**Research Article**

# **Efects of Si on the formation of intermetallic phases in alloying reaction between iron substrate and liquid Zn containing 0.2 wt% Al**

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#### **Abstract**



The Fe–Zn and Fe–Al-based alloying phases are formed on galvanized/galvannealed steels which are extensively used as automobile bodies. This paper investigated the effects of Si on the formation of intermetallic phases in the alloying reaction between an iron substrate and liquid Zn containing 0.2 wt% Al and partitioning of Si between the phases. The addition of Si to the iron substrate was found to scarcely influence the formation and morphology of the Fe<sub>2</sub>Al<sub>5</sub> intermetallic phase layer but to reduce the amount of the  $\delta_1$ -FeZn<sub>7–10</sub> intermetallic phase layer at the substrate/liquid interface and to disperse the phase as grains in the Zn–0.2 wt% Al coating matrix. STEM–EDS analysis demonstrates that Si partitions less into the Fe<sub>2</sub>Al<sub>5</sub> and the δ<sub>1</sub> phases than into the iron substrate. Enrichment of Si around an Si-depleted Fe–Zn intermetallic phase product was also observed in the beginning of the alloying reaction. The results obtained allow us to explain the effect of Si on the intermetallic phase formation in terms of a difficulty in nucleating the  $\delta_1$  phase at the substrate/liquid interface.

**Keywords** Fe–Zn-based intermetallics · Alloying reaction · Alloying efect

## **1 Introduction**

Hot-dip galvanized/galvannealed steels are extensively used for steel sheets as automobile bodies because of good productivity and excellent corrosion resistance due to its sacrificial anodic effect [[1](#page-7-0)]. The Fe-Zn and Fe-Albased alloying (intermetallic) phases are known to be formed as a result of the reaction between Fe in the steel substrate and Zn(Al) in the galvanizing bath during a hotdip galvanizing process and/or a subsequent annealing process [\[2\]](#page-7-1). Since the mechanical properties of the alloying phases and the steel substrate/coating interface highly depend on the types, morphologies and thickness of the phases formed, it is important to understand the mechanisms of the alloying reaction.

According to the previous researches on the alloying reaction [[2](#page-7-1)[–4\]](#page-7-2), the sequence of the reaction is reported as follows. An Fe<sub>2</sub>Al<sub>5</sub>-type intermetallic phase layer firstly forms at the interface between the steel substrate and the liquid Zn-Al. It is generally considered that this Fe–Al phase acts as a barrier for the reaction between Fe and Zn. Fe–Zn-based intermetallic phase layers subsequently form in a way to break the  $Fe<sub>2</sub>Al<sub>5</sub>$  phase layer at grain boundaries of the ferrite phase in the steel substrate. This reaction is called "outburst reaction" due to its outward growth by breaking the Fe<sub>2</sub>Al<sub>5</sub> phase barrier layer. The phase constituents in the outburst products are reported to depend on the reaction temperature and the presence/absence of Al in the Zn bath, but it is known that the  $\delta_1$ -FeZn<sub>7–10</sub> phase is formed as main phase [\[2–](#page-7-1)[4](#page-7-2)] when the reaction temperature is higher than 485 °C [[2](#page-7-1)]. The  $FFe<sub>3</sub>Zn<sub>10</sub>$  phase is subsequently formed in between the  $\delta_1$  phase and the substrate.

It has been reported in recent years that the alloying reaction in the galvanizing/annealing process is retarded by the addition of Si to the steel substrates, which is a serious

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problem in the production of galvanized/galvannealed high-strength steels. Tobiyama et al. [\[5\]](#page-7-3) reported that the retardation of the reaction is due to the formation of Si oxide particles on the steel substrate during a reduction process, which may reduce the contact area between the substrate and the liquid. Yasui et al. [\[6](#page-7-4)] found that the retardation took place even in the absence of oxide particles, and reported that it can be explained by the solid solution of Si into the Fe-Al intermetallic phase to enhance its barrier effect and/ or the solid solution into the  $\delta_1$  phase to retard the interdiffusion between Fe and Zn through the phase. The partitioning of Si into the intermetallic phases during the alloying reaction was, however, rarely reported [7-[9\]](#page-7-6), and the effect of Si on the retardation of the alloying reaction is therefore not fully understood especially in the absence of oxide particles on the substrate/coating interface.

In the present paper, effects of Si on the formation of intermetallic phases in an alloying reaction between an iron substrate and liquid Zn containing 0.2 wt% Al and partitioning of Si between the phases were investigated to understand the alloying reactions during hot-dip galvanizing and annealing of Si doped steels.

# **2 Experimental procedures**

The chemical compositions of the iron alloys used as the substrate in the present study are listed in Table [1.](#page-1-0) The amount of alloying elements except Si was reduced as low as possible to make the investigation simple. The iron alloys are designated by their Si contents (0% Si and 0.2% Si) throughout this paper. The iron alloys were cold rolled to sheets with a thickness of 0.8 mm and then galvanized. In the galvanizing treatment the sheets were reduced in an N<sub>2</sub>–15% H<sub>2</sub> atmosphere (with a dew point of −45 °C) at 800 °C for 40 s, then cooled, dipped into a bath with Zn–0.2% Al in composition at 450 °C for 3 s and followed by  $N<sub>2</sub>$  gas cooling. The galvanized sheets were subsequently cleaned with ethanol and then annealed in a salt bath at 500 °C for 1 min, followed by water quenching.

The microstructures of the galvanized and annealed samples were observed with a feld emission type scanning electron microscope (FESEM) and a scanning transmission electron microscope (STEM). The samples for FESEM observations were prepared by grinding down to 1  $\mu$ m Al<sub>2</sub>O<sub>3</sub> polishing suspension and followed by either polishing using oxide polishing suspension or ion milling with a voltage/current condition of 6 kV/140 μA. The samples for STEM observations were prepared by a pick-up technique using an FIB equipment with a fnal milling/ cleaning condition of 5 kV/~50 pA. The chemical compositions of the elements in the samples were analyzed with energy dispersive spectroscopy (EDS) equipped on FESEM with 20 kV and STEM with 200 kV. Electron backscattering difraction (EBSD) patterns were acquired to support the identifcation of the phases present under a voltage of 20 kV with an acquisition time of a few seconds which is longer than a usual time for typical orientation mapping. The EBSD patterns were analyzed by TSL software.

# **3 Results and discussion**

### **3.1 Formation of intermetallic phases in Si free/ doped iron substrates**

Figure [1](#page-1-1) compares the microstructures formed at the substrate/coating interface in the 0% Si and 0.2% Si steels

<span id="page-1-0"></span>**Table 1** The chemical compositions of the iron-based substrates used in the present study. Sol Al means Al in solid solution in the steels

<span id="page-1-1"></span>**Fig. 1** Backscattered electron images of the samples after hot-dip galvanizing: **a** 0% Si, **b** 0.2% Si, showing the formation of Fe–Al-based intermetallic phase layer along the substrate/coating interfaces in the center. Horizontal lines are formed by milling with FIB





<span id="page-2-0"></span>**Fig. 2** Backscattered electron images of the samples after a hot-dip galvanizing process and a subsequent annealing process: **a** 0% Si, **b** 0.2% Si, showing intermetallic phase layers. It is noted that the Zn coating layer is not imaged in the micrographs







<span id="page-2-2"></span>**Fig. 4** EDS line profle along the line indicated in the BSE image taken from the 0.2% Si sample after annealing for 1 min at 500 °C

<span id="page-2-1"></span>**Fig. 3** EDS line profle along the line indicated in the BSE image taken from the 0% Si sample after annealing for 1 min at 500 °C

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after galvanizing. An alloying layer with relatively dark contrast is formed along the interface in the both samples. The layer is Al rich, as measured by EDS analysis (see Fig. [7](#page-6-0)), and is therefore deduced to be of the  $Fe<sub>2</sub>Al<sub>5</sub>$  intermetallic phase. The interface between the  $Fe<sub>2</sub>Al<sub>5</sub>$  phase and the coating region is bumpy, and the thickness of the layer is about 300 nm in maximum along the direction perpendicular to the substrate/coating interface. It is found from wide area observation that the thickness and the morphology of the Fe<sub>2</sub>Al<sub>5</sub> phase are similar in the two samples.

Figure [2](#page-2-0) displays the distribution of alloying regions formed on the two types of iron substrates after annealing. It can be clearly seen that the alloying regions with a bright contrast are formed in the both steels, but their morphologies and distribution are diferent. In the 0% Si the regions are formed in a continuous and condensed manner and are attached to the iron substrate. An averaged thickness of the regions in the 0% Si was estimated to be  $\sim$  15 µm. In the 0.2% Si, on the other hand, the regions are formed in a dispersed manner. The amount of the alloying phase regions attached to the substrate is obviously less than that in the 0% Si and the regions exist separately with each other on the substrate. It is also recognized that a number of a few micron-sized alloying phase grains are dispersed in the Zn–0.2% Al coating matrix.

Figures [3](#page-2-1) and [4](#page-2-2) show examples of EDS analysis along the alloying regions in the 0% Si and 0.2% Si after annealing, respectively. In the 0% Si, it can be identifed from the EDS profle and a reported chemical composition of Fe–Zn-based intermetallic phases  $[1, 5]$  $[1, 5]$  $[1, 5]$  $[1, 5]$  that a ~1 µm thin layer of  $\Gamma$  phase and a thick layer of  $\delta_1$  phase are formed on the substrate side of the alloying regions. In the 0.2% Si, the detected Fe contents in the alloying layers were in between 9 and 16 at.%, which indicates that the main intermetallic phases formed is the  $\delta_1$  phase and the formation of Γ phase is limited. A fuctuation of the chemical compositions from  $\sim$  2 to 9 at.% detected in the Zn coating/alloying region demonstrates that the  $\delta_1$  grains are dispersed in the matrix of Zn coating, which is designated as η in the diagram.

EBSD patterns were taken from regions with diferent chemical compositions. Figure [5](#page-3-0) shows examples of the patterns. The patterns taken from regions with the Fe content of ~26 at.% are fit with predicted high-intensity EBSD lines that were calculated with the reported crystal symmetry and atom positions of the  $\Gamma$  phase  $[10]$  $[10]$  $[10]$ . A pattern experimentally obtained from a region, marked by A in Fig. [3a](#page-2-1), and the pattern indexed are exemplifed in Fig. [5](#page-3-0)a, b, respectively. The confdence index (CI) value defned in the software was  $\sim$  0.5. EBSD patterns taken from regions whose chemical composition is around Fe–(87–91)at.% Zn are found to show a hexagonal symmetry rather

<span id="page-3-0"></span>**Fig. 5** EBSD patterns obtained from the samples after galvanizing▶ and annealing for 1 min at 500 °C: **a**, **b** a Γ phase pattern taken from a high Fe content region, marked by A in Fig. [3](#page-2-1) in the 0% Si sample, **c**, **d** a pattern taken from a region, marked by B in Fig. [4,](#page-2-2) being assumed to be  $\delta_1$  phase in the 0.2% Si sample, **e**, **f** an  $\eta$ -Zn phase pattern taken from a low Fe content region, marked by C in Fig. [4](#page-2-2). These patterns are indexed using the crystallographic symmetric data summarized in Table [2.](#page-5-0) Confdence index (CI) values in **b**, **c** and **f** are 0.51, 0.34 and 0.73, respectively

than cubic (Γ, Γ<sub>1</sub>-Fe<sub>11</sub>Zn<sub>39</sub>) and monoclinic symmetries  $(\zeta$ -FeZn<sub>13</sub>). A typical pattern and its indexed one are shown in Fig. [5](#page-3-0)c, d. The  $\delta_1$  phase is reported to have a complex hexagonal structure ( $P6<sub>3</sub>/mmc$ ) with 156 atoms in the unit cell [\[11–](#page-7-8)[13](#page-7-9)]. The patterns are reasonably ft with the patterns which were calculated based on their crystallographic data [[12](#page-7-10), [13](#page-7-9)]. It is, therefore, reasonable to identify that the alloying regions are of the  $\delta_1$  phase based on the results obtained from EDS and EBSD. The patterns taken from low Fe content regions were found to show a perfect fit (CI value:  $\sim$  0.7) with the simulated patterns of the hcp structure, which demonstrates that the regions are of the η-Zn phase. The crystallographic symmetry data used for indexing each phase in the EBSD analysis are summarized in Table [2](#page-5-0).

### **3.2 Partitioning of Si to the alloying phase**

Partitioning of Si to the intermetallic phases was investigated in order to understand the role of Si on the alloying reaction. Figure [6](#page-5-1) shows an STEM image and EDS mapping performed for the rectangular areas A and B on a pick-up thin plate taken from the 0.2% Si sample after galvanizing. These areas contain a thin  $Fe<sub>2</sub>Al<sub>5</sub>$  phase layer and a globular region which is a product of outburst reaction. It can be seen in the area A that Al is enriched in the alloying layer along the substrate/coating interface, and Si is slightly diluted in the layer. The enrichment of Zn and O is not recognized. It is recognized in the area B that Al and Zn are enriched in the globular region, and Si is depleted in the globular region and enriched around the region on the substrate side. It should be mentioned that an Fe rich region is present on the right side of the globular region. The reason for the existence of this region is not clear, but it might be formed by the deposition of Fe sputtered from the substrate during the sample preparation using FIB.

Figure [7](#page-6-0) shows EDS elemental maps obtained from the 0.2% Si sample after annealing. It can be seen that Si is depleted in the intermetallic phase layer. The partitioning of Si is in consistent with a recent study which reported that the Si content detected in the  $\delta_1$  and  $\zeta$  phases is much lower than that in the iron substrate [\[7](#page-7-5)].



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Phase	Г	$\delta_1$	η-Zn
Chemical composition	Fe <sub>3</sub> Zn <sub>10</sub>	$FeZn7-10$	Zn
Space group	I-43 m	$P6_{3}/mmc$	$P6_{3}/mmc$
Lattice parameter			
$a(\AA)$	9.018	12.815	2.665
$c(\AA)$		57.35	4.947
Reflectors used for indexing	033	0002	0002
	141	$0 - 117$	$10 - 10$
	060	$1 - 210$	$10 - 11$
	444	$02 - 27$	$10 - 13$
	363	$1 - 327$	$11 - 20$
	093	$03 - 30$	$11 - 22$
		$1 - 2110$	$20 - 21$
		$1 - 21 - 14$	$20 - 23$
			$21 - 31$

<span id="page-5-0"></span>**Table 2** Crystallographic symmetry data used for indexing phases in analyzing EBSD patterns

## **3.3 The efect of Si on the alloying reaction in galvanizing/annealing process**

It has been confrmed in the present study that the addition of Si to the iron substrate reduces the amount and the thickness of the  $\delta_1$  phase layer at the substrate/liquid interface. It has also been found that the Si addition changes a manner of intermetallic phase formation such that the phase is dispersed as grains within the Zn–0.2% Al matrix. The effects of Si on the formation of the  $\delta_1$  intermetallic phase are discussed below.

Several mechanisms were reported to explain the effect of Si to retard the alloying reaction. One mechanism is related to the decomposition of  $Fe<sub>2</sub>Al<sub>5</sub>$  phase which is generally accepted to trigger the outburst reaction. Yasui et al. reported that retardation of the outburst reaction can be explained by a slower decomposition rate of the Fe<sub>2</sub>Al<sub>5</sub> phase by the solid solution of Si into the phase  $[6, 6]$  $[6, 6]$  $[6, 6]$ [14](#page-7-11)]. This mechanism is based on the report that Si occupies the vacancy sites of the Fe<sub>2</sub>Al<sub>5</sub> phase structure [[15](#page-7-12)–[18](#page-7-13)], which may reduce the rate of Al difusion, resulting in a slowed decomposition rate of the phase. Another mechanism is the suppression of diffusion of Fe and Zn in the  $\delta_1$ phase by solid solution of Si in the phase. This thought was encouraged by difusion couple experiments [\[19](#page-7-14)] showing a slower growth rate of the phase in the presence of Si and the literatures [[9,](#page-7-6) [20\]](#page-7-15) which reported on the solubility of Si by 1 at.% in the  $\delta_1$  phase in the Fe–Zn–Si ternary phase

<span id="page-5-1"></span>**Fig. 6** STEM image and corresponding EDS maps taken from A and ► B in a pick-up thin plate of the 0.2% Si sample after hot-dip galvanizing. Horizontal lines are formed milling with FIB and bright area on the right side in the area A is a hole



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<span id="page-6-0"></span>**Fig. 7** Backscattered electron (BSE) image and corresponding EDS elemental maps obtained from the 0.2% Si sample after annealing



<span id="page-6-1"></span>**Fig. 8** Schematic illustration showing an efect of Si addition on thermodynamic stability of the phases and the driving force for the nucleation of the  $\delta_1$  phase

diagram. The validity of this mechanism is, however, in question because the present study which shows that the Si content detected in the intermetallic phase is negligible.

The effect of Si on the alloying reaction is considered in terms of thermodynamic viewpoint below. The microstructural characterization in the present study and in our previous work indicates that Si tends to partition less into the  $\delta_1$  phase than into the ferrite phase in the substrate. This fnding is supported by a report by Wang et al. [[21](#page-7-16)],

which shows that the partition coefficient of Si between the  $\delta_1$  and the  $\alpha$  phases ( $k \delta^{1/\alpha}$ ) is ~0.06. Based on the Si partitioning behavior, one can assume that Si thermodynamically stabilizes the ferrite phase against the  $\delta_1$  phase and thereby reducing the driving force for the nucleation of the intermetallic phase at the substrate/liquid interface. This effect is schematically illustrated in Fig. [8](#page-6-1). This scenario may qualitatively explain the formation of a reduced amount of the intermetallic phase attached to the steel substrate and a dispersion of the phase within the Zn matrix in the presence of Si in the substrate (Fig. [2](#page-2-0)). Quantitative thermodynamic studies might be important to understand the efect of Si on the alloy in reaction in more accurate way.

#### **4 Summary**

In the present paper effects of Si on the formation of intermetallic phases in the alloying reaction between an iron substrate and liquid Zn containing 0.2 wt% Al and partitioning of Si between the phases were investigated to understand the alloying reactions during hot-dip galvanizing and annealing of Si doped steels. The main results obtained are as follows:

- 1. The addition of Si to an iron substrate was found to scarcely influence the formation and morphology of Fe<sub>2</sub>Al<sub>5</sub> intermetallic phase layer but to reduce the amount of  $\delta_1$ -FeZn<sub>7-10</sub> intermetallic phase layer at the substrate/liquid interface and to disperse the phase as grains in the Zn–0.2 wt% Al matrix.
- 2. STEM–EDS analysis demonstrates that Si partitions less into the Fe<sub>2</sub>Al<sub>5</sub> and the  $\delta_1$  phases than into the iron substrate (ferrite) phase. Enrichment of Si around an Si-depleted Fe–Zn intermetallic phase product was also observed in the beginning of the alloying reaction.
- 3. The observed effects of Si on the intermetallic phase formation may be explained by a difficulty in nucleating the  $\delta_1$  phase at the substrate/liquid interface.

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#### **Compliance with ethical standards**

**Conflict of interest** The authors declare that they have no confict of interest.

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