REVIEW ARTICLE

An in‑depth examination of fre‑related damages in reinforced concrete structures‑A review

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Received: 23 November 2023 / Revised: 24 April 2024 / Accepted: 26 April 2024 / Published online: 7 May 2024 © The Author(s), under exclusive licence to Springer Nature Switzerland AG 2024

Abstract

Ensuring fre safety measures is a fundamental necessity in the design of buildings to safeguard the well-being of their occupants. Fire-related incidents pose a substantial danger to the integrity of reinforced concrete structures, even though concrete itself is inherently noncombustible. The exposure of concrete to high temperatures can lead to the deterioration of its characteristics related to chemical, physical and mechanical aspects. This review paper provides an in-depth examination of fre-related damages in reinforced concrete structures. With a focus on enhancing understanding and mitigation strategies, the paper explores the complexities surrounding fres in these structures, which serve as homes and functional spaces for numerous people over their planned lifespan. Key objectives include investigating how reinforced concrete structures respond post-fre and exploring assessment techniques for high-rise structures afected by fre damage. Through analysis of various damage phases and identifcation parameters, the review ofers insights into post-fre structural behavior. Additionally, the paper presents future suggestions aimed at improving active and operational conditions, thereby contributing to the advancement of fre safety in reinforced concrete structures.

Keywords Assessment techniques · Damage phases · Structural behavior · Operational conditions · Building design · Wellbeing · Noncombustible · High temperatures · Deterioration

1 Introduction

Fire disasters are a prevalent and devastating issue worldwide, particularly in underdeveloped nations. Reinforced concrete (R–C) structures displayed impressive resilience, withstanding intense fames without complete collapse. However, most fre disasters are less severe and allow for recovery [[1\]](#page-9-0). Structures encounter various dangers, including earthquakes, hurricanes, fres, and explosions which can lead to structural damage,

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endangering lives and causing substantial fnancial losses [\[2](#page-9-1)]. Fully developed fres can generate temperatures exceeding 1000°C, deteriorating materials such as steel, wood, and concrete, sometimes resulting in irreversible structural damage. This jeopardizes a building's safety during subsequent hazards [\[3–](#page-9-2)[9\]](#page-9-3). Fires in buildings present a substantial risk to human life and safety, especially during both the pre-fashover and post-fashover stages, where poisonous gases like carbon monoxide and hydrogen cyanide are released. Smoke and hot gases can obscure escape routes and reduce oxygen levels, increasing the risk of toxic inhaling gases and experiencing burns. Property damage due to fres amounts to billions of dollars globally [[10–](#page-9-4)[12](#page-9-5)]. Furthermore, fres contribute to environmental pollution, releasing hazardous chemicals into the environment through smoke, frefghting activities, and water contamination. These results in environmental degradation, impacting air, aquatic, and terrestrial ecosystems to ensure the safety of both individuals and the environment, buildings must be designed to withstand various anticipated risks, including fres [[13\]](#page-9-6). Fire damage signifcantly afects reinforced concrete (R–C) structures, but concrete retains better mechanical properties at high temperatures compared to steel and wood. This implies that fre-damaged concrete buildings may still be usable, provided the residual strength of concrete members is assessed accurately [[14\]](#page-9-7). In conclusion, fre is a major hazard that can degrade (R–C) structures, necessitating thorough assessments of fre damage and appropriate treatment techniques to ensure safety and environmental friendliness throughout a building's design life.

2 The purposes of this examination

This article aims to explore the challenges associated with fres in RC buildings. Most structures are designed to endure for many decades, serving as homes and functional spaces for numerous people throughout their planned lifespan. The primary goals of this research are to enhance our comprehension of how (R–C) structures respond after experiencing a major fre and to delve into the techniques employed to assess high-rise structures after being afected by fre damage. Within this analysis it delves into the various phases of damage that (R–C) structures undergo post-fre, including discussions on various identification parameters. It offers future suggestions pertaining to active and operational conditions (Fig. [1\)](#page-1-0).

3 Deterioration of reinforced concrete structures caused by fre

Damage to RC structures following a fre typically does not result in complete destruction [\[1](#page-9-0)]. However, conducting a post-fre assessment is crucial because the condition of the concrete in these buildings is not uniform throughout the cross-section. The concrete layer near the surface tends to experience the most signifcant deterioration [\[16](#page-9-8)]. Even with the damage and lingering deformations that may require maintenance (R–C) structures generally maintain stability after fre incident. Numerous scholars have conducted research into the performance of fre damaged concrete structures [\[14](#page-9-7)]. When compared to stainless steel and wood structures, reinforced concrete buildings offer impressive natural fire resistance $[3]$ $[3]$. This is a result of the fact that as fre penetrates the member cross-section, the concrete layer acts as insulation for the reinforcement, allowing to ensuring the building's load-bearing capacity remains relatively high both during and after a fre. It is worth noting that high strength concrete is less fre resistant than ordinary concrete, whilst lightweight concrete exhibits greater fre resistance. However, unlike steel and wood, concrete is seldom entirely obliterated in a fre [[17](#page-9-9)]. Exposure to high temperatures leads to the degradation of concrete's thermal, physical, and chemical properties, afecting its mechanical characteristics [[18\]](#page-9-10). The exceptional thermal characteristics of different types of concrete, including normal concrete, high-strength concrete, lightweight concrete,shotcrete, and mortars, exhibit similarities [[19](#page-9-11)]. Reinforced concrete beams and slabs near the ceiling which experience increased exposure to upward convective currents during a fre, making them more susceptible to damage [[20\]](#page-9-12). RC structures, when properly maintained after a fre incident, often retain signifcant residual ability owing to its excellent fre-resistant properties of concrete. Consequently, reusing the structure in the future is frequently feasible. However, heat-induced degradation can result in irreversible loss of strength and serviceability.

Thus, a comprehensive assessment of the remaining capacity becomes crucial to make informed choices regarding future utilization and the need for the restoration of structures damaged by fre [[21](#page-9-14)] (Figs. [2](#page-2-0) and [3](#page-2-1)).

3.1 Evaluating the structural impact of fre on reinforced concrete: assessing residual strength

To accurately assess the infuence impact of a fre on the structural load-bearing capacity and safety of a structure, it is crucial to measure the remaining strength of the concrete. This information can determine the structure's suitability for future use and identify the nature and extent of necessary repairs, or necessitate the demolition of the damaged structure. In cases where structural components have been significantly affected by fire, damages and areas of concrete deterioration are readily visible and identifa-ble [\[15](#page-9-13)]. However, in evaluating less damaged components through the initial visual assessment, observing alterations in the concrete's appearance may not be apparent. For a more comprehensive understanding, laboratory and on-site testing can provide valuable insights into the condition and internal structure of the concrete. Among the various factors to consider after fre damage, concrete compressive strength stands out as one of the most critical. It is crucial to ascertain the thickness of the outer layer of the component where the concrete has been signifcantly impacted to be classifed as damaged [[22\]](#page-9-15). Researchers employ various types of fres, including standard fre, parametric fre, and natural fames to study RC structures. Parametric and natural fres are generally considered more accurate repre-sentations of real fires compared to conventional fires [[23](#page-9-16)]. In the assessment of structures following a fre, particular attention is given to determining the thickness of the outer portions where the concrete has been afected to a point where it should be considered as structurally compromised $[16]$ $[16]$ $[16]$ (Fig. [4\)](#page-3-0).

3.2 Evaluation of structural damage and failure analysis of fre exposure

Heat exposure signifcantly impacts the mechanical and thermal properties of both concrete and steel. This can result in a loss of strength and durability, leading to structural component impairments. The transfer of heat from the freafected area to other parts of the structure occurs through thermal propagation. In both concrete and reinforcing

Fig. 2 Instances of foor slab damage (**a**) detachment of the cover in areas with reinforcing bars (**b**) localized cover defects [[15](#page-9-13)]

Fig. 3 Reinforcement covers loss at the edges (**a**) within the span area (**b**) within the support region

Fig. 4 Change in Color of Heated Concrete: Surface with Visible Aggregates and Exterior of the Concrete Sample [[24](#page-9-24)]

materials, the mechanical properties experience changes, including reductions in compression and tension strength, as well as fuctuations in strain [\[25](#page-9-17)]. Fires, particularly those following earthquakes, pose a signifcant threat to human civilization, with far-reaching consequences. The decline in concrete strength at elevated temperatures is associated with chemical-physical processes, and mechanical damage within the concrete microstructure plays a pivotal role in determining the load-bearing capacity of a building under fre conditions. This aspect has attracted considerable attention [[26\]](#page-9-18). When assessing the load-bearing capacity of structures, concrete exposed to temperatures of 500–600 °C is generally considered to be compromised from a practical standpoint. Even after cooling, concrete's strength typically remains lower than that at room temperature [\[27](#page-9-19)]. Concrete's thermal inertia, especially in large-scale members exposed to fre for an extended duration, allows for prolonged temperature adjustments even after the heat source has been extinguished [[16](#page-9-8)]. Collected experimental data illustrates a connection between concrete temperature and the degradation of relative compressive strength. The reduction in concrete strength at elevated temperatures is afected by multiple factors, such as aggregate type, concrete porosity, member size, duration of heating, and loading conditions [[28\]](#page-9-20). Damage due to fre includes the loss of concrete cover along the longitudinal edges in support areas and local regions at the base of major beams, a consequence of the thermal expansion of reinforcing bars. Subsequent testing with a steel hammer revealed more extensive damage, with primary reinforcing bars exposed due to the removal of concrete cover. The absence of concrete cover, typically 35–45 mm thick, resulted in reduced compacted concrete near the supports. However, concrete in the primary beam areas and stirrups remained undamaged and demonstrated the desired strength class according to tests [\[15](#page-9-13)]. The research

revealed several cases of concrete cover loss on the lower surfaces of precast panels, varying from 3 to 4 cm, due to thermal spalling. In certain instances, steel reinforcement was fully exposed, and some bars became detached from the inner concrete layer [\[15](#page-9-13)]. Consequently, the core of the member is exposed to higher temperatures for an extended period, leading to a reduction in concrete member strength. This process can continue for many hours after the fre has been extinguished. Another signifcant factor is the cooling rate, which results in a non-uniform temperature distribution within the member's cross-section, generating tension known as "self-equilibrating" tension. This tension increases as the cross-section temperature gradient becomes steeper, indicating faster cooling [\[29](#page-9-21)]. When compared to elements that cool naturally in the open air, the reduction in compressive strength can be as much as twice as signifcant [\[16\]](#page-9-8). It is commonly recognized that the favorable efect on concrete strength at high temperatures from compressive stress is equivalent to 20–40% of the strength at room temperature [\[27](#page-9-19)]. Continuous watering during a fre can led to rapid cooling, particularly with low-temperature components in the range of 300–350 °C, which are stifer and more susceptible to stress-induced damage from fast cooling [\[29](#page-9-21)]. Changes in concrete color at various temperature ranges experiments have revealed that higher concrete strength leads to increased temperature rises because of greater density and thermal conductivity, facilitating faster heat transfer. These factors also infuence the development of a moisture clog zone, resulting in temperature distribution variations across wall thickness, dependent on the heated region and concrete strength [\[30](#page-9-22)]. Additionally, the strength of steel reinforcement decreases as temperature rises. Concrete spalling plays a crucial role in reducing fre resistance when exposed to high temperatures [[31](#page-9-23)]. The accumulation of pores during heating contributes to this breakdown, and high-strength

concrete is considered more susceptible to pressure build-up due to its increased brittleness compared to ordinary concrete, resulting in reduced fre resistance. Codes of practice dictate that temperature increases can lead to weakening of strength in both steel and concrete, contingent on aggregate type and steel grade [[31\]](#page-9-23). Numerous concrete testing techniques in buildings are currently in use, with previous studies providing comprehensive insights into concrete spalling [\[32,](#page-9-25) [33\]](#page-9-26) (Fig. [5](#page-4-0)).

3.3 Petrographic analysis for evaluating fre‑induced structural damage

Petrographic studies are essential for recognizing distinct minerals, rock textures, grain sizes, and the relative or quantitative proportions of diferent components in geological materials. Additionally, they provide insights into the physicochemical characteristics of stones and their stage of degradation, alongside precise typology [[35](#page-9-27)]. Petrographic examinations are extensively employed to assess the extent of fre damage in reinforced concrete (RC) components, enabling a direct examination of microcracking and mineralogical alterations. Moreover, fre-damaged masonry structures constructed with stone, brick, and mortar can also undergo petrographic analysis, which aids in the precise identifcation of damaged geological materials. This approach leads to cost savings and enhances safety assurance during construction repairs [[36](#page-9-28)]. In a separate study conducted by researchers conducted core strength tests and employed optical microscopy to investigate fre-damaged concrete. Samples were collected from concrete slabs exposed to heat, and laser microscopy was used to examine aggregate morphology, cement paste, cracks, and micro-voids. By evaluating the physical state of the concrete sample and conducting microscopic inspections, petrographers could reasonably estimate the minimum exposure temperature and its relative impact on the depth of concrete damage [[37\]](#page-9-29). Petrographic examination was instrumental in confrming the presence of early-stage alkali-silica reaction (ASR) damage and identifying distinct micro-cracking patterns in specimens containing reactive fne aggregate (RFA) and reactive coarse aggregate (RCA). This observation could potentially explain discrepancies in linear resonance data. Notably, the results of nonlinear resonance tests on both RCA and RFA specimens effectively detected the onset of ASR damage and exhibited a signifcant correlation with ASR expansion across various mix designs. This underscores the high sensitivity and utility of the nonlinear resonance test in quantifying ASR damage in concrete specimens without requiring a baseline measurement [\[38](#page-9-30)]. In a different research effort a comprehensive analysis was conducted on the physical and chemical properties of historical concrete buildings in the Dominican Republic, encompassing their usage and construction between 1917 and 1955. These structures, designed and built by American and Dominican engineers, represent an entire generation of construction history. The study included a detailed examination of the concrete utilized during that period. Various analytical techniques were employed, including X-ray Difraction (XRD), Scanning Electron Microscope with Energy-Dispersive X-ray Spectroscopy (SEM–EDS), X-ray Fluorescence (XRF), Mercury Intrusion Porosimetry (MIP), petrographic inspection, and Visual Testing (VT). The fndings revealed that concrete composition evolved over time. Most of the samples exhibited typical peaks of crystalline phases, including quartz, albite, and calcite, albeit in varying proportions [[39\]](#page-9-31). Petrographic analysis, conducted using the Carl Zeiss Jenapol petrographic microscope, involves examining a thin rock sheet,

Fig. 5 Deterioration of precast deck panels due to concrete spalling when subjected to elevated temperature [[34](#page-9-32)]

typically around 30 µm thick (at such thin thicknesses, rocks become transparent). This technique enables direct scrutiny of a rock's mineralogy, texture, and composition based on its optical characteristics. However, it may have limitations in detecting extremely small minerals and is often complemented by microscopic inspection and X-ray difraction. The examinations adhere to the ASTM C-856 standard and provide insights into factors such as compaction degree, paste matrix homogeneity, and cement dispersion. Chemical analysis results are integrated into the description of each sample, facilitating comparative analysis. For instance, Sample T1 comprises uniform-sized grains in various shades (cream, dark grey, light grey) within a light grey matrix. This sample features numerous altered quartz and feldspar crystals, some displaying mirmechitic textures indicative of breakdown from acidic igneous rocks. The aggregates appear semi-triangular and spherical, ranging in size from four to five millimeters down to less than 100 µm. Notably, there are no indications of alkali-silica reaction halos or deformation fractures, as illustrated in Fig. [6](#page-5-0) [[40\]](#page-9-33). Finally, the exploration of new deep learning methods for concrete petrographic analysis was undertaken by [[41](#page-10-0)]. The study demonstrated the efectiveness of convolutional neural networks (CNN) in segmenting concrete images without relying on phenolphthalein to color the cement paste. In summary, CNNs have the potential to serve as a valuable tool for concrete petrographic analysis, contributing to improved machinebased visual comprehension [[41](#page-10-0)] (Tables [1](#page-5-1) and [2](#page-6-0)).

3.4 Defciencies in frefghting systems for reinforced concrete (rc) structures

Despite the advancements in fre safety technology and prevention methods, fre incidents remain a leading cause of fatalities and property damage in commercial structures worldwide. Extensive research suggests that substandard materials and faulty electrical equipment are predominant

Temperature Range $(^{\circ}C)$	Celsius	Around 300 degrees $300-600$ °C degrees Celsius	$600 - 950$ (°C) degrees Celsius	Above 950 (°C) degrees Celsius
Color	Typical	Pink to red	Whitish grey	Polish
Aspect	Typical	Surface cracking, crazing, aggre- gate spalling	The exposure of reinforced steel as a result of spalling and its persistent presence	Severe spalling
State	Typical	Structurally sound, yet strength might be compromised	Fragile	Intense

Table 2 Variations in concrete structure color across temperature ranges [[24](#page-9-24)]

factors contributing to these disasters in commercial buildings [\[43](#page-10-2)]. Even within confned spaces, there can be signifcant temperature variations during a fre, as indicated by an analysis of compartment fre data [[44\]](#page-10-3). Electrical faults are identifed as the primary cause of fres by 42% of respondents, with 20.5% attributing fres to electrical faults and resident negligence. Ensuring that high-level building personnel are well-versed in fre safety and defense systems could enhance overall safety. Key fre safety components, such as the fre detection system, are often non-operational due to irregular testing and maintenance. While fre extinguishers are available and functional, residents lack awareness of their proper use. Each floor has clear evacuation instructions leading to stairwells in case of a fre, and fre shovels are accessible on each level for frefghters to access water from the main supply. Unfortunately, high maintenance costs have led to the disconnection of these systems. The architect specifed fre safety measures during construction, but these plans were not consistently implemented or maintained, rendering them inefective [\[45\]](#page-10-4).

3.5 Fire damage remediation measures for reinforced concrete structures

Combustion, commonly referred to as fre, constitutes a chemical process where a substance reacts with oxygen from the air, releasing energy in the form of heat when activated by high temperature itself. Fire, in any structure, relies on a consistent supply of heat, fuel, and oxygen. Therefore, attention must be directed towards these three elements a constant source of oxygen from the environment, a heat source, and combustible materials. Incidents of fre in constructed environments are typically unexpected and unplanned events, often caused by human errors or the use of faulty electrical equipment [\[46](#page-10-5)]. Recent developments in structural engineering have led to a new design philosophy known as structural fre engineering. Fire safety design incorporates both active and passive fre prevention technologies. Active systems, like fre detectors, smoke control systems, and sprinklers, activate automatically when a fre starts. Passive systems, on the other hand, include building code limitations, barriers, fre-resistant windows, and construction materials designed to delay or minimize temperature increases in structural elements [\[31\]](#page-9-23). A crucial element in comprehensive fre protection planning for tall structures is a thorough understanding of fre behavior. Without taking the necessary measures, a fre safety strategy cannot be adequately optimized and made robust. Insights from experiments like the Cardington tests and advancements in fnite element modeling have shown that structural systems need to be comprehensively assessed to understand their performance under fre conditions [[47\]](#page-10-6). Fire disaster preparedness involves actions to protect property, limit damage and disruption during and after a disaster, and improve life safety in case of a fre disaster. Common actions associated with fre disaster preparedness include establishing planning procedures for readiness, formulating disaster response plans, stockpiling resources for efective response, and building capabilities and competencies for disaster-related tasks. The training and preparedness of fre disaster managers play a vital role in their efectiveness during and after a fre disaster. Preparedness eforts also ensure that necessary resources and equipment are available and that people are trained to use them efectively [[48\]](#page-10-7). Conducting timely fre safety assessments are crucial to preventing high-rise building fres [[49\]](#page-10-8). Eleven parametric modules for fre safety analysis and risk assessment in buildings have been identifed, and their use can enhance national fre safety engineering practices in construction processes [[50](#page-10-9)]. Designers and property owners must improve their fre safety procedures as highlighted by these fndings. Strict adherence to fre safety measures outlined in building regulations is imperative in high-rise structure design [\[45](#page-10-4)]. Various techniques can be employed for structural repairs, including cast-in-place solutions, shotcrete, trowel-applied mortars, and injecting epoxy resins under pressure into prominent cracks to bond structures in situ. Regardless of the chosen repair technique, the goal is to restore the reinforced concrete asset to its original design intent.To address defciencies in frefghting systems in reinforced concrete structures, remedial measures related to fre safety are necessary. The building's design should facilitate easy access for frefghting equipment in the event of a fre. The construction should be designed in a way that inhibits the spread of fre between foors, with clear signage for escape routes on each foor. Walls should be constructed using poor heatconducting materials like bricks to impede fre penetration.

The building should also incorporate large openings that can serve as ventilation outlets during a fre, and windows should provide natural light to staircases [[49–](#page-10-8)[54\]](#page-10-10).

Spalling leads to a reduction in an element's load-bearing capacity and loss of section. High-temperature concrete spalling occurs in various forms, ranging from total obliteration to the explosive dislodging of concrete pieces of varying thickness, ranging from millimeters to centimeters. In all cases, spalling exposes the reinforcement steel, which is susceptible to high temperatures. The phenomenon of concrete spalling is particularly intriguing in fre conditions and has been extensively described in the literature through experimental studies [[55](#page-10-11)[–57\]](#page-10-12). When concrete is heated, water is carried into cooler areas, leading to the creation of a completely saturated layer known as a moisture clog. This zone is marked due to low permeability and acts as a barrier impervious to gases(refer to Fig. [6](#page-5-0)). Simultaneously, the temperature increase causes the water to turn into steam, unable to escape due to the presence of the moisture clog. Consequently, this situation leads to the buildup of internal pressure [\[58\]](#page-10-13). Pore pressure serves solely as a catalyst for the spalling phenomenon. After the pore pressure initiates the crack, the subsequent growth of the crack and the explosive spalling that occurs as a result are determined by stresses related to temperature variations [[59](#page-10-14)].

3.6 Fire‑induced spalling in reinforced concrete structures

Spalling, the detachment of concrete layers due to high temperatures, poses a signifcant challenge to the structural integrity and fre resistance of various constructions like buildings, parking structures, and tunnels. This study delves into a simplifed method, considering temperatures exceeding 400°C, to assess the thermo-mechanical response of reinforced concrete (RC) slabs under severe fre conditions. Utilizing numerical analysis via SAFIR software, the research systematically evaluates spalling risks by removing concrete layers based on predefned criteria. The comparison of numerical predictions with real-world experiments validates the efficacy of this method in accurately anticipating concrete spalling behavior during hydrocarbon fre exposure.

Moreover, the research underscores the vital importance of factoring in spalling when calculating fre resistance in concrete structures. Despite the complexity arising from multiple infuencing factors, the layering technique emerges as a valuable tool for forecasting RC slab behavior under fre scenarios, eliminating the need for expensive experimental tests. The study achieves satisfactory alignment between numerical simulations and experimental measurements, particularly in terms of temperature distribution and mid-span defections in simply supported RC slabs exposed to sustained gravity and fre loading. Furthermore, the study investigates the ramifcations of thermal spalling on the fre resistance of RC structures postseismic events, employing nonlinear dynamic analyses to evaluate structural damage. It highlights the signifcant role of reinforcement confgurations, including one-layer and two-layer distributions, in mitigating collapse risks under post-earthquake fre conditions. Additionally, the review addresses challenges posed by ultra-high performance concrete (UHPC) in fre-induced spalling, stressing the necessity for robust modeling methods and mitigation strategies to ensure structural safety. The paper also addresses the vulnerability of reinforced high-strength concrete (RHSC) walls to spalling under standard fre conditions. Through experimental trials, it identifes key factors infuencing spalling behavior such as concrete strength, axial load levels, thickness, and reinforcement confgurations. The fndings underscore the signifcance of reducing wall thickness and optimizing reinforcement arrangements to bolster fre resistance in RHSC walls. In summary, this study offers valuable insights into the complexities of fireinduced spalling in concrete structures, providing guidance for enhancing design standards and mitigating fre hazards across various construction applications [[60–](#page-10-15)[69](#page-10-16)]

3.7 The cooling behavior of reinforced concrete elements

Recent literature predominantly focuses on the heating phase of concrete columns concerning potential delayed failure, coupled with a linear descending cooling phase. This area of research has only recently gained attention, particularly revolving around a parametric temperature–time curve, which includes a linear cooling regime as an initial approximation suitable for design purposes. A simple linear relationship between the burn-out resistances of a column subjected to a parametric fre and the ISO fre rating time, particularly applicable to heavily loaded columns. However, it is acknowledged that the linear cooling curve associated with the parametric fre does not adhere to Newton's fundamental law of cooling in transient situations, rendering it non-natural. This underscores the importance of investigating alternative cooling regimes with slopes or shapes that may better refect reality. Moreover, the signifcance of load levels warrants careful examination, as not all columns in real buildings is heavily loaded, leading to variations in dimensions.

To delve deeper into these aspects, a study was conducted involving heating a selected column on four, three, or two sides to examine the effects of cooling regimes and load levels. A combination of thermal loads from the parametric fre, the more natural cooling BFD curve, and a heavily forced,

very slow cooling regime was implemented. The material model incorporated a proposed strength loss of 10% (EN 1994–1-2, 2005), verifed against a 20% loss observed in various experiments from literature. Additionally, explicit formulation of creep was employed to account for timedependent strength loss.

The relevance of this research lies in assessing the residual capacity of concrete structures in post-fre scenarios, which is crucial for determining their load-bearing capacity or post-fre fre rating. Both aspects are essential for evaluating the structural reliability for further use after exposure to fre. It was demonstrated that diferences in cooling regimes, load levels, and the number of exposed sides can lead to failure and signifcantly infuence the post-fre bearing capacity.

Experimental results for "NSC" regular concrete columns subjected to periodic fre with axial load were provided. The aim was to investigate the behavior of reinforced concrete columns under experimental conditions when exposed to fre fame with axial loading. Compared to control samples, the columns experienced a reduction of approximately 82.38%, 77.78%, and 72.80% in their bearing capacity after exposure to periodic burning at 400 °C for one cycle, two cycles, and four cycles, respectively. Moreover, as the number of fre cycles increased, the residual bearing capacity dropped dramatically [\[70](#page-10-17)[–82](#page-10-18)].

3.8 Future studies and suggestions

Enhancing fre safety in reinforced concrete (R–C) structures involves advancing monitoring systems, exploring fire-resistant materials, refining simulation techniques, developing comprehensive protection strategies, addressing multi-hazard resilience, improving building codes, and fostering interdisciplinary collaboration. Tailored monitoring systems for R–C structures facilitate real-time data acquisition during and after fres, aiding accurate post-fre assessments. Research into fre-resistant materials is pivotal for R–C structures to withstand high temperatures while preserving integrity. Enhanced simulation techniques guide proactive safety measures and post-fre evaluations. Developing holistic fre protection strategies, encompassing both passive and active measures, is imperative. Multi-hazard resilience, including seismic and extreme weather events, must be integrated into these strategies. Continuous refnement of building codes ensures adaptability to evolving challenges. Interdisciplinary collaboration drives innovation and comprehensive solutions. Prioritizing these endeavors enhances resilience and sustainability in built environments. Implementing appropriate repair techniques for rehabilitating fre-damaged concrete structures further strengthens safety measures.

4 Conclusions

This study primarily focused on conducting a comprehensive assessment of the damage incurred, post-fre structural responses, and the identifcation of defciencies within frefghting systems specifcally concerning reinforced concrete (RC) structures following severe fre incidents.

The core information essential for evaluating the structural integrity of fire-damaged buildings was precisely examined. This encompassed a wide array of critical factors, including the classifcation of building elements and materials, pinpointing the origins of fre ignition, assessing exposure conditions, gathering necessary data, comprehending the expected fre temperatures, and considering the duration of the fre event. Furthermore, the study underscored the signifcant challenges posed by limited fre prevention equipment and various contributing factors, all of which can potentially culminate in a heightened risk of fre ignition. These fndings strongly advocate for a fundamental enhancement of fre safety measures. Design considerations emerged as a key facet of the study's insights. It highlighted the pivotal role of both designers and property owners in the realm of fre safety procedures. A particular emphasis was placed on high-rise structures, where strict adherence to building regulations governing fre safety is not just advisable but crucial. Moreover, the research incorporated a thorough review of past studies conducted over the last decade, complemented by relevant case studies. This comprehensive approach revealed the prevalence of surveys and case studies centered on fre damage in RC structures. Among the prominent fndings, it was noted that electrical issues, faulty fre detection systems, insufficient firefighting equipment, and impediments in emergency exit routes were recurrent causes of fre damage in RC structures. In light of these fndings, the study advocated for further, detailed research endeavors aimed at controlling fre ignition and addressing the gamut of fre-related concerns specifcally in high-rise buildings. Despite the ongoing efforts of building owners to preempt fres, the study observed that fre prevention remains a persistent challenge, often rooted in human decision-making processes, especially in the selection of building materials. Consequently, the study proposed a series of operational solutions as recommendations to fortify fre safety in RC high-rise buildings. Collectively, these recommendations serve as a comprehensive strategy to enhance fre safety and mitigate the impact of fres in RC high-rise structures.

Author's contribution All authors contributed to the study conception and design. Material preparation, data collection and analysis were performed by G.B. and N.R. The draft of the manuscript was written by G.B. and all authors commented on previous versions of the manuscript. S.R.C. verifed the results section and verifed entire manuscript. All authors read and approved the fnal manuscript.

Funding The authors declare that no funds, grants, or other support were received during the preparation of this manuscript.

Data availability Not applicable.

Declarations

Consent to participate Not applicable.

Consent for publication Not applicable.

Competing interests The authors have no relevant fnancial or nonfnancial interests to disclose.

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