RESEARCH ARTICLE



Effect of Antibacterial Enoxacin on the Properties of Injectable Nano-hydroxyapatite/Polyurethane Cement for Bone Repairing

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Abstract

Biomaterial-associated infection (BAI) is a kind of serious post-operative complication in orthopaedic surgery. Antibioticloaded bone cement shines a light on BAI prevention for convenient manipulation and complex filling. To this aim, we designed an antibacterial bone cement based on Nano-hydroxyapatite/Polyurethane (PUHA) loading with antibiotic Enoxacin (EN). The distinct shear-thinning behavior of the prepolymers was observed, indicating a good injectability. The PUHA bone cement possessed a suitable curing speed, and the addition of EN might slightly expedite the curing process and enhance the mechanical properties. The EN release profile indicated that the EN-loaded bone cement could reach the minimum inhibitory concentration in 2 h, and sustainedly released EN for almost 8 days, exhibiting an antibacterial delivery potential. Antibacterial test further confirmed the antibacterial ability of EN-loaded bone cement is in a dose-dependent manner. However, the osteogenic performance of drug-loaded bone cement with high dosage is not as good as antibacterial activity. When the EN concentration of antibacterial cement was lower than $32 \,\mu g \cdot m L^{-1}$, the proliferation and osteogenic differentiation of rat mesenchymal stem cells could be significantly promoted. Overall, this study verified the potential of the EN-loaded PUHA bone cement in anti-infection and osteogenesis for bone repairing.

Keywords Antibacterial bone cement \cdot Nano-hydroxyapatite/polyurethane \cdot Enoxacin \cdot Shear-thinning behavior \cdot Osteogenesis

1 Introduction

In the aging society, BAI is extremely difficult to prevent and cure due to the fracture fixation meets with osteoporosis treatment [1, 2]. BAI is a kind of acute complication triggered mostly by biofilms on implants in orthopaedic surgery, which could lead to non-union, loss of function, and even amputation [2]. It was reported that the BAI rate was between 2.6 and 45% if tibial plateau fractures managed with Open Reduction and Internal Fixation (ORIF) in bone fracture fixation clinically [3, 4]. A new type of treatment strategy that antibiotic-loaded bone cement was covered on intramedullary nail achieved significant effect for deep infection after ORIF of ankle fractures [5]. Bone cement can form a strong bond in situ with bone tissue to create a mechanically stable interface under the influence of tensile, compressive, and shear forces [6]. Furthermore, bone cement has the capacity to fill bone cavities with complicated geometric shapes on the foundation of excellent liquidity and fix grafts with low risk of refractures caused by stress shielding [7]. Thus, injectable bone cement is attracting more attention from many researchers as a kind of local drug delivery vehicle for BAI prevention.

For now, the mainly bone cement were Polymethyl Methacrylate (PMMA) and Calcium Phosphate Cement (CPC) in clinic. However, both these bone cements had their shortcomings during clinical use. PMMA has undergone an exothermic polymerization reaction that can cause terrible local thermal necrosis during the curing process [8]. What's worse, exothermic polymerization makes some temperature-sensitive antibiotics inactivate, which limits the choice of antibiotics [9]. PMMA causes aseptic loosening due to no bioactivity, and the toxicity of its liquid monomer seriously affects the therapeutic effect [10]. For

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calcium phosphate cement, high bioactivity is preferable for the bone regeneration without heat released during the curing process. However, its curing time was long and the adhesion was relatively poor [11]. Meanwhile, inappropriate mechanical strength and poor fixation performance of CPC in biological environments can exacerbate bone destruction [12]. Therefore, CPC mainly be applied in non- or moderate load-bearing sites. Hence, it is urgent to modify current bone cement [13, 14] or develop a different bone cement system with good mechanical strength, biocompatibility and anti-infection.

Polyurethane (PU), a kind of polymer material with adjustable properties, has attracted much attention from many researchers [15, 16]. There were plenty of strategies to design PU into bone cement, such as one-component PU, two-component PU, and many more [17]. Among them, two-component (component A and component B) system has been often used to design bone cement based on PU [18]. Our previous study incorporated nano-hydroxyapatite (n-HA) nanoparticles into PU to prepare PUHA cement [19]. The setting time and mechanical properties have been largely affected by different contents of nano particles. Although the PUHA cement has promising osteogenesis for the addition of high bioactive n-HA, lack of anti-infection limits its clinical application. Silver has been added in the injectable PU system to provide effectively antimicrobial property [20]. However, the poor cellular viability of Ag⁺ is a major obstacle for the PU cement used in clinic.

Generally speaking, antibacterial activities in biomedical perspective are related to compounds or elements that locally retarding bacteria or killing bacterial, without being in general toxic to surrounding tissues [21]. Most current antibacterial agents, available in medical industries are chemically modified from natural compounds [22], known as antibiotics. It was noteworthy that the antibacterial effect of each antibacterial agent was depending on the species of bacterial strain and its effective mechanism [23]. By and large, BAI was triggered by lots of pathogens including genus Staphylococcus, Acinetobacter and Escherichia, specifically Staphylococcus aureus [24]. Herein, EN is a third-generation fluoroquinolone broad-spectrum antibiotic, especially against Gram-positive bacteria, such as Staph*ylococcus aureus* [25]. It can form a ternary complex of drug-enzyme-DNA that once be trapped, disrupting DNA replication and triggering cell death mechanisms [26]. The antibacterial mechanism of EN help it can kill Staphylococ*cus aureus* with a concentration $\leq 0.8 \ \mu g \cdot m L^{-1}$ [27]. The Minimal Inhibitory Concentration (MIC) of EN is far below Ag, Au and other inorganic antibacterial agent [23]. Thus, EN is an appropriate choice of antimicrobial agents applied for BAI.

In this study, we incorporated the antibacterial drug EN into PUHA composite to prepare an injectable antibacterial

bone cement for the infection prevention in bone repairing. First, we prepared EN-loaded PUHA and investigated their rheological properties, isocyanate group (–NCO) conversion rate, chemical construction, morphology, mechanical properties and drug release behavior of the bone cement. To verify the antibacterial property of EN-loaded PUHA, antibacterial experiment was performed to investigate the inhibitory effect of bone cement on *Staphylococcus aureus* (Gram-positive bacteria) and *Escherichia coli* (Gram-negative bacteria). Finally, the cytotoxicity and osteogenic differentiation properties of bone cement were evaluated by rat Bone Marrow mesenchymal Stem Cells (BMSCs) (Fig. 1).

2 Materials and Methods

2.1 Materials

EN, Isophorone Diisocyanate (IPDI), Polytetramethylene Ether Glycol (PTMEG, $M_n = 2000$), mannitol, and Polyethylene Glycol (PEG₆₀₀, $M_n = 600$) were purchased from Aladdin Industrial Corporation (Shanghai, China). Stannous salt was bought from J & K Scientific Ltd (Beijing, China). The n-HA particles were prepared through a chemical precipitation method, as reported in our previous study [28], and they were dried at 108 °C for 2 h in an electro-thermostatic blast oven. The above reagents are all analytical reagents.

2.2 Fabrication of Polyurethane-Based Bone Cement

2.2.1 Component A: Injectable Prepolymer

Firstly, PTMEG and mannitol were added to a three-necked round bottom flask, stirred with a stir rod under nitrogen atmosphere at 70 °C for 30 min, and then n-HA was added and dispersed for 1 h. Second, IPDI was subsequently added, and the pre-polymerization process was approximately 5 h at 70 °C. Finally, EN was added and stirred under nitrogen atmosphere at ambient temperature for 1 h. The isocyanate index (stoichiometric ratio of NCO/OH) was set at 1.5. Four types of bone cement prepolymers were fabricated as preceding steps and the formulation of each compound is shown in Table 1.

2.2.2 Component B: Curing Reagent

The curing reagent was acquired by mixing stannous salt and PEG_{600} at a mass ratio of 1:3. And then, homogeneous curing reagent was obtained through ultrasonic dispersion for at least 20 min.

20

3

2.2.3 Polymer Preparation

Table 1 Formulation of

prepolymers (n=5)

According to ISO 5833-2002 (Implants for surgery - Acrylic resin cement), component A and component B at a volume ratio of 25:1 were mixed at ambient temperature, and then the homogeneously mixed pastes were injected into a Teflon mold (ϕ 6 mm × 12 mm³) to cure in a 37 °C cabinet for 48 h.

UAE-3

77

2.3 Characterization of Bone Cement

Rheological properties were measured using a rheometer (Discover HR-2, TA, USA). The storage modulus (G') and loss modulus (G'') of the mixture of component A and component B was measured at a frequency of 1.0 Hz at 37 °C during the curing process. The shear-dependence viscosity of four prepolymers of bone cement and component B was measured at 25 °C in a shear rate range between 0.1 and $200 \cdot s^{-1}$.

The chemical shift of carbon in PUHA was characterized by C¹³ solid Nuclear Magnetic Resonance (C¹³-NMR, AVANCE III-500 MHz, Bruker, Switzerland) using a 500 MHz spectrometer for C^{13} nuclei at room temperature. The n-HA, PU and PUHA cement have been characterized by X-ray Diffraction (XRD, EMPYERAN, Panalytical, Netherlands) with Cu Ka radiation. The conditions were at 40 kV and 25 mA. Scans and 20 range was from 10 to 60° at a step size of 0.03° . The chemical functional group of four bone cements and EN were investigated by Attenuated Total Internal Refraction Fourier Transform Infrared spectroscopy (ATR-FTIR, Thermofisher, Nicolet-5700). ATR-FTIR measurements of the compounds were performed using a universal ATR sampling accessory between 4000 and 400 cm^{-1} . In addition, the –NCO conversion rate was tracked during the curing process every 10 min through ATR-FTIR. The n-HA powder were prepared in our lab according to the previous paper [28], which was characterized by Transmission electron microscopy (TEM, Tecnai, G2 F20, Hillsboro, OR, USA). In addition, a clearly observation of the dispersion of n-HA in the PU matrix, was sectioned by cryoultramicrotomy with a diamond knife at a 50 nm thickness.

 95.9 ± 1.5

Cross-linking is a crucial property for the cements formed in situ, which also means the stableness of the PU network. Therefore, the apparent density (ρ) , Swelling Rate (SR) and Gel content (G) of the cements were tested for the crosslinking evalution according to swelling equilibrium method and previous paper [29]. The cement samples ($\phi 6 \text{ mm} \times 12$ mm³) were dissolved into absolute ethanol for 24 h. In addition, ρ , SR and G were defined by the following Eqs. (1), (2), and (3), respectively:

 2.98 ± 0.12

$$\rho = \frac{4m_d}{\pi d^2 h} \tag{1}$$

$$SR = \left(\frac{m_{sw} - m_d}{m_d}\right) \times 100\% \tag{2}$$

$$G = \frac{m_d}{m_0} \tag{3}$$

where m_{sw} and m_d are the samples quality of swelling state and dry state, respectively. m_0 is the m_{sw} after vacuum drying at 37 °C for 24 h. "d" and "h" mean the diameter and high of samples. ρ_1 is the specific density of the ethanol $(0.789 \text{ g}\cdot\text{mL}^{-1})$ and ρ_2 is the density of samples from Eq. (1).

According to ASTM D 5024-95 standard, the mechanical properties of the four types of cured bone cement were tested on samples with a size of $\phi 6 \times 12 \text{ mm}^3$ through a mechanical testing machine (AUTOGRAPH AG-IC 20/50KN, Japan). All the tests were conducted at the speed of $1 \text{ mm} \cdot \text{min}^{-1}$, and the load was applied until the specimen was compressed to approximately 50% of its original length at room temperature. The compressive modulus was calculated by the slope of linear change that appeared for the first time in the stress-strain curve. The compressive strength was calculated according to the following formula (4):

$$\delta = \frac{p}{F} \tag{4}$$

where δ , p and F indicate the compressive strength, stress, and surface area, respectively. Five independent samples were tested for each group.

The microstructure of PUHA, UAE-1, UAE-2 and UAE-3 cements were observed by Scanning Electron Microscopy (SEM, JSM-7500F, JEOL, Japan) in Back-Scattered Electron (BSE) mode. An Energy Dispersive Spectrometer (EDS, JSM-7500F, JEOL, Japan) was used on the surface of the samples to evaluate the distribution of the Ca and P elements. The brittle fracture surfaces of tested samples were obtained by liquid nitrogen and sputter-coated with gold before the examination. The X-ray Photoelectron Spectrometry (XPS, AXIS UltraDLD, UK) was selected to elucidate the presence of EN in the drug-loaded cements by means of observing the peak of F element in XPS spectra.

2.4 In Vitro Drug Release and Antibacterial Assay

In vitro drug release of different samples was carried out according to ISO 10993-12. Different samples (n=5) were immersed in 10 mL DMSO/PBS (v/v=1/200) medium with gentle agitation at 37 °C, then 1 mL of medium taken out for analysis at different timepoints, which were 1 h, 2 h, 8 h, 24 h, 48 h, 4 d, 7 d, 14 d and 30 d. The content of EN was detected at 268 nm by ultraviolet–visible spectroscopy [30] (Shimadzu UV–VIS V-2401, Japan).

Staphylococcus aureus (S. aureus, CMCC (B) 26003) and Escherichia coli (E. coli, CMCC 44103) were chosen as standard bacteria to evaluate the antibacterial activity of PUHA and EN-loaded bone cement [31]. Both bacteria were grown aerobically in broth medium at 37 °C. The test conditions of inhibition zone and antibacterial rate were as follows [32]:

- Zone of inhibition (ZOI): the disk-shaped samples (φ 6 mm × 2 mm³) were placed on agar plates pre-inoculated and incubated at 37 °C for 24 h.
- (2) Antibacterial rate: the disk-shaped samples were incubated with 1×10^{6} CFU·mL⁻¹ *E. coli* at 37 °C for 2 h. After the incubation, the co-cultured bacterial suspensions were diluted by a tenfold dilution method to enumerate the bacteria. The antibacterial ability was recognized by Bacteriostasis Rate (BR), which was defined by the following Eq. (5):

$$BR = \left(\frac{N_0 - N_1}{N_0}\right) \times 100\% \tag{5}$$

where N_0 is the number of colonies for the control sample (PUHA), and N_1 is the number of colonies for UAE-1, UAE-2, and UAE-3.

2.5 In Vitro Cell Evaluation

2.5.1 Extract Solutions Preparation

The extract solutions of EN-loaded bone cement were prepared according to ISO 10993-9. The disc samples ($\phi 6 \times 2 \text{ mm}^3$) were immersed in Alpha Minimum Essential Medium (α -MEM, Gibco) supplemented with 10% Newborn Calf Serum (NBCS) and 1% penicillin/streptomycin. The surface area to extract medium ratio was $1.25 \text{ cm}^2 \cdot \text{mL}^{-1}$, and the immersed samples were kept in a humidified atmosphere with 5% CO₂ at 37 °C for 48 h. Then the extract medium was collected and refrigerated at 4 °C.

2.5.2 Cell Proliferation

Sprague–Dawley (SD) rats were obtained from the DOSSY experimental animals Co, Ltd. The BMSCs were extracted from the femurs and tibiae of the SD rats weighing approximately 100 g. The extraction was according to the normative procedure, which was approved by the Ethics Committee of Sichuan University. The third passage of the BMSCs were utilized in the experiments [33]. BMSCs $(1 \times 10^4 \text{ cells/well})$ were equilibrated in α-MEM medium and extract solutions of EN-loaded bone cement to evaluate cell proliferation. The cell proliferation was evaluated using a Cell Counting Kit-8 (CCK-8) kit (Sigma-Aldrich Co., St. Louis, MO, USA) on days 1, 4 and 7. A multi-label counter (Wallac Victor 31420, PerkinElmer Co., Waltham, MA, USA) was used to detect the absorbance value at 450 nm. The morphology of live BMSCs was observed by a fluorescence microscope. Three samples were tested in each group.

2.5.3 Cell Differentiation

The activities of Alkaline Phosphatase (ALP) and Osteocalcin (OCN) are mostly used to assess osteogenic differentiation of the BMSCs, which were served as early osteogenesis [34] and terminal osteogenesis [35], respectively. In this study, Enzyme-Linked Immunosorbent Assay kits (ELISA, Wuhan Cloud-Clone Corp, CO., Wuhan, China) were employed to evaluate the ALP and OCN content of BMSCs [28]. The BMSCs (8×10^3 cells/well) were seeded in α -MEM medium and extract solutions to evaluate the ALP and OCN content on 7 d and 14 d, respectively.

2.6 Statistical Analysis

The data was expressed as the mean ± Standard Deviation (SD). One-way Analysis of Variance (ANOVA) tests, together with a post-hoc Tukey's test was conducted using the SPSS (version 25.0) software (LEAD Technologies, Inc., Chicago, IL, USA) to examine the data by the following significance levels: p < 0.05, p < 0.01 and p < 0.001, which represented statistically significant, very significant, and extremely significant values, respectively. p > 0.05 indicated that there were no statistically significant values.

3 Results and Discussion

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3.1 Rheological Properties and Isocyanate **Conversion Rate**

The advantage of injectable cement over other biomaterials is excellent fluidity and in situ curing characteristic, which could help bone cement fill irregular bone cavities and fix grafts. Thus, injectable bone cement is supposed to have an appropriate setting time so that the bone cement would have enough time long for clinical operation. Typically, the setting time for clinically available bone cement vary by between 5 and 15 min [36]. The intersections of G' and G'' in the curve demonstrated the gelation points, which can imply setting time to some extent [37, 38]. Therefore, it is worthwhile to explore the rheological properties of the bone cement. In addition, the -NCO conversion rate is tested to determine whether the addition of EN would affect the -NCO conversion rate.

For rheological analysis, storage moduli (G') and loss moduli (G'') of the mixture (component A and component B) implies the elastic nature and the viscous nature, respectively. As shown in Fig. 2a-d, at first, all mixtures exhibited fluidity, because G'' appeared to be greater than G'. The intersections of G' and G'' in the curve exhibited at 21.13 min (PUHA), 16.68 min (UAE-1), 13.35 min (UAE-2), and 11.83 min (UAE-3), respectively. With the proportions of EN increased, the curing time of mixtures became shorter, and the setting procedure was faster. The mixture of component A and component B would solidify when time went by. Therefore, the UAE-2 and UAE-3 both had suitable setting time.

As shown in Fig. 2e, the four types of bone cement prepolymers and component B exhibited distinctly shear-thinning behavior. Shear-thinning behavior conforms to the law of pseudoplastic flow of materials that help the mixture of component A and component B possess the desired flowability when it is injected in vivo. Furthermore, we tested the viscosity of three drug-loaded cement prepolymers which were in the range of 47–100 Pa·s in Fig. 2e. A previous study about a commercial PMMA cement found that the initial viscosity of bone cement would be better if the viscosity is in the range of 50–100 Pa·s [39], which could help the bone cements to prevent leakage while ensuring injectability. To sum up, the shear-thinning characteristic and the viscosity of the EN-loaded bone cement can meet the requirements of good injectability and proper curing time.

In Fig. 2f-i, the peak of isocyanate group decayed with the increasing cure time. The IR spectra presented a typical speeding up trend in different EN-loaded cements when they were consuming the -NCO groups. The relative





Fig. 2 Time-dependent functions of G' and G'' for curing PUHA (**a**), UAE-1 (**b**), UAE-2 (**c**) and UAE-3 (**d**), typical frequency-dependent functions of the viscosity of different composites (**e**), –NCO conversion rate for curing PUHA (**f**), UAE-1 (**g**), UAE-2 (**h**) and UAE-3 (**i**)

content of –NCO in the prepolymer of EN-loaded bone cement decreased with the increase of EN addition. This might be because that EN reagent would react with IPDI and consume an amount of –NCO during pre-polymerization process (see Fig. 4a for more details). The conversion rate of –NCO was accelerated with the presence of EN, which matched the rheological results that the curing time became shorter. Meanwhile, the addition of EN did not influence the total conversion rate of –NCO. All –NCO groups of ENloaded cements was completely consumed at 30 min after curing. The monomer conversion of the PU cement is much higher than MMA-based cement [40], only about 75% at 35 °C. The high conversion of EN-loaded cement can avert the inflammation reaction of injectable materials in clinical application.

3.2 Physiochemical Properties of the Cements

The spectrum of the solid C^{13} -NMR of the PUHA cement was displayed in Fig. 3a. The peak at 158 ppm (C–b) was corresponded to the urethane linkage [41]. The peaks at 71 ppm may be a merged peak of the hard-segment carbons adjacent to the amino group (C–a) and methylidyne carbon adjacent to urethane (C–c) [28]. The presence of C–b and C–c demonstrated that the PTMEG and IPDI had a chemical reaction. The peak at 45 ppm was associated with the methylene (C–d) of the six-membered ring in IPDI. In addition, the peaks ranging from 20 to 40 ppm belonged to the saturated fatty carbons in both the soft segments and the hard segments [41]. The above results demonstrate that the PU was successfully synthesized.



Fig.3 C^{13} -NMR spectrum (**a**) of PUHA; the XRD spectra (**b**) of n-HA, PU and PUHA; (**c**) FTIR spectra of the EN, PUHA, and EN-loaded cements; the TEM micrograph of the n-HA powder (**d**) and the PUHA composite (**e**); EN release curve for 48 h (**f**) and 30 days

(g); the compressive strength (h) and compressive modulus (i) of PUHA and EN-loaded bone cements. ("•" indicates the crystalline phase of HA, "*" indicates poorly crystallized PU phase; p < 0.05, p < 0.01, p < 0.001, (n = 5))

As shown in Fig. 3b, the XRD spectrum of pure PU cement showed only an envelope spectrum with a broad peak centered at 20.1°, indicating the weak crystallized nature of the polymer [42]. On the other side, n-HA showed some sharp peaks, which indicated well crystallinity that were in good agreement with the JCPDS 09-0432. Five obvious diffraction peaks were at 25.8°, 31.8°, 32.2°, 32.9° and 34.9°, which were indexed to the (002), (211), (112), (300) and (202) planes of n-HA, respectively [43]. The composite of PUHA cement showed a combined pattern similar to the individual spectrum of PU and n-HA, except for a relative decrease in the intensity. In addition, the reason of the intensity decreases may be the n-HA particles were covered with the organic network. The XRD results indicated that n-HA particles were incorporated into PU matrix.

The FTIR spectra could be used to confirm the chemical groups or linkages within a polymeric structure, which could determine whether a new substance was successfully synthesized at the molecular level. As shown in Fig. 3c, the appearance of bands at 3326 cm^{-1} (-NH) and the disappearance of the absorption peak at 2260 cm^{-1} (-NCO) synergistically proved that the PU was successfully synthesized. Furthermore, it was noteworthy that a new stretching vibration peak located at 1050 cm⁻¹ (-C-F) appeared in EN-loaded bone cement and strengthened as the content of EN increased, which demonstrated that the EN was successfully embedded into PU. In addition, the band at around 1365 cm⁻¹ was the absorption peak of the amine group in PUHA. The 1365 cm⁻¹ was shifted to 1375 cm⁻¹ with the addition of EN. This redshift was because the amine group in PUHA was protonated by the piperazinyl



Fig. 4 a Possible mechanisms of EN molecule reacting with IPDI in prepolymer, b possible mechanisms of EN molecule participating in cured bone cement (Red arrow: electrostatic attraction between EN molecule and PU matrix)

group in EN molecule. The redshift about 10 cm^{-1} implied the presence of electrostatic attraction between EN molecule and PU matrix [44] (see details in Fig. 4b). Furthermore, the band at 1375 cm⁻¹ was strengthened as the EN content increased. These implied that EN was successfully embedded into PU matrix.

As shown in Fig. 3d, the n-HA crystals synthesized by the chemical precipitation method were mostly in the shape of needles or rods, of which the crystal length was around 100 nm and the width was around 25 nm. In addition, they are basically similar to the shape of natural bone apatite with good crystallinity. As shown in Fig. 3e, the TEM micrograph of PUHA composite was observed from the ultra section confirming the good dispersion of the rod-shaped nano crystals in the PU matrix.

Release behavior of antibiotic EN was studied shown in Fig. 3f, g. A burst release of EN was observed in the first 2 h, and the drug concentration quickly reached at 2 μ g·mL⁻¹, which was much higher than the MIC of EN. Subsequently, the drug release rate slowed down, and the drug was still released slowly until the 8th day. The concentration of EN

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at all release timepoints was greater than the MIC of EN $(0.8 \ \mu g \cdot m L^{-1})$, showing the good potential of EN-loaded bone cement to inhibit bacterial proliferation. The ENloaded bone cement exhibited a slow-release characteristic as a whole, and the EN drug loading in this study was effective and reasonable. In addition, it could be seen that the EN release concentration was dose-dependent at all timepoints. The higher the drug loading content, the greater the concentration of EN released. The reason might be that PUHA was a non-degradable material with a dense structure, and the drug was loaded in a mixed manner before curing. Therefore, only the drug on the surface of PUHA could be released after curing. Therefore, the release concentration of EN presented a dose-dependent trend. On the other hand, BAI caused by implant surgery mostly originate from the implant interface [45]. The EN-loaded bone cement in this study could continuously and slowly release the antibacterial drug EN from the surface to inhibit bacterial proliferation.

The mechanical performances of cured bone cement are critical indicator that determines whether they have enough feasibility to be employed in bone tissue engineering. The compress stress versus strain (%) graph of PUHA, UAE-1, UAE-2 and UAE-3 were displayed in Fig. S1 in the supporting information. As shown in Fig. 3h, i, the compressive strength and compressive modulus of PUHA material were distinctly enhanced (p < 0.001) after incorporating EN component. It was worth noting that the compressive strength had the tendency to enhance with the increasement of EN content. The compressive strength of UAE-3 reached as high as 9.7 ± 1.4 MPa, which was comparable to the high end of compressive strength of cancellous bone (2–10 MPa) [46]. This might result from the fact that EN acted as a crosslinking agent to promote the cross-linking between the soft and the hard segments through hydrogen bond [47], which matched the above FTIR results that the bands at 1365 cm^{-1} were strengthened with the presence of EN. However, there was no significant difference in the compression strength and modulus of UAE-1, UAE-2 and UAE-3. This reason might be the additive amount of EN was too small to show a significant difference.

3.3 The Degree of Cross-Linking and Relative Properties

In our previous study, cured pure PU was a stable and nondegradable materials, of which the solubility was $0.13 \pm 0.07\%$ after 24 h soaking in water and the dimensional expansion was $1.39 \pm 0.38\%$ after immersed in deionized water for 4 weeks [48]. A review has pointed that the presence of nano-particle, such as n-HA, would improve the stability and biocompatibility of polymer materials [49]. Here, shown in Table 2, the *SR* of all drug-loaded PUHA cements were smaller, while the gel contents (*G*) were larger than the PUHA cement when they were soaking in ethanol (p < 0.001). Both the *SR* and *G* results indicated that the EN drug improved the degree of cross-linking of cured PUHAs. Consequently, the presence of EN could enhance the stability of interior structure of PUHA cement, which also resulted the higher compressive property in Fig. 3h, i.

3.4 Properties Influenced by the EN Loading

As shown in Fig. 5a, b, the peak of F element in UAE-2 and UAE-3 was observed according to XPS results. EN is the only component containing F element in the synthesized

bone cements. Besides, the peak of F element has the tendency to strengthen when the content of EN increased. No distinct peak of F element in UAE-1 has been observed, because the EN content was too low. Hence, the XPS results testified that EN was successfully incorporated into PUHA matrix.

As shown in Fig. 5c, the EN concentration in extract solution of cured UAE-1, UAE-2 and UAE-3 was measured, which was $22.38 \pm 3.73 \ \mu g \cdot m L^{-1}$, $25.91 \pm 1.82 \ \mu g \cdot m L^{-1}$, $36.12 \pm 3.53 \ \mu g \cdot m L^{-1}$, respectively. Compared to EN concentration in release curve, the EN concentration in extract solution was much higher. This was because the extract solution was prepared by exposing the culture medium on the surface of the cured bone cement according to ISO 10993-9, which the volume-to-surface area proportion is $1.25 \ cm^2 \cdot m L^{-1}$ for 48 h at 37 °C. It was prepared to evaluate the in vitro biological activity of the drug-loaded bone cements. All biological experiments in vitro were carried out in extract solution for a stable evaluation in this study.

SEM was used to observe the constituent of PUHA, UAE-1, UAE-2 and UAE-3 in BSE mode, which were shown in Fig. S2 in the supporting information. Furthermore, as shown in Fig. 5d–k, the surface scanning by EDS showed that the characteristic elements (Ca and P) were observed in PUHA, UAE-1, UAE-2, and UAE-3. The Ca and P were in the same position, which matched the SEM and TEM results that n-HA particles were observed.

3.5 Antibacterial Properties

3.5.1 Zone of Inhibition (ZOI)

The ZOI of EN-loaded bone cement against *S. aureus* and *E. coli* were exhibited in Fig. 6a, b. The antibacterial effect of EN-loaded bone cement is proportional to the area of antibacterial zone. In addition, the mean area of *ZOI* was presented in the form of histograms (n=3). The inhibition circle could be observed around the EN-loaded bone cement sample. In addition, no bacteriostatic area has been observed around samples of pristine PUHA. Higher EN contents of cements exhibited larger inhibition zones against both two bacteria and the difference were significant (p < 0.01 and p < 0.001).

Table 2Physical properties ofPUHA, UAE-1, UAE-2 andUAE-3

Cements	Swelling rate (SR, %)	Apparent density (ρ , g·cm ⁻³)	Gel content (G , %)
PUHA	145.80 ± 3.58	1.36 ± 0.02	96.86 ± 0.47
UAE-1	$126.61 \pm 2.30 \ (@@@)$	$1.38 \pm 0.05 (@@@)$	98.47±0.21 (@@@)
UAE-2	$123.59 \pm 3.04 \ (@@@)$	$1.41 \pm 0.12 (@@@)$	$98.49 \pm 0.22 \ (@@@)$
UAE-3	$118.97 \pm 1.07 (@@@)$	$1.48 \pm 0.09 (@@@)$	98.60±0.11 (@@@)

n=5. "[@]" Denotes: significant difference from the PUHA, ^{@@@@}p < 0.001



Fig. 5 Full XPS spectra (**a**) and F 1 s spectra (**b**) of the drug-loaded cements; the EN concentration extracted (n = 5) from drug-loaded cements; distribution of Ca (purple, **d**-**g**) and P (green, **h**-**k**) elements on the surface scanning by EDS of PUHA, UAE-1, UAE-2 and UAE-3



Fig. 6 Antibacterial performance of PUHA, UAE-1, UAE-2, and UAE-3. (*p < 0.05, **p < 0.01, ***p < 0.001), n = 3. (Red circles: antibacterial zones)

3.5.2 Bacteriostasis Rate (BR)

As shown in Fig. 6c, *S. aureus* was employed to assess the BR of four types of bone cement. The BR test shows that there was rarely any colony left after *S. aureus* was cocultured with the EN-loaded bone cement samples. Nevertheless, approximately 400 ± 35 colonies were observed after *S. aureus* was cocultured with PUHA samples. The greater the BR value, the better the antibacterial effect. The BR could all even reach over 99%, which indicated that all EN-loaded bone cements had the potential of anti-infection to inhibit bacteria proliferation effectively.

EN is a third-generation fluoroquinolones antibiotic, which can inhibit many kinds of bacterial due to its antibacterial mechanism, especially against Gram-positive bacteria (such as *staphylococci* and *streptococci*), those were the main reason causing BAI [25]. In addition, EN can influence the process of DNA replication of bacterial so that EN can kill bacterial rapidly at a low concentration ($\leq 0.8 \ \mu g \cdot m L^{-1}$) [27]. Combined with the aforementioned drug burst and sustained release behavior, it could be seen that the EN-loaded bone cement had the property of quickly killing bacteria in the early stage and preventing BAI infection in the subsequent.

3.6 In Vitro Biocompatibility

3.6.1 Cell Proliferation

In general, the proliferation of BMSCs increased with the extension of culture time shown in Fig. 7a. It was worth

noting that the OD value of UAE-1 and UAE-2 groups were significantly higher than those of the Ctrl group on the 4th and 7th day, indicating that both UAE-1 and UAE-2 could promote the proliferation of BMSCs. However, there was no significant statistical difference between UAE-1 group and UAE-2 group. Compared with the Ctrl group, the OD value of the UAE-3 group did not show a statistically significant difference. It indicated that the three groups of bone cement had no obvious cytotoxicity. The difference between UAE-3 and the other EN-loaded bone cement might relate to the dose of EN. It was reported that low concentrations of EN were beneficial to promote cell proliferation [50], while EN concentrations greater than $32 \,\mu g \cdot m L^{-1}$ [51] could inhibit cell proliferation to a certain extent. In this study, bone cement extracts with different drug loading content were used, among which the concentrations of UAE-1 and UAE-2 were lower than $32 \,\mu \text{g} \cdot \text{mL}^{-1}$, and the concentration of UAE-3 was slightly higher (see Fig. 5c for details). Therefore, compared with UAE-1 and UAE-2, the UAE-3 group did not show the positive effect of promoting cell proliferation. Besides, the live BMSCs morphology was observed with Fluorescence microscope on day 7. In Fig. 7d, BMSCs of UAE-1 and UAE-2 almost covered the entire field of view, while the cell density of the Ctrl and UAE-3 groups was lower. The BMSCs cultured in UAE-3 had a lower cell density and smaller morphology compared to BMSCs cultured in UAE-1 and UAE-2 groups, which was consistent with the result of CCK-8. In conclusion, the drug-loaded cements (UAE-1 and UAE-2 groups) had good biocompatibility, which exhibited great feasibility in the clinic.



Fig.7 CCK-8 (a), ALP (b) and OCN (c) results of BMSCs grown in Ctrl and extraction solutions of UAE-1, UAE-2, and UAE-3, respectively (n=3). Fluorescence microscopy images (d) of BMSCs after

culturing with α -MEM medium and extraction solutions of ENloaded bone cements (*p < 0.05, **p < 0.01, ***p < 0.001)

3.6.2 Cell Differentiation

To evaluate the influence of materials on osteogenic differentiation, ALP and OCN were chosen as indicators of early and late osteogenic differentiation, respectively. As shown in Fig. 7b, c, the expression of ALP and OCN in the UAE-1 and UAE-2 groups was significantly higher than that in the Ctrl group, while there was no significant statistical difference between UAE-1 and UAE-2. However, the expression levels of ALP and OCN in the UAE-3 group were significantly lower to those in the UAE-1 and UAE-2 groups (p < 0.05and p < 0.001). The weaker expression ALP and OCN in UAE-3 was similar with the CCK-8 results. Similar with the cell proliferation, the expression of osteoblast-related protein also has been largely affected by the drug dosage. Due to the concentrations of extracts UAE-1 and UAE-2 were lower than $32 \,\mu g \cdot m L^{-1}$, they showed the positive effect on promoting osteogenic related proteins. However, the concentration of UAE-3 was slightly higher than 32 μ g·mL⁻¹, so it did not show obvious promoting effect on osteogenic proteins expression. Ultimately, both UAE-1 and UAE-2 groups had excellent osteogenic properties. Especially for UAE-2 group, good potential has been expressed for promoting osteogenic differentiation with high antibacterial activity.

4 Conclusions

In this research, the EN-loaded injectable PUHA cements for BAI prevention were synthesized and characterized by physiochemical and biological experiment in vitro. The antibacterial cements showed a good viscosity and injectability by shear-thinning behavior for convenient manipulation. The addition of EN drug speeded up the conversion of monomers and increased the cross-linking and mechanical properties that enhanced the stability of the cured EN-loaded cements, which is benefit to avoid the inflammation reaction caused by residual monomers. All drug-loaded PUHA cements showed a perfect antibacterial property, while the UAE-3 group did not present good biological response of cell proliferation and differentiation because of high drug dose loading. From the above, the UAE-2 is the promising substitute as anti-infection bone cement with suitable physical properties, antibacterial and in vitro biological properties, which in vivo efficiency would be evaluated in next study.

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Declarations

Conflict of interest The authors have no competing interests to declare that are relevant to the content of this article.

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