase-assisted SCS to deposit Pt onto alumina foams: (a) thermographs during the process and (b) temperature profiles during the process for three different impregnation steps; (c) low-magnification SEM of a coated foam after 3-min synthesis and (d) HRTEM of the 0.6% Pt/ α -Al₂O₃ foam. Data rearranged from [55].

Focusing hydrogen production, Vita et al. [40, 42, 106] prepared both cordierite monoliths and alumina open cell foams by SCS for steam reforming, and oxysteam reforming of methane and biogas to produce syngas. Concerning cordierite monoliths, they first deposited a thin layer of γ -Al₂O₃ [40] or CeO₂ [42] by SCS. They did this dipping the monoliths in a solution of aluminum nitrate [40] or cerium nitrate [42], and urea followed by placing the monoliths in an oven at 600°C for 2 h in calm air. Then, they deposited the active phase of the catalyst, Ru [40], Rh, Pt or Ni [42], by wet impregnation (dipping the monoliths in a solution containing the respective metal nitrate) and calcining for 2 h at 400°C in calm air. The deposition was repeated several times to reach various catalyst loadings (varying from 0.1 to 0.5 mg cm^{-2} , as noble metal deposited over the structure). All monoliths showed excellent mechanical resistance since the coated structures lost less than 0.3% of their weight when subjected to a double ultrasonic treatment in a water/acetone solution for 1 h, at 130 W and 45 kHz. Pressure drop measurements carried out at increasing superficial velocity, up to 15 m s^{-1} , denoted very low values, not exceeding 11 000 Pa m^{-1} , very similar to the values measured on the bare monolith (indicative that the coated catalytic layer is very thin and it does not influence the pressure drop). Figure 7a shows a series of images of the monolith during the various phases of the coating process for the deposition of $Ni/CeO₂$. SEM images (Fig. 7b) show that the catalytic layer is very thin (as confirmed by pressure drop measurements), with uniform distribution along the walls and the corners. XRD measurements confirmed the composition of the desired catalyst deposited on the structure (Fig. 7c). Finally, a series of catalytic tests towards the reaction of oxy-steam reforming of $CH₄$ showed brilliant performance of the structured catalysts (Fig. 7d): in the case of $Ni/CeO₂$, it maintained a full conversion of CH₄ up to 180000 NmL g_{cat}^{-1} h⁻¹, with almost 75% of H_2 produced and a H_2/CO molar ratio equal to 3.2.

Using the procedure previously described, Vita et al. [106] deposited a 1.5% Rh/CeO₂ catalyst by SCS and wetness impregnation over Al_2O_3 open cell foams. They compared the performance of 30 and 40 ppi $Rh/CeO₂$ foams and a 400 cpsi monolith towards the oxy-steam reforming reaction (also known as trireforming reaction) of synthetic biogas. The SCS

Fig. 7. (a) Cordierite monolith uncoated, coated with CeO₂ by SCS, and with Ni by wetness impregnation; (b) SEM images of the Ni/CeO₂ monolith; (c) XRD patterns of CeO₂ and Ni/CeO₂ powders, cordierite monolith and Ni/CeO₂ monolith; and (d) performance of Ni/CeO₂ monolith towards the oxy-steam reforming of methane as a function of the weight space velocity at $T =$ 800° C, O/C = 0.55, and S/C = 1.2. Data rearranged from [40].

deposition produced a very thin catalytic layer, with a specific surface area of $14 \text{ m}^2 \text{ g}^{-1}$, and Rh dispersion of 22%. Figure 8a shows pictures for the 40 ppi foam after $CeO₂$ and Rh/CeO₂ deposition: the catalytic layer appears uniformly distributed on the whole surface of the foam. Figure 8b shows SEM images with EDX mapping, again, the catalyst is homogeneous, completely covering the surface. On top of this, EDX mapping confirms that both Ce and Rh, the active element of the catalyst, are highly homogeneously dispersed. The comparison of the catalytic activity between the monolith and the foam (Figs. 8c, 8d) proves the better performance of the foam over the monolith. In fact, the foam is able to maintain a full $CH₄$ conversion, and a constant 50% CO₂ conversion, for the whole range of weight space velocity (up to 280000 NmL g_{cat}^{-1} h⁻¹), while the monolith decreases the performance when the weight space velocity exceed 80000 NmL g_{cat}^{-1} h⁻¹). The coated foam allows for an almost constant $\rm H_{2}/CO$ molar ratio close to 1.74, while the monolith exhibits a decreasing value from 1.39 to 1.32 with the weight $\rm g_{cat}^{-1}$

space velocity.

Another way to produce hydrogen is via the decomposition of light alcohols. In particular, ethanol decomposition in the presence of nickel-based catalysts represents an easy way to extract hydrogen. The use of a porous support can increase the surface area of the active phase of a catalyst, and thus enhances its structural and thermal stability. Cross et al. [107] demonstrated this effect preparing a series of Ni supported catalysts on $γ$ -Al₂O₃ pellets with a ring geometry (internal/external diameter: 0.1/0.25 in) for the selective decomposition of ethanol to hydrogen. They prepared the supported catalysts by dipping γ -Al₂O₃ pellets in aqueous solution of nickel nitrate hexahydrate and glycine where $\phi = 1.75$, with a varied immersion time from 1 s to 30 min. After a drying period of 24 h, the impregnated catalysts were placed on a hot plate at 500°C to initiate the ignition of the combustion reaction. Figure 9a shows the combustion front propagation as captured by an IR camera; in less than 1 min the combustion reaction is over. The peak temperature reached during the combustion reaction depends on the impregnation time, that is, on the amount of solution the γ -Al₂O₃ pellets adsorbed, as shown in Fig. 9b: the longer the impregnation time,

Fig. 8. (a) 40 ppi alumina open cell foam coated with CeO₂ by SCS, and with Rh by wetness impregnation; (b) SEM images of the Rh/CeO₂ foam with EDX mapping; and performance of Rh/CeO₂ monolith (c) and Rh/CeO₂ open cell foam (d) towards the oxy-steam reforming of biogas as a function of the weight space velocity at $T = 900^{\circ}$ C (for the monolith: S/C = 0.3 and O/C = 0.1; for the open cell foam: $S/C = 0.1$ and $O/C = 0.2$). Data rearranged from [106].

the higher the peak temperature and the shorter the reaction time. A series of SEM characterizations demonstrated that Ni was deposited as a thin layer on the surface of γ -Al₂O₃ pellets. This is due to the alumina support, the impregnated support, and the supported catalysts all appearing very similar (Fig. 9c). In fact, the supported catalysts exhibit a uniform nanostructure with agglomerates smaller than the impregnated catalysts. The authors evaluated the catalytic activity towards the reaction of ethanol decomposition in a fixed bed configuration using a quartz tube reactor. Before testing, the catalysts were reduced in situ in a pure hydrogen flow rate at 300°C for 1 h. The catalytic decomposition of ethanol was investigated over a flow rate of 140 cm³ min⁻¹ of nitrogen saturated with ethanol at 0°C, containing 3.8% ethanol and $O₂/C₂H₅OH$ molar ratio of 0.5. Figures 9d and 9e show ethanol conversion and hydrogen selectivity for the supported Ni/γ -Al₂O₃ catalysts impregnated for 5 s and 1 min, respectively, in comparison with the blank support. The γ -Al₂O₃ exhibits complete ethanol conversion at lower temperature than the Ni-impregnated catalysts, but is also totally non-selective for H_2 . This means that the products of the reaction are water and ethylene. The catalyst impregnated for 5 s has a good activity for ethanol conversion but low values of $H₂$ selectivity, while the catalyst impregnated for 1 min has an opposite behavior. These results mean that the 5-s catalyst produces more water and ethylene than the 1-min catalyst, but less hydrogen and acetaldehyde. These results can be explained by the lower amount of Ni that was deposited on the 5-s catalyst compared to the 1-min one. In fact, the reaction of ethanol to water and ethylene is favored on alumina sites, while the reaction to acetaldehyde and hydrogen is favored in the presence of Ni. A higher dispersion of Ni is attained on the catalysts that were impregnated for 1 min. These results clearly demonstrate that SCS allows for control of the distribution of the active sites of a catalyst (that is, favoring different reaction pathways involved in a multiple step-reaction process) by varying the parameters governing the combustion process; such as the amount of solution impregnated onto the support, and the temperature at which the combustion reaction occurs. This in turns reflects how SCS can be used to drive a reaction towards the desired final products, hydrogen in this case.

Fig. 9. Propagation of the combustion front taken by IR camera (a). Temperature profile of combustion front for samples prepared with 5 s and 1 min impregnation (b). SEM images of $A1_2O_3$ support, impregnated support, and supported catalyst (c). Ethanol conversion (d) and hydrogen selectivity (e) for samples prepared with 5 s and 1 min impregnation, and the original support.

Regarding the catalytic combustion of hydrocarbons, Tacchino et al. [37, 126] proposed and investigated new type of structured catalysts for the combustion of CH_4/H_2 mixtures at different molar ratios in lean conditions. The catalysts consisted of lean conditions. The catalysts consisted of $Pd/NiCrO_4$, $Pd/CeO_2 \cdot ZrO_2$, and $Pd/LaMnO_3 \cdot ZrO_2$ lined over SiC monoliths. The authors prepared the structured catalysts using one-shot SCS, by dipping the ceramic monolith supports in homogeneous aqueous solutions. These solutions contained the metal– nitrate compounds, as oxidizers, and urea (for the preparation of $Nicro₄$ and $Al₂O₃$) or glycine (for the preparation of $CeO₂ · ZrO₂$ and $LaMnO₃ · ZrO₂$) as fuel, along with Pd nitrate in the desired amount. The SCS reaction began in an oven set at 600°C. One-shot SCS allows for the reduction of the manufacturing time of structured catalysts, since all the precursors are mixed together before the initial combustion reaction. Figure 10a shows the general aspect of the structured catalyst wrapped with a vermiculite foil, to better fix it into the reactor. Figure 10b shows SEM images which reveal a very thin and uniform layer of $Pd/NiCrO₄$ catalyst covering the walls of the monolith. In particular, it is evident that the porous structure of the catalyst is due to the gases generated by the decomposition of the reacting precursors. The BET specific surface area increased from 0.2 (base SiC monolith) to 2.2 m^2 g⁻¹ measured on the coated $Pd/NiCrO₄$ structured catalyst. The catalytic activity was evaluated where the structured catalysts generated an overall power density of 7.6 MW m−3. This power density was reached by first burning only $CH₄$ (5% vol

CH₄ in air with $\lambda = 2$), then only H₂ (17 vol % H₂ in air with $\lambda = 2$), then three different CH₄/H₂ lean mixtures at increased H₂ concentration at constant $\lambda = 2$ (see Fig. 10b) The overall flow rate was equal to 200 NmL min⁻¹, equivalent to a gas hourly space velocity of 16000 h−1. Among the various structured catalysts, the best results belonged to the $Pd/NiCrO₄$ catalyst, as shown in Fig. 10c. The SiC monolith reduced the methane half-conversion and light-off temperatures, when compared to the bare counterpart, for all the tested CH_4/H_2 mixtures. The addition of H_2 into the reactive mixture favored $CH₄$ combustion, in that the higher the $H₂$ concentration lowered the half-conversion and light-off temperatures (Fig. 10c, Mix 3). The presence of the catalyst also reduced CO emissions, where the recorded CO peak decreased with increasing $H₂$ concentration.

SCS TO PREPARE STRUCTURED CATALYSTS FOR POLLUTION CONTROL

The abatement of pollutants is one of the biggest challenges in modern society. Pollutant emissions damage our air, water, and soil which compromise the quality of life of this planet.

The particulate matter emitted by diesel engines is a critical issue in urban areas. On top of this, diesel engines produce dangerous NO*x*. Notwithstanding these drawbacks, diesel engines are attractive for their efficiency and durability. Diesel engine emission level standards are always more stringent due to European regulations. A promising approach to lower diesel

Fig. 10. (a) Picture of a SiC structured catalyst wrapped in a vermiculite foil; (b) SEM images of the SiC monolith lined with Pd/NiCrO₄: frontal view of a microchannel and internal surface covered by a spongy layer of catalyst; and (c) catalytic performance of the SiC monolith lined with Pd/NiCrO₄: CH₄ conversion (solid lines), H₂ conversion (broken lines), and CO emissions (dotted lines) vs. *T* as a function of the reactive mixture (*a*: CH₄ alone; *b*: Mix 1 CH₄/H₂ molar ratio 75/25; *c*: Mix 2 CH₄/H₂ molar ratio 50/50; *d*: Mix 3 CH₄/H₂ molar ratio 25/75; *e*: H₂ alone). Data rearranged from [37].

emissions comes from the use of specific catalytic traps, able to concomitantly reduce particulate matter and NO*x*. Particulate filters are made of temperatureresistant porous material, such as ceramics, with an as-high-as-possible filtration area so as to decrease the pressure drop and the related fuel penalty. For this purpose, Fino et al. [71] deposited a perovskite catalyst, $LaCr_{0.9}O_3$, on wall-flow traps used as a support, through use of SCS. They used both cordierite and silicon carbide as supports. The supports were dipped in a solution of La and Cr nitrates, with urea as a fuel, and placed in an oven at 600°C for few minutes. The dipping and heating procedure was repeated until 10% in weight of the catalyst was deposited. Figure 11a shows the SEM characterization of a cordierite trap coated with $LaCr_{0.9}O_3$. The catalyst appears to be strongly bonded to the support, additionally the microstructure seems to have a spongy morphology as a consequence of the evolved gases from the SCS reaction. This feature represents a great advantage as it favors the contact between the catalyst and soot that accumulates within the trap. The catalytic activity of the developed catalytic traps was tested in a pilot plant connected with a diesel engine, to better simulate diesel exhaust gases. Each prepared trap was first loaded with a low temperature exhaust gas (about 200°C) until a pressure drop of 110–160 mbar was reached (corresponding to a particulate hold-up of about $10 g L^{-1}$). Once complete, trap regeneration was induced by post injecting diesel fuel, with a metering pump, in the exhaust gases, and burning the resulting gases in an oxidizing honeycomb catalyst (OXICAT by Johnson Matthey) placed just upstream from the trap. The time needed for completing trap regeneration (e.g., combustion of the soot hold-up) is indicative of the catalyst performance; the higher the catalyst activity, the less amount of time required. Figure 11b shows the activity of a catalyzed cordierite trap compared to a non-catalyzed wall-flow trap. The regeneration was achieved only for the structured catalyst at about 600°C. Figure 11c shows a direct observation of the non-catalytic and catalytic traps, enlightening that the regeneration is not complete. In fact, soot combustion starts in the centre of the structure, where the hotgases concentrated their flow with lower pressure drop and higher temperature. However, the regenerated zone is larger for the catalytic trap than for the noncatalytic one. Interestingly, the catalytic trap made

Fig. 11. (a) SEM images of a cordierite wall-flow trap coated with LaCr_{0.9}O₃; (b) soot loading and regeneration cycles for a catalytic (LaCr_{0.9}O₃) and a non-catalytic wall-flow cordierite trap; and (c) images of the inlet side of a non-catalytic (left) and LaCr_{0.9}O₃ catalytic (right) cordierite wall-flow monoliths after regeneration. Data rearranged from [71].

with SiC resulted fully regenerated. This effect was explained by the higher thermal conductivity of SiC $(55 W m^{-1} K^{-1})$ compared to cordierite $(2.8 W m^{-1} K^{-1})$ ¹). In fact, the 20 times higher value of thermal conductivity of SiC favors the transfer of the heat, released by soot combustion, to adjacent channels. This then ignites regeneration step and completes the regeneration throughout the entire trap.

Volatile organic compounds (VOC) are a large group of low molecular-weight organic chemicals that are emitted from a great variety of sources; such as industrial processes, transport, household activities, and so on. Catalytic oxidation is considered to be one of the most effective techniques for VOC removal. This is because the total oxidation of diluted fuels occurs at relatively low temperatures leading to low emissions of NO*x* and unburned fuels. For this purpose, Piumetti et al. [77] recently synthesized Mn_3O_4 based structured catalysts based on cordierite monoliths, by SCS. They dipped cylindrical cordierite honeycombs in a solution of Mn nitrate and glycine, and placed the impregnated supports in an oven at 500°C for 30 min. The procedure was repeated until 0.48 g of catalyst was deposited on each monolith. Figure 12a shows the difference between a bare and a coated monolith, whereas the SEM images illustrate the thin, spongy catalyst layer that is uniformly distributed along the walls of the monolith. Catalytic tests were carried out in a stainless-steel reactor, heated in a horizontal split tube furnace, by feeding a reactive mixture (containing 1000 ppm of ethylene, propylene, and toluene, 10 vol % oxygen, and nitrogen to balance). The catalytic reaction started when the structured catalyst reached a temperature of 100°C, then it reached full VOC oxidation at 310°C, as shown in Fig. 12b. The excellent catalytic activity was maintained, even increasing the gas hourly space velocity up to four times, which is fundamental for process intensification. The good catalytic activity of Mn_3O_4 was ascribed to the abundantce of Brønsted acidic Mn– OH sites, which are beneficial for the total oxidation of

Fig. 12. (a) Picutre and SEM images of a cordierite monolith coated with $Mn₃O₄$ and (b) catalytic performance of a monolith coated with Mn_3O_4 for the total oxidation of a VOC mixture (1000 ppm mixture of ethylene, propylene, and toluene, 10 vol % O_2 , N_2 = balance) at different gas hourly space velocity. Data rearranged from [77].

VOC, since they are responsible for the adsorption/desorption rates of both reactants and products.

Methane is generated by various human activities, such as natural gas engines or coal mines. Methane is the second most abundant greenhouse gas, where it can trap about 20 times more heat than $CO₂$ and its presence in the atmosphere affects the climate. The abatement of methane emissions lies in the activation of the C−H bonds, which requires high temperature and leads to radical reactions that have low intrinsic selectivity. Thus, catalytic combustion represents a promising option to oxidize nearly 100% of methane, in the exhaust stream, at temperatures below 400°C. Ercolino et al. [45, 46] prepared a series of structured $Pd/Co₃O₄$ catalysts using open cell foams made of alumina, zirconia, and carborundum, comparing their performance against an alumina monolith. All structured catalysts were prepared via SCS, to coat a thin layer of $Co₃O₄$, followed by wet impregnation to deposit Pd, to ensure that all Pd was available on the surface of $Co₃O₄$. First, all structures were cleaned with a solution of water/acetone. The authors dipped each structure in a 3 M solution of Co nitrate and glycine, with $\phi = 0.25$. After removing the solution in excess, the impregnated structures were placed in an oven at 250°C for 15 min. The operation was repeated several times to reach an amount of $Co₃O₄$ equal to 200 mg. The structures were then calcined at 600°C for 4 h in calm air. After this, 3 wt % palladium was deposited by dipping the structure into a solution containing Pd nitrate, followed by calcining again at 600°C for 4 h in calm air. Adhesion tests carried out on both the coated monoliths and foams, demonstrated excellent stability of the catalytic coating, showing a weight loss of $0.7-1.4$ wt % after 1 h sonication (depending on the geometrical properties of the foams [46]). The structured catalysts were tested towards the lean combustion of methane by feeding 0.5 and 1 vol% of methane in nitrogen, with a constant oxygen-to-methane molar ratio equal to 8, at different weight hourly space

velocity (WHSV = 30, 60, and 90 NL $h^{-1} g_{cat}^{-1}$).

Figure 13a shows the catalytic activity of all foams (30 ppi) and the monolith, with $CH_4 = 0.5\%$ and $WHSV = 30$ (bare structures visible in Fig. 13b), along with the activity of pure $Pd/Co₃O₄$ powder for reference. The three structured foams show better catalytic performance compared to the pure $Pd/Co₃O₄$ powder, which is better than the performance of the catalyzed monolith. In particular, among the three types of foams, the better performance belongs to the zirconia catalyzed one. In fact, the coated zirconia can reach full methane conversion below 350°C at 30 WHSV. When WHSV is increased, the performance of all foams worsen slightly, with the order of reactivity being zirconia > alumina > carborundum. The better performance of zirconia foams can be explained considering their lower volumetric heat exchange coefficients, which favor the reaction heat removal by convection via the flue gases. Figure 13c shows SEM images of $Pd/Co₃O₄$ as a powder and as a layer on the foams; the comparison of the two images shows the same truncated octahedron crystals, typical of the $Co₃O₄$ spinel material. This is a clear sign that SCS allows for the preparation of the desired catalytic materials, not only, at powder level, but at structured level, as well. From the preliminary catalytic screening, the best structured catalyst (the coated zirconia 30 ppi), was exposed to a repetitive series of catalytic tests

Fig. 13. (a) Catalytic performance of various 30 ppi foams (zirconia, carborundum, and alumina) and a 100 cpsi alumina monolith coated with 3% Pd/Co₃O₄ for the lean combustion of methane in lean conditions (0.5% CH₄, λ = 2, weight hourly space velocity = 30 NL h $^{-1}$ g $_{\rm cat}^{-1}$); (b) images of the bare structures used as a support and of the Pd/Co₃O₄ powder; (c) FESEM images of Pd/Co₃O₄ as powder and lined over the structrured catalyst; (d) catalytic performance of the 3% Pd/Co₃O₄ coated 30 ppi zirconia foam after 0, 20, and 200 h of TOS at 400 °C in lean combustion conditions (0.5% CH₄, $\lambda = 2$, weight hourly space velocity = 30 NL h⁻¹ g-1); (e) FESEM images of Pd/Co₃O₄ lined over the structured zirconia catalyst after 0 and 200 h TOS; and (f) SEM/EDS overall and combined mapping of 3 wt $\%$ Pd/Co₃O₄ on zirconia foam after 200 h TOS. Data partially rearranged from [45, 46].

for an overall time-on-stream (TOS) of 200 h, with a series of start/stop. Specifically, the reactor was fed with a reactive mixture containing 0.5 vol % methane at 30 WHSV, maintaining a combustion temperature fixed at 400°C. Figure 13d shows excellent results of the catalytic activity in fresh conditions, and after 20 and 200 h of TOS. After 200 h TOS, the shift of the methane conversion curve towards higher temperatures is very limited, and the structured catalyst can fully convert methane at temperatures below 400°C. Figure 13e shows FESEM images of the fresh and used (after 200 h TOS) foams, made up of structured zirconia coated with $Pd/Co₃O₄$. The comparison of the

images enlightens a variation of the morphology of the catalytic layer. In particular, the surface of the aged catalyst appears highly corrugated, with lots of cracks, mainly due to the long-time exposure at relatively high temperature. The apparent increase of the specific surface area is due to the surface roughening and could on one hand reduce palladium dispersion, explaining thus the reduction of the performance, but on the other hand it may enhance the adsorption of product molecules, thus favoring conversion and limiting the decrease in activity. Figure 13f shows SEM/EDS mapping of the surface of the aged catalyst, enlightening homogeneity and good distribution of each element (O, Co, and Pd). The average weight percentage of Pd, 3.75%, is close to the theoretical value of 3%, with small variations depending on the measured area (atomic Pd/Co ratio variable from 0.034 to 0.039).

The presence of Zr in the elemental mapping image strongly suggest that the thickness of the catalytic coating is very thin, less than 50 μm. This is a clear demonstration that deposition of catalysts via SCS, on ceramic supports, is a viable way to synthesize structured catalysts.

OUTLOOK AND FUTURE PERSPECTIVES

Solution combustion synthesis (SCS) is a preparation method for inorganic materials of any nature and shape. This technique was first described at the end of the 1960s, as the solid-flame combustion for the preparation of ceramic and intermetallic compounds. Over the past five decades, SCS become an effective economical process with short reaction times and low energy requirements, needed only during the initial ignition step of the combustion reaction. Moreover, SCS requires relatively cheap reactants, simple equipment, and low-cost facilities, allowing the reduction of production costs, compared to conventional manufacturing processes. These facts imply that energy production must be increased, while managing the unceasing requirements of new products, all while taking care of the environment. Thus, SCS can be envisaged as a manufacturing technique that perfectly suits the requirements of process intensification, such as cleaner, safer, smaller, and more energy-efficient matters. The intrinsic energy-saving and high purity of the desired products make SCS an attractive, innovative, and intriguing technique to produce structured catalysts. The process is easily scaled up to any kind of size, and type of application. Until now, SCS has been used to produce different materials, such as advanced ceramics, catalysts, pigments, composites, intermetallic, nanomaterials, and structured catalysts, with reproducible safe mass productions at a lab-scale up to 1 kg of nano-materials per hour [11, 12]. All the cases reported in this mini-review showed that SCS is a good technique to deposit catalysts on various structures different for geometry (monoliths, spheres, foams, etc.) and materials (cordierite, alumina, zirconia, silicon carbide, iron, etc.). Moreover, these structured catalysts exhibit good performance for different applications, such as syngas production via biogas reforming or ethanol decomposition; methane oxidation; soot, NO*x*, and VOC abatement, to name a few examples.

Lastly, SCS presents some disadvantages, among all, being the formation of NO_x during the combustion reaction [18, 20, 28, 48, 49, 53]. Metal nitrate precursors can undergo partial thermal oxidation, thus releasing NO_x , and the organic fuels that contain nitrogen atoms (urea, glycine, β-alanine, etc.) that decompose to generate NO*x*. Besides this, being the thermal decomposition of N-containing molecules is limited, and only small amounts of NO*x* are released, at the lab-scale. Surely, in the case of industrial scaleup, NO*x* emissions can represent a critical environmental issue. In this case, a specific selective catalytic reduction plant, with ammonia, must be considered. This critical problem could be overcome by carefully, and strategically, selecting the organic fuels necessary to ignite the combustion reaction. In fact, just as an example, the use of glycerol (a free-N containing molecule) as a fuel is particularly interesting to reduce NO*x* emissions [53].

In the end, the SCS method can be considered as a viable, inexpensive, environmentally-friendly, energy saving, and safe manufacturing process used to synthetize structured catalysts for many different applications.

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