



Description and effective parameters determination of the production process of fine-grained artificial stone from waste silica

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Abstract

In this study, waste silica from Alborz silica mineral processing factory was recycled as raw material for the production of a novel artificial stone to be used in civil construction. The size of the waste materials of this plant is less than 100 microns. Waste silica powder was mixed with unsaturated polymer resins as a binder. Under pressure, vibration and vacuum conditions, artificial stone with high compressive strength of 100 MPa, the tensile strength of 37 MPa and flexural strength of 98 MPa was produced within 15 min. Furthermore, in all of the produced artificial stones, due to the usage of resin, the flexural strength is higher than the tensile strength whereas, in natural stones, tensile strength is more than flexural strength. Moreover, using bentonite made a positive effect on the strength and quality of the stone, whereas kaolin declined the quality and the resistance of the artificial stone. Besides, the produced artificial stone has a lower specific gravity (2.14 g/cm^3) and water absorption (0.06 g) than natural stone, which is one of the most prominent advantages of artificial stone. What's more, low corrosion and were obtained against diluted sulfuric acid (0.0097 g) and hydrochloric acid (0.0313 g). Besides, due to the presence of impurities in the waste materials of Alborz silica factory, the produced artificial stones are brown. To reach the desired color, there are several metal oxides which could be added to the combination.

Keywords Waste silica · Artificial stone · Resin · Effective parameters

1 Introduction

Residues generated from all industrial sectors such as industrial ashes and plastic wastes as well as particle residues are currently considered as an environmental problem. Mining and mineral processing operations provide raw materials needed for life. It is inevitable to produce environmental pollutions during such operations, since a great amount of material are left useless as waste. Nowadays, inappropriate disposal of mentioned residues is a worldwide problem. Therefore, finding a way to use such materials to produce useful supplies has great effect in environment protection [1–8].

Silica particles are generated in glass production process, such as grinding, cutting, crushing and sieving operations. Thousands of tons waste silica are produced in mineral processing plants annually, which is a considerable amount. Such impurities are usually discarded in the nature and lead to several environmental hazards, due to the fact that the mentioned residual particles cannot return to the cycle of the nature even in long-term [9–13]. The effects of fine residual particles of silica factories on air quality were briefly addressed in environmental impacts. Also, these particles scratch delicate tissues in respiratory system, causing damage that impairs breathe ability and oxygen delivery to blood stream [14].

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In Iran, fine and coarse silica particles are generated in huge amounts through the country. Glass industry generates thousands of tons residues per year which are disposed in huge landfills. Moreover, Qazvin which has numerous quarries made considerable amount of residues, about of 50,000 tons a year.

Indeed, numerous research works have been allocated to find scientific solutions for declining the environmental troubles of residues. For example, waste materials which have been applied for asphalt concrete pavement fabrication were mixed with cement concrete. Also these waste materials were used in production process of low strength materials, lightweight aggregates and construction materials such as red bricks [2, 15–20].

One of the useful solutions for reducing waste mining material hazards is artificial stones production. Artificial stones are compounds made up of crushed pieces of natural stones and resins [21–25]. Several researches have studied the process of artificial stone production. In Lee and Ko [23] studies, waste glass and stone fragments from stone slab processing were recycled as raw materials to make artificial stone slabs using vibratory compaction in a vacuum environment. The study was based on compaction pressure, vacuum condition, and vibration frequency. The results indicate that artificial stone slabs were made with high compressive strength of 148.8 MPa and flexural strength of 51.1 MPa. In a study conducted by Cruz [22], the process was provided for manufacturing outdoor artificial stone boards by methacrylate resin using vibro-compression under vacuum system. In this research, liquid methacrylate resin with 200–2000 centipoises viscosity and 90–99% content has mixed with methacrylate resin in 1–10% content and lower than 200 centipoises viscosities which result in high quality artificial stone. In the study of Chang et al. [21], waste stone sludge obtained from slab stone processing and waste silt from aggregate washing plants were recycled to manufacture artificial aggregate. The result showed that by mixing fine-powdered stone sludge with waste silt of larger particle size and applying vibratory compaction, the compressive strength was obtained to above 29.4 MPa. A new technique on mechanical behavior of artificial and natural stones has developed by Dos Santos et al. [26] based on young's modulus (E) and temperature from 20 to 200 °C. The results indicate that young's modulus (E) of each materials determined at ambient temperature, and the engineered stones keep almost the same value of E after thermal ageing or thermal shock up to 160 °C. An investigation was carried out by Souza Silva et al. [27] for evaluating the mechanical and physical properties of produced artificial marble based on calcite marble waste and epoxy resin. The results indicated that the artificial stones exhibit a maximum flexural strength of 31.8 MPa, maximum compressive strength of 85.2 MPa and

water absorption below 0.05%. The effects of alkali dosage, slag content and curing age on compressive strength of artificial flood-prevention stone have been evaluated by Wang et al. [28]. The results showed that the specimen made from optimal mix proportion can meet the requirement of flood-prevention stone and the main product in alkali-activated process is C–S–H gel. In a research conducted by Peng and Qin [29], the mechanical behavior and microstructure of artificial stone was studied. Based on their results, artificial stone slabs obtained in this work has high compressive and flexural strengths of 170.9 and 73.5 MPa under a compaction time of 3 min and a curing time of 60 min.

As a matter of fact, the practical possibility of using artificial stone instead of natural one is based on the technical advantages, such as the lower density of the polymeric resin ($\sim 1 \text{ g/cm}^3$) in comparison with the natural stone ($\sim 2 \text{ g/cm}^3$), which makes the artificial stone significantly lighter. Another advantage of artificial stones is lower amount of pores and flaws. Whereas, high porosity and microstructural defects in natural ornamental stones lead to contamination and brittleness, since outside fluids can penetrate to natural stone through pores and propagate cracks. Despite abovementioned positive points of artificial stones, it should be noted that some of them are not resistant enough in high traffic areas, as the materials are vulnerable to abrasion [11, 30, 31].

This work is an investigation on the production of artificial stone by waste silica from residue industrial materials. As a novelty, it is the first time that the size of the residues is less than 100 microns and silica has got impurities. These impurities are difficult to separate from waste materials whereas they are fruitful to increase artificial stone strength. As these impurities cause several environmental problems in the region, this is an appropriate way to abolish them. The main objective of this work is to produce a novel product using process techniques of vibration, vacuum and pressing, which has superior mechanical and physical properties as well as resistance to chemical reactions. Therefore, the production of artificial stone using impure silica declines environmental pollution and also economizes the production process in civil construction applications.

2 Methodology

2.1 Materials

A representative sample of waste silica from Alborz silica factory (Qazvin, Iran) with the size of $\sim 100 \mu\text{m}$ was used for experiments. Table 1 shows the XRF analysis of the sample.

Table 1 XRF analysis of the waste materials of Alborz silica factory

Type of elements (%)	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	K ₂ O	Na ₂ O	LOI
	96.31	1.6	0.185	0.3	0.2	0.65	0.1	0.65

Notably, waste materials of the factory contain large amount of silica (96%). Other impurities such as Al₂O₃, Fe₂O₃ and etc. have positive effect on artificial stone strength and quality.

Also, a high purity silica sample (purity over 99.9%) with size of – 100 micron were used to consider the effect of super pure silica on produced artificial stone. Moreover, orthophthalic unsaturated polymer resins were used as a binder. Figure 1 show the structure of orthophthalic unsaturated resin. Sulfuric acid and hydrochloric acid with 10% concentration were used in this experiment. Cobalt (1–2%) and Methyl Ethyl Ketone Peroxide (2%) were also added to the resin as resin hardeners. Bentonite and kaolinite (Lushan mine in Iran) were used to evaluate the quality of artificial stone. After finding best powder-resin ratio, bentonite and kaolin were used to consider which better filler is.

2.2 Method

First, waste materials were sieved and fine particles smaller than 100 microns used for experiments. Then, orthophthalic unsaturated polymer resins added as a binder. For primary tests, 3 distinct mixtures with different powder-resin ratio have tested.

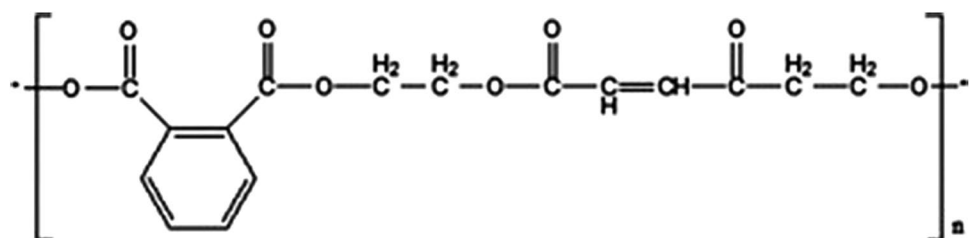
1. The content ratio of 70% powder to 30% resin.
2. The content ratio of 80% powder to 20% resin.
3. The content ratio of 85% powder to 15% resin.

The mixture is mixed to obtain homogeneous material. Incomplete mixing of materials and resins makes inhomogeneous mixture. Moreover, a complete mixing accelerates polymerization reaction and accordingly increases the strength of artificial stone. It should be noted that, mixing

time is extremely crucial since resin is hardened in short period of time. Therefore, production process should be done very quickly. After finding best powder to resin ratio, bentonite and kaolin (3%–3 min) were used to investigate which filler is better. Then, vibration press machine used in vacuum condition. The mixture is placed in a steel vessel and allowed to vibrate in 50 Hz for 3 min. In this machine, obtained paste became completely homogeneous, and air inside particles has released. After vibration stage, material has immediately pressed by 3 tons in 4 min until the block of artificial stone got the mold shape. In fact, Operation time for mixing, vibration and pressure should be less than 15 min, since resin is hardened within 15 min. In next stage, the block is heated at temperature of 90 °C for 55 min to complete polymerization process of resin to reach final strength of the artificial stone as well as releasing moisture. Then, blocks has kept in a desiccator jar to return room temperature, around 22 °C.

Criterion of determining best composition is maximum compressive and flexural strength. In this regard, compressive, tensile and flexural strength experiments have been done based on ASTM C39, ASTM C496 and ASTM C78 standards, respectively. Specific gravity is the ratio of the weight of a given volume of materials, including permeable and impermeable voids in the particles, to the weight of an equal volume of water. The specific gravity and water absorption of the novel artificial stone were measured according to ASTM C642 standard. The resistance to chemical attack has conducted according to the Brazilian NBR 15845 standard. After being subjected to the chemical attack for 24 h of specific reagents, the specimens had corresponding weight loss determined. Moreover, the pore size has studied from the desorption branch of the isotherm using DFT method (Quanta chrome Instruments, 1994–2006).

Fig. 1 Molecular structure of orthophthalic unsaturated resin



3 Results and discussion

3.1 Effective factors in artificial stone production

3.1.1 Effect of powder to resin ratio

One of the most important factors in production process of artificial stone is powder-resin ratio. For testing different compositions, the content ratio of powder was increased from 70 to 85%. Table 2 and Fig. 2 show the average compressive, tensile and flexural strength of artificial stone in 10 samples with powder/resin ratios of 70/30, 80/20 and 85/15 in same experimental condition.

The results show that maximum compressive, tensile and flexural strength were obtained in 80/20 powder/resin ratio. Figure 3 shows manufactured artificial stone with a powder/resin ratio of 80/20 and 85/15. According to Figs. 2 and 3, artificial stone with powder/resin ratio of 80/20 has maximum strength, because of lower porosity in this ratio, also increasing powder amount (over 80%) makes brittle compound which may burst in loading operation. Pore size distributions in different powder/resin ratio (70/30, 80/20 and 85/15) are shown in Fig. 4. Pores diameter is between 3–15 and 3–10 microns in 70/30 and 85/15 powder/cement ratio respectively. Pore size has decreased to 3–8 microns in 80/20 ratio. So pore

Table 2 Compressive, tensile and flexural strength for 10 sample

Powder/resin ratio	Compressive strength (MPa)	Tensile strength (MPa)	Flexural strength (MPa)
70/30	24.51 ± 0.01	15.14 ± 0.01	35.11 ± 0.01
80/20	100.15 ± 0.01	37.33 ± 0.01	98.33 ± 0.01
85/15	40.45 ± 0.01	24.42 ± 0.01	55.54 ± 0.01

Fig. 2 Effect of powder/resin ratio on artificial stone strength

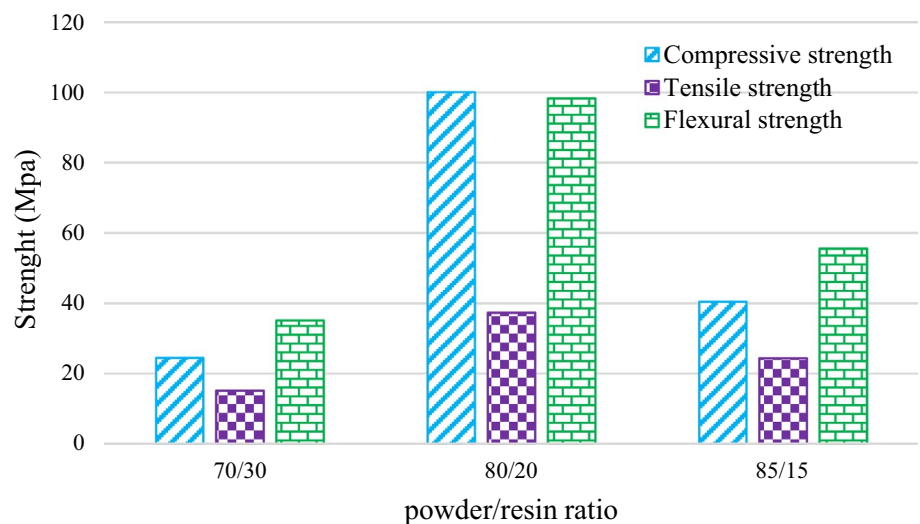


Fig. 3 Artificial stone produced with powder/resin ratio: **a** 80/20, **b** 85/15

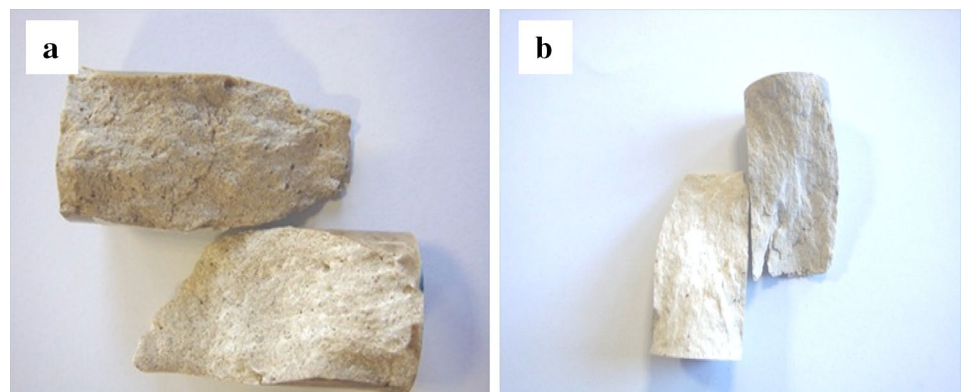
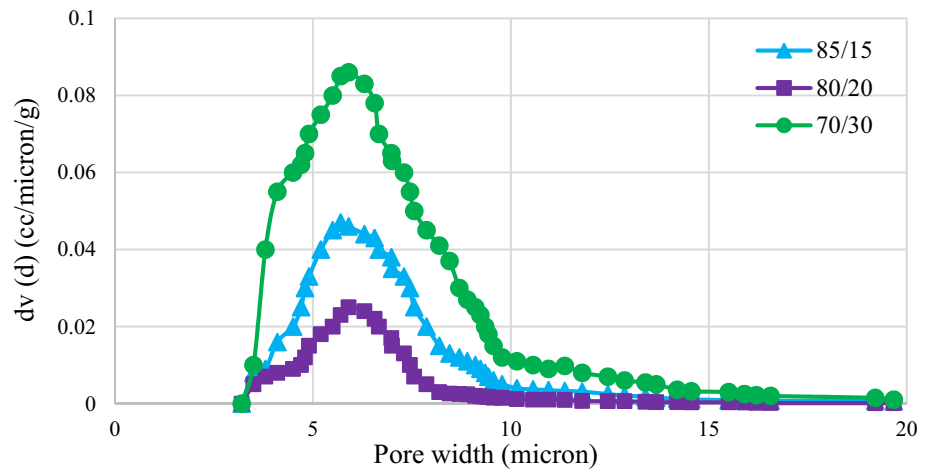


Fig. 4 DFT pore-size distributions of samples with ratio of 70/30, 80/20 and 85/15



size distribution has got broader in more and less ratio of 80/20.

3.1.2 Amount and type of additives

3.1.2.1 Resin additives Resin additives or resin hardeners include cobalt and methyl ethyl ketone peroxide. The process of hardening and polymerization cannot be done without these materials. These additives and resin are complementary and they are not added to the resin before its consumption to prevent early hardening. The process of mixing resins and hardeners should be done very well to reach a homogenous mixture because it spreads hardener particles throughout the mixture and consequently, polymerization would accelerate. In above mentioned conditions artificial stone would reach higher resistance. If resin does not mix well with hardeners, the mixture will not be homogeneous, the reaction between resin and hardener will not be done well and the hardening procedure will perform very slowly or not at all.

3.1.2.2 Mineral additive to waste materials Some minerals such as kaolin and bentonite were used to increase artificial stone quality. Table 3 indicates the average resistances of artificial stones with different compositions in 10 samples.

Figure 5 shows the difference between compressive strength, flexural strength and tensile strength of artificial

stones with different compounds. As is seen, higher compressive strength is obtained in 80/20 powder/resin ratios, using 3% bentonite and 50 Hz vibration. After vibratory compaction, artificial aggregate packing improved and reached a more compacted structure with higher compressive strength. It seems that compressive strengths, regardless of groups, tended to increase with 3% bentonite; while it descended by pure silica. Pure silica does not have positive effect and decrease artificial stone strength. Figure 6 shows artificial stones containing kaolin and bentonite. Applying bentonite makes positive effect on stone quality, while kaolin has opposite result. Bentonite component significantly affects properties of artificial stone, and hence is of importance in construction engineering. Important properties of bentonite include water absorption and swelling, viscosity and thixotropy of aqueous suspensions, colloidal and waterproofing properties, binding and surface properties (properties and uses of Bentonite, [32]). Thus, bentonite increases compressive, tensile and flexural strength of stone without affecting the color and other characteristics of artificial stone. On the other hand, kaolin does not have positive effect on artificial stone's properties. The reason is kaolin's properties such as soft consistency and earthy texture. Also, it is easily broken and can be molded or shaped, especially when wet [33].

In whole produced artificial stones, because of resin and plastic properties, flexural strength is higher than tensile strength whilst natural stones do not resistant

Table 3 The average resistance of artificial stone with different compounds under vibration of 50 Hz for 10 samples

Type of stone	Compressive strength (MPa)	Tensile strength (MPa)	Flexural strength (MPa)
Artificial stone with pure silica	40.15 ± 0.01	15.19 ± 0.01	20.94 ± 0.01
Artificial stone without purification	100.52 ± 0.01	34.33 ± 0.01	95.37 ± 0.01
Artificial stone with 3% kaolin	32.52 ± 0.01	22.13 ± 0.01	85.42 ± 0.01
Artificial stone with 3% bentonite	110.12 ± 0.01	41.35 ± 0.01	105.72 ± 0.01

Fig. 5 Difference between compressive, flexural and tensile strength of artificial stones

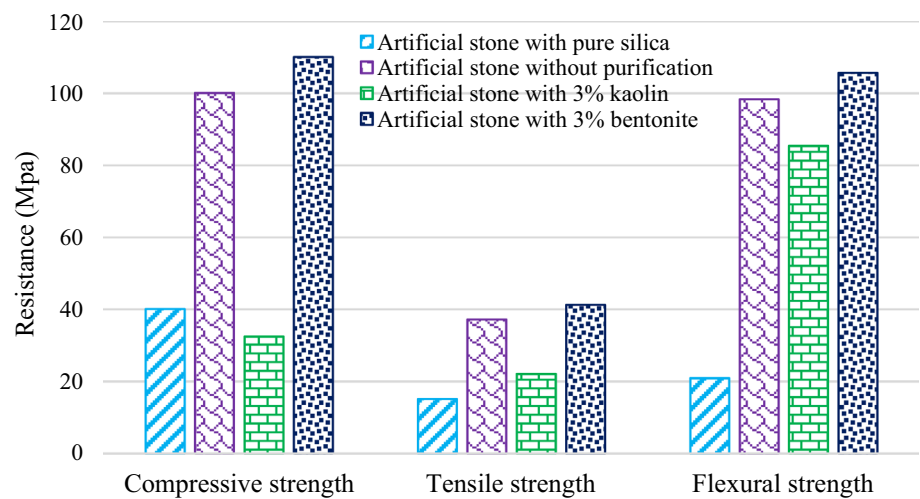
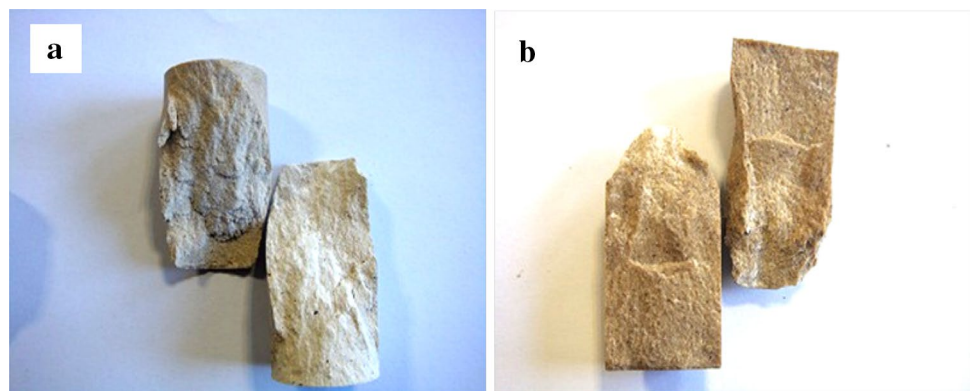


Fig. 6 Artificial stones produced with: **a** kaolin, **b** bentonite



against bending and tensile strength is more than flexural strength. The values of the compressive, tensile and flexural strength of quartz natural stone are obtained 25, 19 and 16 MPa, respectively which is lower than the values in the artificial stone.

According to Fig. 5, impurities in primary waste materials which contain 96% silica and various impurities are desirable and increase the quality and strength of artificial stone. After vibratory compaction, the artificial aggregate packing at each ratio distinctly improved and reached a more compacted structure with higher compressive strength.

Experiments showed that the issue of using impurities could impact on artificial stones production in two ways:

1. Abolishing all impurities is difficult and quite impossible. Moreover, the process of removing these impurities is too much which make the project unreasonable in cost and benefit.
2. Prevent tailing production in purification process. Given that all raw materials are used without any purification, the process of producing artificial stones

produces low amount of tailings and this is one of the most important results achieved in this research.

3.1.3 Effect of temperature

It is generally agreed that temperature is crucial factor in mechanical properties of artificial stone. Figure 7 shows compressive, tensile and flexural strength of artificial stone with 3% bentonite at different temperatures. Maximum compressive strength (110 MPa) has obtained at 90 °C. This parameter has decreased slightly in more and less temperatures. At temperatures more than 90 °C, the stone is baked more that reduces compressive strength below 50 MPa. At temperatures lower than 90 °C, setting process would not be done well which decrease stone quality. Figure 8 shows produced artificial stones at 130 °C with compressive strength of 45 MPa. It is perceived that artificial stones behave more like an elastic–plastic material in comparison to more brittle/elastic behavior of natural stones. By increasing temperature, the polymer–resin matrix starts contributing with its rheological behavior to mechanical properties of composites.

Fig. 7 Effect of temperature on various artificial stone resistances

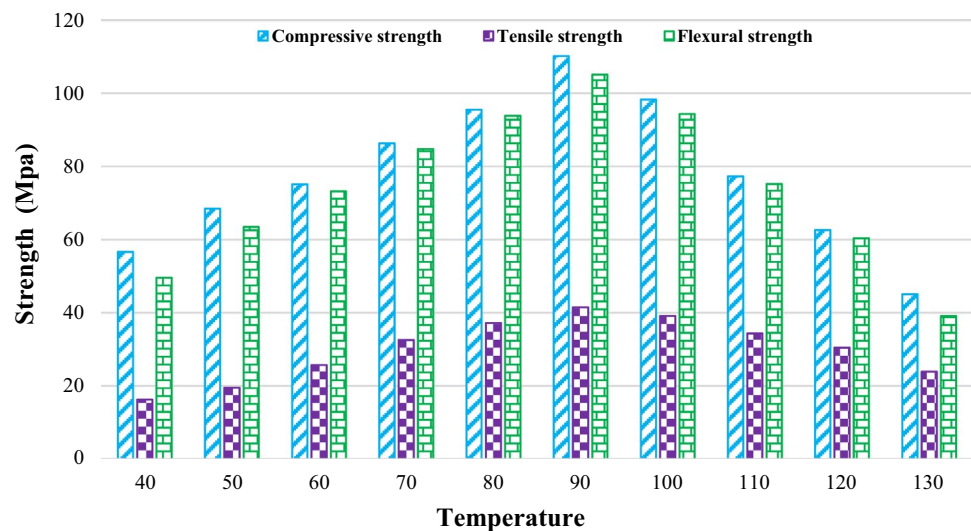


Fig. 8 Artificial stone produced at 130 °C

Table 4 Specific gravity, water absorption and porosity

Specific gravity (g/cm^3)	2.14 ± 0.02
Water absorption (%)	0.06 ± 0.03
Porosity (%)	0.12 ± 0.04

3.1.4 Effect of stone physical properties

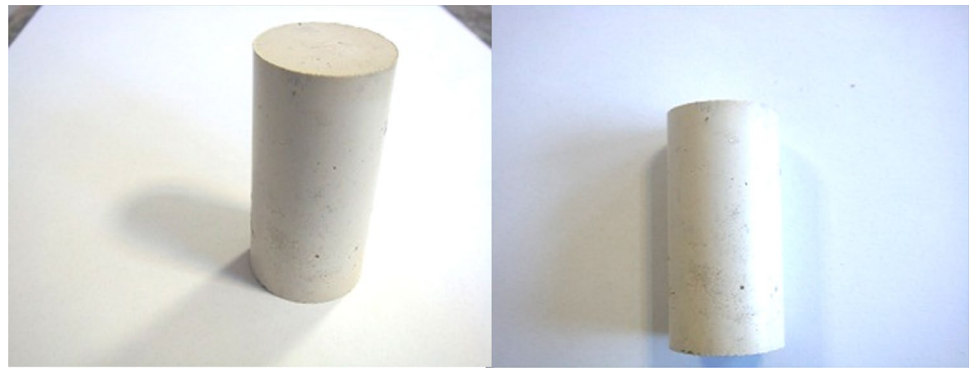
Table 4 shows specific gravity, porosity and water absorption values. It is observed that produced artificial stone has lower specific gravity, which is one of the most prominent advantages of artificial stones properties. Specific gravity of natural granite is $2.7 \text{ g}/\text{cm}^3$ that is almost 30% heavier than artificial stones, while specific gravity of artificial stone in present study is $2.14 \text{ g}/\text{cm}^3$. Binder used in this study is an unsaturated polymer resin which has viscous behavior. On the other hand, once the structure compacted, the air trapped between

aggregates during mixing cannot be easily removed. Air can only be eliminated when compaction is conducted in a vacuum condition. Removing air leads to a lower porosity in production process of artificial stone. So, there are fewer discernible pores in densified structure formed under the vibration of 50 Hz which has compressive strength of 110.12 MPa.

According to Table 4 water absorption of 0.06% gained by this method is significantly lower than other methods. High water absorption of 0.25% and 0.38% reported by Borselino et al. and Carvalho et al., respectively. One of the reason is that the porosity of this method is lower than other methods [34, 35]. A possible explanation is that this artificial stone can be sealed with low water absorption.

3.2 Artificial stone color

The produced artificial stone is brown due to the presence of impurities in waste powders of Alborz silica factory. For various colors, it is necessary to add various metal oxides such as titanium oxide, chromium oxide, copper oxide, zirconium oxide and so on. Figure 9 shows the artificial stones with 3% titanium oxide content with white color. Metal oxides are used up to 3 wt% depending on the quality of silica powder in mixture. Table 5 shows the effect of metal oxides on artificial stone strength. Based on conducted experiment, using metal oxides does not make a significant impact on strength of artificial stone. So, they can be used for dyeing the stone for specific usage. It is interesting that titanium oxide gives white color, combination of titanium oxide and copper oxide makes the artificial stone red and zirconium oxide is a great agent for giving cream color to artificial stone.

Fig. 9 Artificial stones with 3% titanium oxide**Table 5** Effect of metal oxides on artificial stone strength

Metal oxides	Color	Mineral additive (3%)	Compressive strength (Mpa)	Tensile strength (Mpa)	Flexural strength (Mpa)
–	Brown	Bentonite	110.12±0.01	41.35±0.01	105.72±0.01
Titanium oxide	white	Bentonite	108.23±0.01	39.5±0.01	103.42±0.01
Titanium oxide and copper oxide	Red	Bentonite	106.97±0.01	38.32±0.01	101.26±0.01

3.3 Acid resistance

3.3.1 Sulfuric acid test

The sample with powder/resin ratio of 80/20 along with bentonite additive has been used for acid test. First, artificial stone has weighted accurately, and then it is placed within a dilute acid (Sulfuric acid 10%) for 24 h. It makes an opportunity to investigate whether artificial stone is resistant enough against corrosion or not. Artificial stone has weighed after being dried. The difference between initial weight (before being placed in the dilute acid) and final weight (after being dried) indicates the degree of corrosion. The corrosion rate was $0.2\% \pm 0.03$. It is less than corrosion in natural stones (5%) in same condition. So, the results reveal that produced artificial stone is resistant enough against dilute acid. In other words, weight reduction is very low and the corrosion is ignorable.

3.3.2 Hydrochloric acid test

The same procedure has been done to assay the resistance of the produced artificial stone against another dilute acid (hydrochloric acid 10%). The average corrosion rate for 10 samples was $0.65\% \pm 0.03$. It is higher than the amount of corrosion in sulfuric acid test but lower than the corrosion in natural stones (7%) in same condition. Considering the results, Hydrochloric acid causes more corrosion in the artificial stone than Sulfuric

acid. So it is better to use this kind of artificial stones where it is less likely to contact with Hydrochloric acid.

4 Conclusions

In this research paper, artificial stone production using waste material from Alborz silica mineral processing factory has investigated to find the most optimum method of mass production. The maximum compressive strength of artificial stone (110 MPa) obtained in 80/20 powder/resin aggregate ratios, using 3% bentonite at 90 °C while the strength has decreased slightly in other combination. Thus, bentonite increases the strength of the artificial stone without affecting the color and other characteristics. Besides, produced artificial stone has lower specific gravity (2.14 g/cm^3) and water absorption (0.06 g), which are prominent advantages of artificial stone. To have desired color, there are several metal oxides which can be added to the combination. The results showed that using metal oxides does not make a significant effect on artificial stone strength. Also, the corrosion rate using Sulfuric acid and Hydrochloric acid (10%) is $0.2\% \pm 0.03$ and $0.65\% \pm 0.03$, respectively. It is less than corrosion amount in natural stones (5% and 7%) in same condition. Moreover, artificial stone production costs 30 \$ per square meter, while natural quartz is 50 \$ per square meter. So, this artificial stone has a good quality and can be used in civil construction.

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Compliance with ethical standards

Conflict of interest The authors declare that they have no conflict of interest.

References

1. Mannan UA, Islam MR, Tarefder RA (2015) Effects of recycled asphalt pavements on the fatigue life of asphalt under different strain levels and loading frequencies. *Int J Fatigue* 78:72–80. <https://doi.org/10.1016/j.ijfatigue.2015.04.004>
2. Norouzi S, Badii K, Ardejani FD (2010) Activated bauxite waste as an adsorbent for removal of acid blue 92 from aqueous solutions. *Water Sci Technol* 62:2491–2500. <https://doi.org/10.2166/wst.2010.514>
3. Pasandín AR, Pérez I (2017) Fatigue performance of bituminous mixtures made with recycled concrete aggregates and waste tire rubber. *Constr Build Mater* 157:26–33. <https://doi.org/10.1016/j.conbuildmat.2017.09.090>
4. Gomes MLP, Carvalho EA, Sobrinho LN, Monteiro SN, Rodriguez RJ, Vieira CMF (2018) Production and characterization of a novel artificial stone using brick residue and quarry dust in epoxy matrix. *J Mater Res Technol* 7(4):492–498. <https://doi.org/10.1016/j.jmrt.2018.08.012>
5. Raposeiras AC, Vargas-Cerón A, Movilla-Quesada D, Castro-Fresno D (2016) Effect of copper slag addition on mechanical behaviour of asphalt mixes containing reclaimed asphalt pavement. *Constr Build Mater* 119:268–276. <https://doi.org/10.1016/j.conbuildmat.2016.05.081>
6. Rubio M, Moreno F, Belmonte A, Menéndez A (2010) Reuse of waste material from decorative quartz solid surfacing in the manufacture of hot bituminous mixes. *Constr Build Mater*. <https://doi.org/10.1016/j.conbuildmat.2009.09.004>
7. Stefanidou M, Pacht V, Papayianni I (2017) Design and testing of artificial stone for the restoration of stone elements in monuments and historic buildings. *Constr Build Mater* 93:957–963. <https://doi.org/10.1016/j.conbuildmat.2015.05.063>
8. Uliana JG, Calmon JL, Vieira GL, Teixeira JESL, Nunes E (2015) Heat treatment of processing sludge of ornamental rocks: application as pozzolan in cement matrices. *Ibracon Struct Mater J* 8:100–123. <https://doi.org/10.1590/S1983-41952015000200004>
9. Carvalho EAS, Vilela NF, Monteiro SN, Vieira CMF, Silva LC (2018) Novel artificial ornamental stone developed with quarry waste in epoxy composite. *Mater Res* 21:1–6. <https://doi.org/10.1590/1980-5373-mr-2017-1104>
10. Piazzarollo CB, Xavier GC, Alexandre J, Azevedo ARG, Vieira CMF MS (2016) Factorial design for experimental planning of clay ceramic incorporated with ornamental stone waste. *Mater Sci Forum* 869:127–130. <https://doi.org/10.4028/www.scientific.net/MSF.869.127>
11. Ribeiro CEG, Rodriguez RJS (2015) Influence of compaction pressure and particle content on thermal and mechanical behavior of artificial marbles with marble waste and unsaturated polyester. *Mater Res* 18:283–290. <https://doi.org/10.1590/1516-1439.372314>
12. Vieira CMF, Motta TS, Candido VS, Monteiro SN (2015) Addition of ornamental stone waste to improve distinct formulations of clay ceramics. *Mater Sci Forum* 820:419–424. <https://doi.org/10.4028/www.scientific.net/MSF.820.419>
13. Ribeiro CEG, Rodriguez RJS, Vieira CMF, Carvalho EAS, Candido VS, Monteiro SN (2014) Production of synthetic ornamental marble as a marble waste added polyester composite. *Mater Sci Forum* 445–776:341–345. <https://doi.org/10.4028/www.scientific.net/MSF.775-776.341>
14. Minnesota Pollution Control Agency (2016) Air monitoring at minnesota silica sand facilities, State of Minnesota. <https://www.pca.state.mn.us/air/air-monitoring-minnesota-silica-sand-facilities>. Accessed 2017
15. Arabani M, Azarhoosh AR (2012) The effect of recycled concrete aggregate and steel slag on the dynamic properties of asphalt mixtures. *Constr Build Mater* 35:1–7. <https://doi.org/10.1016/j.conbuildmat.2012.02.036>
16. Park SB, Lee BC, Kim JH (2004) Studies on mechanical properties of concrete containing waste glass aggregate. *Cement Concr Res* 34:2181–2189. <https://doi.org/10.1016/j.cemconres.2004.02.006>
17. Pasandín AR, Pérez I (2015) Overview of bituminous mixtures made with recycled concrete aggregates. *Constr Build Mater* 74:151–161. <https://doi.org/10.1016/j.conbuildmat.2014.10.035>
18. Pasandín AR, Pérez I (2014) Mechanical properties of hot-mix asphalt made with recycled concrete aggregates coated with bitumen emulsion. *Constr Build Mater* 55:350–358. <https://doi.org/10.1016/j.conbuildmat.2014.01.053>
19. Wiemes L, Pawlowsky U, Mymrin V (2017) Incorporation of industrial wastes as raw materials in brick's formulation. *J Clean Prod* 142:69–77. <https://doi.org/10.1016/j.jclepro.2016.06.174>
20. Hou Z-Q, Gao Y-F, Qu X-M, Rui Z-Y, MO X-X (2004) Origin of adakitic intrusives generated during mid-Miocene east-west extension in southern Tibet. *Earth Planet Sci Lett* 220:139–155
21. Chang FC, Lee MY, Lo SL, Lin JD (2010) Artificial aggregate made from waste stone sludge and waste silt. *J Environ Manag* 91:2289–2294. <https://doi.org/10.1016/j.jenvman.2010.06.011>
22. Cruz J (2010) Process for manufacturing outdoor artificial stone boards with methacrylate resin by means of the vibro-compression under vacuum system. United States Patent Application 20100063193. Kind Code: A1
23. Lee MY, Ko CH (2008) Artificial stone slab production using waste glass, stone fragments and vacuum vibratory compaction. *Cement Concrete Compos*. <https://doi.org/10.1016/j.cemconcomp.2008.03.004>
24. Lee DJ, Shin IJ (2002) Effects of vacuum, mold temperature and cooling rate on mechanical properties of press consolidated glass fiber/PET composites. *Compos A* 33:1107–1114. [https://doi.org/10.1016/S1359-835X\(02\)00051-9](https://doi.org/10.1016/S1359-835X(02)00051-9)
25. Ismail ZZ, Al-Hashmi EA (2009) Recycling of waste glass as a partial replacement for fine aggregate in concrete. *Waste Manag* 29(2):655–659. <https://doi.org/10.1016/j.wasman.2008.08.012>
26. Dos Santos JPL, Rosa LG, Amaral PM (2011) Temperature effects on mechanical behaviour of engineered stones. *Constr Build Mater* 25:171–174. <https://doi.org/10.1016/j.conbuildmat.2010.06.042>
27. Souza Silvae F, Ribeiro CEG, Rodriguez RJS (2018) Physical and mechanical characterization of artificial stone with marble calcite waste and epoxy resin. *Mat Res*. <https://doi.org/10.1590/1980-5373-mr-2016-0377>
28. Wang B, Li G, Han J, Zheng Y, Liu H, Song W (2017) Study on the properties of artificial flood-prevention stone made by Yellow River silt. *Constr Build Mater* 144:484–492. <https://doi.org/10.1016/j.conbuildmat.2017.03.206>
29. Peng L, Qin S (2018) Mechanical behaviour and microstructure of an artificial stone slab prepared using a SiO₂ waste crucible and quartz sand. *Constr Build Mater* 171:273–280. <https://doi.org/10.1016/j.conbuildmat.2018.03.141>

30. Alexandre J, Azevedo ARG, Xavier GC, Trindade JC, Botelho GK, Monteiro SN (2014) Addition of grog-clay ceramic waste in multiple use mortar. *Mater Sci Forum* 789–799:235–239. <https://doi.org/10.4028/www.scientific.net/MSF.798-799.235>
31. Candido VS, Pinheiro RM, Monteiro SN, Vieira CMF (2014) Microstructural analysis of clay ceramic added with argillite and grog. *Mater Sci Forum* 789–799:219–223. <https://doi.org/10.4028/www.scientific.net/MSF.798-799.219>
32. Grim RE (1978) Chapter 5 Properties and Uses of Bentonite. *Dev Sedimentol* 24:217–248. [https://doi.org/10.1016/s0070-4571\(08\)70615-0](https://doi.org/10.1016/s0070-4571(08)70615-0)
33. Miranda-Trevino JC, Coles CA (2003) Kaolinite properties, structure and influence of metal retention on pH. *Appl Clay Sci* 23:133–139. [https://doi.org/10.1016/s0169-1317\(03\)00095-4](https://doi.org/10.1016/s0169-1317(03)00095-4)
34. Borsellino C, Calbrese L, di Bella G (2009) Effects of powder concentration and type of resin on the performance of marble composite structures. *Constr Build Mater* 23:1915–1921. <https://doi.org/10.1016/j.conbuildmat.2008.09.005>
35. Carvalho EAS, Marques VR, Rodriguez RJS, Ribeiro CEG, Monteiro SN, Vieira CMF (2015) Development of epoxy matrix artificial stone incorporated with sintering residue from steel making industry. *Mater Res* 18:235–248. <https://doi.org/10.1590/1516-1439.367514>

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