

## Scandium on the formation of in situ TiB<sub>2</sub> particulates in an aluminum matrix

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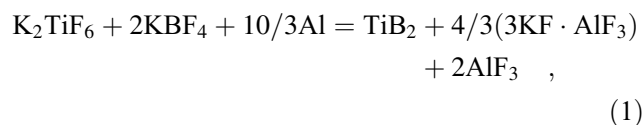
TiB<sub>2</sub> particulates were formed in situ in an aluminum matrix via chemical reactions between an aluminum melt and the mixture of K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> salts. Different effects of Sc addition on the formation of the TiB<sub>2</sub> particulates were revealed depending on the participation of Sc at different stages of the formation of the particulates. The metal–salt reactions resulted in boride layers along the α-Al grain boundaries in the presence of Sc, while the addition of Sc after the metal–salt reactions broke up the boride layers improving the dispersion of the TiB<sub>2</sub> particulates to a limited degree. Sc promoted the growth of the TiB<sub>2</sub> particulates, resulting in the coarsening of TiB<sub>2</sub> particulates. The participation of Sc in the formation of TiB<sub>2</sub> particulates altered the coarsening of the TiB<sub>2</sub> particulates, resulting in different morphologies of the TiB<sub>2</sub> particulates depending on the participation of Sc in the formation of the TiB<sub>2</sub> particulates at different stages.

### I. INTRODUCTION

Aluminum alloys reinforced with ceramic particulates, aluminum metal matrix composites (MMCs),<sup>1,2</sup> show a high potential in meeting the ever-increasing demand for property improvement, such as high strength and high modulus, from the fast growing aerospace, electronics, and automotive industries.<sup>1–4</sup> Aluminum alloys, as matrices, are featured with low density, high thermal conductivity, and plasticity. Meanwhile, the ceramic particulates offer high strength and moduli. Among various ceramic reinforcements, TiB<sub>2</sub> particulates have attracted a great deal of attention due to their high strength, hardness, and strong covalent bonding with the aluminum matrix.<sup>5–15</sup> The most attractive property of TiB<sub>2</sub> as reinforcement is its good wettability by an aluminum melt, resulting in strong bonding to the aluminum matrix, which transfers stress from the matrix to the reinforcing particulates effectively in service with improved strength. A good wettability is also a key factor for obtaining uniform dispersion of the reinforcing particulates and therefore homogeneous properties of the composites. In comparison, other ceramic particulates, such as Al<sub>2</sub>O<sub>3</sub>, SiC, etc., are not wetted by an aluminum melt, causing difficulties in dispersion into an aluminum melt

and therefore weak matrix/reinforcement interfacial bonding and possible premature failure.<sup>1,2,16–19</sup>

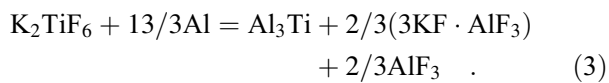
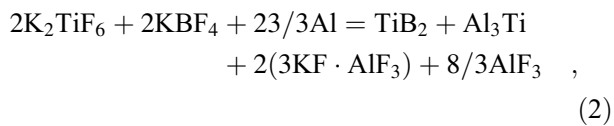
TiB<sub>2</sub> particulates can be introduced into an aluminum matrix as preformed particulates (ex situ) or formed in situ in the matrix. In situ fabrication eliminates possible oxygen contamination, producing a clean TiB<sub>2</sub>/Al interface and, therefore, strong TiB<sub>2</sub>/Al interfacial bonding after solidification.<sup>5–14</sup> A popular method in synthesizing in situ TiB<sub>2</sub> particulates is through salt–metal reactions by adding mixed K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> salts into an aluminum alloy melt derived from the production of Al–Ti–B type master alloys for grain refinement.<sup>20</sup> From the beneficial effects of TiB<sub>2</sub> in aluminum grain refinement, the advantages of TiB<sub>2</sub> particulates as reinforcement are obvious.<sup>5,6</sup> Possible chemical reactions between an aluminum melt and mixed salts are presented as reactions (1)–(3) without the consideration of AlB<sub>2</sub> formation, where Ti and B are reduced from fluoride salts by aluminum.<sup>10</sup> The Ti and B in solution will then form TiB<sub>2</sub> particulates in an Al melt. The formation of AlB<sub>2</sub> as a separate phase or in solid solution with TiB<sub>2</sub> is possible by considering the production of Al–B master alloys from reactions of KBF<sub>4</sub> and an aluminum melt.<sup>21–24</sup>



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According to reactions (1)–(3), TiB<sub>2</sub> and Al<sub>3</sub>Ti particulates in a variable ratio can be produced by reactions between an aluminum melt and a mixture of K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> salts. The formation of Al<sub>3</sub>Ti particulates can be avoided by varying the K<sub>2</sub>TiF<sub>6</sub>/KBF<sub>4</sub> ratio to reaction (1). However, a small amount of excess Ti in solution is beneficial for the dispersion of TiB<sub>2</sub> particulates by promoting the nucleation of aluminum grains on the TiB<sub>2</sub> particulates.<sup>7,25</sup> Among the reaction products, TiB<sub>2</sub> is the most stable phase thermodynamically because of its lowest standard free energy change of formation.<sup>26</sup> However, it is unavoidable to form AlB<sub>2</sub> intrinsic to the chemical reactions, where aluminum participates in the reactions with boron.<sup>12,13</sup> Different diborides form solid solutions in the aluminum melt with a high tendency to transform into mixtures of diborides, TiB<sub>2</sub>, AlB<sub>2</sub>, etc, which is not widely agreed.<sup>5,12,13</sup> TiB<sub>2</sub> is generally treated as the final product in the aluminum melt due to difficulties in distinguishing different diboride phases in an aluminum alloy. The beneficial effects of adding TiB<sub>2</sub> particulates into aluminum alloys have been reported despite the debate about phase formation.<sup>18,19,27</sup> However, the complicated chemical reactions between the salts and aluminum melts and the exothermal nature of the reactions lead to difficulties in controlling the size and morphology of the TiB<sub>2</sub> particulates, which must be resolved before a wide spread application of in situ TiB<sub>2</sub> particulate reinforced aluminum MMCs.

Efforts on producing uniform dispersion of fine in situ TiB<sub>2</sub> particulates have been made mainly through altering the reaction chemistry and applying mechanical agitation. The latter includes mechanical shearing, ultrasonic sonication, electromagnetic stirring, etc., leading to an improved dispersion of the TiB<sub>2</sub> particulates and therefore increased mechanical properties.<sup>26,28,29</sup> Meanwhile, the former focuses on the effects of alloying elements on the growth and dispersion of the in situ TiB<sub>2</sub> particulates.<sup>10,30–36</sup> The effects of different alloying elements have been revealed as either forming solid solutions with TiB<sub>2</sub> leading to coarsening or modifying the interfacial energies to promote the nucleation of the TiB<sub>2</sub> particulates, resulting in fine sized particulates. Specifically, magnesium as an alloying element promotes the nucleation of TiB<sub>2</sub> particulates, while zirconium leads to coarse TiB<sub>2</sub> particulates. Interestingly, TiB<sub>2</sub> particulates also modify the morphology of eutectic Si in an Al–Si

alloy.<sup>36</sup> The addition of alloying elements in modifying the in situ TiB<sub>2</sub> particulates also resulted in the increase of mechanical properties.<sup>30–36</sup>

By considering the significant strengthening effects of Sc in aluminum alloys and the increasing applications of Al alloys containing Sc,<sup>36–38</sup> understanding the effects of Sc on the formation of in situ TiB<sub>2</sub> particulates becomes imminent. However, there is hardly information available about the effects of Sc on the formation of TiB<sub>2</sub> particulates. Sc forms Al<sub>3</sub>Sc in aluminum either as a strong aluminum grain refiner or dispersoid for precipitation hardening depending on its concentration in an alloy.<sup>37</sup> As reported, when being added into the A356 alloy, Sc has combined effects of being an effective grain refiner as well as Si modifier, modifying the morphology of eutectic Si from needle-like to spheroidal particulates.<sup>38</sup>

From the above review, the addition of TiB<sub>2</sub> particulates into aluminum alloys is effective in strengthening the alloys. Additionally, there is a possibility of adding Sc to increase the properties of the in situ TiB<sub>2</sub> particulate reinforced aluminum MMCs. However, information on the effects of Sc addition on the formation and dispersion of the TiB<sub>2</sub> particulates in Al–TiB<sub>2</sub> composites is lacking, which is the knowledge gap that this article tries to fill.

## II. EXPERIMENTAL PROCEDURES

A series of in situ TiB<sub>2</sub> particulate reinforced aluminum MMCs were fabricated with the modification of Sc addition. Pure aluminum (99.99% purity) was placed in a graphite crucible and melted inside an electrical resistant furnace. K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> salts were used to introduce alloying elements Ti and B. Sc was deployed as an Al–2 wt% Sc master alloy. Al–TiB<sub>2</sub>–Sc alloys with 5 wt% TiB<sub>2</sub> particulates and 0.2 wt% Sc were designed. As listed in Table I, an Al–2 wt% Sc master alloy was added under three different sequences to evaluate the effects of Sc addition at different stages of the reactions between the salts and the aluminum melt. When adding

TABLE I. Experimental details for producing Al–TiB<sub>2</sub> (Al–TiB<sub>2</sub>–Sc) MMCs.

Composites	Sample no.	Percentage of Sc added as Al–2 wt% Sc		Holding time (min)
		Before reaction	After reaction	
Al–TiB <sub>2</sub>	1	...	...	15
	2	...	...	60
	3	0.2	...	15
	4	0.2	...	60
Al–TiB <sub>2</sub> –Sc	5	...	0.2	15
	6	...	0.2	60
	7	0.1	0.1	15
	8	0.1	0.1	60

the salts and the Al–Sc master alloy, manual stirring was applied to alleviate the possible agglomeration of reaction products. The reaction temperature was set to 820 °C when the raw materials were melted and alloying elements were added. A holding time for the chemical reaction were set as 15 and 60 min to study their effects on the reaction products. This is based on microstructure analysis showing a 60 min holding time leading to a better dispersion of TiB<sub>2</sub> particulates, whereas a holding time longer than 60 min might not be suitable, as reported by Birol.<sup>21,22</sup> Salt products on top of the melt were decanted before casting the melt into a steel mold. A pouring temperature was chosen as 720 °C and the melt was poured into a steel mold and cooled down to the room temperature. The process is shown in Fig. 1 schematically.

After casting, the ingots were sectioned, ground, polished, and etched following a standard procedure for metallurgical sample preparation for scanning electron microscopy (SEM) and energy dispersive X-ray (EDX) analysis. The SEM images were taken by using an FEI 3D Quanta Dual Beam SEM (ThermoFisher Scientific, Hillsboro, Oregon) operated at 20 kV. Secondary electron images (SEIs) were also taken on deep-etched samples that were prepared by submerging the samples into a solution that consists of 250 mL methanol, 10 g iodine, and 25 g tartaric for 50–60 min, and soaking the samples in acetone until the solvent was clear. The etched samples were then rinsed with acetone and dried up for SEM examination. EDX analysis was performed to reveal the compositions of the particulates.

### III. RESULTS AND DISCUSSION

The overall dispersion of the in situ TiB<sub>2</sub> particulates in the aluminum matrix is presented in Figs. 2(a)–2(h),

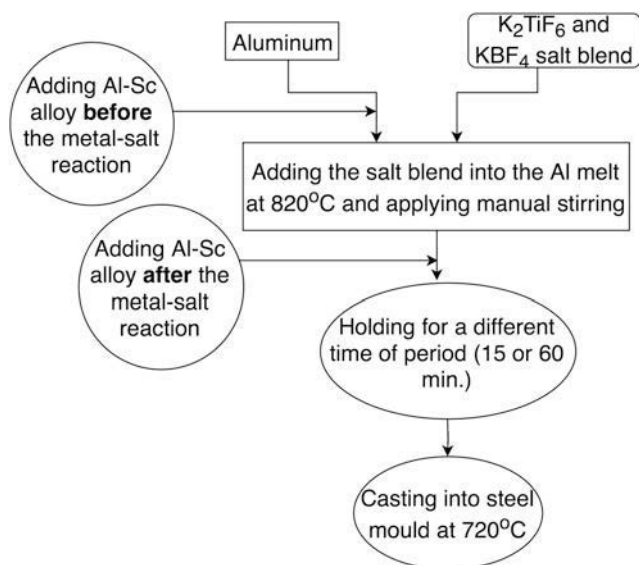


FIG. 1. Schematic processing chart showing the participation of Sc in different stages of the salt–metal reaction.

the back-scattered electron images (BEIs) of eight samples in Table I under a SEM. These images are featured with clusters of diboride particulates along the aluminum grain boundaries, in accordance with the typical dispersion of the diboride particulates in aluminum master alloys, evidencing the weak ability of TiB<sub>2</sub> particulates in nucleating aluminum grains in solidification.<sup>10,11,25,39</sup> The TiB<sub>2</sub> particulates were therefore pushed by the solidifying front of the  $\alpha$ -Al grains to the aluminum grain boundaries during solidification.<sup>7,8,10–12,40,41</sup> The only noticeable difference in the images caused by Sc is the different thickness of the TiB<sub>2</sub> layers.

Figures 2(a) and 2(b) are the micrographs of the in situ Al–TiB<sub>2</sub> composites produced without the addition of Sc for a holding time of 15 and 60 min (i.e., Samples 1 and 2), respectively. TiB<sub>2</sub> particulates agglomerate along the  $\alpha$ -Al grain boundaries under these conditions. Figures 2(c) and 2(d) show the micrographs of Samples 3 and 4, in which Sc was participating in the metal–salt reactions for a holding time of 15 and 60 min. It can be found from Fig. 2(c) that the TiB<sub>2</sub> particulates tend to agglomerate into layers at the  $\alpha$ -Al grain boundaries. This indicates that the participation of Sc in the metal–salt reactions results in a different way of agglomeration of the TiB<sub>2</sub> particulates along the  $\alpha$ -Al grain boundaries from the one without Sc addition in Fig. 2(a). Figures 2(e) and 2(f) show the BEIs of Samples 5 and 6, which have Sc added after the metal–salt reactions for a holding time of 15 and 60 min, respectively. By comparing Figs. 2(b)–2(f) (Samples 2 and 6) with the same holding time but under different Sc addition sequences, it is clear that TiB<sub>2</sub> particulates are dispersed rather broadly in Fig. 2(f) than in Fig. 2(b), though the particulates still agglomerated along the  $\alpha$ -Al grain boundaries. These results suggest that the addition of Sc after the metal–salt reactions promotes the dispersion of TiB<sub>2</sub> particulates though still along the  $\alpha$ -Al grain boundaries comparing with the dispersion of TiB<sub>2</sub> particulates when Sc was participating in the metal–salt reactions. Figures 2(g) and 2(h) present the BSIs of Samples 7 and 8, with the addition of Sc both before and after the metal–salt reactions for holding times of 15 and 60 min, respectively. It is evident that the agglomeration of the TiB<sub>2</sub> particulates alleviated in Fig. 2(h) (Sample 8) compared to Fig. 2(b) (Sample 2).

In brief, the addition of Sc influences the dispersion of the in situ TiB<sub>2</sub> particulates to a certain degree. To be specific, the participation of Sc in the metal–salt reactions causes a layer-like agglomeration of the TiB<sub>2</sub> particulates along the  $\alpha$ -Al grain boundaries, while the addition of Sc after the reactions (without the participation of Sc in the metal–salt reactions) alleviates the agglomeration at the grain boundaries.

Figures 3(a)–3(h) are the SEIs of deep-etched Samples 1–8, showing the overall morphologies of the in situ TiB<sub>2</sub> particulates at the Al grain boundaries. Hexagonal TiB<sub>2</sub>

particulates in the Al–TiB<sub>2</sub> composites are revealed in all the samples, in agreement with other findings.<sup>26,42–44</sup> The growth of the in situ TiB<sub>2</sub> particulates in the absence of Sc with respect to holding time is not clear by comparing Figs. 3(a) and 3(b). In Fig. 3(a), most of the individual TiB<sub>2</sub> particulates are blocky in submicrometer sizes and only a small portion of the TiB<sub>2</sub> particulates have grown into sizes near 2 μm, similar to the TiB<sub>2</sub> particulates in Fig. 3(b). The result indicates that the effects of the

holding time on the growth of the TiB<sub>2</sub> particulates are limited in the absence of Sc. In comparison, Sc addition resulted in the growth of the in situ TiB<sub>2</sub> particulates in different ways depending on the sequence of the addition of Sc and, therefore, its participation in the formation of the TiB<sub>2</sub> particulates at different stages, which is to be discussed in the following paragraphs.

The participation of Sc in the metal–salt reactions resulted in the growth of the TiB<sub>2</sub> particulates for both

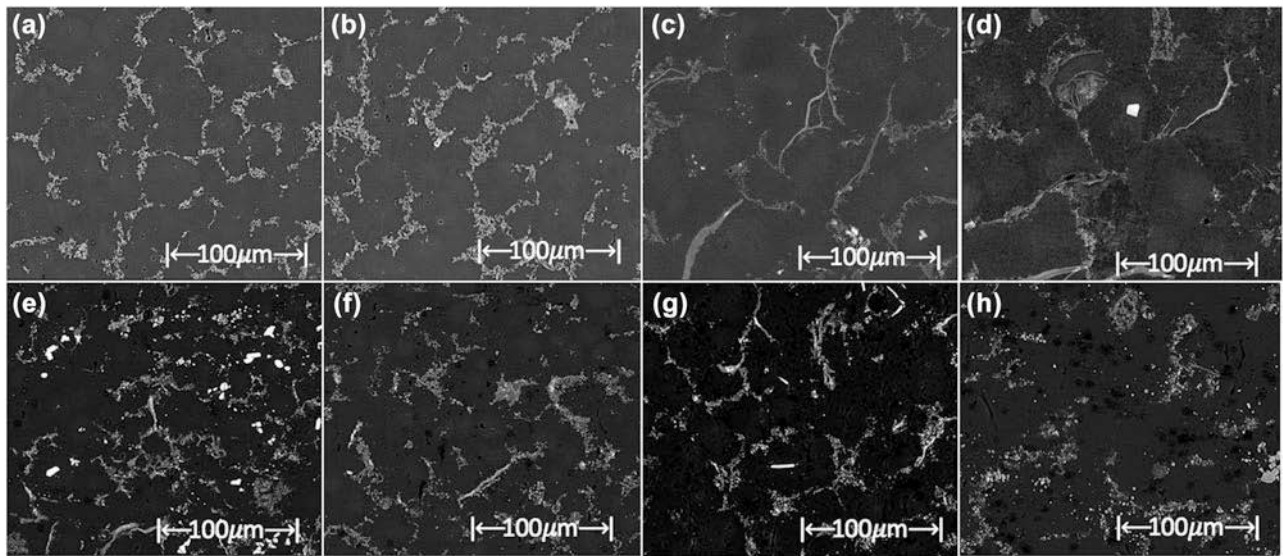


FIG. 2. BSE images of Samples 1–8 showing the dispersion of in situ diboride particles: (a) No addition of Sc (15 min); (b) No addition of Sc (60 min); (c) Adding Sc before the metal–salt reaction (15 min); (d) Adding Sc before the metal–salt reaction (60 min); (e) Adding Sc after the metal–salt reaction (15 min); (f) Adding Sc after the metal–salt reaction (60 min); (g) Adding Sc both before and after the metal–salt reaction (15 min); (h) Adding Sc both before and after the metal–salt reaction (60 min).

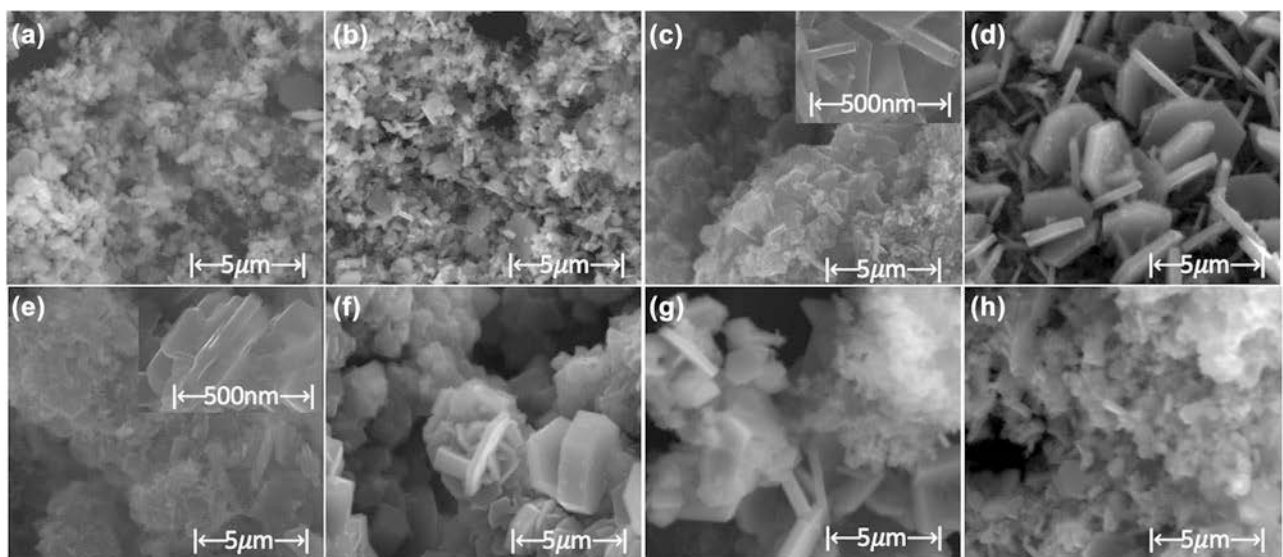


FIG. 3. SEIs of deep-etched Samples 1–8 showing the morphologies of in situ diboride particles: (a) No addition of Sc (15 min); (b) No addition of Sc (60 min); (c) Adding Sc before the metal–salt reaction (15 min); (d) Adding Sc before the metal–salt reaction (60 min); (e) Adding Sc after the metal–salt reaction (15 min); (f) Adding Sc after the metal–salt reaction (60 min); (g) Adding Sc both before and after the metal–salt reaction (15 min); (h) Adding Sc both before and after the metal–salt reaction (60 min) (Inserted figures in (c) and (e) are magnified typical TiB<sub>2</sub> particles).

holding times of 15 and 60 min, which is clear by comparing Figs. 3(c) and 3(d) to 3(a) and 3(b), respectively. Sc promotes the growth of TiB<sub>2</sub> plates through fusion at a short holding time (15 min) and individual plates at a longer holding time (60 min). The effects of holding time on the morphologies of the in situ TiB<sub>2</sub> particulates are clear by comparing Figs. 3(c) and 3(d). A longer holding time of 60 min resulted in the growth of the TiB<sub>2</sub> particulates into about 5 μm in size in Fig. 3(d) from about 2 μm in Fig. 3(c). No obvious growth of the thickness of the hexagonal TiB<sub>2</sub> disks was observed with the increase of holding time, resulting in disks with a larger aspect ratio. These results suggest that the participation of Sc in the metal–salt reactions promotes preferentially the growth of the {0001} planes of the TiB<sub>2</sub> particulates in such a way that it restricts the growth in the [0001] direction comparatively.<sup>5</sup>

When Sc was added after the metal–salt reactions, TiB<sub>2</sub> particulates tend to grow together by {0001} planes at a short holding time (15 min), which is clear in the inset in Fig. 3(e). It can be attributed to that Sc modifies the {0001} planes of the TiB<sub>2</sub> particulates.<sup>5</sup> The growth of the TiB<sub>2</sub> particulates has reached a completion after 60 min, evidenced by the perfect hexagonal shape of the particulates in Fig. 3(f). The growth of TiB<sub>2</sub> particulates is affected largely by the addition sequence of Sc, i.e., the participation in metal–salt reactions or modification of the particulate surfaces. From Fig. 3(e) (Sample 5), it can be found that a large amount of TiB<sub>2</sub> particulates tend to grow up with a blocky morphology with a 15 min holding time. When the holding time increased to 60 min, the TiB<sub>2</sub> particulates coarsened to size of several micrometers and remained blocky. Therefore, it can be proposed that when adding Sc after the metal–salt reactions (without Sc participating in metal–salt reactions), Sc promotes the coarsening of the TiB<sub>2</sub> particulates in all crystal directions though growth or coalescence.

The effects of adding Sc half amount before and the rest half after the metal–salt reactions resulted in TiB<sub>2</sub> particulates in different sizes, which may grow after a longer holding time, as shown in Figs. 3(g) and 3(h). Figure 3(g) shows only a portion of the TiB<sub>2</sub> particulates have grown up to disks about 5 μm, meanwhile the rest are in smaller sizes agglomerated together. A longer holding time (60 min) promoted the growth of the smaller particulates as shown in Fig. 3(h).

Figure 4 is a high magnification SEI of Sample 5 produced by adding Sc after the metal–salt reactions, and Figs. 5(a) and 5(b) are the illustrations of the coarsening of the in situ TiB<sub>2</sub> particulates. As indicated by arrows in Fig. 4, TiB<sub>2</sub> particulates grew in a layer-by-layer manner along the axis of the hexagonal disks. The particulates may grow into a rod-like shape, which is indicated by arrow 1 in Fig. 4 and in Fig. 5(a) or

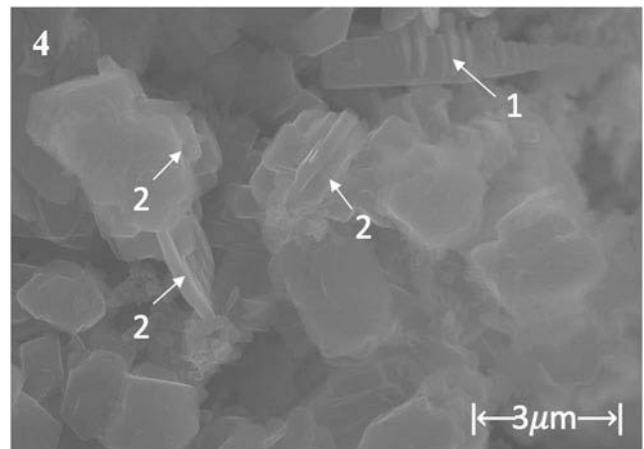


FIG. 4. High magnification SEI of deep-etched Sample 5 showing coarse TiB<sub>2</sub> particles: Arrow (1) rod-like TiB<sub>2</sub> particles; Arrow (2) terrace-like blocky TiB<sub>2</sub> particles.

a terrace-like blocky shape, which is shown by arrow 2 in Fig. 4 and in Fig. 5(b). In Fig. 5(a) (also see arrow 1 in Fig. 4), TiB<sub>2</sub> particulates were growing together separately along a rod-like base parallel to each other. On the other hand, in Fig. 5(b) (also see arrow 2 in Fig. 4), TiB<sub>2</sub> particulates were coalescing upon each other without a distance between neighboring TiB<sub>2</sub> disks [arrow 1 in Figs. 4 and 5(a)]. However, these two growing behaviors of TiB<sub>2</sub> particulates still need further investigation.

By comparing Fig. 4 (Sample 5) and Fig. 3(c) (Sample 3), the coarsening mechanism is not applicable to Sample 3 that was produced by adding Sc before the metal–salt reactions, i.e., the participation of Sc in the metal–salt reactions does not result in similar coarsening of the TiB<sub>2</sub> particulates. The coarsening of the TiB<sub>2</sub> particulates is a direct effect of the modification of the surfaces of the TiB<sub>2</sub> particulates by Sc after the formation of TiB<sub>2</sub> particulates. By considering the high stability of TiB<sub>2</sub> in an aluminum melt,<sup>25</sup> the Ostwald ripening process is unlikely to happen, which is supported by the current results. Therefore, it can be elucidated that Sc modifies the surface of the TiB<sub>2</sub> particulates promoting coarsening of the particulates through a stacking process, i.e., coarsening by stacking TiB<sub>2</sub> disks on their hexagonal surfaces.

Figure 6(a) shows a magnified SEI of deep-etched Sample 4 with an EDX spectrum of a typical TiB<sub>2</sub> cluster from point 1 in the image of Fig. 6(b). EDX spectra from other four locations gave similar compositions to Fig. 6(b). Sc was detected in all the five coarse particulates. EDX analysis validates the participation of Sc in the coarsening of the in situ TiB<sub>2</sub> particulates by modifying the reaction chemistry and the surface energy of the TiB<sub>2</sub> particulates. However, a detailed mechanism about the influence of the Sc during the reaction is still not clear and that requires further investigation.

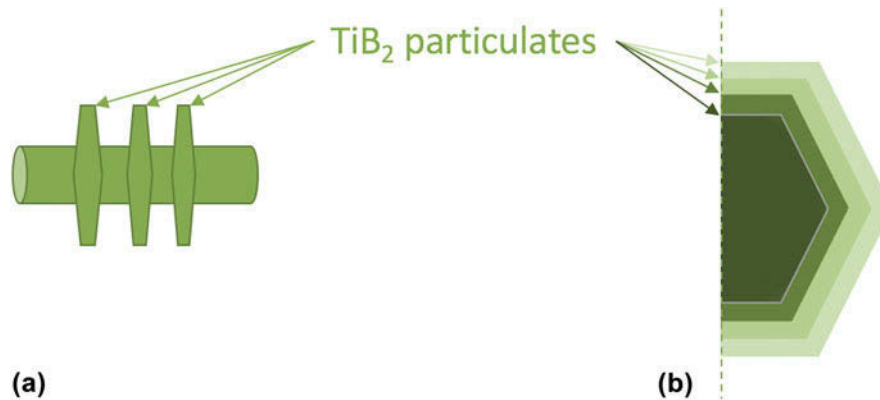


FIG. 5. Schematic drawings of the coarsening mechanisms: (a) rod-like shape and (b) terrace-like block shape.

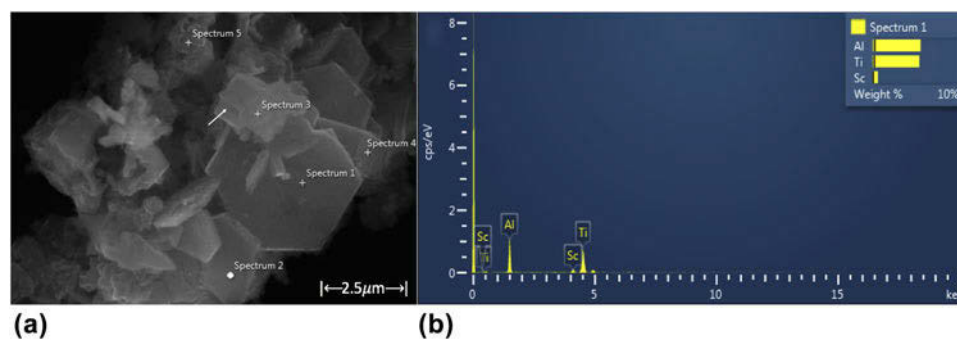


FIG. 6. Magnified SEI of deep-etched Sample 4 (a) with an EDS spectrum (b).

#### IV. CONCLUSIONS

In situ TiB<sub>2</sub> particulates were produced successfully in an aluminum matrix by the reactions of aluminum and a mixture of K<sub>2</sub>TiF<sub>6</sub> and KBF<sub>4</sub> salts with the addition of Sc at different stages of the metal–salt reactions. TiB<sub>2</sub> particulates agglomerated along the Al grain boundaries in all Al–TiB<sub>2</sub>–Sc MMCs and the distribution and growth of the TiB<sub>2</sub> particulates were influenced by the presence of Sc during or after the metal–salt reactions. The addition of Sc resulted in the coarsening of TiB<sub>2</sub> particulates, regardless of the participation of the Sc in the metal–salt reactions or not. The participation of Sc in the metal–salt reactions resulted in the formation of petal-like particulates, meanwhile, the addition of Sc after the metal–salt reactions led to the formation of coarse TiB<sub>2</sub> terraces bonded by the large surfaces of the individual TiB<sub>2</sub> disks. Sc also plays a role in promoting the growth of the {0001} planes when participated in the metal–salt reactions. By contrast, the TiB<sub>2</sub> particulates are blocky terraces, when the addition of Sc was made after the metal–salt reactions. EDX analysis validated the existence of Sc in coarse TiB<sub>2</sub> particulates and evidence of an active role of Sc in the formation of the in situ TiB<sub>2</sub> particulates. The paper focuses on the effects of Sc on the formation of in situ TiB<sub>2</sub> particulates without considering

possible effects on the mechanical properties of the MMCs.

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