

# Effect of Copper Additions on the Thermoelectric Properties of a Layered Calcium Cobaltite Prepared by Hot Pressing

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**Abstract**—Low-porosity layered calcium cobaltite-based ceramics with copper additions have been prepared by hot pressing and their microstructure and electrical transport and thermoelectric properties have been studied. The results demonstrate that the addition of copper particles to the ceramics reduces the average particle size of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  phase and the thermoelectric power and porosity of the samples and increases the electrical conductivity and thermoelectric power factor ( $P$ ) of the ceramics. The highest thermoelectric power factor is offered by the hot-pressed ceramic with the composition  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + 2 \text{ wt } \% \text{ Cu}$  ( $P_{1100} = 521 \mu\text{W}/(\text{m K}^2)$ ), which is a factor of 1.4 higher than that of the basic material  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  having the same thermal history ( $P_{1100} = 363 \mu\text{W}/(\text{m K}^2)$ ) and more than five times the thermoelectric power factor of low-density  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramics prepared by conventional solid-state reactions.

**Keywords:** thermoelectric ceramics,  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$ , Cu, hot pressing, electrical conductivity, thermoelectric power

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## INTRODUCTION

The layered calcium cobaltite  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  is the most promising basic component for designing  $p$ -leg materials for high-temperature thermoelectric generators because it offers high electrical conductivity ( $\sigma$ ) and thermoelectric power ( $S$ ) in combination with low thermal conductivity ( $\lambda$ ) and is stable in air at high temperatures [1]. The functional characteristics (thermoelectric power factor ( $P$ ) and thermoelectric figure-of-merit ( $ZT$ )) of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$ -based ceramics are significantly inferior to those of single crystals but can be appreciably improved by using low-temperature (solution phase) synthesis (an alternative to ceramic processing route) [2–5], the preparation of ceramics via hot pressing [3, 6–8] or spark plasma sintering [4, 9, 10], partial bismuth [6, 11, 12] or rare earth [13, 14] substitution for calcium and transition or heavy metal substitution for cobalt [15, 16], and generation of chemical [17] or phase inhomogeneities [18, 19].

Phase inhomogeneities in layered calcium cobaltite-based ceramics can be produced by annealing them at temperatures above the peritectoid decomposition temperature of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  phase ( $T_p =$

1199 K in air [20]); varying the cation stoichiometry of the starting mixture so as to bring the composition of the ceramic beyond the homogeneity range of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  [21] (according to Sedmidubsky et al. [20], in air a single-phase layered calcium cobaltite exists in the composition range  $\text{Ca}_3\text{Co}_{3.87}\text{O}_{9+\delta}$ – $\text{Ca}_3\text{Co}_{4.07}\text{O}_{9+\delta}$ ); and adding a second phase, such as a binary or mixed metal oxide [19, 22, 23] or metallic silver [6, 8, 24].

In the last case, the addition of Ag, a highly conducting phase, to ceramics makes it possible to considerably increase the electrical conductivity of the resultant composites and, as a consequence, improve their thermoelectric characteristics ( $P$  and  $ZT$ ). In particular, according to Xiang et al. [8] the thermoelectric power factor of a  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}/7.5 \text{ vol } \% \text{ Ag}$  composite at a temperature of 1000 K is  $0.47 \text{ mW}/(\text{m K}^2)$ , which is 40% above that of silver-free  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramics. Kahraman et al. [24] investigated the thermoelectric properties of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Ag}$  ( $x = 0, 1, 3, 5, 10$ ) composites and found that the highest  $P$  was offered by the material with the composition  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + 10 \text{ wt } \% \text{ Ag}$ , which had  $P = 0.43 \text{ mW}/(\text{m K}^2)$  at a tem-

perature of 1073 K, that is, 40% above that of the basic material  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$ .

The purpose of this work was to study the feasibility of improving functional characteristics of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$ -based ceramics produced by hot pressing via modification of them with copper particles.

## EXPERIMENTAL

Layered calcium cobaltite powder was prepared by the glycine–citrate–nitrate process. Aqueous 2 M solutions of calcium and cobalt nitrates prepared from  $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$  (analytical grade) and  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (analytical grade) were mixed with appropriate amounts of amino acetic acid ( $\text{NH}_2\text{—CH}_2\text{—COOH}$ ) (analytical grade) and citric acid ( $\text{C}_6\text{H}_8\text{O}_7$ ) (reagent grade) at a molar ratio of the components  $\Sigma n(\text{M}^{2+}) : n(\text{NH}_2\text{—CH}_2\text{—COOH}) : n(\text{C}_6\text{H}_8\text{O}_7) = 10 : 1 : 3$ . The resultant solution was boiled down with constant stirring on an IKA C-MAG HS-7 magnetic stirrer at a temperature near 373 K until gel formation. The resultant gel was further boiled down in an ITNS 1000 heating mantle at 673 K without stirring, which was accompanied by gel caramelization, foaming, and self-ignition in a separate point, with instantaneous combustion front propagation. The combustion of the xerogel led to the formation of a gray-brown powder, which turned black after calcination in air at 1073 K for 6 h.

The procedures used to synthesize copper nanoparticles (via reduction of copper nitrate with sodium borohydride in aqueous solution) and  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  ( $x = 1, 2, 5$ ) composites were described previously [25].

Sintered ceramics in the form of disks 20 mm in diameter and 2–5 mm in thickness were produced by hot pressing on a DSP-507 sintering press (Dr. Fritsch, Germany) in an argon atmosphere at a temperature of 1173 K and pressure of 16.7 MPa for 15 min. For electrical conductivity and thermoelectric power measurements, samples in the form of rectangular parallelepipeds  $4 \times 4 \times 7$  and  $4 \times 4 \times 20$  mm in dimensions were cut from the sintered ceramics and Ag electrodes were made on their end faces [26].

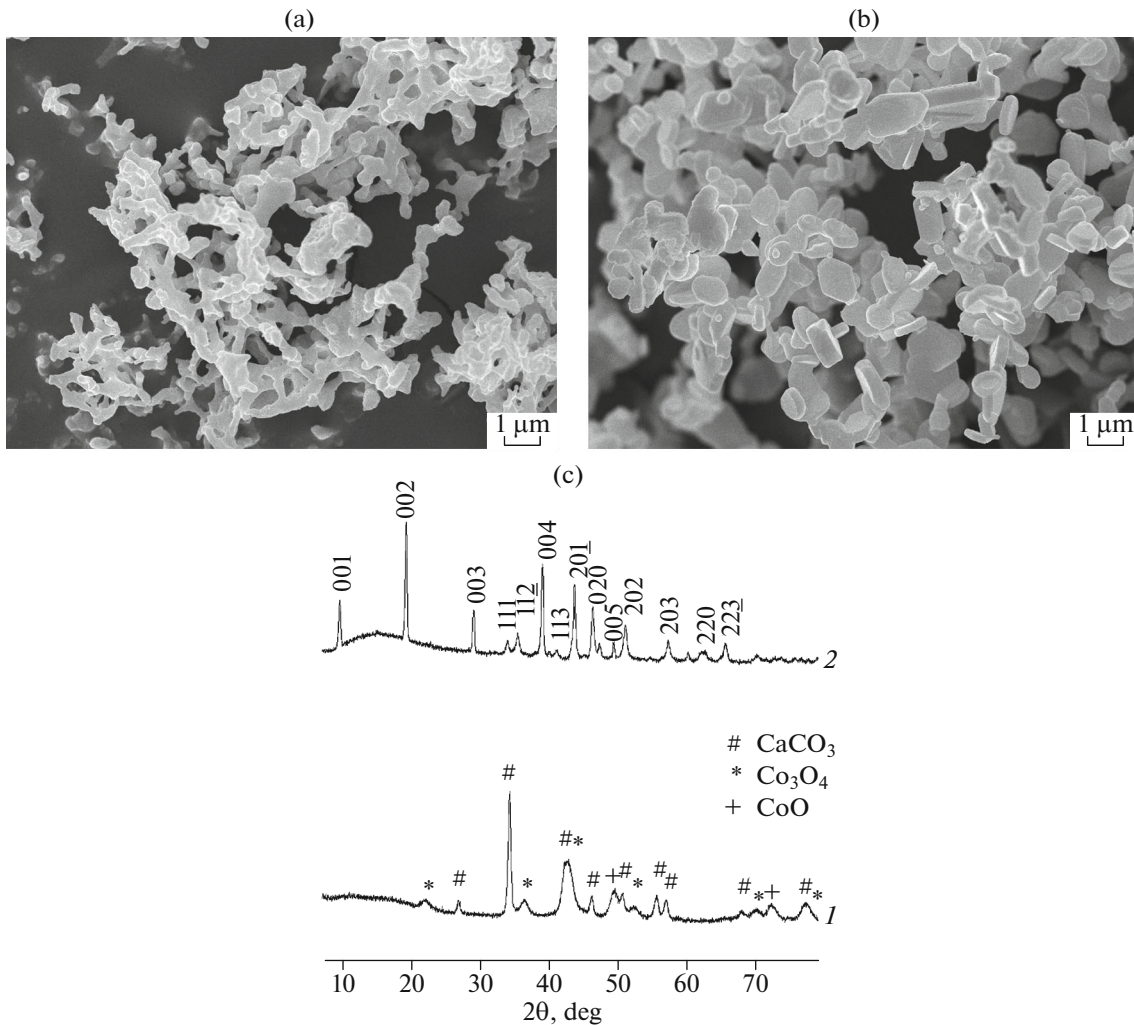
The phase composition of the samples was determined by X-ray diffraction on a STOE Theta/Theta diffractometer (Germany) with  $\text{CoK}_\alpha$  radiation. Their microstructure was examined by scanning electron microscopy (SEM) on a JEOL JSM-7500F (Tokyo, Japan). The apparent density ( $\rho_{\text{app}}$ ) of the sintered ceramics was determined by measuring the mass and dimensions of the samples, and their porosity was calculated as  $\Pi = (1 - \rho_{\text{app}}/\rho_x) \times 100\%$ , where  $\rho_x$  is the X-ray density of the samples ( $\rho_x = 4.677 \text{ g/cm}^3$  [27]).

The electrical conductivity and thermoelectric power of the materials were determined in air at temperatures from 300 to 1100 K in a direction perpendicular to the pressing axis, as described previously [26]. The activation energy ( $E_a$ ) for electrical conduction in the samples was evaluated using linear portions in plots of  $\ln(\sigma T)$  against  $1/T$ . The thermoelectric power factor was calculated as  $P = S^2\sigma$  [1]. The thermal diffusivity ( $\eta$ ) of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  ( $x = 1, 2, 5$ ) samples was measured at 300 K in a direction parallel to the pressing axis by the laser flash method with a Linseis LFA 1000 instrument (Germany). The thermal conductivity ( $\lambda$ ) of the samples was found using the relation  $\lambda = \eta\rho_{\text{app}}c_{\text{sp}}$ , experimentally determined thermal diffusivity and apparent density, and specific heat ( $c_{\text{sp}}$ ) evaluated from data reported by Sedmidubsky et al. [20]. The phonon ( $\lambda_{\text{ph}}$ ) and electron ( $\lambda_{\text{e}}$ ) contributions to the thermal conductivity of the ceramics were evaluated using the relations  $\lambda = \lambda_{\text{ph}} + \lambda_{\text{e}}$  and  $\lambda_{\text{e}} = \sigma LT$ , where  $\sigma$  is the electrical conductivity of the ceramics and  $L$  is the Lorenz number ( $L = 2.45 \times 10^{-8} \text{ V}^2/\text{K}^2$ ). The  $ZT$  of the materials was determined as  $ZT = (PT)/\lambda$  [1].

## RESULTS AND DISCUSSION

The powder obtained as a result of the combustion of the xerogel was formed by agglomerated particles ranging in size from 200 to 500 nm (Fig. 1a). According to X-ray diffraction data, they consisted of calcium carbonate ( $\text{CaCO}_3$ ) (ICDD PDF-2, release 2004, card no. 01-086-2341) and the cobalt oxides  $\text{Co}_3\text{O}_4$  (ICDD PDF-2, release 2004, card no. 01-080-1539) and  $\text{CoO}$  (ICDD PDF-2, release 2004, card no. 01-089-7099) (Fig. 1c, scan 1; Table 1). After calcination, the powder particles had the form of well-crystallized platelets ranging in size from 500 nm to 1  $\mu\text{m}$ , with a habit characteristic of the layered calcium cobaltite (Fig. 1b). In the X-ray diffraction pattern of the powder, we identified reflections from only one phase,  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  (Fig. 1c, scan 2; Table 2) [28]. Its unit cell parameters were  $a = 0.4832 \text{ nm}$ ,  $b_1 = 0.4567 \text{ nm}$ ,  $b_2 = 0.2843 \text{ nm}$ ,  $c = 1.083 \text{ nm}$ , and  $\beta = 98.24(1)^\circ$ , in agreement with those reported by Masset et al. [28]:  $a = 0.48376(7) \text{ nm}$ ,  $b_1 = 0.45565(6) \text{ nm}$ ,  $b_2 = 0.28189(4) \text{ nm}$ ,  $c = 1.0833(1) \text{ nm}$ , and  $\beta = 98.06(1)^\circ$ .

The X-ray diffraction patterns of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  ( $x = 1, 2, 5$ ) composites (Fig. 2, Table 2) showed sharp reflections from the layered calcium cobaltite as the major phase and weak reflections from copper as an impurity phase (ICDD PDF-2, release 2004, card no. 01-089-2838). The intensity of the weak reflections was found to increase with increasing  $x$ .



**Fig. 1.** (a, b) Electron micrographs and (c) X-ray diffraction patterns of the layered calcium cobaltite powder prepared by the glycine–citrate–nitrate process (a; c, scan 1) after xerogel combustion and (b; c, scan 2) additional calcination at 1073 K for 3 h. The numbers at scan 2 are the Miller indices of the reflections from the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  phase.

The apparent density of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramic prepared by hot pressing was  $3.480 \text{ g/cm}^3$ , considerably exceeding that of ceramics produced by conventional solid-state reactions ( $2.47 \text{ g/cm}^3$  [18]). The density of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  composites was much higher, ranging from  $4.378$  to  $4.524 \text{ g/cm}^3$ , which corresponded to porosities from 3 to 6% (Table 3). Thus, the addition of copper particles to layered calcium cobaltite-based ceramics produced by hot pressing allows one to obtain low-porosity ( $\Pi < 7\%$ ) ceramics whose apparent density approaches their X-ray density.

As seen in Fig. 3a, the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramic had a layered microstructure and consisted of well-crystallized platelets (“flakes”) 2–10  $\mu\text{m}$  in size and 500 nm to 1  $\mu\text{m}$  in thickness, oriented predominantly in a direction perpendicular to the pressing axis. The particle size of the major phase, that is, the layered cal-

cium cobaltite, in the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  composites was considerably smaller, in the range 1–5  $\mu\text{m}$  (Figs. 3b, 3c). The present SEM results lead us to conclude that the addition of copper nanoparticles to layered calcium cobaltite-based ceramics significantly hinders grain growth during the sintering process and makes it possible to obtain finer crystalline and lower porosity ceramics.

Near room temperature, the electrical conductivity of the ceramics exhibited metallic behavior ( $\partial\sigma/\partial T < 0$ ), which changed to semiconducting behavior ( $\partial\sigma/\partial T > 0$ ) near 500 K (Fig. 4a). The electrical conductivity of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramic was considerably higher ( $\sigma_{300} \approx 45 \text{ S/cm}$ ) than that of materials produced by standard solid-state reactions or citrate processes ( $\sigma_{300} \approx 20$ – $25 \text{ S/cm}$  [5, 12, 14, 16, 18]), which was due to its lower porosity. The addition of copper particles to the

**Table 1.** Peak positions of reflections in the X-ray diffraction pattern of the xerogel combustion product.

experiment*	2 $\theta$ , deg		
	CaCO <sub>3</sub>	Co <sub>3</sub> O <sub>4</sub>	Co <sub>2</sub> O <sub>3</sub>
21.76		21.83	
26.84	26.81		
34.18	34.04		
36.20	36.06	36.02	
42.18	42.16		
42.64		42.51	42.71
46.20	46.10		
49.58			49.73
50.62	50.67		
51.74		51.85	
55.48	55.03		
56.94	56.65		
67.88	67.97		
70.06		69.22	
72.30	71.86		72.97

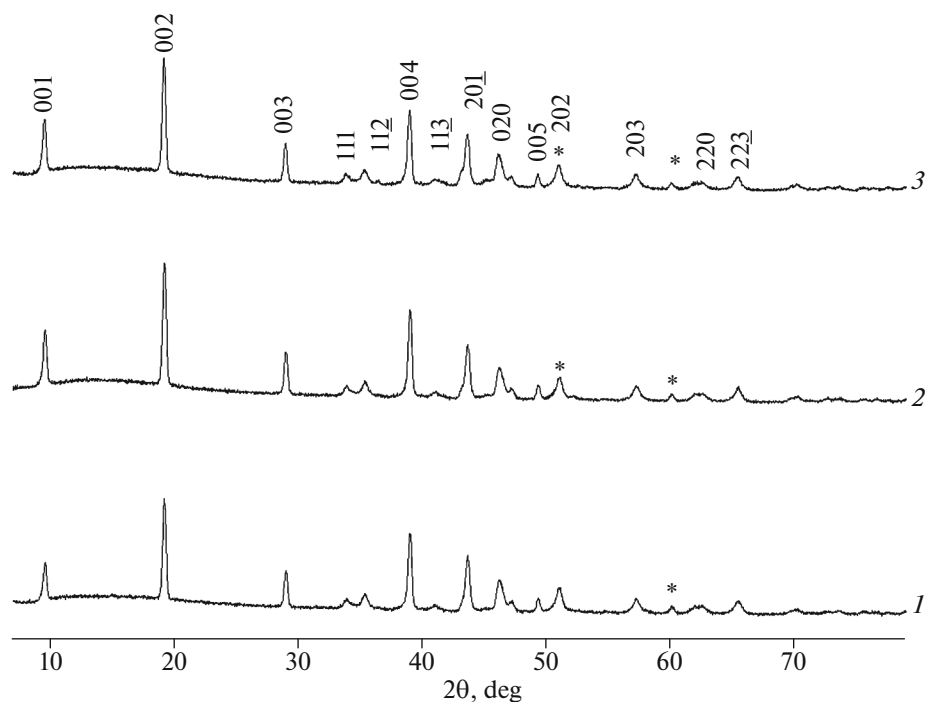
\* Figure 1c, scan 1.

ceramic increased its electrical conductivity more than twofold, which increased further as the copper content of the composites increased (Fig. 4a). The

activation energy for electrical conduction in the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  sample was 0.137 eV, and that in the copper-modified materials was markedly lower: 0.092–0.111 eV (Table 3). Thus, as would be expected the addition of copper particles to the layered calcium cobaltite leads to an increase in the electrical conductivity of the forming materials and a decrease in the activation energy for electrical transport.

The ceramics studied in this work had a positive thermoelectric power, which led us to conclude that the majority carriers in them were holes. Their thermoelectric power was found to increase with increasing temperature and decrease with increasing copper content (Fig. 4b). This correlates with results obtained by Xiang et al. [8] and Kahraman et al. [24], who reported the  $S$  of Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub> /Ag composites to decrease with increasing silver content.

The thermoelectric power factor of the materials studied here was found to increase with increasing temperature. Moreover, the  $P$  of the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  +  $x$  wt % Cu composites considerably exceeded that of the basic material with the composition Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  (Fig. 4c), which was due to their high electrical conductivity. The highest thermoelectric power factor was offered by the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub> Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  + 2 wt % Cu composite:  $P_{1100} = 521 \mu\text{W}/(\text{m K}^2)$ . This is a factor of 1.4 higher than that of the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  matrix mate-

**Fig. 2.** X-ray diffraction patterns of the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  +  $x$  wt % Cu composites with  $x = (1)$  1,  $(2)$  2, and  $(3)$  5. The numbers at scan 3 are the Miller indices of the reflections from the Ca<sub>3</sub>Co<sub>4</sub>O<sub>9+ $\delta$</sub>  phase.

**Table 2.** Peak positions of reflections in the X-ray diffraction patterns of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ( $x = 0$ ) (Fig. 1c, scan 2) and  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x$  wt % Cu (Fig. 2) samples

2 $\theta$ , deg					
$x = 0$	$x = 1$	$x = 2$	$x = 3$	$\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$	Cu
9.56	9.58	9.56	9.52	9.57	
19.18	19.18	19.20	19.16	19.21	
29.02	29.00	28.98	28.96	28.98	
33.94	33.88	33.88	33.78	33.92	
35.38	35.36	35.36	35.30	35.39	
38.98	39.02	39.00	38.98	38.97	
41.00	40.94	41.10	40.90	41.00	
43.66	43.66	43.66	43.64	43.63	
46.26	46.26	46.20	46.16	46.29	
47.26	47.24	47.14	47.16	47.33	
49.36	49.38	49.32	49.32	49.30	
	50.90	50.96	50.96		50.79
51.04	51.04	51.04	51.02	50.98	
57.16	57.26	57.26	57.22	57.18	
	59.92	59.90	59.90		59.37
60.06	60.08	60.06	60.10	60.07	
62.66	62.52	62.54	62.58	62.58	
65.58	65.54	65.46	65.48	65.56	
70.04	70.18	70.12	70.16	70.09	

rial ( $P_{1100} = 363 \mu\text{W}/(\text{m K}^2)$ ) and more than five times the thermoelectric power factor of low-density  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramics produced by conventional solid-state reactions ( $P_{1100} = 100 \mu\text{W}/(\text{m K}^2)$ ) [18].

The thermal diffusivity of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x$  wt % Cu materials at a temperature of 300 K varies in the range  $(5.25\text{--}5.75) \times 10^{-7} \text{ m}^2/\text{s}$ , and the thermal conductivity evaluated from these data is  $\sim 2.2\text{--}2.5 \text{ W}/(\text{m K})$  (Table 3), which is typical of low-porosity layered calcium cobaltite-based ceramics [5]. The electron component of the thermal conductivity is rather low ( $\lambda_e/\lambda \approx 3\%$ ), and the phonon thermal conductivity prevails ( $\lambda_{\text{ph}}/\lambda \approx 97\%$ ) (Table 3), which is characteristic of this type of material [12, 14].

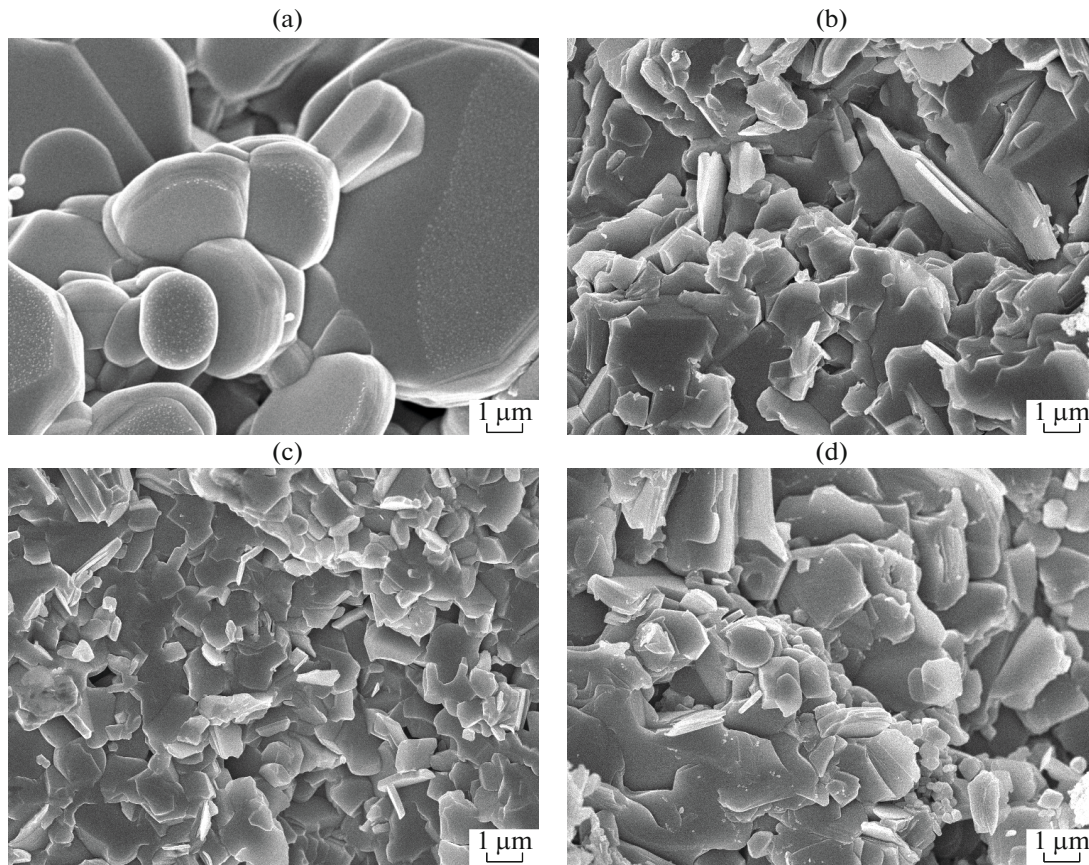
The 300 K  $ZT$  ( $ZT_{300}$ ) of the layered calcium cobaltite-based ceramics modified with copper particles is  $0.0228\text{--}0.0275$ , and estimated  $ZT_{1100}$  (evaluated with no allowance for the temperature dependence of  $\lambda$ ) exceeds 0.2 (Table 3), which is considerably higher than that of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  materials produced by standard solid-state reactions and approaches the  $ZT$  of high-density ceramics produced by hot pressing or spark plasma sintering [5].

## CONCLUSIONS

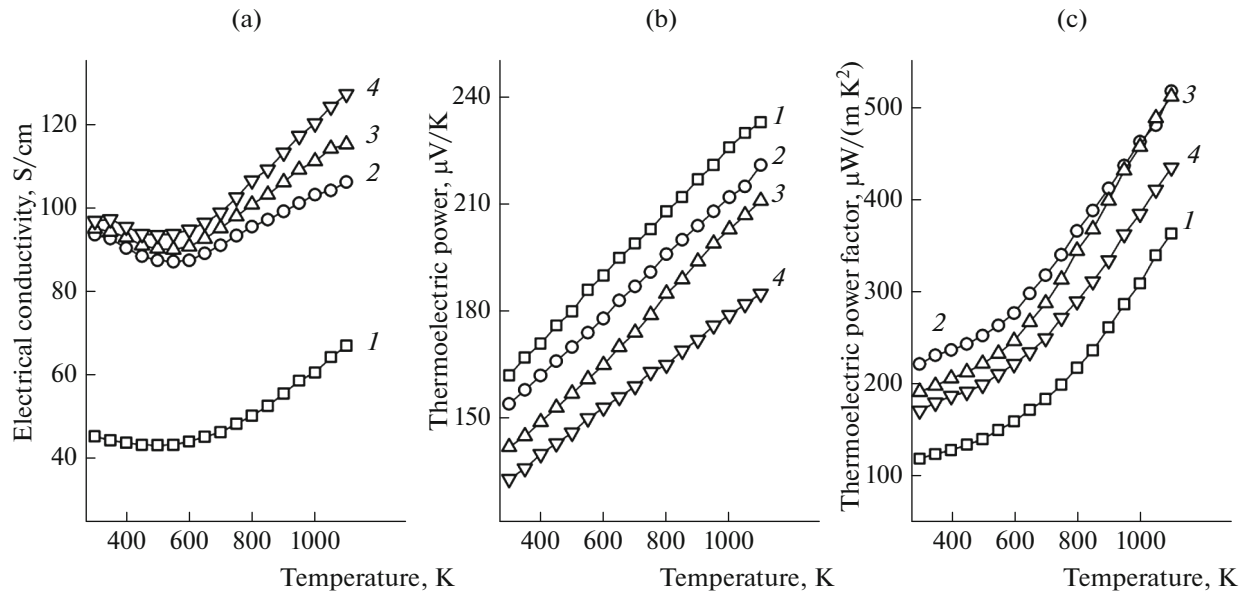
High-density  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$ -based ceramics containing copper particles have been produced by hot pressing and their microstructure and electrical transport, thermophysical, and thermoelectric properties have been investigated.

**Table 3.** Apparent density ( $\rho_{\text{app}}$ ), porosity ( $\Pi$ ), activation energy for electrical conduction ( $E_a$ ), thermal diffusivity ( $\eta_{300}$ ), total thermal conductivity ( $\lambda_{300}$ ), phonon thermal conductivity ( $\lambda_{\text{ph},300}$ ), electron thermal conductivity ( $\lambda_{e,300}$ ), and thermoelectric figure of merit ( $ZT_{300}$  and  $ZT_{1100}$ ) of the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x$  wt % Cu composites

$x$	1	2	5
$\rho_{\text{app}}$ , g/cm <sup>3</sup>	4.378	4.524	4.401
$\Pi$ , %	6.4	3.3	5.9
$E_a$ , eV	0.092	0.103	0.111
$\eta_{300}$ , m <sup>2</sup> /s	$5.62 \times 10^{-7}$	$5.75 \times 10^{-7}$	$5.25 \times 10^{-7}$
$\lambda_{300}$ , W/(m K)	2.414	2.527	2.246
$\lambda_{\text{ph},300}$ , W/(m K)	2.346	2.458	2.176
$\lambda_{e,300}$ , W/(m K)	0.068	0.069	0.070
$ZT_{300}$	0.0275	0.0227	0.0228
$ZT_{1100}$	0.236	0.223	0.213



**Fig. 3.** Electron micrographs of fracture surfaces (perpendicular to the pressing axis) in the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  ceramics with  $x =$  (a) 0, (b) 1, (c) 2, and (d) 5.



**Fig. 4.** (a) Electrical conductivity, (b) thermoelectric power, and (c) thermoelectric power factor as functions of temperature for the  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + x \text{ wt } \% \text{ Cu}$  samples with  $x =$  (1) 0, (2) 1, (3) 2, and (4) 5.

The results demonstrate that modifying hot-pressed layered calcium cobaltite with copper particles makes it possible to obtain high-density, fine-grained ceramics having high electrical conductivity and improved functional (thermoelectric) characteristics.

Among the samples studied here, the highest thermoelectric power factor is offered by the ceramic with the composition  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta} + 2 \text{ wt } \% \text{ Cu}$ ,  $521 \mu\text{W}/(\text{m K}^2)$  at a temperature of 1100 K, which is a factor of 1.4 higher than that of the basic material  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  having the same thermal history ( $P_{1100} = 363 \mu\text{W}/(\text{m K}^2)$ ) and a factor of 5.2 higher than the thermoelectric power factor of  $\text{Ca}_3\text{Co}_4\text{O}_{9+\delta}$  ceramics produced by a conventional processing route ( $P_{1100} = 100 \mu\text{W}/(\text{m K}^2)$ ) [16].

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