

# An approach for selection of solid waste treatment and disposal methods based on fuzzy analytical hierarchy process

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#### Abstract

Solid waste management is a severe challenge in India due to massive and rapid growth in waste generation rates, environmental difficulties, and financial constraints for proper treatment. Poorly managed municipal solid waste (MSW) has substantial negative consequences for society, including financial and aesthetic harm, contamination of natural resources, environmental pollution, and severe health danger. Both qualitative and quantitative factors are required to select the appropriate solid waste treatment and disposal technologies. Multi-Criteria decision-making tools helped in analyzing solid waste in terms of qualitative and quantitative factors. In this paper, seven criteria and their sub-criteria are selected for ranking solid waste treatment and disposal technology using fuzzy-analytic hierarchy process. The results showed that composting is the most suitable option for solid waste treatment and disposal technology, followed by refuse-derived fuel. The incineration and sanitary landfills are the least preferred MSW management alternatives. The sensitivity analysis reveals a high consistency, robustness, and stability level.

Keywords Fuzzy-analytic hierarchy process · Solid waste management · Composting · Refuse-derived fuel · Incineration

# Introduction

Urbanization, industrialization, economic integration, and population growth have increased the huge quantity of municipal solid waste (MSW) [1]. As the population increases, the MSW generation in India also increases the additional pressure on existing resources and infrastructure for appropriate and safe disposal [2, 3]. In India, about 143,449 metric tons of MSW is generated per day, of which 111,000 metric tons were collected and only 35,602 metric tons received treatment [4]. There was an exponential increase in solid waste generation rate from 0.24 kg to 0.85 kg of solid waste per person per day from 2001 to 2018 [5]. Waste generation continues to grow at

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<sup>1</sup> Department of Civil Engineering, Motilal Nehru National Institute of Technology Allahabad, Allahabad 211004, India an alarming rate, and MSW is concerned about hygienic and safe disposal [4]. If it is not appropriately managed, the enormous amount of MSW will negatively affect the environment, such as air, water, and soil pollution [6], food chain contamination with bacteria & viruses, etc. [7].

Biological treatment and thermal conversion technologies are commonly used to handle solid waste in India [8–10]. The biological treatment method, mainly composting, can convert organic wastes and residual sludge into compost (manure) or methane (waste to energy). Thermal conversion technologies include incineration of MSW with or without heat recovery, pyrolysis, gasification, and refuse-derived fuel (RDF) production. Solid waste is sometimes disposed off in sanitary landfills, either directly without treatment or indirectly, i.e., after treatment.

Solid waste management and disposal are complex problems that involve political, social, economic, technological, and environmental considerations. A series of trade-offs hamper reaching the best treatment technology among various stakeholders with differing objectives and viewpoints. As a result, technical, economic, environmental, managerial, and social issues must be assessed, which can be done using quantitative, qualitative, or mixed methodologies. The appropriate solid waste treatment technology and disposal choice vary from country to country. It is influenced by various factors, including the types and composition of waste, land availability, labor requirement, capital cost, public awareness, the calorific value of waste, energy availability, policy and subsidy, employment and environmental impact. Thus, MSW management must be considered a task requiring Multi-Criteria Decision Making (MCDM) for appropriate management. Many researchers have worked on various aspects of solid waste management and disposal methods using various MCDM tools, such as Delphi method, analytic hierarchy process (AHP) method, technique for order preference by similarity to ideal solution (TOPSIS) method, and rapid impact assessment matrix (RIAM) method [11–13].

In several areas of environmental management, the AHP technique is recommended as an excellent technique for solving multi-criteria decision-making [14]. Apart from environmental management, there are many applications, such as the selection of waste management strategies for hospitals [15], municipal wastes [16], hazardous waste transportation [17], sites [18], waste collection [19], and waste allocation [20]. Interestingly, decision-making in AHP involves judgment based on the expert's knowledge; however, different opinions and decision-making modes cannot reflect the same thinking [21]. As a result, AHP has always been criticized for various reasons, including being unrealistic, not covering all ranges of human thinking templates, and the uncertainty in the analysis [22].

The development of fuzzy set theory proposes more flexible methods and addresses the typical difficulties mentioned above. The crisp set has only two states: non-membership and full membership, so in fuzzy theory, a crisp set is expanded, allowing for more accurate real-time decision modeling and comparative membership [23]. Mikhailov and Tsystinov were the first to combine AHP with fuzzy theory, termed FAHP (fuzzy analytic hierarchy process) modeling, which is frequently utilized in many management modeling projects to address uncertainty, lack of knowledge, and the presence of non-statistical information [24]. For the first time, Van Laarhoven and Pedrycz employed FAHP to compare fuzzy ratios given by the triangular fuzzy [25]. To optimize and analyze various environmental concerns, such as urban solid waste management, site selection, and ocean disposal sites, fuzzy sets are combined with multi-criteria decision-making approaches, especially AHP. FAHP determines the relative importance of every criterion through pairwise evaluation given utilizing area experts or selection makers [26]. Fuzzy computing in FAHP is used to describe and address uncertainties by simulating human intelligence. Consequently, modified FAHP is adopted in this paper to select the best option among MSW treatment and disposal systems with seven criteria and 21 sub-criteria.

# Materials and methodology

# Selection of solid waste treatment and disposal technology

This study considers six alternatives: composting, sanitary landfill, gasification, incineration, RDF, and pyrolysis for solid waste treatment and disposal. These alternatives are briefly explained as follows:

- Composting: the biochemical process of creating biogas through microbial decomposition of organic material in the presence of oxygen is known as the composting process [27]. The operating process involves pre-treatment, separation of non-digestible materials, shredding, digestion, and residue treatment.
- Incineration: incineration is a controlled and complete combustion process that burns solid wastes. The temperature of the incinerators ranges from 980 °C to 2000 °C [28]. The ability to reduce the original volume of combustible solid waste by 90% is one of the most attractive characteristics of the incineration process [29].
- 3. Gasification: this is a thermochemical process that uses heat and low-oxygen [30] to partially oxidize carbonaceous materials like biomass or MSW, and converts them into flammable gases [31]. Gasification, unlike incineration, converts solid or liquid waste feedstock into a gaseous product by exposing it to a range of high temperatures (>700 °C) in a controlled supply of oxygen. The gasification occurs in a sealed stainless-steel vessel-filled plasma reactor with air. Gasification can reduce volume by up to 90% while producing almost no toxic emissions.
- 4. Pyrolysis: pyrolysis is the thermochemical decomposition of organic waste at high temperatures in an oxygenfree environment or with too little oxygen for combustion or gasification.
- 5. RDF: RDF is a combustible fraction of MSW that has been separated. The flammable percentage of the waste is compressed into fuel pellets or shredded and converted into fluff, which is then increased in organic content by removing inorganic materials and moisture.
- 6. Sanitary landfill: open, uncontrolled, and poorly managed dumps regularly occur in many metropolitan areas, resulting in considerable environmental deterioration. For the final disposal of MSW, sanitary landfilling is a viable and recommended option. Because all other solutions produce some residue that must be disposed off through landfilling, it is a necessary component of MSW management. However, landfilling appears to be the most generally adopted practice in the upcoming years, and at that time, will require various adjustments to ensure sanitary landfilling.

# Selection of criteria and sub-criteria

Evaluation of each technology depends on the application of the main criteria and sub-criteria, with the opinion of the expert, field engineers, and literature, the seven main criteria and 21 sub-criteria identified for the FAHP study as presented in Table 1. The details of the criterion and subcriteria with references to data collection are as follows.

- Waste quality and quantity: the quantity and quality of waste generation play a vital role in selecting waste processing technologies. It has three sub-criteria. (a) Desirable moisture content (b) Waste acceptance: waste acceptance criteria are the technical criteria that must accept waste at storage, treatment, or disposal facilities for Indian MSW conditions. (c) Suitability (quantity): the higher capacity of treatment technology to tackle solid waste, the higher preference should be given.
- 2. Environmental criteria: the treatment and disposal technology application should be free from environmental safety. It is critical to meet this condition since waste constitutes a severe concern in these areas and one of the primary requirements of treatment technologies is to eliminate this risk. Four sub-criteria are selected under environmental criteria: (a) Greenhouse gase are given higher preference. (b) Adverse impacts: all qualitative impacts of treatment technology considered. The lower the impact is, the higher the priority. (c) Land requirement: technology that requires less land area should be

given higher prioritized and (d) Leachate pollution: less leachate pollution from technology is preferred.

- Opportunities criteria: technology prominence/establishment and Generation/ recovery of other valuable products are selected as sub-criteria of opportunities for the selection of MSW treatment and disposal technology.
- 4. Managerial criteria: there is a need for expertise and labor to operate technology. There is a massive scarcity of expertise in India. The managerial criteria have two sub-criteria; these are labor requirements and technical expertise.
- 5. Technical criteria: the overall system efficiency, retention time, volume reduction and power generation are selected as technical sub-criteria for choosing the best treatment technology for MSW.
- 6. Economic criteria: the three Sub-criteria are used to address the economic aspects:(a) Capital cost, (b) Operating cost, (c) Pre-treatment costs. Capital cost is the cost required to establish a plant, including all costs associated with the project's construction and implementation. Operating cost is the total amount of money spent on the plant's operation over its entire lifetime.
- 7. Social and political criteria: local support and community participation are the most critical factors for the sustainable functioning of technology in any locality. The process of selecting social criteria is complicated, and in this study, three factors were considered: policy & subsidy, employment and public acceptability. The policy and subsidy play a significant role in selecting solid waste treatment and disposal technology. In many cases, MSW management programs have failed due to a

Criteria	Sub-criteria	References
Waste quality and quantity (WQQ)	Desirable moisture content (DEMC) Waste acceptance (WAAC) Suitability Quantity (SUQU)	[28, 31–33]
Environmental criteria (ENV)	GHG emission (GHEM) Adverse impacts (ADIM) Land requirement (LANRE) Leachate pollution (LEPO)	[28, 32–35]
Managerial criteria (MNG)	Labour requirement (LARE) Lack of resources/Technical expertise (LORTE)	[28, 33, 34, 36]
Economic criteria (ECO)	Capital cost (CACO) Operating cost (OPCO) Pre-treatment costs (PTCO)	[34, 37]
Technical criteria (TEC)	Overall system efficiency (OVSE) Residence time (RETI) Power generation (POGE) Volume reduction (VORE)	[28, 32, 34–36, 38–40]
Opportunities criteria (OPP)	Technology prominence/establishment (TEPE) Generation/recovery of other valuable products (ROVP)	[34]
Social and political impact criteria (SPI)	Policy & subsidy (POSU) Employment (EMPL) public acceptability (PUAC)	[36, 41, 42]

Table 1 Specification of alternatives of solid waste treatment technology based on different sub-criteria with reference to data collection

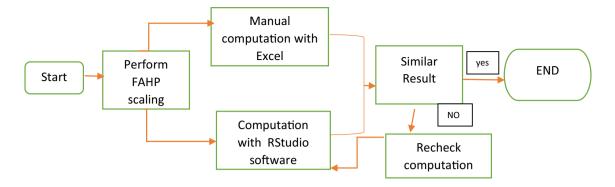


Fig. 1 Overall approach of the study. FAHP fuzzy analytic hierarchy process

lack of funds. Currently, the number of employees is a significant indicator.

#### FAHP methodology

The FAHP is a well-known and tested methodology used worldwide. However, the problem lies where the steps are lengthy and consumes time. Due to the lengthy calculation, there is a risk of error. For this reason, we used two calculation methods to find the priority of criteria/sub-criteria and the priority of alternatives based on each sub-criteria: one using MS Excel software and the software package RStudio. If the final result from both approaches is not the same, the methods must be rechecked and labeled for mismatches and the overall approach of the study is presented in Fig. 1. The FAHP method on the enhanced extent analysis approach has the following steps and is briefly shown in Fig. 2.

Step 1: Developing a decision Model.

The FAHP solves the problem using a hierarchy of four levels and a schematic diagram represented in Fig. 3 to select optimal treatment and disposal technology. The top or first level of the hierarchy is the goal, i.e., ranking of MSW treatment and disposal technology. The intermediate or second level of the hierarchy is based on relevant evaluation criteria. In this study, seven criteria are considered: waste quality & quantity, environmental, managerial, economical, technical, opportunity and social & political. The third level consists of subcriteria of evaluation criteria mentioned in level second. Here, 21 sub-criteria are as follows: 3 sub-criteria for waste quality and quantity, 4 sub-criteria for environmental, 2 sub-criteria for managerial, 3 sub-criteria for economic, 4 sub-criteria for technical, 2 sub-criteria for opportunity criteria, and 3 subcriteria of social & political criteria. Finally, the hierarchy's lowest or fourth level comprises alternatives or options; in this work, six alternatives are considered, i.e., composting, RDF, incineration, gasification, pyrolysis and sanitary landfill.

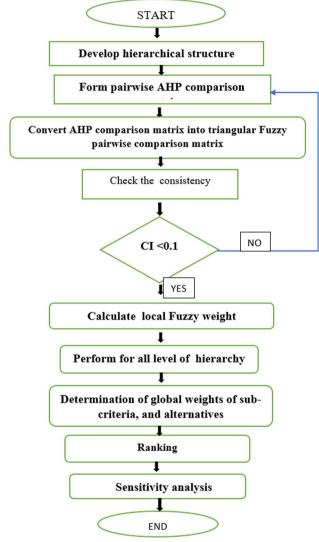


Fig. 2 Methodology of FAHP

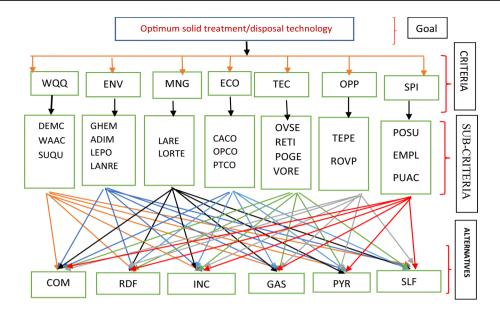


Fig. 3 The hierarchical structure for the prioritization of treatment and disposal technology for solid waste management. WQQ Waste quality and quantity, DEMC Desirable Moisture Content, WAAC Waste ASTE Acceptance, SUQU Suitability Quantity; ENV Environmental criteria, GHEM GHG Emission, ADIM Adverse impacts, LANRE Land requirement, LEPO Leachate Pollution; MNG Managerial criteria, LARE Labour Requirement, LORTE Lack of resources/ Technical expertise;ECO Economic Criteria, CACO Capital cost, OPCO Operating cost, PTCO Pre-treatment costs;TEC Technical cri-

Step 2: Formulation of fuzzy pairwise comparison decision matrix.

The comparison between criteria and sub-criteria is based on the AHP scale given from the opinion of the expert, field engineers and literature review. The comparison between treatment and disposal technology concerning criteria was made with the help of collected data and a literature review. The fuzzy comparison is generated by transforming the AHP pairwise comparison matrix into a triangular fuzzy number matrix represented in Table 2.

Step 3: According to [43], the geometric mean of fuzzy comparison values of each criterion is calculated by Eq. (1). Here,  $\tilde{r}_l$ , "tilde" represents the triangular number demonstration.

$$\tilde{r}_{l} = \left(\prod_{j=1}^{n} \tilde{x}_{ij}\right)^{l/n}, i = 1, 2, 3, \dots, n,$$
(1)

Step 4: The fuzzy priorities of each criterion can be found in Eq. (2) with the help of steps 4a, 4b, and 4c.

Step 4a: Find the vector summation of each  $\tilde{r}_l$ .

teria, OVSE Overall system efficiency, RETI Residence time, POGE Power Generation, VORE Volume reduction; OPP Opportunities criteria, TEPE Technology prominence/establishment, ROVP Generation/recovery of other valuable products; SPI Social and Political impact Criteria, POSU Policy & subsidy, EMPL Employment, PUAC public acceptability;COM Composting, RDF Refuse-derived fuel, INC Incineration, GAS Gasification, PYR Pyrolysis, SLF Sanitary landfill

Step 4b: Find the (-1) power of the summation vector, which replaces the fuzzy triangular number, to make it in increasing order.

Step 4c: Find the fuzzy priority of criterion  $i(\tilde{w}_l)$  multiply each  $\tilde{r}_l$  with this reverse vector.

$$\tilde{w}_{i} = \tilde{r}_{i\otimes} \left( \tilde{r}_{1} \oplus \tilde{r}_{2} \oplus \tilde{r}_{3} \oplus \dots \oplus \tilde{r}_{n} \right)^{-1}$$

$$= (lw_{i}, mw_{i}, uw_{i}).$$
(2)

Step 5: Defuzzify the fuzzy priorities:

Defuzzification is the process of obtaining a single crisp number from the fuzzy set to convert the fuzzy set output into a crisp output. The defuzzification is done using center of area method proposed by [44] by applying the Eq. (3)

$$M_i = \frac{(lw_i + mw_i + uw_i)}{3} \tag{3}$$

Step 6: After defuzzification,  $M_i$  is a non-fuzzy number. However, it needs to be normalized by Eq. (4). The 6 steps are performed to find the normalized priorities of criteria, sub-criteria, and alternatives.

AHP scale	Fuzzy number	Invers value of fuzzy number	Definition
1	(1, 1, 1)	(1, 1, 1)	Just equal
1	(2, 1, 1/2)	(1/2, 1, 2)	Equally important
2	(1, 2, 3)	(1/3, 1/2, 1)	Scale between the same and slightly more important
3	(2, 3, 4)	(1/4, 1/3, 1/2)	Low supremacy
4	(3, 4, 5)	(1/5, 1/4, 1/3)	Scale between low supremacy and high supremacy
5	(4, 5, 6)	(1/6, 1/5, 1/4)	High supremacy
6	(5, 6, 7)	(1/7, 1/6, 1/5)	Scale between high supremacy and very high supremacy
7	(6, 7, 8)	(1/8, 1/7, 1/6)	Very high supremacy
8	(7, 8, 9)	(1/9, 1/8, 1/7)	Scale between very high supremacy and absolute supremacy
9	(8, 9, 9)	(1/9, 1/9, 1/8)	Absolute supremacy

 Table 2
 The triangular fuzzy scale for pairwise comparison in FAHP

FAHP fuzzy analytic hierarchy process

Table 3 Random index (RI) values for matrix of size 15. Reprinted from [44] with permission

Size (n)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
RI	0.00	0.00	0.58	0.90	1.12	1.24	1.32	1.41	1.45	1.49	1.51	1.54	1.56	1.57	1.59

$$N_i = \frac{M_i}{\sum_{i=1}^n M_i} \tag{4}$$

Step 7: Consistency check.

First, find the largest eigenvalue of the decision matrix to check the consistency decision matrix ( $\lambda_{max}$ ). It is computed by Eq. (5)

$$\lambda_{\max} = \sum_{j=1}^{n} x_{ij} \otimes w_i \ i, j = 1, \ 2, \ 3, \dots n.$$
(5)

The consistency check is calculated using Eqs. (6) and (7)

$$CR = \frac{CI}{RI}$$
(6)

$$CI = \frac{\left(\lambda_{\max} - n\right)}{(n-1)},\tag{7}$$

where CR is the consistency ratio, CI is the consistency index and RI is the random index.  $\lambda_{max}$  is the largest eigenvalue decision matrix, and n is the number of criteria. The value of RI depends on the dimension (order) of the comparison matrix. Table 3 shows the random index values for the matrix up to size 15 and the acceptable limit of CR value presented in Table 4.

Step 8: Global priority.

The results of the global fuzzy number are derived by multiplying the local fuzzy number of each sub-criteria by their respective fuzzy number of the criteria.

#### Table 4 Acceptable limit of consistency ratio [45, 46]

Matrix size	3×3	4×4	≥5×5
Acceptable CR limit	≤0.05	≤0.08	≤0.10

# **Results and discussion**

The selection of the most appropriate technology from six technology alternatives is evaluated by considering 7 main criteria and 21 sub-criteria for the FAHP study. It is evaluated by the use of MS Excel software and the software package RStudio as:

# Comparison matrix of criteria and their priorities

The first step is to use an MS Excel data sheet to import a pairwise comparison matrix. Then, using the fuzzy package's command "pairwise comparison Matrix()", an AHP comparison matrix is created. Following that, using the command "fuzzyPairwiseComparisonMatrix()" the pairwise is turned into a triangular fuzzy number, as shown in Table 5.

# **Consistency check**

After forming the consistency of the fuzzy pairwise comparison matrix, it is necessary to check the result. The command "consistency index ()" is used to determine the consistency index. The consistency ratio is determined using the fuzzy AHP package command "consistency Ratio()". The fuzzy

Item	WQQ	ENV	MNG	ECO	TEC	OPP	SPI
WQQ	(1;1;1)	(1/9;1/8;1/7)	(1/5;1/4;1/3)	(1/6;1/5;1/4)	(1/6;1/5;1/4)	(1/3;1/2;1)	(1/4;1/3;1/2)
ENV	(7;8;9)	(1;1;1)	(2;3;4)	(1;2;3)	(1;2;3)	(5;6;7)	(2;3;4)
MNG	(3;4;5)	(1/4;1/3;1/2)	(1;1;1)	(1/3;1/2;1)	(1/3;1/2;1)	(2;3;4)	(1;2;3)
ECO	(4;5;6)	(1/3;1/2;1)	(1;2;3)	(1;1;1)	(1/2;1;2)	(3;4;5)	(1;2;3)
TEC	(4;5;6)	(1/3;1/2;1)	(1;2;3)	(1/2;1;2)	(1;1;1)	(3;4;5)	(1;2;3)
OPP	(1;2;3)	(1/7;1/6;1/5)	(1/4;1/3;1/2)	(1/5;1/4;1/3)	(1/5;1/4;1/3)	(1;1;1)	(1/3;1/2;1)
SPI	(2;3;4)	(1/4;1/3;1/2)	(1/3;1/2;1)	(1/3;1/2;1)	(1/3;1/2;1)	(1;2;3)	(1;1;1)

Table 5 Fuzzy AHP pairwise comparison matrix of different criteria with respect to goal

CI=0.014817, The consistency ratio of modal values is 0.0109756347131029

pairwise comparison matrix is consistent for calculations when the consistency ratio is smaller than 0.1. Table 5 shows the results of the consistency index and consistency ratio of the fuzzy AHP pairwise comparison matrix between different criteria.

### Priority vectors (synthetic degree value)

Equation 1 is used to obtain the geometric mean of the fuzzy comparison values of each criterion after the first three steps of the process have been completed. The order of the numbers in the last row is modified since the fuzzy triangular number should be in increasing order. Table 6 shows the result of the relative fuzzy priorities of each criterion by both manual calculation using MS Excel software and with the software package RStudio.

The synthetic degree value of the FAHP criterion (fnMin, fnModal, fnMax) was generated using the RStudio Fuzzy AHP package software. "calculateWeights()" is the code that is used to find synthetic degree values; then, the priority score is defuzzified as indicated, and synthetic degree value of the FAHP criterion (fnMin, fnModal, fnMax) is shown in Table 6. Taking the average of fuzzy numbers for each criterion, the relative non-fuzzy priority value of each criterion (Mi) is calculated using the non-fuzzy Mi normalized priority value of each criterion.

After prioritizing the main criteria, the sub-criteria within each main criterion are prioritized in the same way. The consistency ratio of each comparison matrix that was found to be less than 0.1 is acceptable. The six solid waste management technologies are then individually compared for each of the 21 sub-criteria, resulting in 21 pairwise comparison matrices of order  $18\times6$  representing priority vectors of each technology within each sub-criterion.

The global priority value of sub-criteria is evaluated by multiplying each of the main criteria priority values by the local priority of the sub-criteria in the respective main criteria category. The local priority and global priority of subcriteria are shown in Table 7. In waste quality and quantity criteria, waste acceptance is considered the essential sub-criterion at the local level, whereas desirable moisture content is regarded as the least important. If a single form of alternative cannot handle all types of waste, other types of alternatives are needed. All types of waste should be accepted to

 Table 6
 Geometric means of fuzzy comparison values and relative fuzzy priority of each criterion by manual calculation using Excel and with RStudio

Manual calculation us	ing Exce	1							Calculation using RStudio					
	$\widetilde{r}$			$\widetilde{w}$			Mi	Ni	fnMin	fnModal	fnMax	Mi	Ni	
WQQ	0.244	0.298	0.395	0.019	0.033	0.064	0.039	0.033	0.0250	0.0332	0.0478	0.035	0.034	
ENV	2.026	2.901	3.676	0.162	0.324	0.597	0.361	0.307	0.2362	0.3238	0.3885	0.316	0.308	
MNG	0.774	1.104	1.626	0.062	0.123	0.264	0.150	0.127	0.0822	0.1232	0.1893	0.132	0.128	
ECO	1.104	1.694	2.457	0.088	0.189	0.399	0.226	0.192	0.1201	0.1891	0.2755	0.195	0.190	
TEC	1.104	1.694	2.457	0.088	0.189	0.399	0.226	0.192	0.1201	0.1891	0.2755	0.195	0.190	
OPP	0.335	0.445	0.615	0.027	0.050	0.100	0.059	0.050	0.0357	0.0497	0.0720	0.052	0.051	
SPI	0.566	0.820	1.292	0.045	0.092	0.210	0.116	0.098	0.0604	0.0915	0.1496	0.100563	0.098	
Total	6.153	8.956	12.516				1.175	1.000				1.026	1.000	
Reverse power (-1) and increasing order	0.080	0.112	0.163											

 Table 7
 Local and global priority of sub-criteria with ranking

Sub-criteria	Local pric	ority of sub c	riteria	Mi	Ni	R	Global pr	iority			R
DEMC	0.0786	0.1000	0.1352	0.1046	0.104	3	0.0020	0.0033	0.0065	0.0039	21
WAAC	0.4665	0.6000	0.6817	0.5827	0.581	1	0.0117	0.0200	0.0326	0.0214	16
SUQU	0.2158	0.3000	0.4330	0.3163	0.315	2	0.0054	0.0100	0.0207	0.0120	20
GHEM	0.3536	0.4747	0.5578	0.4620	0.452	1	0.0835	0.1538	0.2167	0.1513	1
ADIM	0.1044	0.1630	0.2604	0.1760	0.172	3	0.0247	0.0528	0.1012	0.0596	6
LEPO	0.1525	0.2551	0.3838	0.2638	0.258	2	0.0360	0.0826	0.1491	0.0893	4
LANRE	0.0757	0.1072	0.1775	0.1202	0.118	4	0.0179	0.0347	0.0690	0.0405	11
LARE	0.2500	0.3333	0.5000	0.3611	0.361	2	0.0206	0.0411	0.0947	0.0521	9
LORTE	0.5000	0.6667	0.7500	0.6389	0.639	1	0.0411	0.0822	0.1420	0.0884	5
CACO	0.6708	0.7267	0.7608	0.7194	0.718	1	0.0806	0.1374	0.2097	0.1426	2
OPCO	0.1576	0.2000	0.2560	0.2045	0.204	2	0.0189	0.0378	0.0705	0.0424	10
PTCO	0.0633	0.0734	0.0955	0.0774	0.077	3	0.0076	0.0139	0.0263	0.0159	19
OVSE	0.0917	0.1411	0.2343	0.1557	0.152	4	0.0110	0.0267	0.0646	0.0341	15
RETI	0.1574	0.2627	0.3898	0.2700	0.264	2	0.0189	0.0497	0.1074	0.0587	7
POGE	0.0897	0.1411	0.2426	0.1578	0.154	3	0.0108	0.0267	0.0669	0.0348	14
VORE	0.3314	0.4550	0.5345	0.4403	0.430	1	0.0398	0.0861	0.1473	0.0911	3
TEPE	0.2500	0.3333	0.5000	0.3611	0.361	2	0.0089	0.0166	0.0360	0.0205	17
ROVP	0.5000	0.6667	0.7500	0.6389	0.639	1	0.0179	0.0331	0.0541	0.0350	13
POSU	0.3874	0.5396	0.6337	0.5202	0.514	1	0.0234	0.0494	0.0948	0.0559	8
EMPL	0.1919	0.2970	0.4434	0.3108	0.307	2	0.0116	0.0272	0.0663	0.0350	12
PUAC	0.1172	0.1634	0.2599	0.1802	0.178	3	0.0071	0.0150	0.0389	0.0203	18

R ranking

rely on one type of alternative. Because the moisture content of solid waste can be changed by drying in sunlight, it is given less priority. This is why the expert has been given more priority to waste acceptance compared to the other two sub-criteria of waste quality and quantity criteria for the selection of solid waste treatment and disposal technology. Greenhouse gas emission is given the highest priority in environmental criteria, followed by leachate pollution, adverse impacts and land requirements. Lack of resources/ technical expertise has given higher priority to labor requirements due to new technology requiring expertise to operate and scarcity of expertise while labor is readily available. Capital cost is favored in terms of economic factors. Volume reduction, retention time, power production, and overall system efficiency are technical criteria with priority values of 0.430, 0.264, 0.154 and 0.152, respectively. Regarding social and political impact, policies and subsidies, employment and public acceptance. The greenhouse gas emission had the highest global priority of 0.153, while the desired moisture content had the lowest priority of 0.0039, for MSW treatment and disposal technology selection.

The overall priority is determined in terms of the fuzzy number to reduce information loss and avoid questionable outcomes during defuzzification. The priority of alternatives concerning sub-criteria is multiplied by their respective global priority of sub-criteria. Then, the fuzzy impact of alternatives is obtained by adding synthetic degree values Si priority value by corresponding fuzzy composite relative priorities of parent node criterion shown in Table 8. After that, a fuzzy impact on the alternative is obtained by adding the composite relative synthesis value summation. Then, the final ranking is obtained as represented in Table 9, after defuzzification and the normalization of fuzzy values. Composting is the most recommended technology for treating and managing solid waste, with a priority of 0.2308, while incineration and sanitary landfills are the least preferred MSW management alternatives. RDF comes second with a priority score of 0.1970 for solid waste treatment. Gasification and pyrolysis are ranked third and fourth, with priority scores of 0.1584 and 0.1537, respectively.

According to a similar study based on the AHP model, composting is the most preferred technology, followed by RDF, while sanitary landfills and incineration are the worst options for solid waste treatment and disposal. The third favored technology is gasification [47, 48].

### Sensitivity analysis for FAHP

The sensitivity analysis is required to find the sensitive parameter or criterion in FAHP analysis. For that, eight cases are formed based on (i) each criterion having an equal

#### Table 8 Synthesis degree values for the alternatives solid waste treatment and disposal technology

	INC						RDF						GAS					
tem	Local sy	nthesis val	ue	Compos value	ite relative	synthesis	Local sy	nthesis va	alue	Compos value	ite relative	synthesis	Local sy	nthesis val	ue	Compos value	ite relative	synthesis
	l	т	и	l	т	и	l	m	и	1	т	и	l	т	и	l	т	и
EMC	0.0580	0.1000	0.1733	0.0001	0.0003	0.0011	0.0580	0.1000	0.1733	0.0001	0.0003	0.0011	0.0580	0.1000	0.1733	0.0001	0.0003	0.0011
VAAC	0.1477	0.2359	0.3289	0.0017	0.0047	0.0107	0.1223	0.1872	0.2764	0.0014	0.0037	0.0090	0.0511	0.0749	0.1184	0.0006	0.0015	0.0039
UQU	0.2978	0.3886	0.4453	0.0016	0.0039	0.0092	0.0292	0.0389	0.0543	0.0002	0.0004	0.0011	0.1775	0.2401	0.3301	0.0010	0.0024	0.0068
HEM	0.0643	0.0885	0.1401	0.0054	0.0136	0.0304	0.1070	0.1686	0.2498	0.0089	0.0259	0.0541	0.1070	0.1686	0.2498	0.0089	0.0259	0.0541
DIM	0.0562	0.0818	0.1271	0.0014	0.0043	0.0129	0.1439	0.2250	0.3155	0.0036	0.0119	0.0319	0.0793	0.1299	0.2044	0.0020	0.0069	0.0207
.EPO	0.0709	0.1205	0.2155	0.0026	0.0100	0.0321	0.1312		0.3374	0.0047	0.0190	0.0503	0.1312	0.2298	0.3374	0.0047	0.0190	0.0503
ANRE	0.1376	0.2229	0.3277	0.0025	0.0077	0.0226	0.1376		0.3277	0.0025	0.0077	0.0226	0.1376	0.2229	0.3277	0.0025	0.0077	0.022
ARE	0.1292	0.2094	0.2955	0.0027	0.0086	0.0280	0.0896		0.2128	0.0018	0.0060	0.0201	0.0630	0.0979	0.1578	0.0013	0.0040	0.0149
ORTE	0.0707	0.1138	0.1668	0.0029	0.0094	0.0237	0.0572		0.1346	0.0024	0.0072	0.0191	0.0464	0.0678	0.1096	0.0019	0.0056	0.015
CACO	0.1253	0.1842	0.2700	0.0101	0.0253	0.0566	0.1513		0.3213	0.0122	0.0319	0.0674	0.0367	0.0507	0.0721	0.0030	0.0070	0.015
OPCO	0.0273	0.0334	0.0472	0.0005	0.0013	0.0033	0.2802	0.3778		0.0053	0.0143	0.0316	0.0410	0.0589	0.0836	0.0008	0.0022	0.0059
PTCO	0.4515	0.5225	0.5775	0.0034	0.0072	0.0152	0.0377		0.0920	0.0003	0.0007	0.0024	0.0466	0.0690	0.1122	0.0004	0.0010	0.003
OVSE	0.0745	0.1126	0.1967	0.0008	0.0030	0.0127	0.1392		0.3147	0.0015	0.0060	0.0203	0.1002	0.1593	0.2542	0.0011	0.0043	0.0164
RETI	0.1036	0.1589	0.2349	0.0020	0.0079	0.0252	0.3004	0.3893		0.0057	0.0193	0.0491	0.1537	0.2292	0.3133	0.0029	0.0114	0.033
POGE	0.1258	0.1747	0.2608	0.0014	0.0047	0.0174	0.0280		0.0408	0.0003	0.0009	0.0027	0.2049	0.2968	0.3729	0.0022	0.0079	0.024
VORE	0.1379	0.2368	0.3350	0.0055	0.0204	0.0493	0.0737		0.2146	0.0029	0.0107	0.0316	0.1240	0.2110	0.3086	0.0049	0.0182	0.045
TEPE	0.0295	0.0371	0.0490	0.0003	0.0006	0.0018	0.1762		0.3416	0.0016	0.0042	0.0123	0.0973	0.1385	0.2076	0.0009	0.0023	0.007
ROVP	0.0513	0.0791	0.1270	0.0009	0.0026	0.0069	0.0513		0.1270	0.0009	0.0026	0.0069	0.0949	0.1462	0.2172	0.0017	0.0048	0.011
POSU	0.0413	0.0568	0.0772	0.0010	0.0028	0.0073	0.1960	0.2965		0.0046	0.0147	0.0367	0.1098	0.1604	0.2470	0.0026	0.0079	0.023
EMPL	0.0246	0.0287	0.0358	0.0003	0.0008	0.0024	0.1313		0.2813	0.0015	0.0052	0.0187	0.1856	0.2826	0.3685	0.0022	0.0077	0.024
UAC	0.0546	0.0750	0.1050	0.0004	0.0011	0.0041	0.1411	0.2250	0.3268	0.0010	0.0034	0.0127	0.1411	0.2250	0.3268	0.0010	0.0034	0.012
				0.0473	0.1402	0.3729				0.0634	0.1961	0.5018				0.0465	0.1513	0.414
											0.2538							
					0.1868												0.2040	
	DVD				0.1868 0.1451		6014				0.1971		ar F				0.1584	
	PYR				0.1451		СОМ				0.1971		SLF				0.1584	
	Local sy	nthesis val	ue	value		synthesis		nthesis v	alue	value		synthesis	[	nthesis val	ue	Compos value		synthes
		rnthesis val	ue	1	0.1451	synthesis u		nthesis va m	alue u		0.1971	synthesis u	[	nthesis val	ue u		0.1584	synthes u
tem	Local sy			value	0.1451 ite relative	-		т		value	0.1971 ite relative	•	[			value	0.1584 ite relative	и
item	Local sy l	m	и	value l	0.1451 ite relative <i>m</i>	u	Local sy	m 0.3000	и	value l	0.1971 ite relative <i>m</i>	u	Local sy	т	u	value l	0.1584 ite relative <i>m</i>	<i>u</i> 0.002
item DEMC WAAC	Local sy <i>l</i> 0.0580	m 0.1000	и 0.1733	value <i>l</i> 0.0001	0.1451 ite relative m 0.0003	<i>u</i> 0.0011	Local sy <i>l</i> 0.1973	m 0.3000 0.1298	и 0.3947	value <i>l</i> 0.0004	0.1971 ite relative <i>m</i> 0.0010	<i>u</i> 0.0026	Local sy <i>l</i> 0.1973	<i>m</i> 0.3000	и 0.3947	value <i>l</i> 0.0004	0.1584 ite relative <i>m</i> 0.0010	<i>u</i> 0.0020 0.0120
tem DEMC WAAC SUQU	Local sy <i>l</i> 0.0580 0.0511	<i>m</i> 0.1000 0.0749	<i>u</i> 0.1733 0.1184	value <i>l</i> 0.0001 0.0006	0.1451 ite relative m 0.0003 0.0015	<i>u</i> 0.0011 0.0039	Local sy <i>l</i> 0.1973 0.0811	m 0.3000 0.1298 0.0658	u 0.3947 0.2099	value <i>I</i> 0.0004 0.0009	0.1971 ite relative m 0.0010 0.0026	<i>u</i> 0.0026 0.0068	Local sy <i>l</i> 0.1973 0.1810	<i>m</i> 0.3000 0.2972	<i>u</i> 0.3947 0.3870	value <i>l</i> 0.0004 0.0021	0.1584 ite relative m 0.0010 0.0059	<i>u</i> 0.002 0.012 0.000
tem DEMC WAAC SUQU GHEM	Local sy 1 0.0580 0.0511 0.1775	<i>m</i> 0.1000 0.0749 0.2401	<i>u</i> 0.1733 0.1184 0.3301	value <i>l</i> 0.0001 0.0006 0.0010	0.1451 ite relative m 0.0003 0.0015 0.0024	<i>u</i> 0.0011 0.0039 0.0068	Local sy / 0.1973 0.0811 0.0480	m 0.3000 0.1298 0.0658 0.3820	u 0.3947 0.2099 0.0876	value <i>l</i> 0.0004 0.0009 0.0003	0.1971 ite relative m 0.0010 0.0026 0.0007	<i>u</i> 0.0026 0.0068 0.0018	Local sy 1 0.1973 0.1810 0.0227	<i>m</i> 0.3000 0.2972 0.0265	<i>u</i> 0.3947 0.3870 0.0357	value <i>l</i> 0.0004 0.0021 0.0001	0.1584 ite relative m 0.0010 0.0059 0.0003	<i>u</i> 0.002 0.012 0.000 0.006
tem DEMC WAAC SUQU GHEM ADIM LEPO	Local sy <i>l</i> 0.0580 0.0511 0.1775 0.1070	<i>m</i> 0.1000 0.0749 0.2401 0.1686	<i>u</i> 0.1733 0.1184 0.3301 0.2498	value <i>l</i> 0.0001 0.0006 0.0010 0.0089	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259	<i>u</i> 0.0011 0.0039 0.0068 0.0541	Local sy / 0.1973 0.0811 0.0480 0.3009	<i>m</i> 0.3000 0.1298 0.0658 0.3820 0.3707	<i>u</i> 0.3947 0.2099 0.0876 0.4437	value <i>l</i> 0.0004 0.0009 0.0003 0.0251	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587	<i>u</i> 0.0026 0.0068 0.0018 0.0962	Local sy 1 0.1973 0.1810 0.0227 0.0206	<i>m</i> 0.3000 0.2972 0.0265 0.0237	<i>u</i> 0.3947 0.3870 0.0357 0.0290	value <i>l</i> 0.0004 0.0021 0.0001 0.0017	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036	<i>u</i> 0.002 0.012 0.000 0.006 0.010
tem DEMC WAAC SUQU GHEM ADIM LEPO	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044	value <i>I</i> 0.0001 0.0006 0.0010 0.0089 0.0020	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726	<i>m</i> 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205	<i>u</i> 0.3947 0.2099 0.0876 0.4437 0.4457	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196	<i>u</i> 0.0026 0.0068 0.0018 0.0962 0.0451	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626	<i>u</i> 0.3947 0.3870 0.0357 0.0290 0.1061	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033	<i>u</i> 0.002 0.012 0.000 0.006 0.010 0.016
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE	Local sy <i>l</i> 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374	value <i>I</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503	Local sy / 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746	<i>m</i> 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875	<i>u</i> 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100	<i>u</i> 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696	<i>u</i> 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057	<i>u</i> 0.002 0.012 0.000 0.006 0.010 0.016 0.001
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE LARE	Local sy 7 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226	Local sy <i>l</i> 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873	<i>u</i> 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053 0.1188	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030	<i>u</i> 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210	<i>u</i> 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.001
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE LARE LORTE	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149	Local sy l 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159	<i>u</i> 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445	Local sy / 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623	<i>u</i> 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0009	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0007	u 0.0020 0.0120 0.000 0.006 0.010 0.016 0.0016 0.0010 0.009 0.0309
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE LARE LORTE CACO	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0358	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786	value <i>I</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0040	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677	<i>m</i> 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242	u 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053 0.1188 0.4703 0.5569	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430	<i>u</i> 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445 0.0791	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0009 0.0041	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0007 0.0026 0.0131	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.030
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE LARE LORTE CACO DPCO	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0358 0.0367	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507	u 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786 0.0721	value 1 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0040 0.0040 0.0070	u 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.0867	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999	u 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053 0.1188 0.4703 0.5569 0.1894	value 1 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430 0.0171	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445 0.0791 0.0397	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356	value 1 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0009 0.0041 0.0203	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0492	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.030
tem DEMC WAAC SUQU GHEM ADIM	Local sy           0.0580           0.0511           0.1775           0.1770           0.0703           0.1312           0.1376           0.0630           0.0358           0.0357           0.0410	<i>m</i> 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0589	u 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786 0.0721 0.0836	value 1 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030 0.0008	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0077 0.0040 0.0070 0.0040 0.0070 0.0022	u 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151 0.0059	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.0867 0.2334	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736	value 1 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0074	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430 0.0171 0.0113	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445 0.0791 0.0397 0.0264	Local sy / 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581 0.1713	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0009 0.0041 0.0203 0.0024	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0492 0.0065	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.091 0.017 0.005
tem DEMC VVAAC SUQU HEM ADIM LEPO LANRE LARE LORTE CACO DYCO DYCO DVSE	Local sy           0.0580           0.0511           0.1775           0.1770           0.1312           0.1376           0.0630           0.0358           0.0367           0.0410           0.0619	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0589 0.1002	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786 0.0721 0.0836 0.1532	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030 0.0008 0.0008 0.0005	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0169 0.0070 0.0040 0.0040 0.0040 0.0040 0.0040 0.0070 0.0042 0.0014	u 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151 0.0059 0.0040	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.0867 0.2334 0.0636	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0044 0.0005	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430 0.0171 0.0113 0.0014	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0445 0.0445 0.0791 0.0397 0.0264 0.0042	Local sy / 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0888	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120	value <i>l</i> 0.0004 0.0021 0.0017 0.0011 0.0018 0.0003 0.0009 0.0041 0.0203 0.0024 0.0007	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0037 0.0007 0.0026 0.0131 0.0265 0.0021	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.091 0.017 0.005 0.005
tem DEMC VAAC UQU HEM DDIM EPO AANRE AARE CACO DCO CO CO CO CO CO CO CO CO CO CO CO CO C	Local sy 7 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0358 0.0367 0.0410 0.0619 0.1684	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0589 0.1002 0.2838	u 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786 0.0721 0.0836 0.1532 0.3721	value <i>I</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030 0.0008 0.0008 0.0005 0.0019	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0077 0.0040 0.0077 0.0040 0.0040 0.0070 0.0040 0.0070	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151 0.0059 0.0040 0.0240	Local sy l 0.1973 0.0811 0.0480 0.2726 0.0746 0.0746 0.0667 0.2807 0.4677 0.0867 0.2334 0.0636 0.1013	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2509	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0044 0.0005 0.0011	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0143 0.0113 0.0113 0.014 0.0043	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0455 0.0791 0.0397 0.0264 0.0042 0.0162	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0888 0.0438	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.0878	value <i>l</i> 0.0004 0.0021 0.0017 0.0011 0.0018 0.0003 0.0009 0.0041 0.0203 0.0024 0.0007 0.0005	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0037 0.0007 0.0026 0.0131 0.0492 0.0065 0.0021 0.0016	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.091 0.017 0.005 0.005 0.005
tem DEMC VAAC UQU HDIM LEPO AANRE AARE AARE ORTE CACO DPCO VVSE RETI VOSE	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0358 0.0367 0.0410 0.0619 0.1684 0.0853	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2298 0.0929 0.0482 0.0507 0.0589 0.1002 0.2838 0.1202	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0786 0.0721 0.0886 0.0721 0.0886 0.0721 0.0836	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0013 0.0013 0.0030 0.0008 0.0008 0.0005 0.0019 0.0016	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0040 0.0040 0.0040 0.0040 0.0040 0.0070 0.0022 0.0014 0.0076 0.0060	u           0.0011           0.0039           0.0068           0.0541           0.0207           0.0503           0.0226           0.0112           0.0151           0.0059           0.0040           0.0240           0.0192	Local sy / 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0746 0.0667 0.2807 0.4677 0.0867 0.2334 0.0636 0.1013 0.0637	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747	<i>u</i> 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2509 0.1232	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.01970 0.0044 0.0005 0.0041 0.0005	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0159 0.0430 0.0113 0.0014 0.0043 0.0041	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0045 0.0045 0.0045 0.0264 0.0042 0.0264 0.0042 0.0162 0.0132	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0888 0.0438 0.0181	m 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.0878 0.0222	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0004 0.0003 0.0024 0.0007 0.0005 0.0003	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0492 0.0065 0.0021 0.0065	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.091 0.017 0.005 0.005 0.005 0.005 0.002 0.001
tem DEMC VAAC SUQU HEM HEM ANRE ARE ORTE CACO DPCO VTCO VSE LETI VOSE LETI VOSE	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0358 0.0367 0.0410 0.0619 0.1684 0.0853 0.2049	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0589 0.1002 0.2838 0.1002 0.2838 0.1202 0.2968	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0752 0.0721 0.0836 0.1532 0.3721 0.1790 0.3729	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0013 0.0015 0.0008 0.0005 0.00019 0.0016 0.0022	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0077 0.0040 0.0070 0.0022 0.0014 0.0076 0.0060 0.0079	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151 0.0059 0.0040 0.0240 0.0249	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.2807 0.4677 0.2334 0.0636 0.1013 0.0637 0.1264	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.0767	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1587 0.2509 0.1232 0.2595	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0012 0.0058 0.0192 0.0005 0.0004 0.0005 0.00011 0.00012 0.0012 0.0014	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0159 0.0430 0.0113 0.0014 0.0043 0.0041 0.0047	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0042 0.0445 0.0391 0.0397 0.0264 0.0042 0.0042 0.00162 0.0132 0.0174	Local sy l 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0433 0.0996 0.2523 0.1246 0.0888 0.0438 0.0438 0.0438 0.0438	m 0.3000 0.2972 0.0265 0.0237 0.0626 0.0596 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189 0.0233	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.2120 0.0878 0.0222 0.0287	value <i>l</i> 0.0004 0.0021 0.0001 0.0017 0.0011 0.0018 0.0003 0.0003 0.00041 0.0224 0.0007 0.0005 0.0003 0.0002	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0045 0.0021 0.0065 0.0021 0.0016 0.0009 0.0006	u 0.002: 0.012: 0.000 0.010 0.010 0.011 0.009 0.030 0.091 0.017: 0.005 0.005 0.005 0.002 0.0012 0.0012 0.001 0.005 0
tem DEMC VAAC UQU HEM JHEM JANRE JARD JANRE JARD JANRE JARD JANRE JARD JANRE JARD JANRE JARD JANRE JARD JANRE JARD JANRE JARD JARD JARD JARD JARD JARD JARD JARD	Local sy 1 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1376 0.0630 0.0367 0.0410 0.0619 0.1684 0.0853 0.2049 0.1026	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0589 0.1002 0.2838 0.1002 0.2838 0.1202 0.2968 0.1757	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3374 0.3277 0.1578 0.07621 0.0721 0.0836 0.3721 0.1790 0.3729 0.2655	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0015 0.0005 0.0005 0.0005 0.00019 0.0016 0.0022 0.0041	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0077 0.0040 0.0070 0.0022 0.0014 0.0076 0.0060 0.0079 0.0151	<i>u</i> 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.00159 0.0040 0.0240 0.0240 0.0249 0.0249 0.0391	Local sy 1 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.2807 0.4677 0.2334 0.0636 0.1013 0.0637 0.1264 0.0527	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.0767 0.3961	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4457 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2509 0.1223 0.2595 0.1273	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0044 0.0005 0.0011 0.0012 0.0014 0.0021	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0330 0.0159 0.0430 0.0111 0.0113 0.0014 0.0043 0.0041 0.0047 0.0066	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445 0.0082 0.0445 0.0791 0.0264 0.0042 0.0042 0.00162 0.00132 0.0174 0.0187	Local sy l 0.1973 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0888 0.0438 0.0438 0.0438 0.0181 0.0215 0.1014	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0596 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189 0.0233 0.1757	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.2120 0.0878 0.0222 0.0287 0.2709	value / 0.0004 0.0021 0.0017 0.0011 0.0018 0.0003 0.00041 0.0024 0.0007 0.0005 0.0003 0.0002 0.0002 0.00040	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0007 0.0026 0.0131 0.0492 0.0065 0.0021 0.0016 0.0009 0.0006 0.0151	u 0.002 0.012 0.000 0.006 0.010 0.001 0.001 0.009 0.030 0.005 0.002 0.002 0.001 0.039 0.002
tem DEMC WAAC SUQU GHEM ADIM LEPO CACO PCO CACO PCO VSE RETI VOGE VOGE VOGE RETE PE ROVP	Local sy           0.0580           0.0511           0.1775           0.1070           0.0793           0.1312           0.1376           0.0630           0.0358           0.0367           0.0410           0.0619           0.1684           0.0853           0.2049           0.1026           0.0973	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0589 0.1002 0.2838 0.1202 0.2838 0.1202 0.2968 0.1757 0.1385	u 0.1733 0.1184 0.301 0.2498 0.2044 0.3374 0.3277 0.1578 0.0721 0.0836 0.0721 0.0836 0.3721 0.1790 0.3729 0.2655 0.2076	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0015 0.0005 0.0019 0.0016 0.0022 0.0041 0.0009	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0190 0.0077 0.0040 0.0077 0.0040 0.0070 0.0022 0.0014 0.0076 0.0069 0.0079 0.0051 0.0079	u           0.0011           0.0039           0.0068           0.0541           0.0207           0.0503           0.0226           0.0149           0.0112           0.0059           0.0040           0.0240           0.0192           0.0240           0.0391           0.0075	Local sy l. 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4677 0.2807 0.4677 0.0867 0.2334 0.0636 0.1013 0.1264 0.0527 0.3042	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.0767 0.3961 0.4417	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2599 0.1232 0.2595 0.1273 0.4548	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0044 0.0005 0.0011 0.0012 0.0014 0.0021 0.0027	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0106 0.0030 0.0159 0.0430 0.0171 0.0113 0.0014 0.0043 0.0047 0.0066 0.0066	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0082 0.0445 0.00791 0.0397 0.0264 0.0042 0.0162 0.0132 0.0174 0.0187 0.0164	Local sy l 0.1973 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0488 0.0438 0.0438 0.0181 0.0215 0.1014 0.0286	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0696 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189 0.0233 0.1757 0.0371	<i>u</i> 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.2472 0.2120 0.0878 0.0222 0.0287 0.2709 0.0509	value <i>l</i> 0.0004 0.0021 0.0017 0.0017 0.0018 0.0003 0.0003 0.0009 0.0041 0.0203 0.0024 0.0007 0.0005 0.0005 0.0002 0.0002 0.0004 0.0002 0.0002	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0003 0.0005 0.0007 0.0026 0.00131 0.00492 0.0065 0.0021 0.0016 0.0006 0.0006 0.0006	u 0.002 0.012 0.000 0.006 0.010 0.001 0.001 0.009 0.030 0.005 0.002 0.001 0.039 0.001 0.003 0.001 0.003
tem DEMC VAAC UQU GHEM ADIM LDIM LEPO AANRE ARE CORE CACO DVSE RETI VOGE COGE COGE COGE COGE COGE COGE COGE C	Local sy           0.0580           0.0511           0.1775           0.1070           0.0793           0.1312           0.1376           0.0630           0.0358           0.0358           0.0367           0.0410           0.0619           0.1684           0.0853           0.2049           0.1026           0.0973           0.1455	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2229 0.0229 0.0482 0.0507 0.0589 0.1002 0.2838 0.1002 0.2838 0.1002 0.2968 0.1757 0.1385 0.2109	u 0.1733 0.1184 0.301 0.2498 0.2048 0.3277 0.1578 0.0786 0.0721 0.0836 0.0721 0.0836 0.1532 0.3721 0.1790 0.3729 0.2655 0.2076 0.2818	value <i>l</i> 0.0001 0.0066 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030 0.0005 0.0019 0.0019 0.0012 0.0041 0.0009 0.0026	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0059 0.0190 0.0077 0.0040 0.0077 0.0040 0.0077 0.0040 0.0070 0.0022 0.0014 0.0076 0.0079 0.0151 0.0023 0.0070	u 0.0011 0.0039 0.0068 0.0541 0.0207 0.0503 0.0226 0.0149 0.0112 0.0151 0.0059 0.0040 0.0240 0.0249 0.0249 0.0249 0.0249 0.0249 0.0251 0.0255	Local sy l. 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.4867 0.2807 0.4867 0.2334 0.0636 0.1013 0.1264 0.0527 0.3042 0.3674	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.0875 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.0767 0.3961 0.4417 0.2965	u 0.3947 0.2099 0.0876 0.4437 0.2053 0.1188 0.4703 0.4703 0.4703 0.4703 0.4703 0.4703 0.4703 0.4549 0.1232 0.2295 0.1273 0.4548 0.4962	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0022 0.0022 0.0058 0.0192 0.0070 0.0044 0.0005 0.0011 0.0014 0.0014 0.0021 0.0027 0.0026 0.0014	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430 0.0171 0.0113 0.0014 0.0043 0.0047 0.0066 0.0066 0.0066 0.0146	и 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0445 0.0445 0.0791 0.0397 0.0264 0.0042 0.0162 0.0174 0.0187 0.0164 0.0268	Local sy l 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.2523 0.1246 0.0888 0.0438 0.0215 0.1014 0.0286 0.0318	m 0.3000 0.2972 0.0265 0.0237 0.0626 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0233 0.1757 0.0371 0.0430	u 0.3947 0.3870 0.0357 0.0290 0.1005 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.0878 0.0227 0.2120 0.0878 0.02277 0.2709 0.0509 0.0685	value <i>l</i> 0.0004 0.0021 0.0017 0.0017 0.0013 0.0003 0.0003 0.0009 0.0041 0.0203 0.0024 0.0005 0.0005 0.0005 0.0005 0.0005 0.0002 0.00040 0.0002 0.00040 0.0002	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0492 0.0065 0.0021 0.0065 0.0021 0.0006 0.0016 0.0006 0.0151 0.0006 0.0014	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.001 0.005 0.002 0.005 0.002 0.001 0.003 0.002 0.001 0.003 0.000 0.001 0.000 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.000 0.000 0.000 0.001 0.000 0.000 0.001 0.001 0.001 0.000 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.0000 0.0000 0.0000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000
tem DEMC WAAC SUQU GHEM ADIM LEPO LANRE LORTE CACO DPCO PTCO	Local sy 7 0.0580 0.0511 0.1775 0.1070 0.0793 0.1376 0.0630 0.0367 0.0410 0.0619 0.1684 0.0853 0.2049 0.1026 0.0973 0.1455 0.1098	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0589 0.1002 0.2838 0.1002 0.2838 0.1202 0.2968 0.1757 0.1385 0.2109 0.1604	<i>u</i> 0.1733 0.1184 0.301 0.2498 0.2044 0.3277 0.1578 0.0786 0.0721 0.0836 0.1532 0.3721 0.1532 0.3721 0.1532 0.3721 0.1532 0.2765 0.2076 0.2818 0.2470	value <i>l</i> 0.0001 0.006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0013 0.0015 0.0030 0.0005 0.0019 0.0005 0.0019 0.0022 0.0041 0.0009 0.0026 0.0026	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0070 0.0040 0.0070 0.0040 0.0070 0.0040 0.0070 0.0022 0.0014 0.0076 0.0076 0.0076 0.0151 0.0023 0.0070 0.0079	u           0.0011           0.0039           0.068           0.541           0.0207           0.0303           0.0226           0.0149           0.0112           0.0151           0.0059           0.040           0.0240           0.0240           0.0391           0.0075           0.0152           0.0234	Local sy / 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.2807 0.2807 0.2334 0.0636 0.1013 0.0637 0.1264 0.0527 0.3042 0.3042 0.3674 0.1998	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.3961 0.4417 0.2965 0.0800	u 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2509 0.1287 0.2595 0.1273 0.4548 0.4962 0.3819	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0027 0.0012 0.0058 0.0192 0.0070 0.0044 0.0005 0.0011 0.0012 0.0012 0.0021 0.0027 0.0026 0.0012 0.0021 0.0027 0.0026 0.0014 0.0005 0.0014 0.0005 0.0014 0.0005 0.0014 0.0005 0.0014 0.0005 0.0014 0.0005 0.0014 0.0005 0.0015 0.0005 0.0015 0.0057 0.0015 0.0057 0.0015 0.0057 0.0015 0.0015 0.0057 0.0012 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0012 0.0027 0.0012 0.0012 0.0057 0.0012 0.0027 0.0012 0.0027 0.0012 0.0027 0.0027 0.0012 0.0027 0.	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0100 0.0030 0.0159 0.0430 0.0159 0.0430 0.0171 0.0113 0.0014 0.0043 0.0041 0.0066 0.0066 0.0066 0.0066	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.03082 0.0445 0.0445 0.0445 0.0445 0.0445 0.0445 0.042 0.0162 0.0162 0.0174 0.0187 0.0164 0.0268 0.0362	Local sy l 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0433 0.0996 0.2523 0.1246 0.0888 0.0438 0.0181 0.0215 0.1014 0.0226 0.0318 0.0248	<i>m</i> 0.3000 0.2972 0.0265 0.0237 0.0626 0.0210 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189 0.0233 0.1757 0.0371 0.0430 0.0294	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.0878 0.0227 0.2709 0.0509 0.0509 0.0685 0.0379	value <i>l</i> 0.0004 0.0021 0.0017 0.0017 0.0011 0.0003 0.0009 0.0041 0.0203 0.00024 0.0005 0.0005 0.0005 0.0003 0.0005 0.0003 0.0006 0.0006 0.0006	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0026 0.0131 0.0492 0.0065 0.0021 0.0016 0.0092 0.0006 0.0151 0.0006	u 0.002 0.012 0.000 0.006 0.010 0.016 0.001 0.009 0.030 0.091 0.005 0.005 0.002 0.001 0.003 0.001 0.003 0.001 0.003 0.001 0.001 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00
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tem DEMC WAAC UQU GHEM ADIM JEPO AANRE CACO DECO TCO CACO DECO TCO CACO DECO TCO CACO DECO TCO CACO DECO TCO CO CACO DECO TCO CO CO CO CO CO CO CO CO CO CO CO CO C	Local sy 7 0.0580 0.0511 0.1775 0.1070 0.0793 0.1312 0.1312 0.0630 0.0630 0.0358 0.0367 0.0410 0.0619 0.1684 0.0853 0.2049 0.1026 0.0973 0.1455 0.1098 0.1856	m 0.1000 0.0749 0.2401 0.1686 0.1299 0.2298 0.2229 0.0979 0.0482 0.0507 0.0482 0.0507 0.0589 0.1002 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.0577 0.1385 0.2109 0.1686 0.1202 0.0577 0.1385 0.2102 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1202 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.1012 0.2838 0.2109 0.2109 0.2826 0.2926 0.2	<i>u</i> 0.1733 0.1184 0.3301 0.2498 0.2044 0.3277 0.1578 0.0786 0.0721 0.0836 0.0721 0.0836 0.1532 0.3721 0.1790 0.3729 0.2655 0.2076 0.2818 0.2470 0.3685	value <i>l</i> 0.0001 0.0006 0.0010 0.0089 0.0020 0.0047 0.0025 0.0015 0.0015 0.0015 0.0030 0.0008 0.0005 0.0019 0.0016 0.0022 0.0016 0.0022 0.0041 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0026 0.0027 0.0005 0.0010 0.0005 0.0010 0.0005 0.	0.1451 ite relative m 0.0003 0.0015 0.0024 0.0259 0.0069 0.0077 0.0040 0.0040 0.0070 0.0040 0.0070 0.0022 0.0014 0.0076 0.0060 0.0079 0.0151 0.0023 0.0070 0.0079 0.0077 0.0034	u           0.0011           0.0039           0.0068           0.0541           0.0207           0.0503           0.0226           0.0112           0.01151           0.0059           0.0040           0.0192           0.0240           0.0192           0.0249           0.0075           0.0152           0.0234           0.0244           0.0127	Local sy / 0.1973 0.0811 0.0480 0.3009 0.2726 0.0746 0.0667 0.2807 0.2807 0.4677 0.2807 0.4677 0.2804 0.0636 0.1013 0.0637 0.1264 0.0527 0.3042 0.3674 0.1998 0.0588	m 0.3000 0.1298 0.0658 0.3820 0.3707 0.1205 0.3873 0.5233 0.1242 0.2999 0.1032 0.1593 0.0834 0.1747 0.3961 0.4417 0.2965 0.0800	u 0.3947 0.2099 0.0876 0.4437 0.4457 0.2053 0.1188 0.4703 0.5569 0.1894 0.3736 0.1587 0.2509 0.1232 0.2595 0.1273 0.4548 0.4962 0.4548 0.4962 0.3819 0.1195	value <i>l</i> 0.0004 0.0009 0.0003 0.0251 0.0067 0.0012 0.0070 0.0012 0.0070 0.0014 0.0012 0.0014 0.0021 0.0021 0.0021 0.0027 0.0066 0.0047 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0001 0.0001 0.0005 0.005 0	0.1971 ite relative m 0.0010 0.0026 0.0007 0.0587 0.0196 0.0196 0.0130 0.0430 0.0430 0.0113 0.0014 0.0043 0.0041 0.0043 0.0041 0.0047 0.0066 0.0146 0.0146 0.0147 0.0022 0.0034	u 0.0026 0.0068 0.0018 0.0962 0.0451 0.0306 0.0445 0.0397 0.0264 0.0042 0.0162 0.0132 0.0174 0.0164 0.0268 0.0268 0.0269 0.027	Local sy 1 0.1973 0.1810 0.0227 0.0206 0.0434 0.0500 0.0194 0.0443 0.0996 0.02523 0.1246 0.0888 0.0438 0.0438 0.0438 0.0438 0.0438 0.0438 0.0181 0.0215 0.0215 0.0318 0.0248 0.0318 0.0221	m 0.3000 0.2972 0.0265 0.0237 0.0626 0.0290 0.0623 0.1592 0.3581 0.1713 0.1515 0.0596 0.0189 0.0233 0.1757 0.0371 0.0371 0.0371 0.0430 0.0294 0.1344	u 0.3947 0.3870 0.0357 0.0290 0.1061 0.1095 0.0237 0.1021 0.2180 0.4356 0.2472 0.2120 0.0878 0.0222 0.0287 0.2209 0.0509 0.0509 0.0509 0.0509 0.0517	value <i>l</i> 0.0004 0.0021 0.0017 0.0017 0.0018 0.0003 0.0009 0.0041 0.0203 0.0024 0.0007 0.0005 0.0003 0.0002 0.0003 0.0002 0.00040 0.0006 0.0006 0.0006 0.0001 0.0006	0.1584 ite relative m 0.0010 0.0059 0.0003 0.0036 0.0033 0.0057 0.0007 0.0026 0.0131 0.0492 0.0065 0.0021 0.0016 0.009 0.0006 0.0151 0.0006 0.0014 0.0015 0.0017 0.0004	

COM Composting, RDF Refuse-derived fuel, INC Incineration, GAS Gasification, PYR Pyrolysis, SLF Sanitary landfill

priority of 14.29, and (ii) one criterion being 50% and 50% for other criteria with an equal priority value. *Case 1:* providing an identical priority of 14.29% to each criterion. *Case 2:* social and political impact has been given a priority of 50%, while the remaining priority value is equally divided among other criteria. *Case 3:* the opportunity criterion has a priority value of 50%, while the remaining priority value

is equally divided into other criteria. *Case 4:* technical criterion has a priority value of 50%, while the remaining priority value is equally divided into other criteria. *Case 5:* economical criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria. *Case 6:* managerial criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria. *Case 6:* managerial criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria. *Case 6:* managerial criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria.

Alternative	l	т	u	Weight vector	Overall priority (nor- malised)	Ranking
INC	0.0472	0.1402	0.3729	0.1868	0.1450	5
RDF	0.0634	0.1960	0.5018	0.2537	0.1970	2
GAS	0.0464	0.1513	0.4142	0.2040	0.1584	3
PYR	0.0456	0.1471	0.4012	0.1980	0.1537	4
COM	0.0956	0.2453	0.5506	0.2972	0.2308	1
SLF	0.0436	0.1198	0.2802	0.1479	0.1148	6

Table 9 Ranking of solid waste treatment and disposal technology based on Goal

Note: total weight vector is 1.2876

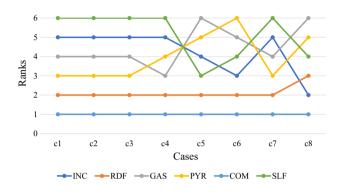


Fig. 5 Sensitivity analysis based on FAHP model for the 8 cases of the solid waste treatment and disposal technologies

7: environmental criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria. And *Case 8:* the waste quality and quantity criterion has a priority of 50%, while the remaining priority value is equally divided into other criteria.

The results of the sensitivity analysis shown in Fig. 4 represent the priorities of different cases. Composting is ranked first among other alternatives in all cases with varying priority values. RDF is second except in *Case 8*, with priority values varying between 0.15 and 0.22. Finally, in terms of solid waste treatment and disposal technology, incineration and sanitary landfills are considered the last alternative in most cases.

Figure 5 shows the "What if Analysis" results to check whether any treatment options ranking changed. The results show no changes in the ranked results, indicating that the composting alternative is still the best option for treating solid waste treatment and disposal technology. Except in *Case 8*, RDF is the second-best technology for solid waste treatment. The sanitary landfilling and incineration technology ranked last in most of cases. It should be emphasized that the rank of solid waste treatment and disposal systems may vary depending on the system's progress.

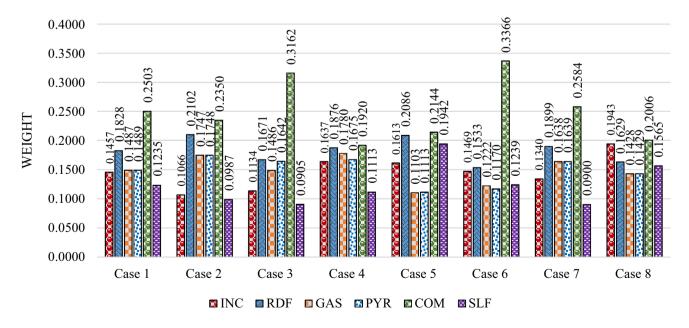


Fig. 4 Overall evaluation of solid waste treatment and disposal technology for Cases 2–8

### Conclusions

The selection of solid waste treatment/disposal technology is a complex multi-criteria decision-making process, with the essential characteristics being uncertainty, complexity and hierarchy. The FAHP approaches present a realistic way to select and prioritize solid waste treatment and disposal technology problems. In this study, the FAHP method is used in two ways: manually with the MS Excel software and with the RStudio software package, and the results from both are consistent, proving the accuracy of the final results. Out of seven criteria, the environmental criterion has demonstrated great importance compared to the other criteria. In contrast, a pairwise comparison revealed that the waste quality and quantity criterion is the least important of the criteria. The most favored solid waste treatment technology for the treatment and disposal of solid waste is composting. The organic component of solid waste is significant; hence, this technology is ideal. Gasification, pyrolysis and incineration are not favored technologies due to a large amount of organic waste, environmental issues, and strong public opposition due to perceptions relevant to human health risks. In many places in India, open landfilling is still performed, with massive piles of rubbish piled around the landfilling in the most unsanitary manner. Sanitary landfilling is the least preferred alternative due to associated disadvantages such as the need for a huge amount of land, negative impacts on surrounding communities, and a long residence duration of solid waste. In this context, the established methodology will aid planners and policymakers in selecting India's most appropriate solid waste treatment technologies.

The study was limited to seven criteria and only six treatment and disposal technologies. Since gasification and pyrolysis are still in the early stages of commercialization, their application to MSW in India should be investigated further, with real evidence from technology. Other multiple criterion methods, such as AHP-GIS, Picture fuzzy AHP, Pythagorean fuzzy AHP, Fuzzy TOPSIS and ELECTRE, etc., can be employed in future studies to evaluate the MSW treatment process.

### Declarations

Conflict of interest The authors declare no conflict of interest.

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