RESEARCH ARTICLE

Low‑Cost, Scalable Fabrication of All‑Fabric Piezoresistive Sensors via Binder‑Free, In‑Situ Welding of Carbon Nanotubes on Bicomponent Nonwovens

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Abstract

Wearable piezoresistive sensors have shown enormous application prospects in fexible electronics and human–machine interfaces. However, current piezoresistive sensors sufer from common defciencies including high fabrication cost, poor comfort and low attachment fastness of conductive substances on substrates, thereby impeding their large-scale production and practical use. Herein, a three-dimensional all-fabric piezoresistive sensor is reported based on coating multi-wall carbon nanotubes (MWCNTs) on bicomponent nonwovens composed of core-sheath fbers. The combination of core-sheath fbers with a heat-induced welding strategy greatly improves the adhesion fastness and stability of MWCNT network. The multilayered all-fabric structure provides as-prepared sensors with high sensitivity (9.43% kPa^{−1} in 0–10 kPa and 0.076% kPa^{−1} in 20–120 kPa), wide pressure-sensing range (0–120 kPa), fast response/relaxation time (100 and 60 ms), good reproducibility and air permeability. Application of the sensor is demonstrated through the detection of human activities (such as pulse, cough and joint movements) and the wireless monitoring of forefnger bending. Moreover, our sensor is fabricated out of cost-efective materials, using scalable approach without using glue or binders. The method established in this work may provide an efficient strategy for the design and production of high-performance all-fabric piezoresistive sensors.

Keywords Piezoresistive pressure sensors · Core-sheath fbers · All-fabric · Multi-wall carbon nanotubes · In-situ welding

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Introduction

Wearable piezoresistive sensors have attracted immense research interests for their important application potential in flexible electronics $[1, 2]$ $[1, 2]$ $[1, 2]$ $[1, 2]$, speech recognition systems $[3]$ $[3]$, healthcare monitoring [[4](#page-9-3), [5\]](#page-9-4), human–machine interfaces [[6\]](#page-9-5) and intelligent robots [\[7](#page-9-6)]. Similar to mechanoreceptors of human skin, piezoresistive sensors featuring the excellent advantages of concise signal detection, high reliability, simple device confgurations and low energy consumption are capable of sensing external mechanical stimuli through resistance or current change signals [\[8](#page-9-7), [9\]](#page-9-8). Compared with metal foil gauges [[10](#page-9-9)], conductive polymeric composites (CPCs) display greater potential in wearable piezoresistive sensors because of their light weight, good fexibility, and high sensitivity [[11](#page-9-10), [12\]](#page-9-11). A class of CPCs has been developed by blending conductive substances into an elastic polymer matrix [\[13](#page-9-12)[–15\]](#page-9-13). As conductive substances are easily wrapped by insulative polymers, the proportion of conductive substances must be high enough to ensure the conductivity of CPCs, thus may inevitably afect the processing difficulty, cost, and flexibility of CPCs. The most commonly used strategy to resolve these problems is to uniformly coat fexible substrates with conductive substances, such as carbon nanotubes [[16\]](#page-9-14), graphene [\[17](#page-9-15)], MXene nanosheets [[18](#page-9-16)], silver nanowires [[19\]](#page-9-17), poly(3,4-ethylened ioxythiophene):poly(styrenesulfonate) [\[20](#page-9-18)] and polyaniline [\[21\]](#page-9-19).

To date, multifarious fexible substrates, including rubber flms [[22\]](#page-9-20), sponges [[23](#page-9-21)], papers [\[24](#page-9-22)], aerogels [\[25](#page-9-23)], leatherwear [[26\]](#page-9-24) and fabrics [[27\]](#page-9-25), have been employed for developing high-performance CPCs. Among them, fabric-based CPC (FCPC) is one of the most preferred candidates for wearable piezoresistive sensors, because of their exceptional flexibility, compressibility, breathability, and skin affinity [\[28–](#page-9-26)[31\]](#page-10-0). The resistance change of FCPCs is mainly attributed to the microporous structure deformation of fabrics under external pressure. To satisfy the requirements for fullscale monitoring of both subtle physiological signals (e.g., pulse, breath and facial expression) and large activities (e.g., joint motions) from the human body, considerable efforts have been made to design FCPCs with outstanding compression resilience and large structural deformation [[17,](#page-9-15) [20,](#page-9-18) [32](#page-10-1)]. This is because the large but stable architecture deformation of three-dimensional (3D) microporous FCPCs leads to a greater variation in conductive pathways, which is benefcial for increasing the sensitivity and sensing range of piezoresis-tive sensors [[33](#page-10-2)].

Despite the encouraging advances of FCPCs, less attention has been paid to improving the adhesion fastness between conductive substances and fbers. Since conductive substances usually adhere to the fber surface, the resultant sensor is vulnerable to the repeated exertion of wearing and washing in practical use. The subsequent loss of conductive substances causes an irreversible decrease in conductivity, thus impeding the long-term repeatability and service life of the sensor. While a trustworthy adhesion fastness of conductive coating on fabrics was reported in a few times [[34](#page-10-3)[–36](#page-10-4)], these reports required additional binders and/or a sophisticated fabrication approach, which hindered the broad applicability of resulting sensors. Moreover, most FCPC-based sensors contain polymeric flms (such as polydimethylsiloxane (PDMS) and polylactic acid) [[37](#page-10-5), [38\]](#page-10-6), but the airproof structure of these flms may easily result in skin irritation and discomfort in daily usage. Therefore, it has been challenging to develop a binder-free, scalable technology for fabricating 3D all-fabric piezoresistive sensors with robust anchoring of conductive substances.

Herein, we demonstrate the facile fabrication of a 3D allfabric piezoresistive sensor through dip-coating multi-wall carbon nanotubes (MWCNTs) on bicomponent spunbond nonwoven (NW) composed of core-sheath flaments with polypropylene (PP) as the core and polyethylene (PE) as the sheath. The introduction of hydrophilic PP into PE component (fber sheath) made the PE/PP spunbond NWs hydrophilic, which was conducive to the attachment of MWCNTs. An in-situ welding technology was adopted to enhance the attachment fastness between MWCNTs and PE/PP fbers. To construct large structural deformation that could increase the electric touchpoints and contact areas under pressure, multiple layers of 2D conductive NWs were laminated into 3D sensors. The relationship between the number of conductive fabric layers and the sensing performances of the sensor was systematically studied. The as-prepared sensor was proven efective in real-time detection of various types of human motions, such as pulse, breath, cough, muscle contraction and joint movement, and the detection was capable of being wireless.

Experimental Section

Materials

PE [melt index: 20 g/(10 min)] and PP [melt index: 35 g/ (10 min)] polymer chips were provided by PetroChina, China. Hydrophilic PP (melt index: 25 g/(10 min)) polymer chips were purchased from Shanghai Huzheng Industrial, China. Commercial dispersants (XFZ20) were provided by Nanjing Xianfeng Nano Material Technology, China. MWC-NTs (diameter = $10-20$ nm, length < $30 \mu m$) were obtained from Chengdu Organic Chemical, China.

Fabrication of PE/PP NW

PE and PP were melted and extruded by two screws to spinneret to form PE (sheath)/PP (core) melt fuid (the volume ratio of PE and PP was 50–50). A small proportion of hydrophilic PP (5 wt.%) was further blended with PE as the sheath component to change the wettability of PE/PP fbers. The temperature of both screws was 230 °C, and the extrusion capacity of the metering pumps was 300 cc/min. High-speed cool air (speed=20.1 m/s, temperature=12 $^{\circ}$ C) was used to quench and draw the melted polymer to form continuous PE/PP flaments with high strength. The flaments were further collected on a mesh apron (at a speed of 2 m/min) through negative pressure to obtain a fber web. Finally, the formed fber web was consolidated into NW (areal density=36 g m⁻²) through thermal bonding technology with a hot air temperature of 135 °C.

Fabrication of MWCNT Dispersion

MWCNTs (0.2 g) were added into 100 mL of deionized water containing 0.08 g of XFZ20, followed by probe ultrasonication (Shanghai Bilang Instrument Manufacturing, China) for 2 h at a frequency of 20 kHz. The resultant dispersion was gently centrifuged at a speed of 2000 r/min for 20 min to remove free MWCNTs.

Fabrication of NWs Coated with MWCNTs (MWCNT‑NWs)

The as-prepared NW was immersed in the MWCNT dispersion for 10 min and dried in an air-circulating oven at 70 °C. The above coating procedure was repeated three times to acquire MWCNT-NWs with high conductivity. The MWCNT-NWs were then treated at diferent temperatures (120, 130 and 140 °C) in an air-circulating oven for 2.5 min. The resultant samples were labeled MWCNT-NW-120, MWCNT-NW-130 and MWCNT-NW-140.

Fabrication of Piezoresistive Sensors

The MWCNT-NWs were cut into squares with the dimensions of 1 cm \times 1 cm \times 0.08 cm (length \times width \times height). Five layers of MWCNT-NW-130 were stacked and then wrapped by a thin layer of spunbond NWs to construct a multi-layered piezoresistive sensor. To accurately detect the resistance signals of the sensor, two thin copper wires $(diameter=0.1 \text{ mm})$ were connected to its top and bottom layers by using conductive silver paste as the electrode. For comparison, 1-, 3- and 7-layered piezoresistive sensors were also fabricated.

Characterization

The surface and cross-sectional morphologies of the samples were observed by a SU8010 feld-emission scanning electron microscope (FE-SEM, Hitachi, Japan). Raman spectra were obtained by an inViaRefex Raman system (Renishaw, UK) with 632 nm excitation in the range from 550 to 3200 cm⁻¹. The static water contact angle (WCA) was measured by an OCA15EC contact angle measuring system (Dataphysics, German), and air permeability was tested in an automatic permeability tester (Ningbo Textile Instrument, China). Thermal gravimetric analysis (TGA) was performed under a nitrogen atmosphere using a TGA 4000 thermogravimetric analyzer (PerkinElmer, USA) from 50 to 700 °C at a heating rate of 10 °C min⁻¹. The abrasion test was conducted by applying the Martindale measurement (Ningbo Textile Instrument, China) under a 200 g load for 600 cycles. The washing test was performed by stirring samples in deionized water for 30 h at a speed of 1000 r/min. The mechanical properties of the samples in cross-sectional direction (CD) and machine direction (MD) were characterized by a universal material tester (Shenzhen Suns Technology, China) according to the GB/ T3923 strip method. Piezoresistive performances of sensors were measured by connecting the universal material

tester with a DAQ6510 data acquisition multimeter system (Keithley, USA). Current–voltage (I–V) curves were obtained by a Model 2450 source meter (Keithley, USA).

Sensitivity (*S*) of the sensor was calculated by Eq. ([1](#page-2-0)):

$$
S = \frac{|\Delta R/R_0|}{\Delta P} \tag{1}
$$

where ΔP , ΔR and R_0 refer to the change in pressure, the relative change in resistance, and the initial resistance of the sensor without pressure, respectively. Depending on the change of resistance with pressure, sensitivity was categorized as S1 in the small pressure range (0–10 kPa) and S2 in the large pressure range (20–120 kPa), and was then ftted linearly to evaluate the sensing performances of the sensor. Additionally, to attain the response/relaxation time of the piezoresistive sensor, a compressing-holding-releasing cycle was performed, in which the holding time, loading pressure and loading/unloading speed were set as 3.1 s, 3 kPa and 100 mm/min, respectively.

Results and Discussion

Fabrication and Characterization of MWCNT‑NWs

Figure [1a](#page-3-0) depicts the fabrication procedure for our multi-layered all-fabric piezoresistive sensors. The low melting temperature $(T_m, \sim 130 \text{ °C})$ of PE enabled tight thermal bonding of neighboring fbers without applying any glue or binders. It also inspired us to realize the attachment fastness of MWC-NTs on the surface of fbers facilitated by the PE sheath. To confrm our hypothesis, bicomponent NWs composed of coresheath flaments with PP as the core and PE as the sheath were manufactured using industrialized spunbond technology. Owing to the hydrophobic nature of PE and PP, the as-prepared PE/PP NW displayed a high WCA of 136.8° (Fig. S1), which might block the penetration of MWCNT dispersion into the inter-fber pores of NW. Hence, hydrophilic PP (5 wt.%) was introduced to change the wettability of PE/PP NW. It can be observed from Fig. [1](#page-3-0)b that fbers of the PE/PP NW presented a typical sheath-core cross-sectional structure. In thermal bonding, hot air (135 °C) passed through the fbrous web to partially melt the fber sheath (PE) and bind adjacent fbers together, and the WCA of NW was 48.6°(Fig. [1c](#page-3-0)). In comparison with other modifcation technologies (chemical coating, plasma treatment, etc.) [[39](#page-10-7)[–41](#page-10-8)], the method of directly adding hydrophilic polymers in spinning process was particularly advantageous in durability. The resultant PE/PP NW became permanently hydrophilic, and its mechanical properties (Fig. $1d$) were sufficient to meet the demands for wearable piezoresistive sensors.

Fig. 1 a Schematic illustration for fabricating multi-layered all-fabric piezoresistive sensors. **b** FE-SEM image showing the sheath-core fber structure. **c** FE-SEM image of NW. Inset is the WCA of NW.

The binding points of adjacent fbers are indicated by yellow circles. **d** Stress–strain curves of NW and **e** color of NWs before and after loading MWCNTs

The coating of MWCNTs was then triggered by repeatedly impregnating hydrophilic spunbond NWs in the MWCNT aqueous dispersion. After decorating with MWC-NTs, the color of NWs changed from white to black, but the dimensions of NWs remained unchanged (Fig. [1](#page-3-0)e). For MWCNT-NWs, the interfacial connection between MWCNT network and PE/PP fbers mainly relied on van der Waals forces, and thus was vulnerable to repeated external forces such as wear and washing. This caused poor conductivity stability of MWCNT-NWs, which was usually associated with unfavorable durability of pressure sensors.

We developed an in-situ welding method to overcome this problem. According to the diferential scanning calorimetry (DSC) endotherms of PE/PP spunbond NW (Fig. S2), we set the welding temperature at 120, 130, and 140 °C. Since the T_m of fiber core (PP) reached ~160 °C, the shape of the PE/PP fbers was well retained under these temperatures. When treated at 120 °C for 2.5 min, the MWCNT network could not be embedded into PE/PP fbers, and the surface morphology before and after treatment was highly compa-rable (Fig. [2](#page-4-0)a and b), suggesting that 120° C was insufficient to embed MWCNTs into PE/PP fbers. When increasing the temperature to 130 °C, the MWCNT network was successfully welded into PE/PP fbers (Fig. [2c](#page-4-0)), which could be attributed to the low T_m of PE (~130 °C). The fiber sheath partially melted at this temperature, and a proportion of the MWCNTs on the fber surface entered the fber sheath due to the movement of the PE molecular chain. Therefore, the interfacial connections between MWCNTs and PE/PP fbers were greatly enhanced. When the temperature reached

140 °C, however, much of the PE was blended with the MWCNT network (Fig. [2d](#page-4-0)). Due to the insulative nature of PE, the connection of the MWCNT network was weakened, thus causing an increased volume resistance (Fig. [2](#page-4-0)e) that was not benefcial to the design of the piezoresistive sensors.

The infuence of welding temperature on the attachment fastness between MWCNT network and PE/PP fbers was further examined by rubbing the MWCNT-NWs under a 200 g load and stirred washing of the MWCNT-NWs at 1000 r/min. Here, the relative resistance variation ($\Delta R/R_0$, where ΔR is the change in resistance under applied stimulation and R_0 is the initial resistance without stimulation) of MWCNT-NWs after repeated abrasion or washing was measured as a pivotal index to refect the adhesion fastness of MWCNTs. After 600 rubbing cycles, the $\Delta R/R_0$ of MWCNT-NW-130 and MWCNT-NW-140 remained stable, but a clear increase in $\Delta R/R_0$ was found in MWCNT-NW-120, indicating a low adhesion fastness (Fig. [2](#page-4-0)f). The similar phenomenon was also found after continuous washing the sample for 30 h (Fig. [2](#page-4-0)g). These results proved that the heat-induced welding method was feasible and reliable for improving the adhesion fastness between MWCNTs and NWs. Due to the low volume resistance (4.53 kΩ) and high adhesion fastness, we selected 130 °C as the optimal welding temperature. The high adhesion fastness of MWCNTs at this temperature was further validated by the cross-sectional morphology of MWCNT-NW-130 (Fig. S3), in which distinct characteristic peaks of MWCNTs (1328, 1581, and 2644 cm⁻¹) were observed in Raman spectra (Fig. [2](#page-4-0)h).

Fig. 2 a FE-SEM images of MWCNT-NWs without welding treatment. Inset is the FE-SEM image of MWCNTs. FE-SEM images of MWCNT-NWs treated with welding temperatures of **b** 120 °C, **c** 130 °C and **d** 140 °C for 2.5 min. **e** The relationship between welding temperature and volume resistance. $ΔR/R₀$ changes of MWCNT-NWs

treated at diferent temperatures with **f** rubbing cycles and **g** washing time. **h** Raman spectra of pristine NW, MWCNT and MWCNT-NW-130. **i** TGA plots of pristine NW and MWCNT-NW-130. **j** Digital photographs displaying the fexibility of MWCNT-NW-130

TGA results in Fig. [2](#page-4-0)i suggested that the total proportion of MWCNTs on the PP/PE NW was 6.97%, which was much lower than those reported in previous methods [\[42,](#page-10-9) [43](#page-10-10)]. Considering the high price of MWCNTs (300 USD/kg), a low amount was used to reduce the cost. More importantly, the attachment of MWCNTs and subsequent welding treatment had no infuence on the fexibility of MWCNT-NW-130 (Fig. [2j](#page-4-0)). To the best of our knowledge, this is the frst time that heat-induced surface welding method was employed in PE/PP sheath-core fbers to enhance the adhesion fastness of MWCNTs, as previous reports usually used single-component fbers as substrates, and therefore required additional binders that can reduce the initial fexibility and permeability of the fabric substrate [[34,](#page-10-3) [44\]](#page-10-11).

Assembly and Characterization of All‑Fabric Piezoresistive Sensors

Because most fabrics are 2D (i.e., they are thin in the thickness direction) with limited structural deformation under external pressure, the transformation of 2D fabrics into 3D fabrics with large but stable structural deformation is a signifcant step in designing fabric-based piezoresistive sensors. Toward this goal, up to seven layers of 2D MWCNT-NW-130 were stacked and assembled into 3D sensors with multi-layered architecture. The relationship between the number of MWCNT-NW-130 layers and the sensitivity of the sensor is illustrated in Fig. [3a](#page-5-0). As the number of MWCNT-NW-130 layers increased from 1 to 7, the sensitivity of sensors in 0–10 kPa (small pressure range) and 20–120 kPa (large pressure range) increased. The sensitivity diference of sensors containing diferent layers of MWCNT-NW-130 could be attributed to the existence of inter-layer air gaps, which resulted in a relatively high resistance when no pressure was applied. Upon exposure to the applied pressure, these air gaps disappeared, leading to a rapid decrease in resistance. Consequently, when the number of layers increased from 1 to 7, the sensitivity of sensors in 0–10 kPa increased sharply. Air permeability of the sensors decreased from 1382.12 to 465.57 mm/s with increasing MWCNT-NW-130 layers (Fig. [3](#page-5-0)b). To accurately detect both small and large motions from the human body, we selected a sensor with 5 layers of MWCNT-NW-130 for the following experiment. This sensor presented high sensitivity (9.43% and 0.076% kPa⁻¹ in 0–10 kPa and 20–120 kPa, respectively) and favorable air permeability (927.88 mm/s). The efects of immersion time were also studied, and the results indicated that both the volume resistance of MWCNT-NWs and the piezoresistive behavior of the sensor changed slightly when the immersion time exceeded 10 min (Fig. S4).

As we expected, the sensor was also capable of responding to dynamic pressure, and the corresponding variation in $\Delta R/R_0$ was highly repeatable under different applied pressures ranging from 0.25 to 80 kPa (Fig. [3c](#page-5-0)). It is worth noting that pressures smaller than 0.25 kPa might also be detected by our sensor, but the resolution limit of the dynamometer is 0.25 kPa. The response time of the sensor was ∼100 ms under the pressure of 3 kPa, and the recovery

Fig. 3 a Resistance changes and **b** air permeability changes of sensors with diferent numbers of MWCNT-NW-130. **c** Resistance variation under various cyclic pressures. **d** Response time and relaxation time of the sensor. **e** Resistance response with a pressure of 10 kPa

at diferent frequencies. **f** Resistance response during 4000 repeated compression-release cycles with a pressure of 100 kPa, and **g** magnifed waveforms drawn from **f**. **h** I–V characteristics of sensors at static pressure

time was ~60 ms (Fig. [3d](#page-5-0)). The $\Delta R/R_0$ change was stable when the rate of pressure loaded to the sensor increased from 5 to 100 mm/min (Fig. [3e](#page-5-0)). Repeated compression and release of 4000 cycles was further performed to evaluate the long-term durability of sensor. Figure [3f](#page-5-0) shows that a slight drop in $\Delta R/R_0$ was generated within the first 158 cycles, and the variation in $\Delta R/R_0$ became unapparent during the rest of the cycles (Fig. [3](#page-5-0)g). The initial drop in $\Delta R/R_0$ could be attributed to the small but permanent plastic deformation of the fber-stacking structure under pressure, which was in accordance with the fabric-based piezoresistive sensors reported previously [\[33](#page-10-2), [45](#page-10-12)]. The response capacity to static pressure was proven by I–V characteristics (Fig. [3](#page-5-0)h). The slopes of I–V curves increased linearly when increasing the static pressure (from 0.5 to 80 kPa), signifying the good "ohmic" behavior and the wide sensing range of our sensor.

Table [1](#page-6-0) compares the basic performances (e.g., sensitivity, sensing range, response/relaxation time, reproducibility and air permeability) of our sensor with those of cutting-edge sensors [\[33](#page-10-2), [46](#page-10-13)[–54](#page-10-14)]. Deriving from the multi-layered all-fabric architecture and the high compressional resilience, our sensor exhibited exceptional overall performance. In particular, the large structural variation of the sensor enabled a high sensitivity, and a schematic illustration of the structural change under pressure is presented in Fig. [4a](#page-7-0). With the exertion of a small pressure, the decrease in the distance among MWCNT-NW-130 layers formed more electrical contact points among conductive fbers, resulting in a signifcant decrease in contact resistance and a high sensitivity in the range of 0–10 kPa. When the pressure ascended to a higher value, the MWCNT-NW-130 layers were all compressed, causing an increase in contact areas and a further decline in contact resistance. To more distinctly refect the pressure-sensitive property, the sensor was coupled into a circuit composed of nine light-emitting diode bulbs and a power supply (3 V). The light intensity of bulbs became higher as the loaded weight increased from 20 to 200 g (Fig. [4b](#page-7-0)). Taken together, these results led us to conclude that the loose connections among the MWCNT-NW-130 layers of our multi-layered sensor were ideal for detecting the structural variation and the contact resistance change under pressure.

Real‑Time Monitoring Human Motions Using All‑Fabric Piezoresistive Sensors

We fnally applied the sensors to diferent body parts to simultaneously detect both small and large human activities (Fig. [5a](#page-8-0)). The sensor attached to the volunteer's wrist served as a monitor to capture the blood pulse signal of the radial artery, and a reproducible $\Delta R/R_0$ waveform with a

Table 1 A comparison of our sensor with previously reported pressure sensors

Pressure sensor Materials		Sensitivity (kPa^{-1})	Sensing-range (kPa) Stability (times)		Breatha- bility (mm/s)
Ref 33	3D CNTs/NWs	0.057 0.00113	$0 - 131.32$	5000	553.85
Ref 46	Double-layered PDMS/CNTs	0.3 0.05	$0 - 2$	5000	airtight
Ref 47	3D polyurethane sponge coated with graphene and polyaniline	0.0021 0.0044 0.0109	$0 - 25$	10000	N/A
Ref 48	Electrospun carbon nanofiber films + PDMS films	0.96 0.12	$0 - 2$	3000	airtight
Ref 49	Multilayered graphene-paper $+$ polyimide (PI) tape	0.172 0.001	$0 - 20$	300	airtight
Ref 50	Highly-oriented and free-standing CNTs sheets	0.0013 0.0004	$0 - 40$	6000	airtight
Ref 51	CNTs/PDMS sponge	0.033 0.008	$0 - 150$	200	N/A
Ref 52	Graphene/polyurethane sponge	0.26 0.03	$0 - 10$	1000	N/A
Ref 53	PEDOT:PSS/PI aerogels	0.021 0.054 0.019	$0 - 17$	200	N/A
Ref 54	PI nanofiber/MXene aerogel	0.14 0.002	$0 - 85$	1000	N/A
This work	Multilayered bicomponent NWs coated with CNTs	0.0943 0.00076	$0 - 120$	4000	927.88

Fig. 4 a Schematic illustration showing the structural change of the sensor. **b** Resistance variation of the sensor under diferent loaded weights

periodicity of 84 times/min was acquired (Fig. [5](#page-8-0)b). The magnifed wave of a single pulse displayed three typical characteristic peaks (Fig. [5](#page-8-0)c): the percussion wave (P), the tidal wave (T) and the diastolic wave (D). Based on the intensity of these peaks, the radial augmentation index (defned as T/P) could be calculated as an important reference for the evaluation of arterial stifness and cardiovascular diseases. The radial augmentation index (0.76) was consistent with reference data for healthy men, suggesting the cardio-vascular ftness of the volunteer [[48,](#page-10-15) [55](#page-10-16)]. The sensor-equipped mask detected a respiration rate of 19 times/min (Fig. [5](#page-8-0)d), while the sensor mounted on the throat successfully detected the muscle movements in cough (Fig. [5](#page-8-0)e). The sensor was also used to sense muscle contraction by making a fist. As exhibited in Fig. [5](#page-8-0)f, regular variation in $\Delta R/R_0$ could be acquired when the volunteer made a fist repeatedly, and the recorded waveforms were highly comparable. The high sensitivity and wide sensing range of our sensor further enabled the detection of knee joint movements. Bending speed of the knee joint was precisely reflected by different frequencies of $\Delta R/R_0$ (Fig. [5g](#page-8-0)). These fndings supported the application potential of our sensor in noninvasive healthcare monitoring, wearable human–machine interfaces and physical training.

With the advent of the "Internet of Things" era, the transmission of signal waveforms to portable ports (e.g., mobile phones) has become increasingly important in applications such as medical wisdom [[56\]](#page-10-17). Therefore, we connected the sensor with a microcontroller unit and a Bluetooth module for remote wireless monitoring (Fig. [5](#page-8-0)h). A smart glove loaded with our sensor was then developed to realize wireless monitoring of fnger bending. When bending a forefnger at a regular frequency, the real-time resistance variation success-fully emerged on the screen of a mobile phone (Fig. [5](#page-8-0)i and movie S1). The resistance variation during the whole bending process was regular, steady and highly distinguishable $(Fig. 5j)$ $(Fig. 5j)$ $(Fig. 5j)$.

Pressure sensors should be manufactured by using costefective materials and scalable fabrication techniques. The PP/PE NW substrates in our sensor have been extensively used in medical supplies (such as masks and surgical gowns) at a cost of 0.1 USD/ m^2 . Although the prices of MWCNTs are high (300 USD/kg), their proportion was only 6.97% of the total mass of our sensors. In addition, the fabrication approaches in this work, including spunbond, solution coating and welding treatment have all been industrialized, without involving sophisticated facilities or time-consuming procedures. Therefore, the overall cost of our sensor (1 cm^2) was only ~ 0.02 USD, which is readily affordable in most applications.

Conclusions

In summary, we report the low-cost and scalable fabrication of a 3D all-fabric piezoresistive sensor based on PP/PE bicomponent nonwoven and MWCNTs. The combination of core-sheath fbers and a binder-free, in-situ welding strategy greatly enhanced the adhesion fastness of the MWCNT network. The multi-layered fabric architecture provided the sensor with high sensitivity, wide pressure-sensing range, fast response/relaxation, excellent long-term durability and

Fig. 5 a Diagram showing motion detection from human body parts. **b** Captured $\Delta R/R_0$ signals of wrist pulse and **c** enlarged waveform from one pulse signal. Regular Δ*R*/*R*0 signals resulting from **d** respiration and **e** cough. Reproducible Δ*R*/*R*0 signals of **f** muscle contraction and **g** knee bending. **h** Diagram demonstrating the concept of remote wireless monitoring using the sensor. **i** Digital photograph

good air permeability, and thus the sensor could be applied for real-time detection of various human activities. Remote wireless monitoring of forefnger bending was also achieved. We propose that the facile, versatile, low-cost and scalable approach developed in this work may ultimately lead to the showing both detection of forefnger bending and wireless transmission of resistance signals. Magnifed photograph is the corresponding real-time resistance variation signals transmitted wirelessly to a mobile phone. **j** Recorded resistance variation during the whole process of forefnger bending

manufacture and application of commercialized fabric-based pressure sensors.

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Data availability The data that support the fndings of this study are available from the corresponding author upon reasonable request.

Declarations

Conflict of Interest The authors declare that they have no known competing fnancial interests or personal relationships that could have appeared to infuence the work reported in this paper.

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