### **RESEARCH ARTICLE**



# **Hybrid Polymer Membrane Functionalized PBO Fibers/Cyanate Esters Wave‑Transparent Laminated Composites**

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### **Abstract**

Hybrid polymer membrane (TA-APTES), synthesized by tannic acid (TA) and aminopropyl trethoxysilane (APTES) based on the Schif's base and Michael addition reaction, is deposited on the surface of poly(*p*-phenylene-2, 6-benzobisoxazole) (PBO) fbers, and then grafted with epoxy-terminated polysesquisiloxane (POSS) to obtain POSS-*g*-PBO@TA-APTES fbers. The POSS-*g*-PBO@TA-APTES fbers reinforced bisphenol A dicyanate ester (BADCy) resins (POSS-*g*-PBO@TA-APTES fbers/BADCy) wave-transparent laminated composites are prepared. The interlaminar shear strength and fexural strength of POSS-*g*-PBO@TA-APTES fbers/BADCy composites are respectively enhanced from 36.7 and 587.4 MPa to 42.8 and 645.8 MPa, increased by 16.6% and 9.9% compared with those of PBO fbers/BADCy composites. At 1 MHz, the corresponding dielectric constant and dielectric loss are reduced to 2.85 and 0.0047, respectively, lower than those of PBO fbers/BADCy (3.06 and 0.006) composites. Meanwhile, the simulated wave transmittance rate of POSS-*g*-PBO@TA-APTES fbers/BADCy composites with the thicknesses of 1.5–3.5 mm is higher than 86.2% at 0.3–40 GHz. The volume resistivity and breakdown strength of POSS-*g*-PBO@TA-APTES fibers/BADCy composites are  $2.8 \times 10^{15}$  Ω·cm and 19.80 kV/mm, higher than PBO fibers/BADCy composites  $(2.2 \times 10^{15} \Omega \cdot cm$  and 17.69 kV/mm), respectively. And the corresponding heat resistant index is 221.5 °C, lower than PBO fbers/BADCy composites (229.6 °C).

**Keywords** Poly(*p*-phenylene-2, 6-benzobisoxazole) fbers · Bisphenol A dicyanate ester resins · Wave-transparent laminated composites · Interlaminar shear strength · Surface functionalization

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### **Introduction**

Polymer matrix wave-transparent composites can effectively protect the electromagnetic equipments inside antenna system from adverse external environment and ensure high electromagnetic wave transmission, which are widely used as electromagnetic window materials for military weapons and civilian telecommunication base stations [\[1](#page-9-0), [2\]](#page-9-1). However, with the rapid development of the new generation of military equipment and 5G telecommunication, higher requirements of mechanical properties and wave-transparent performances are put forward for advanced polymer matrix wave-transparent composites [[3\]](#page-9-2).

Compared with quartz fibers  $[4, 5]$  $[4, 5]$  $[4, 5]$  $[4, 5]$ , basalt fibers  $[6]$  $[6]$ , and aramide fbers [[7,](#page-9-6) [8](#page-9-7)], the high modulus poly(*p*-phenylene-2, 6-benzobisoxazole) (PBO) fbers possess superior mechanical properties, better chemical and thermal stability, and ultra-lower dielectric constant (*ε*) and dielectric loss (tan*δ*) (Table S1) [\[9](#page-9-8), [10\]](#page-9-9). However, the interfacial bonding strength of PBO fbers reinforced polymer matrix laminated composites is extremely weak [[11,](#page-9-10) [12](#page-9-11)]. Besides, the poor interfacial compatibility between PBO fbers and polymer matrix will produce strong interfacial polarization under external electric field, which would lead to larger  $\varepsilon$  and tan $\delta$  values [\[13](#page-9-12)].

As far as we know, chemical etching [\[14](#page-9-13)], radiation treatment  $[15]$  $[15]$ , plasma treatment  $[16]$  $[16]$ , coating  $[3, 17]$  $[3, 17]$  $[3, 17]$ , and grafting [[18,](#page-9-17) [19\]](#page-9-18), etc., are usual surface modifcation methods of PBO fbers. Chemical etching, radiation treatment, and plasma treatment methods apply strong acid or high-energy ray to etch PBO fbers, which can generate active groups to improve the surface chemical inertness of PBO fbers [\[20,](#page-9-19) [21](#page-9-20)]. However, strong acid and high-energy ray would destruct the structure of PBO fbers. Coating and/or grafting an active layer on the surface of PBO fbers can efectively improve the chemical inertia of PBO fbers without compromising the mechanical properties [[22,](#page-9-21) [23\]](#page-9-22). Liu et al*.* coated the synthesized hydroxyphosphide castor oil (PCO) on PBO fbers followed by blending with epoxy resins (E-51). When the ratio of PCO to E-51 was 3:1, the single fber pull-out strength of PBO fber/PCO/epoxy resins composites was 12.03 MPa, increased by 154.8% [[24](#page-9-23)]. Hu et al*.* prepared graphene-based coaxial hybrid PBO fbers (PBO-CHFs) by uniformly coating graphene and metal–organic framework hybrid layer on PBO fbers. The corresponding interlaminar shear strength (ILSS) of PBO-CHFs fbers/epoxy resins composites was 74.56 MPa, increased by 17.8% [[25\]](#page-10-0).

Dopamine (DA) can self-polymerize to form polydopamine (PDA) layers on the surface of various substrates by mimicking the adhesion mechanism of mussels. Chen et al*.* grafted graphene oxide onto the surface of PBO fbers coated by PDA, which signifcantly increased its roughness and UV resistance. The ILSS of the modifed PBO fbers/epoxy

resins composites was 68.2 MPa in compare with the PBO fbers/epoxy resins composites (40.4 MPa) [[26\]](#page-10-1). Shao et al*.* coated PDA on PBO fbers, and then fxed BN nanosheets on the above PBO fbers to obtain BN-PDA-PBO fbers. Compared with PBO fbers/polyurethane (TPU), the ILSS of BN-PDA-PBO/TPU composites increased to 70.45 MPa [[27](#page-10-2)]. In our pervious work, Gu et al*.* utilized PDA and KH-560 functionalized PBO (KH-560/PBO@PDA) fbers as reinforcement, and fuorinated bisphenol A cyanate (*m*-BADCy) resins as matrix to prepare KH-560/PBO@PDA fbers/*m*-BADCy laminated composites. The ILSS and fexural strength were respectively 49.5 and 652.2 MPa, better than those of the PBO fbers/*m*-BADCy composites (39.9 and 601.6 MPa). And the corresponding *ε* and tan*δ* values decreased to 2.86 and 0.00576, respectively [[28](#page-10-3)].

Tannic acid (TA), a type of polyphenol extracted from plants, is similiar to DA, and can rapidly, gently, and stably adhere to the surface of various materials (polymers, metals and their oxides, inorganic non-metallic materials, etc.) through oxidative self-polymerization, which enables the simple and efficient surface functionalization of the substrates [\[29,](#page-10-4) [30\]](#page-10-5). Meanwhile, the tannic acid-aminopropyl trethoxysilane (TA-APTES) hybrid membrane, generated by the reaction of TA oxidation with 3-aminopropyl trethoxysilane (APTES), has a large number of reactive groups (hydroxyl and amino groups, etc*.*), which could provide abundant chemical reaction sites for secondary functionalization [\[31](#page-10-6), [32\]](#page-10-7), which is very attractive for surface functionalization of PBO fbers [\[33\]](#page-10-8).

In this paper, the TA-APTES hybrid membrane, synthesized by TA and APTES via Schif's base and Michael addition reaction, is constructed on the surface of PBO fbers by *in-situ co*-deposition method, and then grafted with polysesquisiloxane (POSS) to prepare POSS-*g*-PBO@TA-APTES fbers (Fig. [1\)](#page-2-0). And the POSS-*g*-PBO@TA-APTES fbers are utilized as reinforcement, and bisphenol A dicyanate ester (BADCy) resins with excellent dielectric properties, outstanding mechanical properties and heat resistance [[34–](#page-10-9)[36\]](#page-10-10) as matrix to prepare POSS-*g*-PBO@TA-APTES fbers reinforced BADCy resins (POSS-*g*-PBO@TA-APTES fbers/ BADCy) wave-transparent laminated composites. Fourier transform infrared (FTIR) spectroscopy, X-ray photoelectron spectroscopy (XPS), scanning electron microscopy (SEM), and atomic force microscopy (AFM) are used to analyze the composition and morphologies of PBO fbers before and after surface functionalization. The efects of synergistic functionalization for POSS-*g*-PBO@TA-APTES fbers on the mechanical properties, wave-transparent performance, electrical insulation properties, and heat resistance of POSS-*g*-PBO@TA-APTES fbers/BADCy composites are investigated.



<span id="page-2-0"></span>**Fig. 1** Schematic diagram of preparation for POSS-*g*-PBO@TA-APTES fber

# **Results and Discussion**

## **PBO Fibers Before and After Surface Functionalization**

Figure [2](#page-3-0)a shows the FTIR spectra of PBO fbers before and after surface functionalization. The absorption peaks at 3059, 1614, and 1556  $cm^{-1}$  are attributed to the vibration of unsaturated C–H, C=C, and C–C on the benzene ring of PBO fbers, respectively. Moreover, peaks at 1630 and 1053 cm−1 correspond to the vibration of C=N and C–O–C in oxazole ring of PBO fbers, respectively. After surface functionalization, the wide absorption peak at 3500−3300 cm−1 in PBO@TA-APTES fbers can be attributed to the vibration of  $-NH_2$ ,  $-NH_2$ , and  $-OH$  in the TA-APTES hybrid membrane. In addition, the characteristic peaks of C=O and Si–O appear at 1705 and 1053 cm<sup>-1</sup>, indicating that TA-APTES membrane is successfully deposited on the surface of PBO fbers. C–H stretching vibration peaks at 2916 and 2848 cm−1 can be attributed to the alkyl groups of POSS structure. Meanwhile, the absorption peak at 3417 cm−1 in POSS-*g*-PBO@TA-APTES fbers is attributed to the vibration of –NH– and –OH, which would be caused by the reaction of the epoxy group of POSS with  $-NH<sub>2</sub>$  and  $-OH$  of TA-APTES [[37](#page-10-11)].

Figure [2](#page-3-0)b shows the TGA curves of PBO fibers before and after surface functionalization. Pristine PBO fbers show excellent heat resistance showing negligible weight loss before 650 °C. The weight loss rate of PBO@TA-APTES

fbers gradually increases with the increase of temperature. Moreover, the weight loss rates of PBO@TA-APTES fbers are higher than that of pristine PBO fbers at the same temperature, which is caused by the decomposition of TA-APTES membrane. For POSS-*g*-PBO@TA-APTES fbers, the TGA curve shows a weight loss at 284.1 °C, mainly attributed to the thermal decomposition of POSS on the surface (Fig. S1). Difraction peaks with 2θ degrees of 16.22° (200), 25.76° (010), 27.62° (210), and 32.70° (400) in the XRD spectra of Fig. [2](#page-3-0)c are corresponded to the main crystal planes of PBO fbers, indicating that the crystal structures of PBO fbers are not damaged after synergistic functionalization of TA-APTES membrane and POSS.

Figure [2](#page-3-0)d demonstrates the XPS spectra of PBO fibers before and after surface functionalization, and the concentration of corresponding elements can be seen in Fig. [2](#page-3-0)e. PBO@TA-APTES fbers show the peaks of Si 2 s and Si 2p and the content of O element signifcantly increases compared to pristine PBO fbers, which can be attributed to the large number of the phenolic hydroxyl groups in TA-APTES membrane. After grafting POSS, the Si and O element contents on the surface of PBO@TA-APTES fbers increase. Besides, PBO@TA-APTES fbers (Fig. [2d](#page-3-0)″) show peaks of  $-NH<sub>2</sub>$  and  $-NH<sub>-</sub>$  at 401.8 and 400.7 eV, respectively, indicating TA-APTES membrane is successfully deposited on PBO fibers. Moreover, the peak intensity of -NH<sub>2</sub> on the surface of POSS-*g*-PBO@TA-APTES fbers (Fig. [2](#page-3-0)d‴) is signifcantly reduced, which is due to the surface grafting reaction between -NH<sub>2</sub> and the epoxy group of POSS under acidic conditions Fig. [2f](#page-3-0).



<span id="page-3-0"></span>**Fig. 2** FTIR (**a**), TGA (**b**), XRD (**c**), and XPS (**d**) curves of pristine PBO, PBO@TA-APTES, and POSS-*g*-PBO@TA-APTES fbers; Corresponding concentration of various elements (**e**); Schematic diagram of POSS grafting mechanism (**f**)

Figure [3](#page-4-0) demonstrates the SEM  $(a-c)$  and AFM  $(d-f)$ morphologies of PBO fbers before and after surface functionalization. A uniform TA-APTES layer is observed on the PBO@TA-APTES fbers surface. The corresponding surface roughness increases from 15 nm of pristine PBO fbers (Fig. [3d](#page-4-0)) to 47 nm (Fig. [3](#page-4-0)e). This can be attributed to the hydrophilic nanospheres formed through TA oxidation and APTES hydrolysis products. Additionally, the surface of POSS-*g*-PBO@TA-APTES fibers displays increased amount of coating. The corresponding surface roughness is further increased to 52 nm (Fig. [3f](#page-4-0)). Besides, EDS spectra demonstrate that C, N, and Si elements are evenly distributed on the POSS-*g*-PBO@TA-APTES fbers (Fig. [3c](#page-4-0)′–c‴), suggesting the even distribution of TA-APTES and POSS hybrid membrane.

Figure [4a](#page-5-0), b show the single fber tensile strength and retention of pristine PBO, PBO@TA-APTES, and POSS*g*-PBO@TA-APTES fbers under diferent UV aging time, respectively. PBO@TA-APTES (5.2 GPa) and POSS*g*-PBO@TA-APTES (5.1 GPa) fibers display slightly

decreased single fiber tensile strength in compare with pristine PBO fibers (5.4 Ga). Besides, the single fiber tensile strength and retention of pristine PBO, PBO@TA-APTES, and POSS-*g*-PBO@TA-APTES fbers decrease gradually with the increase of UV aging time due to the gradual destruction of oxazole rings of PBO fbers under UV irradiation [[38](#page-10-12)]. After 288 h irradiation by UV lights, the absorption peaks of  $-OH$ ,  $-NH_2$ , and  $-C=O$ – appear in the FTIR spectrum of pristine PBO (Fig. [4c](#page-5-0)). As shown by the SEM images of the surface for pristine PBO fber in Fig. [4e](#page-5-0)1–3, the degradation products gradually increase with the increase of UV aging time (96–192 h). After 288 h irradiation by UV lights, there are a lot of obvious defects on the surface of pristine PBO fibers, which significantly reduces the single fber tensile strength. Compared with the pristine PBO fbers (2.7 GPa and 50.0%), the single fber tensile strength and retention rate of the PBO@TA-APTES fbers are 3.0 GPa and 57.7%, respectively, under the same UV aging time (288 h). This is because a large number of benzene rings existing in the uniform TA-APTES layer on the



<span id="page-4-0"></span>**Fig. 3** SEM and AFM morphologies of the pristine PBO (**a**, **d**), PBO@TA-APTES (**b**, **e**), and POSS-*g*-PBO@TA-APTES fbers (**c**, **f**); EDS images of POSS-*g*-PBO@TA-APTES fbers (**c**′–**c**‴)

surface of PBO@TA-APTES fbers can absorb the energy of the ultraviolet lights, thus reducing the damage of PBO fbers. This can be illustrated by the gradually decomposed TA-APTES layer and nearly undamaged PBO fbers surface as shown in Fig. [4](#page-5-0)e4–6. Compared with PBO@TA-APTES, the single fber tensile strength and retention rate of the POSS-*g*-PBO@TA-APTES fbers increase to 3.1 GPa and 60.8%, respectively. This can be attributed to the high bond energy and excellent irradiation resistance of Si–O bonds in POSS [\[39](#page-10-13)]. Compared with PBO@TA-APTES, UV–vis absorption peak intensity of the POSS-*g*-PBO@TA-APTES fbers decreases signifcantly (Fig. [4d](#page-5-0)). Meanwhile, the introduction of POSS increases the surface roughness of PBO fbers, thus increasing the scattering of the ultraviolet lights on the surface of POSS-*g*-PBO@TA-APTES fbers and further improving its UV resistance (Fig. [4](#page-5-0)e7–9).

fbers before and after surface functionalization. The single fber pull-out strength of POSS-*g*-PBO@TA-APTES fbers/ BADCy micro-composites is increased by 31.0% to 3.8 MPa in compared with pristine PBO fbers (2.9 MPa), also higher than PBO@TA-APTES fbers/BADCy (3.6 MPa). This is because the large number of reactive groups in TA-APTES layer signifcantly improves the interfacial compatibility between PBO fbers and BADCy resin. Meanwhile, the introduction of TA-APTES membrane and grafting of POSS improves the surface roughness of PBO fbers, resulting in the increased mechanical engagement between PBO fbers and BADCy matrix, which is benefcial to increasing the single fber pull-out strength of PBO fbers.

Figure [5a](#page-6-0) shows the single fber pull-out strength of PBO

**PBO fbers/BADCy micro‑composites**



<span id="page-5-0"></span>**Fig. 4** Tensile strength (**a**), tensile strength retention (**b**), and FTIR spectra (**c**) of diferent PBO fbers after UV aging; UV–vis absorption spectra of diferent PBO fbers (**d**); SEM morphologies of PBO

(**e1**–**e3**), PBO@TA-APTES (**e4**–**e6**), and POSS-*g*-PBO@TA-APTES (**e7–e9**) fbers surface after diferent UV aging time

Compared with the smooth surface of pristine PBO fbers (Fig. [5](#page-6-0)c1), obvious residual BADCy resins appear on the surface of PBO@TA-APTES fbers after single fber pull-out test (Fig. [5](#page-6-0)c2). In addition, POSS groups on the surface of POSS-*g*-PBO@TA-APTES fbers can form physical entanglement with molecular chains of BADCy cured network  $[40]$  $[40]$ , which further improves the single fiber pullout strength. In Fig. [5](#page-6-0)c3, the surface of POSS-*g*-PBO@ TA-APTES fbers is coarser than that of PBO@TA-APTES fbers after single fber pull-out test. Schematic diagram of interfacial strengthening mechanism for POSS-*g*-PBO@ TA-APTES fbers/BADCy micro-composites is shown in Fig. [5](#page-6-0)b.

## **PBO fbers/BADCy wave‑transparent laminated composites**

Figure [6a](#page-7-0)1–a2 show the dielectric properties of the diferent PBO fbers/BADCy wave-transparent laminated composites at 1 MHz and the corresponding theoretical wavetransparent performance (theoretical wave transmittance rate ( $|T|^2$ ), reflection coefficient ( $|T|^2$ ), and energy loss (*A*)). The detail formulas are shown in Supplementary Material. The POSS-*g*-PBO@TA-APTES fbers/BADCy composites display lower *ε* and tan*δ* values of 2.85 and 0.0047, respectively, than those of PBO fbers/BADCy (3.06 and 0.006) and PBO@TA-APTES fbers/BADCy (2.92 and 0.0054) at 1 MHz. In addition, it shows a higher  $|T|^2$  of 93.4% than that of PBO fbers/BADCy (92.6%) and PBO@TA-APTES

fbers/BADCy (93.1%). Larger interfacial polarization due to poor interfacial compatibility in the external electric feld results in higher *ε* and tan*δ* values, which increases the interfacial refection and the internal energy losses of electromagnetic wave and decreases the  $|T|^2$  values. The interfacial compatibility improves as the surface activity of PBO@TA-APTES fbers is increased, thus causing the weakened charge accumulation at the interface of PBO fbers and BADCy matrix, and decreasing the *ε* and tan*δ* values. In addition, the low polar Si–O bonds and unique nanocavity of POSS further reduce the molecular polarizability and the number of polarized molecules, which further decreases the *ε* and tan*δ* of POSS-*g*-PBO@TA-APTES fbers/BADCy composites, thus increasing the  $|T|^2$  values. The corresponding mechanism of improving dielectric properties for POSS*g*-PBO@TA-APTES fbers/BADCy composites is shown in Fig. [6a](#page-7-0)3.

Based on the principle of transmission/refection method, the electromagnetic wave transmission models of PBO fbers/BADCy composites with the diferent thicknesses (*d*, 1.5–3.5 mm) were established by the fnite element analysis [[41,](#page-10-15) [42\]](#page-10-16). Figure [6](#page-7-0)b–d shows the simulation results (simulated wave transmittance rate, E*T(simulation)*) of wave-transparent performance at broadband (0.3–40 GHz). The detail building process of electromagnetic wave transmission models is shown in Supplementary Material. Figure [6](#page-7-0)b3–d3 are projections of the three-dimensional diagrams (Fig. [6](#page-7-0)b2–d2) of the relationship between  $E_{T(\text{simulation})}$ , *d*, and electromagnetic wave frequency of the composites. The E*T(simulation)*



<span id="page-6-0"></span>**Fig. 5** Single fber pull-out strength of PBO fbers before and after surface functionalization (**a**); Schematic diagram of interfacial enhancement mechanism of PBO fbers before and after surface func-

tionalization (**b**); SEM images of diferent PBO fbers surface after single fber pull-out test (**c1**–**c3**)

values of PBO@TA-APTES fbers/BADCy and POSS-*g*-PBO@TA-APTES fibers/BADCy composites are obviously improved in compared with PBO fibers/BADCy. The black area  $(E_{T(\text{simulation})} < 86.2\%)$  gradually disappears. This is because the *ε* and tan*δ* of PBO@TA-APTES fbers/ BADCy composites decrease, which weakens the interfacial refection and the internal energy loss of the electromagnetic wave, resulting in improved  $E_{T(\text{simulation})}$  values [[44](#page-10-17)]. Moreover, the low polar Si–O bonds and unique nanocavity of POSS can further decrease the *ε* and tan *δ* of POSS-*g*-PBO@TA-APTES fbers/BADCy composites, resulting in further increase of the  $E_{T(\text{simulation})}$  values.

Figure [7a](#page-8-0) demonstrates the gel contents and saturated water absorption of diferent PBO fbers/BADCy composites. The gel contents of PBO fbers/BADCy, PBO@TA-APTES fbers/BADCy, and POSS-*g*-PBO@TA-APTES fbers/BADCy composites are 34.1%, 35.0%, and 35.6%, respectively. The introduction of TA-APTES membrane and POSS improves the chemical inertia of PBO fbers surface, enabling PBO@TA-APTES and POSS-*g*-PBO@ TA-APTES fbers to adsorb more BADCy resins [[45\]](#page-10-18). The saturated water absorption of PBO fbers/BADCy,

PBO@TA-APTES fbers/BADCy, and POSS-*g*-PBO@TA-APTES fbers/BADCy composites are respectively 2.5%, 2.1%, and 1.8%. This is also attributed to the signifcant improvement of interfacial compatibility between PBO fbers and BADCy matrix after the synergistic functionalization with TA-APTES membrane and POSS, which reduces difusion of water, resulting the reduced fnal saturated water absorption. Besides, better interfacial compatibility between POSS-*g*-PBO@TA-APTES fbers and BADCy matrix leads to the higher gel contents and lower water absorption.

Figure [7](#page-8-0)b shows ILSS and flexural strength of different composites. PBO@TA-APTES fibers/BADCy composites shows improved ILSS (40.3 MPa) and flexural strength (638.6 MPa) compared to those of pristine PBO fibers/BADCy (36.7 and 587.4 MPa) while POSS-*g*-PBO@TA-APTES fibers/BADCy shows the highest ILSS and flexural strength of 42.8 and 645.8 MPa, increased by 16.6% and 9.9%, respectively. The interfacial bonding strength of PBO fibers/BADCy is highly weak, resulting the lowest ILSS (there is tiny amount of BADCy resins on the surface of PBO fibers after ILSS tests as shown



<span id="page-7-0"></span>**Fig. 6** Dielectric properties (**a1**–**a2**) of the PBO fbers/BADCy (Sample 1), PBO@TA-APTES fbers/BADCy (Sample 2), and POSS*g*-PBO@TA-APTES fbers/BADCy (Sample 3) wave-transparent laminated composites at 1 MHz; Mechanism of improvement of the

dielectric properties for Sample 3 (**a3**); Simulated wave-transparent performances of Sample 1 (**b1**–**b3**), Sample 2 (**c1**–**c3**), and Sample 3 (**d1–d3**) at 0.3~40 GHz

in Fig. S2a). The introduction of TA-APTES active layer significantly increases the surface roughness and chemical activity of PBO fibers, which effectively enhances the mechanical engagement and chemical adhesion between PBO@TA-APTES fibers and BADCy matrix (lots of BADCy resins adhere to the surface of PBO fibers and less PBO fibers detach from the BADCy matrix as shown in Fig. S2b). Furthermore, introducing POSS on the surface of POSS-*g*-PBO@TA-APTES fibers increases the surface roughness, resulting further improved mechanical properties (large number of BADCy resins adhere on the

surface of POSS-*g*-PBO@TA-APTES fibers after ILSS test as shown in Fig. S2c).

Figure [7](#page-8-0)c shows the electrical insulation properties (volume resistivity  $(\rho_0)$  and breakdown strength  $(E_0)$  of different composites. The  $\rho_0$  and  $E_0$  values of POSS-*g*-PBO@TA-APTES fibers/BADCy composites are respectively  $2.8 \times 10^{15} \Omega$ ·cm and 19.80 kV/mm, higher than those of PBO fbers/BADCy  $(2.2 \times 10^{15} \Omega \cdot cm$  and 17.69 kV/mm) and PBO@TA-APTES fibers/BADCy  $(2.5 \times 10^{15} \Omega \cdot cm$  and 18.54 kV/mm). This is due to the signifcantly improved interfacial compatibility



<span id="page-8-0"></span>**Fig. 7** Properties comparison of PBO fbers/BADCy (Sample 1), PBO@TA-APTES fbers/BADCy (Sample 2), and POSS-*g*-PBO@TA-APTES fbers/BADCy (Sample 3) wave-transparent laminated composites

between PBO@TA-APTES fbers and BADCy matrix, which reduces the defects at the interface, resulting in increased  $\rho_0$ and  $E_0$  values. In addition, the unique hollow structure of POSS can decrease the number of carriers and inhibit the migration of carriers, thus further increasing the  $\rho_0$  and  $E_0$  values of POSS-*g*-PBO@TA-APTES fbers/BADCy composites.

Figure [7](#page-8-0)d and e demonstrate the TGA and DMA curves of different composites. The corresponding  $T_{Heat\text{-}resistance\text{ index}}$  $(T_{HRI}$ , the calculation process of  $T_{HRI}$  is shown in Table S2) and glass transition temperature  $(T_g)$  values are shown in Fig. [7](#page-8-0)f. Each of the TGA curves for three diferent wave-transparent laminated composites shows three weight loss stages: the volatilization of small molecules (50–300 °C), the breakage of BADCy molecular chains and carbonization (300–600 °C), and the pyrolysis of PBO fibers at higher temperature (600–900 °C). PBO@TA-APTES fbers/BADCy and POSS*g*-PBO@TA-APTES fbers/BADCy composites show lower  $T_{HRI}$  values of 226.3 °C and 221.5 °C, respectively, than that of PBO fbers/BADCy (229.6 °C), indicating a slightly decreased thermal stability. It can be mainly ascribed to the lower thermal stability of TA-APTES and POSS hybrid membrane.

The corresponding  $T<sub>g</sub>$  value of PBO@TA-APTES fibers/ BADCy composites increases from 247.1 °C of PBO fbers/BADCy to 249.9 °C, and further increases to 251.2 °C for POSS-*g*-PBO@TA-APTES fbers/BADCy composites. This can be ascribed to the signifcantly promoted interfacial binding forces between PBO@TA-APTES fbers and BADCy matrix, resulting restricted rotation of molecular chains of the BADCy resins and causing an increased  $T_{\rm g}$ 

value. Furthermore, POSS molecules can form physical entanglement points with the molecular chains of BADCy resins, thus increasing further the  $T_g$  value of POSS-g-PBO@TA-APTES fbers/BADCy composites. For the comparison of properties of the composites investigated in this work with those of some recent similar works, see Table S3.

# **Conclusions**

Surface of PBO fbers is successfully functionalized by depositing the TA-APTES polymer membrane followed by the synergistic grafting of POSS (POSS-*g*-PBO@TA-APTES fbers). The interfacial interaction between PBO fbers and BADCy matrix is signifcantly improved by the abundant reactive groups in TA-APTES membrane. The low polar Si–O bonds and hollow structures of POSS further reduce the interfacial polarization between PBO fbers and BADCy matrix. POSS*g*-PBO@TA-APTES fbers/BADCy composites display excellent mechanical properties, outstanding wave-transparent performance & electrical insulation properties, and excellent thermal stability. The ILSS and fexural strength of POSS-*g*-PBO@TA-APTES fibers/BADCy composites are 42.8 and 645.8 MPa, respectively, increased by 16.6% and 9.9% compared to those of PBO fbers/BADCy (36.7 and 587.4 MPa). At 1 MHz, the corresponding *ε* and tan*δ* values are reduced to 2.85 and 0.0047, respectively, lower than those of PBO fbers/BADCy (3.06 and 0.006). Meanwhile, the corresponding E*T(simulation)* of POSS-*g*-PBO@TA-APTES fbers/BADCy

composites with diferent thicknesses (1.5–3.5 mm) are higher than 86.2% at 0.3–40 GHz. The corresponding volume resistivity, breakdown strength, and  $T_{HRI}$  are  $2.8 \times 10^{15}$   $\Omega$ ·cm, 19.80 kV/mm, and 221.5 °C, respectively.

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### **Declarations**

**Conflict of interest** There are no conficts to declare.

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