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# A novel Schiff base of pyridine-2-amine derivative as an effective inhibitor of the dissolution of N80 pipeline steel in 1 M HCl

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Received: 9 March 2023 / Revised: 10 July 2023 / Accepted: 19 July 2023 / Published online: 25 July 2023 © The Author(s), under exclusive licence to Springer Nature Switzerland AG 2023

#### Abstract

An investigation of the performance of recently synthesized pyridine-2-amine derivative namely, N-(5-methoxy-2-hydroxybenzylidene)pyridine-2-amine (N5MHP) as inhibitor of N80 steel corrosion in 1 M HCl environment was carried out using surface analysis, electrochemical impedance, polarization and weight loss method. Results obtained reveal that N5MHP performed well in protecting the steel surface, achieving an inhibition efficiency of 97.0% at 303 K with 1.0 mM concentration from weight loss method. Increasing temperature depreciated the corrosion inhibition efficiency of N5MHP but increase in concentration enhanced the protection performance of the inhibitor. Electrochemical tests results agreed with weight loss results. Langmuir isotherm was obeyed by N5MHP in its adsorption on the steel surface. Polarization studies revealed that N5MHP acted as mixed-type inhibitor. Surface morphology characterized using scanning electron microscopy (SEM) displayed a more protected surface of the X60 steel in the presence of N5MHP in the acid media. Theoretical calculations were performed by employing Density Functional Theory (DFT).

Keywords Pyridine-2-amine  $\cdot$  N80 steel  $\cdot$  Electrochemical impedance  $\cdot$  Langmuir isotherm  $\cdot$  Corrosion inhibition  $\cdot$  DFT calculations

# Introduction

Corrosion creates different serious problems in various industries due to its precarious and damaging effect on metals. It is one of the main causes of structural deterioration in offshore and marine structures (Anwar et al. 2019, 2021). Cleaning of pipework steel in order to remove undesirable rust and scale is usually done with acid solutions like hydrochloric acid which subjects the steel to corrosion (Abd-Elaal et al. 2013). In acid solutions, apart from metal dissolution (anodic process) corrosion is usually accompanied by cathodic processes which predominantly involve hydrogen gas evolution. The study of steel corrosion in acid media has been of interest to researchers due to increased applications of acid solution. Pipework steel protection with corrosion inhibitors has greatly been investigated and found to be one of the most desirable corrosion prevention methods (Njoku et al. 2021; Iroha and Nnanna 2021; Kousar et al. 2021). These inhibitors are chemicals usually added in small quantity to the corrosive environments to slowdown the corrosion rate (Iroha and James 2019). Several organic compounds (Arrousse et al. 2021; Kacimi et al. 2017; Poojary et al. 2021; Iroha et al. 2005) have been applied as inhibitors for steel corrosion in acidic media and found to be effective in reducing the corrosion rate. These compounds exert inhibitive action by adsorption of their molecules onto the steel surface, thereby creating a protective barrier to attack of the corrodant. Based on extensive study, the organic compounds are able to adsorb effectively on the metal surface most likely because of the presence of multiple bonds, aromatic rings, heterocyclic and, N, O, S and P atoms present in their molecules. These atoms contain electron lone pairs which are available to the iron empty d-orbital to form a dative bond.

Schiff bases with general formula RC = NR' have in their structure, features that make them potent as corrosion inhibitors. Schiff bases are compounds produced by the condensation of amines and a carbonyl compound. The ease of synthesis of these compounds from affordable materials is one

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the great advantages of Schiff bases in their use as corrosion inhibitors. Recent reports have shown the effectiveness of Schiff bases as inhibitors of steel corrosion in acid media (Yurt et al. 2014; Okey et al. 2020). Literature survey has also revealed the use of Schiff bases derived from pyridine as corrosion inhibitors (Ansari et al. 2015; Iroha et al. 2021). This synthesized pyridine derivative is a non-toxic organic compound which is also useful and important intermediate in various medicinal compounds preparations (Cocco et al. 2003; Hughes et al. 2008). This type of Schiff base contains heterocyclic compounds with nitrogen atoms which can be protonated easily in acidic environment to display effective inhibition of metals corrosion in acid solution.

In an attempt to contribute to this research area which is growing and solving industry problems, we have in our laboratory, synthesized and used some Schiff bases (Dueke Eze et al. 2022; Iroha and Dueke-Eze 2021) which have performed well as corrosion inhibitors. This present work is aimed at studying the inhibitory performance of Schiff base N5MHP on the corrosion of N80 steel in 1 M HCl environment using electrochemical and weight loss techniques. This compound was chosen on the basis of molecular structure, while considering the active centers and the kind of substituents. To correlate the inhibition performance of N5MHP with its structure, quantum chemical calculations were performed.

## Experimental

# Preparation of metal specimen and corrosion medium

The metal specimens (N80 steel) used for the study contained; 0.92% Mn, 0.01% P, 0.31% C, 0.008% S, 0.19% Si, 0.2% Cr and the remainder Fe. The steel specimens were first cut into  $2 \times 4$  cm<sup>2</sup> dimensions for both weight loss and electrochemical measurements and then abraded with emery papers (grades 400–1200). The specimens were thereafter rinsed with distilled water, dried in an oven after degreasing with acetone and then utilize for the experiment. Exposed area of 1 cm<sup>2</sup> for the samples was utilized in electrochemical studies. The blank corrosion medium consists of 1 M HCl solution prepared from analytical grade 37% HCl (Merck) by diluting with distilled water.

#### Synthesis of N5MHP

5-methoxy-2-hydroxybenzaldehyde solution (24.5 mg, 0.20 mmol) in 10 mL of ethanol and formic acid (two drops) were mixed with 2-aminopyridine solution (18.8 mg, 0.20 mmol) in 10 mL of ethanol and stirred. For 6 h the mixture was refluxed and the precipitate formed was filtered and then

recrystallized to yield N-(5-methoxy-2-hydroxybenzylidene) pyridine-2-amine (N5MHP). Detailed characterization by NMR and IR has been earlier reported (Dueke-Eze et al. 2013). The molecular structure of N5MHP is shown in Fig. 1.

## **Electrochemical measurements**

Electrochemical measurements were perform by utilizing the conventional three-electrode electrolytic cell with N80 steel as working electrode, platinum foil as counter electrode and saturated calomel electrode (SCE) [Hg/Hg<sub>2</sub>Cl<sub>2</sub>/KClsat] as reference electrode. All measurements were performed using Gamry framework at 30 °C. Samples were mounted in epoxy resin with an exposed area of  $1 \text{ cm}^2$  to the test solution. The experiment proceeded by first letting the working electrode attain a steady state via immersion in the test solution for 30 min at open circuit potential (OCP). The electrochemical impedance spectroscopy (EIS) measurement performed on the N80 steel electrode at OCP proceeded by applying a signal amplitude of 10 mV within the range of frequency 100 kHz to 0.01 Hz. Fitting and analyses of the EIS data were done with Echem Analyst software version 5.50. The polarization measurement were performed from potential (cathodic) of -0.25 V vs. OCP to potential (anodic) of +0.25 V vs. OCP at a scan rate 1 mVs<sup>-1</sup>. Results reproducibility was tested by repeating the measurements three times.

#### Weight loss measurement

The weight loss measurements were conducted using ASTM G31-72 standard (ASTM 2004). In this measurement, the N80 steel specimens were weighed and suspended in solutions containing 100 mL bare 1 M HCl and different concentrations of N5MHP for 6 h immersion time at 30 °C, 40 and 50 °C temperatures unstirred. The N80 steel specimens were retrieved washed, dried and accurately re-weighed. The average of three weight loss measurements was recorded. The corrosion rate ( $C_R$ ), surface coverage ( $\theta$ ) and inhibition efficiency (IE<sub>WL</sub> %) for N5MHP were respectively computed using Eqs. 1, 2 and 3:



Fig. 1 Molecular structure of N5MHP

$$C_R = \frac{\Delta W}{S.t} \tag{1}$$

where  $\Delta W$  represents mean weight loss (mg), t and S stand for immersion time (s) and surface area (cm<sup>2</sup>) respectively.

$$\theta = \frac{C_R - C_{R(i)}}{C_R} \tag{2}$$

$$IE_{WL}\% = \frac{C_R - C_{R(i)}}{C_R} \times 100$$
(3)

where  $C_R$  and  $C_{R(i)}$  are corrosion rate values of X60 steel without and with the inhibitors respectively.

#### **SEM** analysis

SEM micrographs of the N80 steel specimen immersed in blank 1 M HCl and inhibited with  $1 \times 10^{-2}$  M N5MHP were examined utilizing Ziess Evo 50 XVP model of scanning electron microscope. The SEM operating at 20 kV recorded the topography of the surface with resolution of electron microscope of 1.5 nm. The SEM images were taken at 2000× magnification. After 6 h immersion at 30 °C, the specimens were retrieved from the test solutions, washed properly with distilled water and dried in air before SEM analysis.

#### **Quantum Chemical Calculations**

The quantum chemical calculations were performed using Spartan 14.0 software. The calculations and geometrical optimization of N5MHP inhibitor were carried out utilizing the B3LYP model of density functional theory (DFT) in combination with the 6-311G (d, p) basis sets. The HOMO energy ( $E_{HOMO}$ ), LUMO energy ( $E_{LUMO}$ ) and the energy gap ( $\Delta E = E_{LUMO} - E_{HOMO}$ ) were calculated to determine the inhibition behavior of N5MHP. The calculated  $E_{HOMO}$  and  $E_{LUMO}$  were used to calculate some important parameters like electron affinity ( $EA = -E_{LUMO}$ ), ionization potential ( $IP = -E_{HOMO}$ ) and other such as electronegativity ( $\chi$ ), global hardness ( $\eta$ ) and global softness ( $\sigma$ ) as shown in Eqs. (4)–(6) (Zhang et al. 2015; Iroha et al. 2022a):

$$\chi = \frac{IE + EA}{2} \tag{4}$$

$$\eta = \frac{IP - EA}{2} \tag{5}$$

$$\sigma = \frac{1}{\eta} \tag{6}$$

The change in the number of transported electrons ( $\Delta N$ ) from the inhibitors to the Fe surface was calculated by Eq. (7) (Xia et al. 2015; Maduelosi and Iroha 2020):

$$\Delta N = \frac{\chi_{Fe} - \chi_{inh}}{2(\eta_{Fe} + \eta_{inh})}$$
(7)

where  $\chi_{Fe}$  and  $\chi_{inh}$  are the electronegativity of Fe and inhibitor molecules, while  $\eta_{Fe}$  and  $\eta_{inh}$  are the global hardness of Fe and inhibitor molecules. From Pearson's electronegativity scale, the theoretical values of  $\eta_{Fe}$  and  $\chi_{Fe}$  are 0 eV and 7 eV (Zhang et al. 2019).

# **Results and discussion**

#### Potentiodynamic polarization measurements (PDP)

A potentiodynamic polarization test was carried out to gain insight into the kinetics of the anodic and cathodic reactions. The anodic reaction involves N80 steel dissolution through oxidation process as earlier described (Hamani et al. 2014; Iroha et al. 2022b):

$$Fe + Cl^{-} \rightleftharpoons (FeCl^{-})_{ads}$$
 (8)

$$(FeCl^{-})_{ads} \rightleftharpoons (FeCl)_{ads} + e^{-} \tag{9}$$

$$(FeCl)_{ads} \to (FeCl)^+ + e^- \tag{10}$$

$$(FeCl)^+ \rightleftharpoons Fe^{2+} + Cl^- \tag{11}$$

While on the contrary, the cathodic reaction has to do with the hydrogen evolution through reduction process as follows described (Hamani et al. 2014; Iroha et al. 2022b):

$$Fe + H^+ \rightleftharpoons (FeH^+)_{ads}$$
 (12)

$$(FeH^+)_{ads} + e^- \to (FeH)_{ads} \tag{13}$$

$$(FeH)_{ads} + H^+ + e^- \to Fe + H_2 \tag{14}$$

The polarization curves without and with various concentrations of N5MHP in 1 M HCl media are depicted in Fig. 2. Figure 2 shows that both the anodic and branch cathodic reactions were influenced by the addition of N5MHP, which reduced both the cathodic hydrogen evolution and the anodic N80 steel dissolution (Mobin and Rizvi 2017; James and Iroha 2021). This indicates that N5MHP behaved as a mixedtype inhibitor. The electrochemical polarization parameters like corrosion current density ( $i_{corr}$ ), corrosion potential ( $E_{corr}$ ), inhibition efficiency ( $IE_{PDP}$ , %), anodic branch slope ( $\beta_a$ ) and cathodic branch slope ( $\beta_c$ ) were deduced by means



Fig. 2 Potentiodynamic polarization curves of N80 steel in 1 M HCl solutions without and with various concentrations of N5MHP of N5B2HP at 30  $^\circ$ C

of Tafel extrapolation and listed in Table 1. The  $IE_{PDP}$  was calculated as follows:

$$IE_{PDP} = \frac{I_{corr}^0 - I_{corr}^i}{I_{corr}^0} \times 100$$
(15)

where  $I_{corr}^0$  and  $I_{corr}^i$  are the corrosion current densities without and with N5MHP inhibitor respectively. The results as shown in Table 1 indicate that the presence of various concentrations of N5MHP cause a significant decrease in the  $i_{corr}$ values. The observed decrease of the  $i_{corr}$  values was due to the inhibitor adsorption on the N80 steel/HCl interface (Obot et al. 2015; Iroha and Akaranta 2020). Maximum inhibition efficiency was obtained at the concentration of 1.00 mM of N5MHP. Generally, a shift in  $E_{corr}$  above 85 mV, categorizes the inhibitor as cathodic or anodic and a shift lower than 85 mV (as seen in this study) suggest that the inhibitor is mixedtype (Olasunkanmi et al. 2017; Abeng et al. 2023; Iroha and Ukpe 2020). The Tafel slopes ( $\beta_a$  and  $\beta_c$ ) decrease with an increase in N5MHP concentration, which further suggests the suppression of both cathodic and anodic partial reactions.

#### **Electrochemical impedance measurement**

The impedance study was carried out to elucidate the kinetics and characteristics of the metal/solution interface and how N5MHP obstructed the reaction. The Nyquist plots of N80 steel in 1 M HCl medium without and with various concentrations of N5MHP is depicted in Fig. 3. The figure clearly shows a depressed semicircular shape for all the impedance spectra. Slight deviations of the shape from a perfectly circle suggest interfacial impedance frequency dispersion (Da-Rocha et al. 2010; Pavithra et al. 2010). The equivalent circuit used in modeling the N80 steel/HCl solution interface is depicted as an insert in Fig. 3, where  $R_s$ denotes solution resistance,  $R_{ct}$  stands for charge transfer resistance and CPE is the constant phase element used to replace double layer capacitance ( $C_{dl}$ ). The CPE impedance is expressed as:

$$Z_{CPE} = \frac{1}{Y_o} (j\omega)^{-n} \tag{16}$$

where  $Y_0$  denotes CPE constant,  $\omega$  is angular frequency,  $j^2 = -1$  is imaginary number and *n* is the CPE exponent which presents information on the degree of surface inhomogeneity resulting from inhibitor adsorption, surface roughness and formation of porous layer (Abdel-Gaber et al. 2009). The  $C_{dl}$  values are computed from CPE utilizing Eq. 17:

$$C_{dl} = Y_0 (\omega_{max})^{n-1} \tag{17}$$



Fig. 3 Nyquist plot of N80 steel in 1 M HCl without and with various concentrations of N5MHP (insert: equivalent circuit)

Table 1         Potentiodynamic
polarization data of N80 steel
in 1 M HCl without and with
various concentrations of
N5MHP at 30 °C

Conc. (mM)	$i_{\rm corr}$ (µA cm <sup>-2</sup> )	$E_{\rm corr}$ (mV/SCE)	$\beta_a (\mathrm{mV}\mathrm{dec}^{-1})$	$\beta_{\rm c} ({\rm mV}{\rm dec}^{-1})$	$\eta_{PDP}(\%)$
Blank	796.3	-569.1	117.4	166.9	-
0.50	233.7	-502.8	102.5	142.8	70.7
0.75	139.9	-488.0	113.9	137.2	82.4
1.00	52.6	-477.6	115.8	124.3	93.4

Where,  $\omega_{max}$  denotes the frequency at which the impedance imaginary part has attain maximum value. The impedance parameters such as  $R_{ct}$ ,  $C_{dl}$  and inhibition efficiency ( $IE_{EIS}$ , %), are listed in Table 2. The  $IE_{EIS}$  was computed as follows:

$$IE_{EIS} = \frac{R_{ct} - R_{ct}^0}{R_{ct}} \times 100$$
(15)

where  $R_{ct}^0$  and  $R_{ct}$  are the charge transfer resistances without and with N5MHP inhibitor respectively. It is obvious that  $R_{ct}$ values increase with increasing N5MHP concentrations. This indicates a decrease in corrosion rate in the inhibitor presence and an increase in  $IE_{EIS}$ . On the other hand, the  $C_{d1}$  values were found to decrease on adding N5MHP inhibitor, which indicates a decrease in local dielectric constant and/or an increase in the electrical double layer thickness, suggesting that N5MHP function by protective layer formation on the N80 steel surface (Ostovari et al. 2009; Iroha et al. 2023a, b).

#### Weight loss method

#### Effect of concentration

The variation of weight loss parameters with the concentrations of N5MHP is depicted in Fig. 4. It is observed that N5MHP protected N80 steel corrosion in the HCl solution at all studied concentrations i.e. 0.50 to 1.00 mM, with  $C_R$ decreasing with an increase in the inhibitors concentration while the reverse was the case for IE<sub>WL</sub> %. However, the

Table 2 Electrochemical impedance parameters for N80 steel in 1 M HCl without and with various concentrations of N5MHP at 30  $^\circ C$ 

Conc. (mM)	$R_{\rm s} (\Omega {\rm cm}^2)$	$R_{\rm ct}  (\Omega  {\rm cm}^2)$	$C_{\rm dl} (\mu {\rm F~cm^{-2}})$	n	$\eta_{EIS}(\%)$
Blank	0.864	123.8	20.67	0.838	-
0.50	0.886	495.2	16.51	0.849	75.0
0.75	0.903	661.0	8.91	0.864	81.3
1.00	0.975	2189.6	3.11	0.882	94.3

Schiff base pyridine-2-amine derivative showed maximum protection at 303 K with 1.00 mM concentration. The results in Fig. 1b reveal that N5MHP performed well in protecting the steel surface, achieving an inhibition efficiency of 97.0% at 303 K with 1.0 mM concentration. The corrosion rate on the other hand, decreased from 8.465 mg/cm<sup>2</sup>/h to 0.452 mg/ cm<sup>2</sup>/h in the presence of 1.00 mM N5MHP at 303 K. This observed result is related to increased adsorption of inhibitor species leading to hydrophobic thin film formation on the acid-substrate interface (Iroha et al. 2015).

#### Impact of temperature

The impact of temperature on N80 steel corrosion behaviour in inhibited and uninhibited test solutions was studied. The observed variation of  $C_R$  and  $IE_{WL}$ % with temperature ranging from 303 to 323 K are displayed in Table 3. The table reveals that  $C_R$  of X60 steel in both inhibited and uninhibited solutions increased with increase in temperature while  $IE_{WL}$ % for N5MHP at constant concentration, decreased with temperature rise. This observation could be due to desorption of adsorbed inhibitor species caused by elevated temperature (Fragoza-Mar et al. 2012; Mourya et al. 2016).

Activation and thermodynamic parameters were considered to help in the understanding of the adsorption and inhibition mechanism. The  $C_R$  is observed to depend on temperature and this dependency on temperature is expressed

**Table 3** Variation of  $C_R$  and  $IE_{WL}$  with temperature without and with 1.00 mM N5MHP in 1 M HCl

	C <sub>R</sub> (mgcm <sup>-2</sup>	$h^{-1}$ )	IE <sub>WL</sub> (%)	
T (K)	Blank	N5MHP	N5MHP	
303	8.465	0.254	97.0	
313	12.160	0.746	93.9	
323	16.090	1.694	89.5	

**Fig. 4** Variation of a  $C_R$  and **b**  $IE_{WL}$  with N5MHP concentration for N80 steel at different temperatures



utilizing the Arrhenius equation (Verma et al. 2016; Chokor et al. 2022):

$$\log C_R = \frac{-E_a}{2.303RT} + \log A \tag{16}$$

Where  $E_a$  is denotes activation energ, T is the absolute temperature, R stands for gas constant, and A denotes preexponential factor. Plot of  $log C_R$  against 1/T (Arrhenius plot) for N80 steel dissolution without and with different concentrations of N5MHP is displayed in Fig. 5a. The  $E_a$  values deduced from the Arrhenius plot slope are listed in Table 4. The data in Table 4 clearly shows that  $E_a$  values in presence of N5MHP were higher when compared with the values without N5MHP. This observation indicates that N5MHP retards the dissolution N80 steel by causing an increase in the energy barrier involved in corrosion (Krishnegowda et al. 2013). An alternative formula for the Arrhenius equation is the Eyring's transition state equation given as:

$$\log \frac{C_R}{T} = \log\left(\frac{R}{Nh}\right) + \left(\frac{\Delta S^*}{2.303R}\right) - \left(\frac{\Delta H^*}{2.303RT}\right)$$
(17)

where N is Avogadro's number, h denotes Planck's constant,  $\Delta S^*$  stands for activation entropy,  $\Delta H^*$  denotes activation enthalpy. From the slope ( $-\Delta H^*/2.303R$ ) of the plot of log C<sub>R</sub>/T against 1/T (Transition state plot) depicted in Fig. 5b,  $\Delta H^*$  values were computed. The  $\Delta S^*$  values were deduced from the intercept, [log (R/Nh) + ( $\Delta S^*/2.303R$ )] of the same plot. These values are listed in Table 4. The positive  $\Delta H^*$  values obtained shows the endothermic nature of the N80 steel dissolution in the presence of N5MHP. The values  $\Delta S^*$  in the presence of N5MHP and its absence are both negative with less negative values in the presence of N5MHP. This suggests that the activation complex in the rate determining step denotes association instead of

 Table 4
 Activation parameters for the dissolution of N80 steel in the absence and presence of various concentrations of N5MHP.

Conc(mM)	$E_a(kJ/mol)$	$\Delta H^*(kJ/mol)$	$\Delta S^*(J/mol/K)$
Blank	31.63	27.51	-159.31
0.50	38.19	33.86	-144.64
0.75	42.75	39.01	-138.99
1.00	50.46	42.68	-122.53

dissolution step, which implies decreased disorderliness on going from reactants to activated complex. The negative  $\Delta S^*$  values also shows the non-spontaneous nature of the N80 steel dissolution by adding N5MHP (Ikeuba et al. 2015).

#### Adsorption isotherm

Adsorption isotherm was studied to better understand the interaction between the N80 steel surface and N5MHP in 1 M HCl environment. Among the various adsorption isotherms tested, Langmuir isotherm gave the best fit. The Langmuir isotherm is given as:

$$\frac{C_{inh}}{\theta} = \frac{1}{K_{ads}} + C_{inh} \tag{17}$$

where  $C_{inh}$  denotes N5MHP concentration and  $K_{ads}$  stands for adsorption equilibrium constant. A plot of  $C_{inh}\theta$  against  $C_{inh}$  as depicted in Fig. 6, gives a straight line with the values of regression coefficient (R<sup>2</sup>) and slope very close to unity suggesting that N5MHP adsorption on the N80 steel surface in test solution obeys the Langmuir adsorption isotherms (Iroha et al. 2012). The  $K_{ads}$  is related to the adsorption free energy ( $\Delta G_{ads}^0$ ) as follows:



Fig. 5 a Arrhenius plots and b Transition state plots for N80 steel in the absence and presence of different concentrations of N5MHP



Fig. 6 Langmuir isotherm for the adsorption of N5MHP on N80 steel surface using weight loss method

 Table 5
 Thermodynamic parameters for the adsorption of N5MHP

 on N80 steel in 1 M HCl at various temperature

Temp. (K)	$R^2$	Slope	Intercept	$K_{ads} (\mathrm{M}^{-1})$	$\Delta G_{ads}^0$ (kJ/mol)
303	0.9851	0.8318	0.2095	4773	-31.46
313	0.9953	0.8512	0.2198	4550	-32.37
323	0.9988	0.9013	0.2192	4562	-33.41

$$\Delta G_{ads}^o = -RT \ln \left( 55.5 K_{ads} \right) \tag{18}$$

where R denotes the gas constant and T stands for absolute temperature. The value, 55.5 is the molar concentration of water in solution. The computed values of  $K_{ads}$  and  $\Delta G_{ads}^0$  are presented in Table 5. The values of the Langmuir isotherm slopes show deviations from unity expected for ideal an ideal Langmuir isotherm equation. The deviation from 1 could be as a result of interactions between the adsorbed molecules on

steel **a** exposed to 1 M HCl **b** exposed to 1 M HCl containing 1.00 mM N5MHP.

Fig. 7 SEM images for N80

the X60 steel surface. The observed negative  $\Delta G_{ads}^0$  values show that the adsorption process is spontaneous. General,  $\Delta G_{ads}^0$  values of within  $-20 \text{ kJmol}^{-1}$  are associated with physisorption while values more negative than  $-40 \text{ kJmol}^{-1}$ are compatible with chemisorption (Yadav et al. 2015a). The computed  $\Delta G_{ads}^0$  values for N5MHP are between -31.46 to  $-33.41 \text{ kJmol}^{-1}$  which are within the threshold values for physisorption and chemisorption, suggesting that the adsorption process of N5MHP on N80 steel surface involves both chemical and physical adsorption (Yadav et al. 2015b).

#### **SEM analysis**

The surface morphology of uninhibited and inhibited N80 steel samples after immersion period of 6 h are depicted in Fig. 7. The SEM image of the specimen immersed in uninhibited 1 M HCl environment (Fig. 7a) is porous and rough due to aggressive and fast acid corrosion reaction. Moreover, the SEM images of the N80 steel specimen in presence of N5MHP (Fig. 7b) is less damaged, indicating a retardation of the corrosion attack and protective film formation of N5MHP on the steel surface.

#### Quantum chemical calculation

The frontier molecular orbitals (FMOs) are very important tool in determining the chemical reactivity of the inhibitor adsorbed onto metal surfaces (Daoud et al. 2015). Figure 8 shows graphical representations of the HOMO and LUMO density distribution of N5MHP. The depiction in Fig. 8 shows that the HOMO and LUMO orbitals' sites of distribution are mainly the azomethine group,  $\pi$ -electrons, including the heteroatoms of oxygen and nitrogen. The quantum chemical properties of the neutral and protonated forms of N5MHP are listed in Table 6. The E<sub>HOMO</sub> values are generally related to the ability of the inhibitor molecules to donate electron to the unoccupied metal surface's d-orbital. Higher values of E<sub>HOMO</sub> imply



that the electron donating ability including the inhibition efficiencies of the inhibitor would be high. However, ELUMO values are related to the ability of the inhibitor molecule to accept electron from the metal. Therefore, the electron accepting properties including the inhibition efficiency increases with reduced  $E_{LUMO}$  values (Verma et al. 2016). As observed in Table 6, the high E<sub>HOMO</sub> of neutral N5MHP is stabilized in N5MHP-H<sup>+</sup> (protonated form) which suggests lower electron-donating ability of N5MHP-H<sup>+</sup>. The energy band gap ( $\Delta E$ ) relates the stability and chemical reactivity of the inhibitor molecules. Lower values of  $\Delta E$  facilitate and increase the adsorption of the inhibitor molecule on the metal surface through donoracceptor process (Boughoues et al. 2020). In the present study,  $\Delta E$  of N5MHP-H<sup>+</sup> is lower than that of N5MHP, which promotes its adsorption to the N80 steel surface and enhances its efficiency. The hardness  $(\eta)$  and softness  $(\sigma)$ are other properties that are related to molecular reactivity and stability. A hard molecule has higher  $\Delta E$  between the  $E_{LUMO}$  and  $E_{HOMO}$  and is related to lower reactivity and inhibition efficiency. On the other hand, a soft molecule has a lower  $\Delta E$  between the  $E_{LUMO}$  and  $E_{HOMO}$  and is related to larger reactivity and inhibition efficiency (Mohamed et al. 2021). The fraction of transferred electrons ( $\Delta N$ ) from our study are less than 3.6 for N5MHP and N5MHP-H<sup>+</sup> molecules, suggesting transfer of electrons from the molecules to N80 steel leading to formation of dative bonds. This promotes protective layer formation against corrosion.

# Conclusion

The present study has shown that the synthesized N-(5-methoxy-2-hydroxybenzylidene)pyridine-2amine (N5MHP) can function as an effective corrosion inhibitor for N80 pipeline steel in 1 M HCl solution

Fig. 8 Frontier molecular orbitals HOMO and LUMO of neutral and protonated N5MHP

Table 6 Calculated quantum chemical parameters for N5MHP and N5MHP-H<sup>+</sup> molecules

Theoretical parameters	N5MHP	N5MHP-H <sup>+</sup>
$E_{\rm HOMO} ({\rm eV})$	-4.34	-8.33
$E_{\rm LUMO} ({\rm eV})$	-2.21	-6.85
$\Delta E (E_{LUMO} - E_{HOMO}) (eV)$	2.13	1.48
Ionization energy (I)	4.34	8.33
Electron affinity (A)	2.21	6.85
Electronegativity ( $\chi$ )	3.28	7.59
Global hardness (η)	1.07	0.74
Global softness $(\sigma)$	0.93	1.35
Fraction of transferred electrons ( $\Delta N$ )	1.74	-0.40

and the inhibition efficiency increases with increasing concentration of the inhibitor. The corrosion process was inhibited by adsorption of the Schiff base molecules on N80 steel surface leading to the formation of a protective film on the metal/acid solution interface, decreasing the dissolution of the steel. Results from Potentiodynamic polarization showed that the studied inhibitor exhibit mixed-type inhibition activity. The results of the EIS reveal that there is a decrease in the charge transfer resistance in the presence of N5MHP. The impact of temperature on the inhibition performance of N5MHP was investigated using weight loss measurements and the results indicated that the inhibition efficiency of N5MHP decreases with increase in temperature. Adsorption of the studied inhibitor obeys Langmuir adsorption isotherm. The results obtained from EIS, weight loss and polarization techniques are in good agreement. Surface analysis by SEM confirms the adsorption performance of the inhibitor and the development of a protective film on the steel surface. Additionally, the results obtained by the DFT-based quantum chemical calculations supported the experimental findings.



**Acknowledgements** The authors thankfully acknowledge the Tertiary Education Trust Fund (TETFUND), Nigeria for providing financial support under Institution Based Research (IBR) scheme.

Author contributions Nkem B. Iroha: Designed the study, Wrote the first draft of the manuscript, Performed the electrochemical experiments and surface analysis, Cordelia U. Dueke-Eze: Performed the weight loss experiments and DFT, Managed the literature searches, Took part in the manuscript writing. Both authors Wrote, Edited and finalized the manuscript.

**Funding** This work was funded by TETFUND Institution Based Research Scheme.

**Data availability** All data generated or analysed during this study are included in this published article.

#### Declarations

Ethical approval Not applicable.

**Competing interests** The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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