



# A preliminary study of fuel mixtures of industrial sludge, bottom ash, and municipal solid waste for co-firing in coal boilers

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**Abstract** Wastewater treatment in the textile factory produces sludge classified as toxic and hazardous waste, which is harmful if left untreated. This study assessed the potential of utilizing sludge from a textile factory in Bandung Regency, Indonesia, as a co-firing fuel in coal boiler furnaces employed in the factory. The study aimed to improve the performance of sludge to meet the required standards for fuel substitution. The analysis involved proximate, ultimate, and ash element tests with correlation of the results with calorific values. The sludge was mixed with coal bottom ash produced by the textile factory and biomass (local refuse-derived fuel) at different ratios. An environmental impact analysis was also carried out with the toxicity characteristic leaching procedure (TCLP) and air emission testing. The results showed that the sludge did not meet the fuel substitution requirements if it was used as a single material. However, the sludge could be used as a substitute for coal by mixing it with bottom ash and biomass; the optimum composition was a ratio of 20% sludge, 40% bottom ash, and 40% biomass by weight. TCLP and air emission test results showed that this mixture was safe for human health and the environment and met the fuel substitution requirements. This study provides a practical solution to the problem of reducing toxic and hazardous waste.

**Keywords** Air emission · Biomass · Calorific value · Hazardous waste · Toxic waste

## 1 Introduction

Textile manufacturing is one of the main global industries responsible for producing wastewater that pollutes the environment. The textile production process uses large amounts of water that is eventually discharged as wastewater, which requires treatment to remove pollutants before being released into the environment. Textile wastewater harms the environment and human health because it contains complex pollutants (Haryono et al. 2018). The pollutant material of textile wastewater generally comes from synthetic dyes using. Synthetic dyes often used are rhodamine B and azo that are not easy to degrade. Rhodamine B contains heavy metals (Mahatmanti et al. 2019), and dyes containing azo groups are also suspected to be carcinogenic (Eskak and Salma 2020), which can produce chloro-aniline (Suhendra and Kardena 2013). Because it is difficult to degrade, textile wastewater requires treatment that combines physical–chemical methods with biological methods to get a better result (Valerie et al. 2018).

However, the various methods applied to treat wastewater still produce sludge that requires rigorous handling. So the utilization of sludge is increasingly receiving attention. Previous studies have utilized sludge from various types of wastewaters. The high organic content in the sludge resulting from biological treatment has been used as an alternative to adding nutrients on ultisol soils (Pandapotan et al. 2017) and as an alternative energy source (Kurniawan et al. 2018) or solid biomass fuel (Awere et al. 2020). In particular, sludge of textile wastewater has also been used as constituent building materials (Anwar et al. 2018) or a mixture of bricks (Arbunowo et al. 2019). The combustion process of constituent building materials or bricks can inhibit the movement of heavy metals, oxidize organic

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materials completely, and eliminate pathogens of sludge (Arbunowo et al. 2019).

According to Indonesian regulation, textile industry sludge is classified as toxic and hazardous waste, which makes it an obligation for every producer to manage and utilize the waste. The sludge disposal techniques commonly used are incineration and landfilling (Anwar et al. 2018). These methods need optimization according to resource availability to reduce costs in the context of global competition. The Indonesian government has encouraged the management and utilization of industrial sludge without specifying any methods to do so. One technology that is rapidly developing is the use of toxic (Chuah et al. 2016a) and hazardous waste (Skaggs et al. 2018) as alternative fuels. Based on the government's recommendations, utilization of sludge as a direct fuel source in boilers to generate thermal energy is an appropriate application. Many studies have utilized biomass as an energy alternative, such as sawdust and oak wood mixed plastic waste (Zannikos et al. 2013); agriculture waste (Ribeiro and Dalmolin 2020); firewood and charcoal (Oladeji 2015); solid waste (Igoni and Harry 2017; Nayono 2009); bamboo species (Marafon et al. 2019), but investigations using wastewater sludge as an alternative fuel are still scarce (Anwar et al. 2018; Arbunowo et al. 2019; Putri and Sukandar 2013). Research on the utilizing of various biomass wastes as an energy alternative has been still developing.

The wastewater treatment plant (WWTP) from a textile factory in the Bandung Regency produces of sludge approximately  $3 \text{ t.day}^{-1}$ . This factory also operates three boilers of different types to supply energy for the textile production process, which produce bottom ash approximately  $650 \text{ kg.day}^{-1}$ . According to Indonesian regulation, bottom ash is also classified as toxic and hazardous waste. Currently, 10–30% by weight of the global production of fly ash and bottom ash (FABA) is recycled or reprocessed for raw material. So the integrated utilization of these wastes has significant potential for both saving energy and reducing greenhouse gas emissions (Damayanti 2018). The recycling of bottom ash can also reduce the factory's cost burden in toxic and hazardous waste management. However, the utilization of toxic and hazardous waste, such as sludge and bottom ash, requires adherence to strict regulatory standards.

In addition to the problem of toxic and hazardous waste, governments and researchers are also concerned about municipal solid waste (MSW), particularly in developing countries (Santos et al. 2019). The MSW generation has caused air, water, and soil pollution without treatment (Das et al. 2019). Nearly 33% by weight of MSW from cities worldwide goes to dump sites without proper treatment (Haraguchi et al. 2019). In Indonesia, the rate of MSW

generation is not proportional to the speed in its management (Mahyudin 2017). Related to contributions to global warming from solid waste management (Maalouf and El-Fadel 2019), many countries face this MSW challenge by developing technology (Xu et al. 2016).

The management of MSW has become an increasingly complex problem with population growth and changes in people's lifestyles. Consequently, waste processing technology has not kept pace with MSW generation, and the final destination of much of the solid waste is landfill. At the same time, finding suitable sites for landfill construction is challenging (Utomo et al. 2017) because they must have specific characteristics (Rugatiri 2021). To overcome these problems, many countries have adopted the 3R (reduce, reuse, and recycle) concept as the first principles of solid waste management (Peprah et al. 2015; Rugatiri 2021; Somneuk 2020). The 3R principles have progressed to 4R (reduce, reuse, recycle, and recover). The term "recover" refers to the extraction of valuable materials from solid waste or to the transformation of waste to a material of value (Hannon and Zaman 2018; Popli et al. 2017). The concept of solid waste management has further evolved to 5R (4R + refuse). The term "refuse" means reducing plastic waste and is a guiding standard for consumers, industry, and authorities to control the impact of plastic waste on health and the environment (Hussein et al. 2021; Kumar et al. 2021). The government of Indonesia also encourages the business sector to support solid waste management under the 5R principles of 3R + replace and replant, especially for food, beverages, or other industry-generated organic waste. In this case, the term "replace" is concerned with replacing hazardous material as well as plastics with eco-friendly material, and "replant" refers to the restoration of degraded land using organic waste or using organic waste as growing media (Prabawanti 2021; Wirahadi 2016).

The 3R principles are fundamental to MSW management because the cost of collecting the waste can reach 40–60% of the total landfill management costs. At the same time, in situ solid waste treatment can save money and reduce  $\text{CO}_2$  gas emissions from transport vehicles (Jouhara et al. 2017). The population of the Bandung metropolitan area is 8,679,973 (BPS West Java Province 2020). The estimate of urban solid waste per capita in Indonesia is  $0.65 \text{ kg.d}^{-1}$  or  $2.75 \text{ L.d}^{-1}$  (Yusbendar et al. 2020). So the solid waste generated in the Bandung Metropolitan is estimated at  $5.64 \times 10^6 \text{ kg.d}^{-1}$  or  $23.87 \times 10^6 \text{ L.d}^{-1}$ . The utilization of MSW makes a significant contribution if it is supported by comprehensive policies or regulations in all regions to reduce its generation and solve land use problems. One solution is to treat MSW in situ at the temporary place storage (TPS) to generate refuse-derived fuel (RDF),

which can then be used as a substitute fuel for co-firing with coal.

Many initiatives have been carried out to create renewable energy alternative. They were different on material using and its direct application. Previous study created a briquette as an alternative fuel. The briquette of mixture 60 wt% of bottoms ash and 40 wt.% of biomass (RDF) was applied as co-firing. Its trial burning test showed increase in the efficiency combustion in steam boiler (Marganingrum et al. 2000), and the air emission was below the required standard (Nurhayati et al. 2021). From the observations at the same study site, it was found that the availability of wastewater sludge is much greater than bottom ash. This study aims to increase the potential value of the textile factory's waste sludge as a fuel by combining it with coal bottom ash and RDF. This sludge may be categorized as biomass so that it or RDF has the potential to replace other biomass resources such as agricultural residual or wood as a future fuel alternative. Obviously, the sludge addition to the first briquettes composition needs to be re-evaluated. This study used an existing formula to evaluate the characteristics and gross calorific value (GCV) of the materials within the constraints of the regulatory limits to their use as fuel.

## 2 Materials and methods

### 2.1 Sources of fuel material

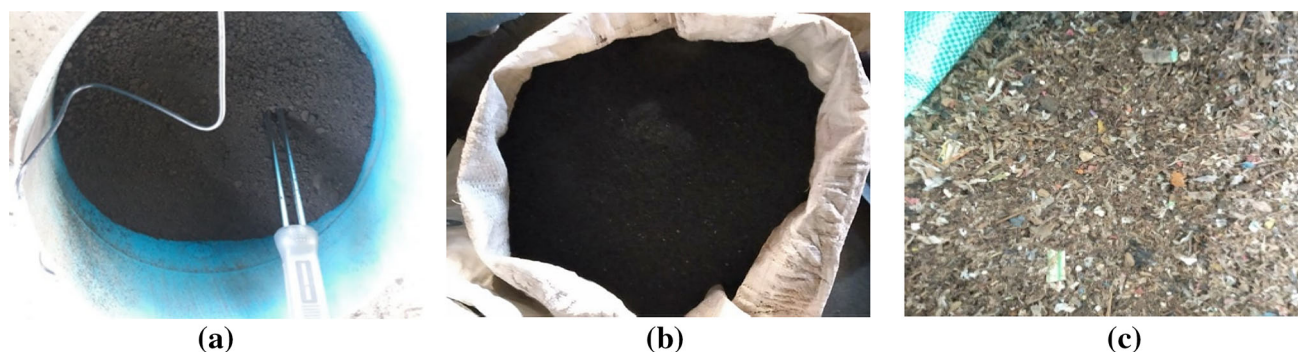
This study used sludge, bottom ash, and biomass. The sludge samples were obtained from the WWTP of a textile factory in Bandung Regency. Bottom ash samples were obtained from the coal-burning boiler of the same factory. Biomass used in this study was biomass produced from urban MSW processed in the Bandung area. The biomass was produced by dry fermentation of MSW using an aerobic bio-drying method called *peuyemisasi* in the local

language (Marganingrum et al. 2020). Figure 1 shows the material used in this study.

### 2.2 Parameters and methods of analysis

This study analyzed the characteristics of sludge, bottom ash, and biomass before and after mixing them following the applicable regulations for the optimal composition of the mixture as a fuel. The analyses were conducted according to the American Society for Testing and Materials (ASTM) International test standards. The characteristics of the materials as fuel were tested using proximate, ultimate, and calorific value tests (Chuah et al. 2016b). Proximate analysis determined the percentages of moisture, ash, volatile matter (VM), and fixed carbon (FC) on a dry weight basis. The standard methods used for the analysis were ASTM D3173 for moisture, ASTM D3174 for ash, ASTM D3175 for VM, and ASTM D3172 for FC. Ultimate analysis determined the composition of the material in terms of the percentage of carbon (C), hydrogen (H), nitrogen (N), oxygen (O), and sulfur (S) by weight. The standard methods used for the ultimate analysis were ASTM D5373 for C, H, N, and O and ASTM D4239 for S. Proximate and ultimate analyses used the LECO 701 apparatus. To obtain the calorific value, a bomb calorimeter was used with the standard method of ASTM D5865. This study also analyzed the chlorine content of the material using Eschka's mixture according to ISO 587. The proximate, ultimate, and calorific values and the chlorine content of the material were obtained at the Tekmira Laboratory of the Ministry of Energy and Mineral Resources of Indonesia.

To obtain the sulfur content in sludge, this study measured the wastewater sulfate content by tracing its source to control the total sulfur content of the sludge—water samples were taken at each stage of the wastewater treatment process. The sulfate concentration was determined by the turbidimetric method at a wavelength of 420 nm using an ultraviolet–visible spectrophotometer (UV-PharmaSpec



**Fig. 1** The fuel material used in this study include **a** sludge, **b** bottom ash, and **c** biomass (RDF)

1700) at the LIPI Laboratory of the Research Center for Geotechnology.

This study also analyzed the heavy metal content of the material and applied the toxicity characteristic leaching procedure (TCLP) to determine whether the material complied with applicable regulations. It also ensured that the materials used as fuel substitutes in this study were safe for human health and the environment. TCLP determines the level of toxicity of waste materials and classifies them as hazardous or not (Agustini et al. 2017). TCLP testing conducted by refer to US. EPA, SW.846 Test Method 1311 only for heavy metal content. The closed acid digestion method, also known as microwave digestion, was used to determine the metal content of the material. The products of the digestion were measured using an atomic absorption spectrophotometer (AA-7000). Heavy metal analysis and TCLP were conducted only for sludge and bottom ash at the Tekmira Laboratory of the Ministry of Energy and Natural Resources, Indonesia. These tests were not performed for biomass from MSW as it is not categorized as toxic and hazardous waste.

### 2.3 The effects of proximate compounds and ultimate elements on calorific value

The GCV, sometimes termed higher heating value (HHV), and the composition of solid fuels are essential properties that define their energy content and determine their clean and efficient use. The ultimate analysis of fuels provides a variety of correlations for predicting HHV. A few HHV correlations from proximate analysis have appeared in the solid fuel literature in the past, but they were focused on one fuel or were dependent on the country of origin. The formula based on ultimate analysis is generally more accurate than that based on proximate analysis. The quality of the correlations based on chemical analysis was found to be very poor because of the variation in the properties of components and the chemical composition of biomass. As a preliminary study, this work introduces a general correlation based on the proximate analysis of solid fuels using direct laboratory tests and only a few data points and further experimental data points. The entire spectrum of solid carbonaceous materials like sludge, bottom ash, and biomass was considered based on proximate analysis and calculated with the coal tests of ASTM D5865, although they were not all coal-based materials. To determine the accuracy of the test, this study used a proximate correlation formula (Özyüğüran et al. 2018; Parikh et al. 2005):

$$\text{HHV} = 0.3536\text{FC} + 0.1559\text{VM} - 0.0078\text{Ash} \text{ (Mjkg}^{-1}\text{)} \quad (1)$$

where fixed carbon (FC) was 1.0–91.5%, volatile matter (VM) was 0.92–90.6%, and ash was 0.12–77.7% as the analyzed content in wt.% on a dry basis.

The average absolute error of this correlation was 3.74% and the bias error was 0.12% for the measured value of HHV, which was much less than that of previous correlations of a similar kind. The advantage of this correlation is the ability to compute HHV of any fuel simply from its proximate analysis to provide a valuable tool for modeling combustion, gasification, and pyrolysis processes (Olatunji et al. 2019; Parikh et al. 2005). By definition, sludge and biomass were categorized as biomass residue resources. The formula for biomass materials was generated from ultimate analyses, with high S content, and the ultimate formula was simplified (Toscano and Foppa Pedretti 2009; Yaman 2004) as follows:

$$\text{GCV} = 430.2 \text{ C} - 186.7 \text{ H} - 127.4 \text{ N} + 178.6 \text{ S} + 184.2 \text{ O} - 2,379.9 \text{ (Mj kg}^{-1}\text{)} \quad (2)$$

where carbon (C), hydrogen (H), nitrogen (N), oxygen (O), and sulfur (S) were analyzed as wt.% on a dry basis and 2379.9 was a correction factor.

## 3 Results and discussion

The sludge from the textile industry's WWTP is categorized as a general specific source of the toxic and hazardous waste category 2 with the waste code B322-3. As a by-product of the textile industry's wastewater treatment process, sludge poses problems for handling and storage. The Indonesian government regulates the use of toxic and hazardous waste, in either solid or liquid phase, as a substitute for energy sources under the following conditions: (1) it can be categorized as waste B3, which, when burned, produces heat and energy; (2) it is able to reduce primary fuel consumption, and (3) it meets environmental standards according to the provisions of the legislation. The other specifications that are regulated are shown in Table 1. Generally, sludge has a moisture content of more than 80% by weight. Reducing the moisture content is essential during its conversion into usable energy (Ali and Akilli 2019). An appropriate test is needed to reduce the water content in sludge to apply cost-effective drying technology, especially in developing countries like Indonesia. Sun drying is an inexpensive option (Awere et al. 2020), although it is a time-consuming process. In this study, the textile factory used a belt press to reduce the sludge water content until under 20% by weight before keeping it in temporary place storage (TPS). The maximum period for storing sludge in TPS is 90 days (government regulation

**Table 1** The standards for toxic and hazardous waste material used as a fuel substitution in Indonesia

Parameter	Standard
Calorific value	$\geq 2,500 \text{ kcal.kg}^{-1}$ (dry weight) or $10.7 \text{ Mj.kg}^{-1}$ $\geq 1,000 \text{ kcal.kg}^{-1}$ (wet weight) or $4.2 \text{ Mj.kg}^{-1}$
The total organic content of halogen/TOX (amount of organic chlorine and fluorine)	Maximum of 2% (dry weight)
Sulfur content	Maximum of 1% (dry weight)

Source: The Ministry of Environmental Regulation of the Republic of Indonesia, regulation number 18 of 2020

number 101 of 2014 article 28). This study aims to reduce sludge waste to avoid its overaccumulation in storage.

### 3.1 Characterization of sludge, bottom ash, and biomass as a single material

Table 2 shows the proximate, ultimate, and calorific values of sludge, bottom ash, and biomass used in this study. Based on these analyses, none of the materials met the calorific requirement. Sludge's sulfur content did not conform to the upper limit requirement. The analyzed sludge sample had an average total sulfur content of 1.91% by weight or almost double the mandatory requirement ( $\leq 1 \text{ wt}\%$ ). Several attempts must be made to reduce the sulfur content in sludge before it can be used as a fuel substitute. The sulfur content of sludge is influenced by the WWTP processing chemicals as well as the characteristics of the treated liquid waste. Low efficiency of chemical use can result in a significant pollution hazard (Anwar et al. 2018).

Figure 2 provides a flowchart of the waste treatment process until sludge formation and the points at which wastewater was sampled. And Fig. 3 shows the results of the test for the sulfate content in the wastewater. The textile

factory in this study used aluminum sulfate [ $\text{Al}_2(\text{SO}_4)_3$ ] as a coagulant. Coagulation plays an essential role in the water treatment process by significantly reducing turbidity and colloidal particles (1–200  $\mu\text{m}$  in size) in suspension (Naje et al. 2017). The direct use of aluminum sulfate increases the sulfur content in the sludge. Based on Figs. 2 and 3, the highest contribution of sulfur came from the wet scrubber wastewater. The sulfate concentrations of the Omnical wet scrubber water were  $865 \text{ mg.L}^{-1}$ , and from of the Thompson boiler wet scrubber water was  $1115 \text{ mg.L}^{-1}$ .

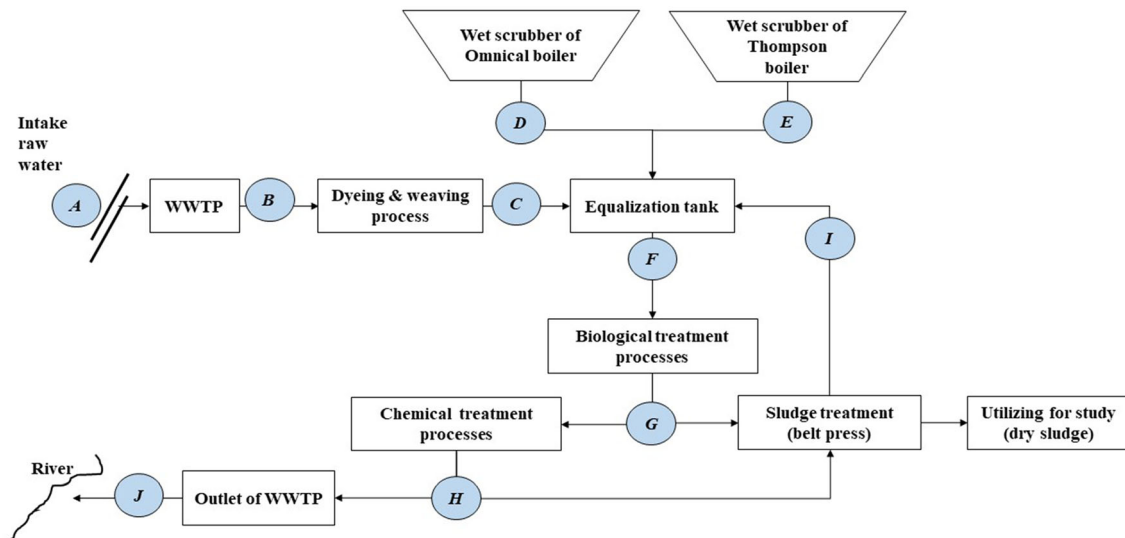
The wet scrubber's sulfur content is influenced by the type of coal used and the boiler's combustion performance. Wastewater from the two wet scrubbers is discharged into the equalization unit before going into the biological and chemical processing units, which produce a large quantity of sludge (Arbunowo et al. 2019). The sulfur content from both boilers will increase the sulfur concentration in the resulting sludge. Therefore, despite this wastewater treatment system recycling the wastewater extracted by the belt press into the equalization tank, if the wastewater in the equalization tank contains high levels of sulfur, the total amount of sulfur in the sludge will remain high.

The sulfur content in a fuel should not be more than 1% by weight because high levels of sulfur harm the

**Table 2** The typical values and their ranges obtained from the proximate, ultimate, and calorific tests of sludge (SL), bottom ash (BA), and biomass (BM)

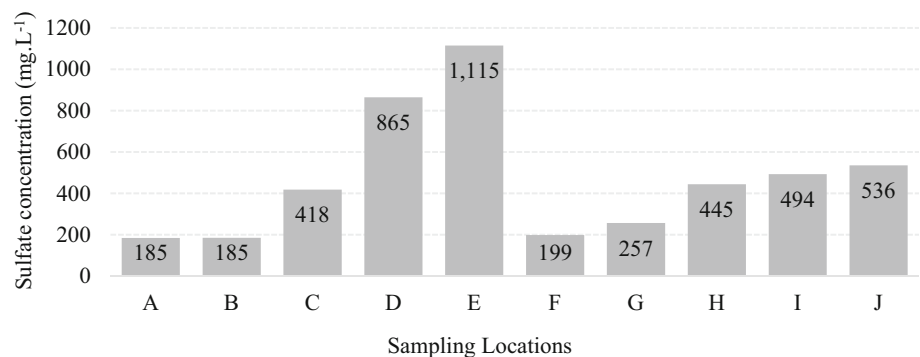
Parameter	SL <sup>a</sup>		BA <sup>a</sup>		BM <sup>a</sup>	
	Typical	Range	Typical	Range	Typical	Range
<i>Proximate</i>						
Moisture (wt%)	6.83	< 10	4.72	< 10	5.89	< 10
Ash (wt%)	44.1	40–60	63.26	50–90	45.39	30–50
Volatile matter (wt%)	44.85	> 40	5.1	< 10	43.0	> 30
Fixed carbon (wt%)	4.26	< 10	26.91	20–40	5.74	< 10
<i>Ultimate</i>						
Total sulfur (wt%)	1.91	1–3	0.88	< 1	0.27	< 0.5
Carbon (wt%)	25.45	> 20	29.43	> 20	20.83	> 20
Hydrogen (wt%)	4.2	> 3	0.83	< 1	3.71	> 4
Nitrogen (wt%)	1.3	> 1	0.42	< 1	0.99	> 1
Oxygen (wt%)	23.03	> 20	5.19	< 10	27.71	> 20
Gross calorific value ( $\text{kcal kg}^{-1}$ )	2405	> 2200	2111	< 2200	2366	> 2200

<sup>a</sup>Air-dried samples

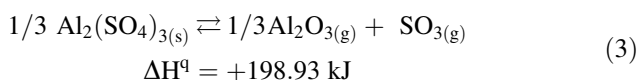


**Fig. 2** Scheme for sulfate measurement at each step of the water treatment process. (A to J are the points at which wastewater was sampled)

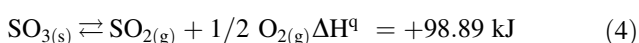
**Fig. 3** The sulfate concentration at each sampling location in the water treatment process (see Fig. 2 for an explanation of the locations)



combustion process (Chuah et al. 2015). Combustion of fuel with a high sulfur content will increase SO<sub>x</sub> gas (Sarbasov et al. 2018), a toxic aerosol emission (Zhao et al. 2016). In addition, SO<sub>x</sub> reacts readily with water to form sulfuric acid, which causes corrosion at low temperatures (Cullis and Mulcahy 1972; Srivastava et al. 2004). Aluminum sulfate undergoes a decomposition reaction at a temperature of 923–1223 K or 650–950 °C. Metal sulfate reactions are usually endothermic or absorb energy and are always reversible (Sarbasov et al. 2018). The decomposition reaction of aluminum sulfate is as follows (Ghasri-Khouzani et al. 2009; Tompkin 1976; Tagawa 1984):



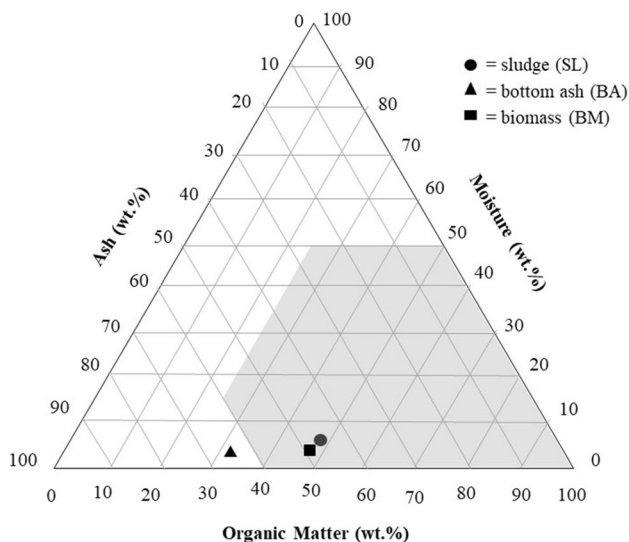
During the combustion process, most (about 83–93% by weight) of the resulting sulfur trioxide is oxidized to sulfur dioxide, while a small portion remains as sulfur trioxide. The reactions that occur are as follows:



Based on these equations, the sulfur content of sludge used as a fuel should be lowered to reduce its sulfur emission value.

The GCV of all three materials used in this study was below the required standard (see Table 2). The GCV resulting from the combustion processes involved a balance between all the proximate and ultimate parameters. As bottom ash was a solid waste generated from a coal combustion process, it was difficult to burn again. The GCV of bottom ash was low because it had a low VM content. In contrast, the GCV of sludge and biomass did not meet the standard because they had a low FC content.

In general, the properties of combustible material can be assessed using a Tanner diagram. The Tanner model states that if the moisture, ash, and combustible compound (FC and VM) content of a material is within the combustible zone (the gray area in Fig. 4), so the material has the potential to burn without using additional fuel (Anggoro et al. 2017; Lombardie et al. 2015; Pasek et al. 2013; Siddiqi et al. 2019). In this study, sludge had an ash content of less than 60% by weight, moisture content of less than



**Fig. 4** The Tanner diagram of the characteristics of the fuels used in this study

50% by weight, and combustible materials above 25% by weight, and the composition of these three parameters was in the combustible zone (Fig. 4). The percentages of moisture, ash, and organic matter content of bottom ash were outside the combustible zone (Fig. 4). It means that each material cannot be burned alone without other materials. Although it was not combustible, the FC content of bottom ash was still relatively high at almost 27% by weight. The high FC content indicates that fuel processing was less efficient (James et al. 2012). The remaining carbon in bottom ash should be considered for reuse as an energy source (Marganingrum and Estiati 2020). It would be harmful to the environment and ecologically not

**Table 4** Proximate, ultimate, and calorific analysis of a nearly balanced mixture of sludge (SL) and biomass (BM)

Parameter	SL and BM in mixture <sup>a,b,c</sup>
<i>Proximate</i>	
Moisture (wt%)	6.5
Ash (wt%)	58.6
Volatile matter (wt%)	15.53
Fixed carbon (wt%)	19.37
<i>Ultimate</i>	
Total sulfur (wt%)	0.7
Carbon (wt%)	28.24
Hydrogen (wt%)	2
Nitrogen (wt%)	0.7
Oxygen(wt%)	9.92
Gross calorific value (kcal.kg <sup>-1</sup> )	2274

<sup>a</sup>Air-dried samples

<sup>b</sup>Percentage ratio by weight

<sup>c</sup>The composition of SL:BM is 40%:60% by weight

sustainable to discharge bottom ash without further processing.

Although the sulfur content of biomass met the requirements for a substitute fuel, its GCV was below 2,500 kcal.kg<sup>-1</sup>. This low GCV was due to biomass's low FC content. So biomass needs other materials to meet the fuel substitution requirements. However, the Tanner diagram shows that biomass can be burned without the need for additional material. It was shown that the percentages of moisture, ash, and combustible matter content in biomass were within the gray zone (Fig. 4).

**Table 3** Proximate, ultimate, and GCV analysis of sludge (SL) and bottom ash (BA) mixtures

Parameter	SL and BA in mixture <sup>a,b</sup>						
	70:30	60:40	50:50	40:60	30:70	20:80	10:90
<i>Proximate</i>							
Moisture (wt%)	7.52	7.08	6.91	7.86	4.78	3.80	3.18
Ash (wt%)	47.74	47.80	50.24	49.21	70.42	73.50	75.86
Volatile matter (wt%)	39.32	35.66	28.51	27.31	18.11	14.07	8.87
Fixed carbon (wt%)	5.42	9.46	14.34	15.62	6.69	8.63	12.09
<i>Ultimate</i>							
Total sulfur (wt%)	1.90	1.70	1.64	1.45	1.26	1.18	1.02
Carbon (wt%)	27.98	28.12	29.75	23.11	17.34	17.65	17.82
Hydrogen (wt%)	3.70	3.44	3.08	2.48	1.92	1.63	1.07
Nitrogen (wt%)	1.36	1.12	1.02	0.84	0.53	0.47	0.51
Oxygen(wt%)	17.32	17.82	14.27	11.20	8.53	5.57	3.72
Gross calorific value (kcal kg <sup>-1</sup> )	2436	2462	2488	2696	1473	1366	1296

<sup>a</sup>Air-dried samples

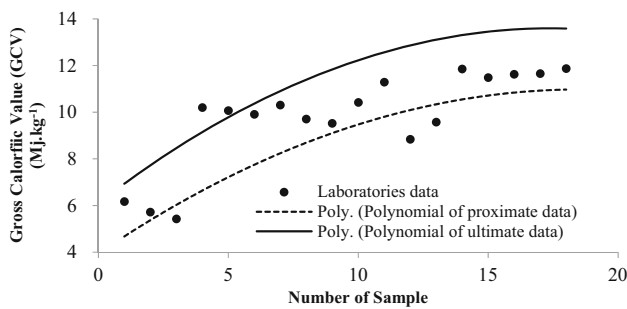
<sup>b</sup>Percentage ratio by weight

**Table 5** Proximate, ultimate, and calorific analysis of mixtures of sludge (SL), bottom ash (BA), and biomass (BM) in several ratios

Parameter	SL:BA:BM in mixture <sup>a,b</sup>						
	16:42:42	17:50:53	20:40:40	23:38:39	25:45:30	35:30:35	50:30:20
<i>Proximate</i>							
Moisture (wt%)	6.24	6.50	5.46	5.90	5.84	9.56	9.88
Ash (wt%)	46.41	47.70	45.34	46.90	50.25	53.30	51.40
Volatile matter (wt%)	28.10	23.60	29.02	29.08	22.72	20.23	17.02
Fixed carbon (wt%)	19.25	22.20	20.18	18.12	21.19	16.91	21.70
<i>Ultimate</i>							
Total sulfur (wt%)	0.68	0.72	0.66	0.70	0.78	0.70	0.95
Carbon (wt%)	31.68	32.12	31.95	31.72	31.85	29.20	27.49
Hydrogen (wt%)	2.82	2.62	2.98	2.77	2.62	2.51	2.40
Nitrogen (wt%)	0.52	0.68	0.78	0.74	0.70	0.70	0.95
Oxygen (wt%)	17.89	16.15	18.29	17.17	13.80	13.57	17.06
Gross calorific value (kcal kg <sup>-1</sup> )	2784	2777	2836	2831	2743	2318	2286

<sup>a</sup>Air-dried samples

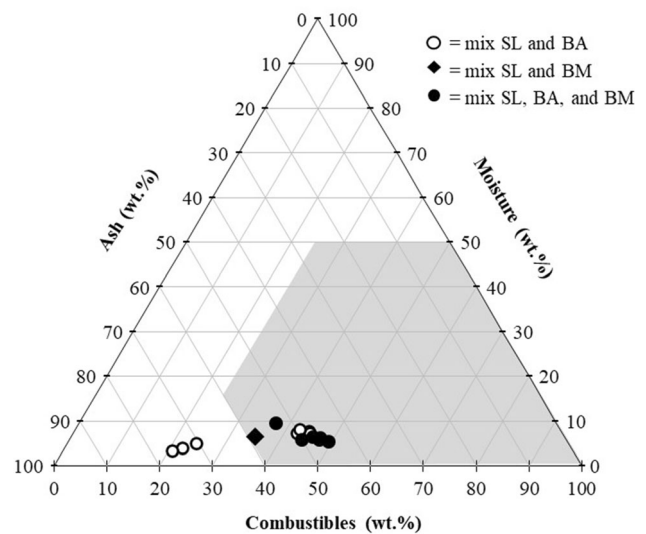
<sup>b</sup>Percentage ratio by weight



**Fig. 5** The gross calorific value (GCV) of each material tested in the laboratory compared to the GCV calculated from proximate and ultimate analyses (including sulfur content)

### 3.2 Characteristics of sludge mixed with other materials

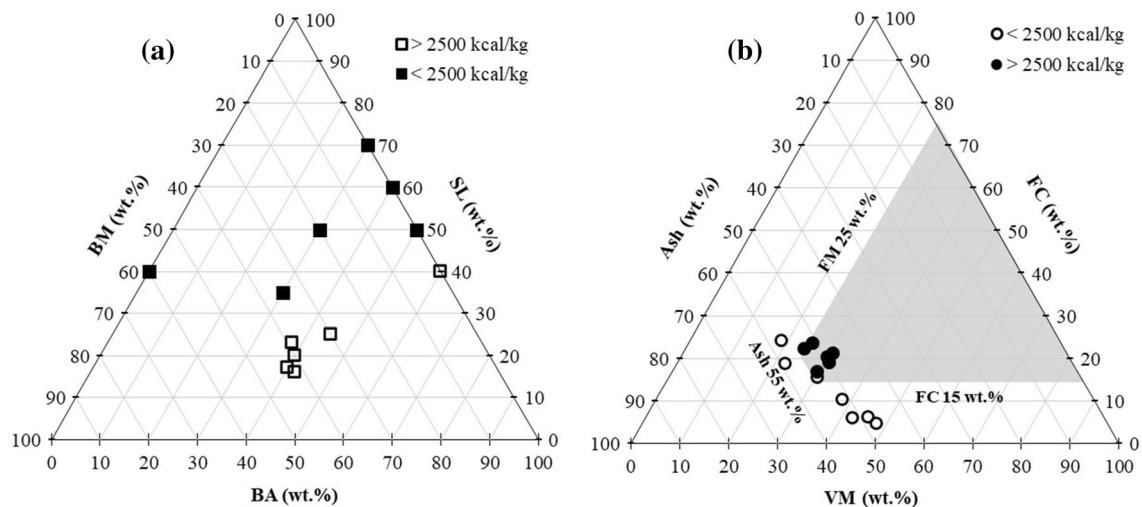
This study sought an effective solution to change the composition of sludge to increase GCV and reduce sulfur levels to meet the requirements for fuel substitution. One of the efforts was to mix sludge with other materials to overcome this shortcoming. The high VM in sludge and the residual carbon content in bottom ash can increase GCV in mixtures of these two waste materials. Table 3 shows the results of proximate and ultimate analysis of sludge and bottom ash mixtures of various compositions. Table 4 shows the results of proximate and ultimate analysis of sludge and biomass mixtures. The reason for including biomass in the mixture was to replace bottom ash and reduce the sulfur content of sludge. It is challenging to reduce the sulfur content below 1% by weight (Fig. 4), and the sludge and bottom ash mixtures did not meet this



**Fig. 6** Tanner diagram of the tested mixtures of sludge (SL), BA (bottom ash), and biomass (BM)

requirement. The composition and GCV of sludge and biomass were approximately similar. Table 4 shows the results for the 40% sludge and 60% biomass mix by weight; clearly, the addition of biomass reduced sulfur levels, but it did not increase GCV. Biomass and sludge have some similar characteristics because of high VM but relatively low carbon content. So, the other material, such as bottom ash, is still needed to provide additional carbon in the mixture. This study considered various mixes of





**Fig. 7** Tanner diagrams of **a** mixes of sludge (SL), bottom ash (BA), and biomass (BM) to determine those with a calorific value above  $2500 \text{ kcal.kg}^{-1}$ , and **b** fixed carbon (FC), volatile matter (VM), and

ash to determine the mixes with a calorific value above  $2500 \text{ kcal.kg}^{-1}$ . The gray area in **b** represents the combustible zone

sludge, bottom ash, and biomass, and the results of their proximate, ultimate, and GCV analysis are shown in Table 5.

The results of GCV tests of the materials were compared to Eqs. 1 and 2 (Fig. 5). All samples tested by ASTM D5865 were still correlated to these formulas. According to Fig. 5, the samples with an SL:BA ratio of 30:70, 20:80, and 10:90 wt% were not suitable for use as a fuel as the ash content was at least 60% by weight (see Fig. 6); these mixes will not be further discussed.

The data in Tables 3, 4, and 5 were used to create Tanner diagrams to assess the tested sample materials to identify those that were within the areas for calorific values below and above  $2500 \text{ kcal.kg}^{-1}$  (Fig. 7). The number of samples was not enough to create more detailed figures. All tested samples had high ash content (at least 40% by weight), and the calorific value of biomass was usually above  $2800 \text{ kcal.kg}^{-1}$ . This study shows that mixes with less than 35% by weight of sludge or up to 60% by weight of bottom ash were feasible as fuels.

### 3.3 Environmental analysis

The Indonesian regulation number 101 of 2014 (Attachment III) classifies waste as toxic and hazardous if it is explosive, flammable, reactive, infectious, corrosive, and/or toxic. Both textile factory sludge and bottom ash have the same toxicity properties because they contain heavy metals (Damayanti 2018; Kurniawan et al. 2018). Tables 6 and 7 show the heavy metal content of sludge and bottom ash used in this study. Table 6 is heavy metal content in ash and Table 7 is heavy metal content in raw material by TCLP testing.

**Table 6** The heavy metal content of the textile industry sludge (SL) and bottom ash (BA)

Heavy metal	SL	BA
Copper (Cu) ( $\text{mg kg}^{-1}$ )	34.77	49.74
Zinc (Zn) ( $\text{mg kg}^{-1}$ )	212.18	65.24
Lead (Pb) ( $\text{mg kg}^{-1}$ )	38.46	10.07
Chrome (Cr) ( $\text{mg kg}^{-1}$ )	39.21	0.04
Cadmium (Cd) ( $\text{mg kg}^{-1}$ )	3.87	0.71
Nickel (Ni) ( $\text{mg kg}^{-1}$ )	20.97	0.01
Cobalt (Co) ( $\text{mg kg}^{-1}$ )	24.20	–
Manganese (Mn) ( $\text{mg kg}^{-1}$ )	219.79	0.14

The heavy metal content of sludge was dominated by zinc and manganese, while bottom ash was dominated by zinc and copper. This heavy metal content will increase the hazard level of the waste released into the environment (Damayanti 2018). Therefore, Indonesian regulation states that toxic and hazardous waste should not leave its source and obliges the waste producers to manage it themselves or to transfer the management to another party that has been certified to handle such waste. Toxic and hazardous waste is classified as category 1 if the heavy metal content discharged during the leaching process is more than the TCLP-A level. The hazardous waste category 1 has acute effects on exposed humans. Category 2 toxic and hazardous waste is classified as such if the heavy metal content released during the leaching process is more than the TCLP-B level but is less than the TCLP-A level. Category 2 hazardous waste has a chronic effect on exposed humans. The levels of heavy metal leaching from the material used

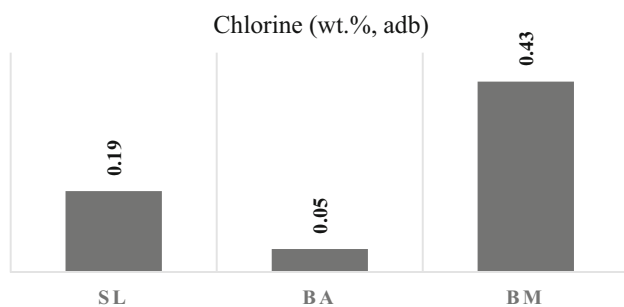
**Table 7** TCLP analysis of a mixture of sludge (SL), bottom ash (BA), and biomass (BM)

Parameter	TCLP-A <sup>a</sup>	TCLP-B <sup>a</sup>	TCLP samples			Method reference
			SL	BA	Mixture <sup>b</sup>	
Silver (Ag) (mg.L <sup>-1</sup> )	40	5	< 0.04	0.06	< 0.04	AAS/SNI 6989–84:2019
Barium (Ba) (mg.L <sup>-1</sup> )	210	35	0.823	1.17	2.87	AAS/SNI 6989–84:2019
Zinc (Zn) (mg.L <sup>-1</sup> )	300	50	0.267	0.426	0.918	AAS/SNI 6989–84:2019
Copper (Cu) (mg.L <sup>-1</sup> )	60	10	0.013	0.009	0.008	AAS/SNI 6989–84:2019
Cadmium (Cd) (mg.L <sup>-1</sup> )	0.9	0.15	< 0.01	< 0.01	< 0.01	AAS/SNI 6989–84:2019
Hexavalent chrome (Cr-VI) (mg.L <sup>-1</sup> )	15	2.5	< 0.01	< 0.01	< 0.01	Spectrophotometry/SNI 6989–71:2009
Arsenic (As) (μg.L <sup>-1</sup> )	3,000	500	60.09	31.34	32.79	AAS-Grafit Furnace
Lead (Pb) (mg.L <sup>-1</sup> )	3	0.5	< 0.08	10.05	< 0.076	AAS/SNI 6989–84:2019
Nickel (Ni) (mg.L <sup>-1</sup> )	21	3.5	< 0.013	0.073	< 0.013	AAS/SNI 6989–84:2019
Mercury (Hg) (μg.L <sup>-1</sup> )	300	50	3.22	0.514	0.602	AAS/SNI 6989–84:2019
Selenium (Se) (μg.L <sup>-1</sup> )	3,000	500	< 1	< 1	< 1	AAS-Grafit Furnace

<sup>a</sup>The standard according to the Republic of Indonesia regulation number 101 of 2014

<sup>b</sup>The mixture ratio of SL:BA:BM was 20:40:40 wt%

SNI is Indonesian National Standard



**Fig. 8** The chlorine percentage of materials used in this study (wt%, air-dried samples)

in this study are safe for humans because they were lower than the TCLP-B levels.

In addition to TCLP, this study measured chlorine content related to dioxins (polychlorinated dibenzo-p-dioxins/PCDDs) or furans (polychlorinated dibenzofurans/PCDFs) issue. These two compounds are known as the most harmful persistent organic pollutants, which are chlorine-based compounds (Kim et al. 2005). Dioxins or furan issue related to incineration technology is due to the lack of landfill sites (Ni et al. 2009). It is an attractive alternative to treat MSW because it does not depend on biological processes that take a long time and can reduce the volume of MSW quickly up to 85–90% by volume (Chang et al. 2009; McKay 2002). Therefore the formation and control technology in gas emission that related to MSW burning has been the focus of many kinds of research (Kim et al. 2005). Dioxins or furans are produced in the combustion process by synthetic precursors. The

formation rate can be affected by incomplete combustion processes due to improper air supply resulting in a lack of oxygen (Ni et al. 2009; Rathna et al. 2018). Figure 8 shows chlorine content of raw material used in this study. Based on the analysis, the chlorine content in both sludge, bottom ash, and biomass is less than 1% by weight. It means that the materials met the requirement of regulations.

To ensure that the mixture of sludge, bottom ash, and biomass (at a ratio of 20:40:40% by weight) was appropriate for co-firing and a safe fuel for the environment, a trial burning test (TBT) was conducted in the boiler of the factory concerned. The three materials were mixed, and briquettes were made using 2% by weight starch as an adhesive. This briquette fuel was substituted of 10–15% by weight for co-firing in the boiler. The emissions from the co-firing are shown in Table 8; all tested parameters had values below the relevant quality standard limits, including that for chlorine gas.

## 4 Conclusions

Sludge and biomass had similar characteristics, as demonstrated by their VM and FC content, but the mixing of sludge and biomass did not increase GCV because of the low carbon content of both materials. On the other hand, bottom ash had a higher carbon content, and the mixing of bottom ash with sludge or bottom ash with sludge and biomass increased GCV significantly to a value higher than that of each material on its own. The high FC and high VM in the mixtures were favorable for raising their GCV.

**Table 8** The results of the emission test for the fuel mixture<sup>a</sup> of sludge (SL), bottom ash (BA), and biomass (BM) used in the co-firing of the factory boiler

No	Parameter	Standard	Emission	Method reference
<i>Non-heavy metals</i>				
1	Ammonia (NH <sub>3</sub> ) (mg.Nm <sup>-3</sup> )	0.5	0.018	SNI 19-7117.6:2005
2	Chlorine (Cl <sub>2</sub> ) (mg.Nm <sup>-3</sup> )	10	0.179	Kep.Ka.Bapedal No. Kep.205/BAPEDAL/07/1996
3	Hydrogen chloride (HCl) ((mg.Nm <sup>-3</sup> )	5	2.94	SNI 19-7117.8:2005
4	Hydrogen fluoride (HF) (mg.Nm <sup>-3</sup> )	10	0.1531	SNI 19-7117.9:2005
5	Nitrogen oxide (NO <sub>2</sub> ) (mg.Nm <sup>-3</sup> )	1000	17	SNI 03.25.06.3:2015 (gas analyzer)
6	Opacity (%)	35	< 20	SNI 02.25.15.1:2015 (opacity meter)
7	Particulates (mg.Nm <sup>-3</sup> )	350	13.53	SNI 19-7117.12:2005
8	Sulfur dioxide (SO <sub>2</sub> ) (mg.Nm <sup>-3</sup> )	800	11	SNI 03.25.07.3:2015 (gas analyzer)
9	Total sulfur reduction (H <sub>2</sub> S) (mg.Nm <sup>-3</sup> )	35	< 0.002	SNI 19-7117.7:2005
10	Flow rate (m <sup>3</sup> .s <sup>-1</sup> )	–	4.8	SNI 19-7117.1:2005
<i>Heavy metals</i>				
1	Mercury (Hg) (mg.Nm <sup>-3</sup> )	5	0.004	SNI 7117.20:2009
2	Arsenic (As) (mg.Nm <sup>-3</sup> )	8	< 0.001	SNI 7117.20:2009
3	Antimony (Sb) (mg.Nm <sup>-3</sup> )	8	< 0.006	SNI 7117.20:2009
4	Cadmium (Cd) (mg.Nm <sup>-3</sup> )	8	< 0.012	SNI 7117.20:2009
5	Zinc (Zn) (mg.Nm <sup>-3</sup> )	50	< 0.010	SNI 7117.20:2009
6	Lead (Pb) (mg.Nm <sup>-3</sup> )	12	< 0.034	SNI 7117.20:2009

<sup>#</sup>Gas volume in the standard state (25 °C and 1 atm pressure)

<sup>a</sup>The mixture of SL:BA:BM at a ratio of 20:40:40 wt%

SNI is Indonesian National Standard

Based on this study, the best material composition that proper of regulation was 20 wt% of sludge, 40 wt% of bottom ash, and 40 wt% of biomass. This study provides an avenue for reducing toxic and hazardous waste, a burdensome waste management challenge as well, especially for developing countries such as Indonesia. Finding of this composition needs to be reapplied on a broad and massive scale by government regulation supporting through the Ministry of Environmental and Forest of the Republic of Indonesia. These findings contribute a practical solution for governments in their efforts to encourage factories that produce wastewater sludge and use coal as an energy source to take measures to tackle the highly critical problem of industrial and urban waste. The following study was needed to decrease the moisture and sulfur content of sludge to increase the performance of sludge as an alternative fuel to ensuring the sustainability and development of clean technologies.

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**Author contributions** DM contributed to conceptualization, methodology, analysis on data of proximate, ultimate, calorific value, wastewater quality, TCLP, heavy metal, chlorine, air emission, and writing, review and editing; H contributed to analysis of sulfur content, and writing; SJSJ contributed to conceptualization, analysis on data of proximate, ultimate, calorific value, sulfur content, and writing.

#### Declarations

**Conflict of interest** The authors declare that they have no conflict of interest in the publication of this article. The authors also confirm that the data are original and the paper is free of plagiarism.

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