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Self-healing materials enable free-standing seamless large-scale 3D printing

Han Zuo¹, Zenghe Liu¹, Luzhi Zhang¹, Gengxin Liu^{1,2}, Xikai Ouyang^{1,2}, Qingbao Guan¹, Qilin Wu^{1*} and Zhengwei You^{1*}

ABSTRACT Three-dimensional (3D) printing has had a large impact on various fields, with fused deposition modeling (FDM) being the most versatile and cost-effective 3D printing technology. However, FDM often requires sacrificial support structures, which significantly complicates the processing and increases the cost. Furthermore, poor layer-to-layer adhesion greatly affects the mechanical stability of 3D-printed objects. Here, we present a new Print-Healing strategy to address the aforementioned challenges. A polymer ink (Cu-DOU-CPU) with synergetic triple dynamic bonds was developed to have excellent printability and room-temperature self-healing ability. Objects with various shapes were printed using a simple compact 3D printer, and readily assembled into large sophisticated architectures via self-healing. Triple dynamic bonds induce strong binding between layers. Additionally, damaged printed objects can spontaneously heal, which significantly elongates their service life. This work paves a simple and powerful way to solve the key bottlenecks in FDM 3D printing, and will have diverse applications.

Keywords: dynamic bonds, self-healing, 3D printing, supportfree, interlayer adhesion

INTRODUCTION

Three-dimensional (3D) printing can readily fabricate complex 3D structures, which is hard to achieve by traditional processing methods [1,2]. Therefore, 3D printing has wide applications in various fields, such as electronics, biomedical engineering, energy industry, and aerospace [3–14]. There are many types of 3D printing technologies such as digital light processing (DLP), selective laser sintering (SLS), stereolithography (SLA), fused deposition modeling (FDM), and direct ink writing (DIW) [15,16]. Among these techniques, FDM is the most popular in several industries due to its low cost, simplicity of operation, and compatibility with a wide range of materials [17–19].

However, FDM of typical polymers faces some challenges. First, auxiliary sacrificial support structures are usually necessary for sophisticated objects, to maintain the desired shape during the printing process. Moreover, post-processing is required to remove the supports [17]. Support structures increase the processing steps, require relatively complex 3D printers, and lead to high production costs. Furthermore, removing the supports may damage the printed objects [20]. Recently, multi-axis 3D printing systems have been developed to reduce the need for support structures [21–23]. However, adding degrees of freedom to a 3D printing system makes it challenging to define slicing and avoid collision during printing, and increases the complexity and cost. Second, the layer-bylayer process in all FDM typically causes weak interlayer adhesion in printed objects [24]. Accordingly, cracks and deformations are easily generated during use, which greatly shorten the service life of the fabricated objects. Introducing crosslinks between layers provides an appealing solution to weak interlayer adhesion [19,25,26]. Via high energy ionizing irradiation, crosslinking has been induced in 3D-printed polymer objects [26]. However, this approach requires complicated processing, and irradiation dosages must be precisely controlled to prevent degradation of mechanical properties due to chain scission becoming dominant. The thermo-induced Diels-Alder reaction has been employed to improve the interlayer adhesion [19]. However, extra cooling system in addition to a 3D printer is needed to maintain the shape during printing. Furthermore, the dense crosslinking makes these polymers rigid. Third, the customized 3D

¹ State Key Laboratory for Modification of Chemical Fibers and Polymer Materials, Shanghai Belt and Road Joint Laboratory of Advanced Fiber and Low-Dimension Materials (Donghua University), College of Material Science and Engineering, Donghua University, Shanghai 201620, China

² Center for Advanced Low-Dimension Materials, Donghua University, Shanghai 201620, China

^{*} Corresponding authors (emails: wql@dhu.edu.cn (Wu Q); zyou@dhu.edu.cn (You Z))

printed objects are integrally formed, and thus cannot easily be partially repaired upon damage. Recently, dynamic polymers have been used to solve this problem [27–29]. Nevertheless, the requirement for external stimuli such as heat, light, and solvents greatly impedes their application. Fourthly, the sizes of printed objects are often limited by the size of the 3D printer. It is difficult to obtain large-scale objects using compact printers [30].

To the best of our knowledge, there is no effective method to solve all the above problems simultaneously. We propose a print-healing strategy based on spontaneous self-healing materials with dynamic networks to address these challenges. Here, we demonstrate this strategy via Cu(II)-dimethylglyoxime-urethane (DOU)complex-based thermoset polyurethane polymers (Cu-DOU-CPU) with multiple dynamic bonds including reversible DOU, Cu(II)-DOU coordination, and hydrogen bonds. A suitable combination of these enables the material to be FDM 3D-printed at elevated temperatures, quickly solidified at room temperature, and possess excellent self-healing capability (Fig. 1). Inspired by Lego bricks, we took advantage of the room-temperature selfhealing property to assemble 3D-printed blocks into large sophisticated objects without utilizing support structures. Moreover, the triple dynamic bonds significantly improved layer-to-layer adhesion in the printed objects. Furthermore, subsequent mechanical damage can generally be readily repaired via self-healing without any external stimulus.

EXPERIMENTAL SECTION

Materials

Polytetramethylene ether glycol (PTMEG, $M_n = ~1000 \text{ g mol}^{-1}$), polypropylene glycol (PPG, $M_n = ~2000 \text{ g mol}^{-1}$), isophorone diisocyanate (IPDI, 99%) and dibutyltin dilaurate (DBTDL, 95%) were purchased from Aladdin. Dimethylglyoxime (DMG, 98%), glycerol (99%), and copper(II) chloride (CuCl₂, 99%) were purchased from Sinopharm Chemical Reagent Co. Acetone (99.8%) was purchased from Yonghua Chemical Technology (Jiangsu) Co. All reagents were used as received without further purification unless otherwise noted.

Synthesis of Cu-DOU-CPU polymers

Cu-DOU-CPU_{0.3}-T synthesis is discussed below. The other Cu-DOU-CPU polymers were synthesized in a similar procedure (detailed various formulations are shown in Table S1). PTMEG (6 g, 2 mmol), DMG (0.696 g, 2 mmol), glycerol (0.0414 g, 0.3 mmol) and CuCl₂

(0.0064 g, 0.016 mmol) were added to 20 mL of acetone in a glass vessel and stirred with a magnetic stirrer to form a homogeneous solution. IPDI (2.9637 g, 4.45 mmol) and DBTDL (0.09 g) were added and reacted for 2 h at 50°C. Then, the mixture was poured into a Teflon mold and reacted at 50°C for 24 h before further curing in a vacuum oven at 70°C for another 24 h to produce Cu-DOU-CPU_{0.2}-T.

3D printing

Printing was carried out using a GeSiM BioScaffolder BS3.2 printer with a nozzle diameter of 0.4 mm. The 3D models of the samples were designed using Solidwork software. Cu-DOU-CPU_{0.3}-T polymer was crushed into small pieces and loaded into the print-head, the printhead temperature was set to 100°C, and held at this temperature for 10 min to completely de-crosslink the polymer before printing. The extrusion speed and deposition speed were 0.005 and 4.5 mm s⁻¹, respectively. All printing paths were controlled by an external personal computer control system. After printing, 3D-printed parts were assembled by hand into the designed architectures. Finally, the assembled architectures and 3D printed objects for tensile tests were moved to an ambient environment at 25°C for 72 h before testing.

General characterizations

Attenuated total reflectance Fourier transform infrared (ATR-FTIR) spectra were collected using a Nicolet 8700 spectrometer with ATR attachment. In-situ variabletemperature FTIR spectra were collected using the spectrometer with a programmable heating device. Rheological measurement was performed on a Haake Mars III rheometer using 8-mm parallel-plate geometry. Strain sweeps were performed to determine the linear viscoelastic region. Temperature sweeps were performed at a fixed frequency of 10 rad s⁻¹ and a fixed strain of 0.1% from 25 to 130°C at a heating rate of 3°C min⁻¹. Isothermal frequency sweeps were conducted to determine the storage moduli (G') and loss moduli (G'') over a frequency range from 0.1 to 10 Hz under a fixed strain of 0.1% at 25 and 100°C, respectively. The steady-state viscosities under different shear rates were evaluated at 100°C between 0.1 and 100 s⁻¹. Thermogravimetric analysis (TGA) was performed on a Discovery TGA. The sample was heated at a constant rate of 20°C min⁻¹ from 40 to 800°C under a nitrogen atmosphere. Dynamic mechanical analysis (DMA) was performed on a TA-Q800 DMA utilizing rectangular films (ca. 1 mm (T) × $3 \text{ mm}(W) \times 6 \text{ mm}(L)$). Samples were tested at a fre-

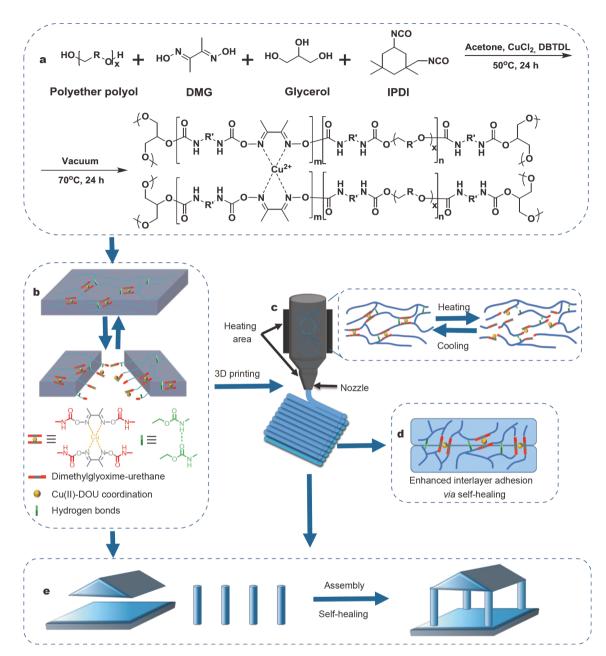


Figure 1 Design of print-healing strategy and corresponding self-healing polymer ink Cu-DOU-CPU. (a) Synthesis of the Cu-DOU-CPU polymers; (b) schematic of self-healing of Cu-DOU-CPU polymers; (c) 3D printing process of Cu-DOU-CPU; (d) enhanced interlayer adhesion of 3D-printed object; (e) schematic showing assembly of 3D-printed parts.

quency of 1 Hz, a strain of 0.1%, and a heating rate of 10°C min⁻¹ in air. The glass transition temperature (T_g) was calculated from the peak of the loss modulus curve. Mechanical properties were investigated using an MTS E42 tensile machine with a 100-N load cell. Rectangular tensile bars (ca. 1 mm (T) × 3 mm (W) × 20 mm (L)) cut from synthetic Cu-DOU-CPU_{0.3}-T sheets and 3D-printed sheets with different print patterns were used. At least five

specimens were tested for each sample. A deflection rate of 100 mm min^{-1} was used for tests at room temperature (25°C).

Self-healing experiments

Self-healing tests were investigated by surface scratch recovery and restoration of mechanical properties for different durations. A blade was used to make 15- to 30µm-wide scratches on a Cu-DOU_{0.3}-CPU-T film. The changes of the scratch were monitored by an optical microscope (MDA2000, Future Optics) at room temperature. Restoration of the mechanical properties was performed by bringing the two individual cut specimens back into contact at room temperature for various time periods. The mechanical properties of final healed specimens were obtained after healing for 120 h.

Statistical analysis

Statistical analysis was performed using independent *t*-test with a minimum confidence level of <0.05 for statistical significance. All values are reported as the mean \pm standard deviation (s.d.).

RESULTS AND DISCUSSION

Synthesis and printability of the Cu-DOU-CPU polymers

For FDM 3D printing, it is important that the ink has good printability. Accordingly, we prepared a series of Cu-DOU-CPU materials with triple dynamic bonds including reversible DOU, Cu(II)-DOU coordination, and hydrogen bonds and investigated their printability. Samples of Cu-DOU-CPU_x-y were synthesized via polycondensation of DMG, polyether polyol, glycerol, IPDI, CuCl₂, and catalyst DBTDL ((Fig. 1a and Table S1) [31]. Here, x represents the molar ratio of glycerol, where x =0.3 or 0.5; y = T represents using PTMEG as the polyether polyol, and y = P represents using PPG. 3D-printable polymer must possess suitable viscoelastic properties to allow flow during shearing and extrusion, and retain the 3D structure without collapse after extrusion [17,32,33]. Both Cu-DOU-CPU_{0.3}-P and Cu-DOU-CPU_{0.5}-P had an amorphous soft sticky state at room temperature and could not retain the desired shape, and thus were not suitable for 3D printing. Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU05-T could be extruded from an injection syringe at 130°C and solidified quickly upon cooling (Table S1). ATR-FTIR was used to characterize the structures of Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU_{0.5}-T. The peak at around 2271 cm^{-1} assigned to the N=C=O bond disappeared, whereas the peaks at 3312 and 1718 cm⁻¹ respectively corresponding to N-H and C=O bonds increased, which revealed the formation of urethane group and complete reaction of the monomer IPDI (Fig. S1).

Next, their suitability for FDM 3D printing was studied in detail by rheological analysis. The energy storage moduli (G'), loss moduli (G''), and complex viscosities of Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU_{0.5}-T obviously decreased with increased temperature (Fig. 2a and b). This result indicates that the disassociation of triple dynamic bonds at elevated temperatures disconnected the molecular network of the polymer, making the flow units smaller and easier to move. Cu-DOU-CPU05-T showed higher G', G", and complex viscosity than Cu-DOU- $CPU_{0,3}$ -T, owing to the increased crosslinking degree corresponding to higher glycerol ratio. The increased crosslinking degree made the flow units larger and reduced their mobility. The point of intersection between G'and G" indicates the transition from solid to liquid state [34]. The transition temperatures of Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU05-T were 88 and 124°C, respectively. To reduce the potential side reactions of dissociated isocyanate group at higher temperatures [35], Cu-DOU-CPU_{0.3}-T was selected for further study. The results of the frequency sweep rheological experiment revealed that Cu-DOU-CPU_{0.3}-T possessed an elastic-like behavior at 25°C where G' was higher than G'', and a fluid-like behavior at 100°C where G" was higher than G' (Fig. 2c and d). Cu-DOU-CPU_{0.3}-T showed a diminishing trend in the viscosity with increasing shear rate at 100°C, which demonstrated the shear-thinning ability of the polymer (Fig. 2e). Hence, Cu-DOU-CPU_{0.3}-T polymer could be smoothly squeezed out of the 3D-printer nozzle at 100°C. Printed filaments showed good shape retention at room temperature after extrusion, which is necessary for layer-bylayer deposition (Fig. S2). TGA confirmed good thermal stability of Cu-DOU-CPU_{0.3}-T with a 5% weight loss at 221°C, which indicated that stable printing at moderate temperature would be possible (Fig. S3).

The complex viscosity of Cu-DOU-CPU_{0.3}-T decreased under the heating process, which was attributed to the disassociation of triple dynamic bonds. Hydrogen bonds and metal coordination bonds have been proved to be thermo-reversible [30,36]. The thermal reversibility of the DOU bonds was characterized by in situ variable-temperature FTIR spectroscopy (Fig. 2f). There was almost no characteristic peak at 2271 cm⁻¹ corresponding to N=C=O bonds below 90°C. Whereas the peak appeared and increased as the temperature rose above 100°C, which implicated the dissociation of DOU bonds. The dissociation of hydrogen bonds, DOU bonds, and Cu(II)-DOU coordination bonds at elevated temperatures disconnected the molecular network of Cu-DOU-CPU03-T and enabled printing (Fig. 1c). In addition, DMA was performed to investigate the thermal properties of Cu-DOU-CPU_{0.3}-T. The T_g of Cu-DOU-CPU_{0.3}-T was -33.1°C (Fig. S4), which indicated the flexibility of Cu-DOU-CPU_{0.3}-T at room temperature.

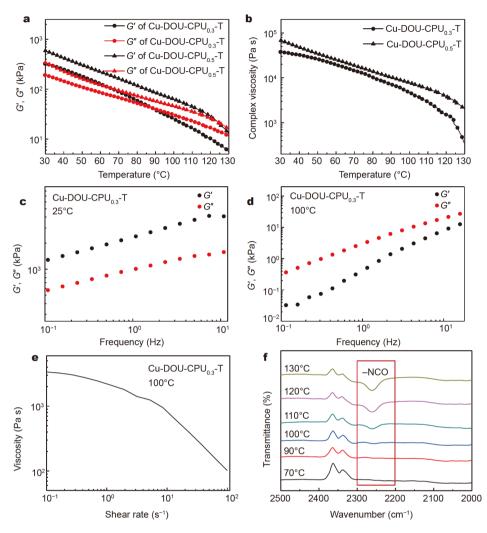


Figure 2 Dynamic properties and printability of Cu-DOU-CPU polymers. (a) Temperature-dependent curves of storage modulus (*G*["]) and loss modulus (*G*["]) for Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU_{0.5}-T; (b) corresponding complex viscosity curves of Cu-DOU-CPU_{0.3}-T and Cu-DOU-CPU_{0.5}-T; (c, d) frequency-dependent curves of storage modulus (*G*["]) and loss modulus (*G*["]) for Cu-DOU-CPU_{0.3}-T at (c) 25°C and (d) 100°C; (e) curve of the viscosity of Cu-DOU-CPU_{0.3}-T as a function of shear rate at 100°C; (f) *in situ* variable-temperature FTIR spectra of Cu-DOU-CPU_{0.3}-T.

Self-healing properties of the Cu-DOU-CPU_{0.3}-T polymer The room-temperature self-healing properties of the Cu-DOU-CPU_{0.3}-T polymer were evaluated in detail. An optical microscope was used for monitoring the surface scratch recovery of Cu-DOU-CPU_{0.3}-T. A blade was used to make 15- to 30-µm-wide scratches on a Cu-DOU-CPU_{0.3}-T film. The crack disappeared almost completely after healing at room temperature for 75 min (Fig. 3a). The instant bulky self-healing ability of Cu-DOU-CPU_{0.3}-T was assessed. The specimen was cut into two pieces, which were brought back into contact under ambient conditions without external force. After 3 min, the healed specimen could be stretched to 150% without fracture (Fig. 3b). Uniaxial tensile testing was further applied to quantitatively evaluate the final self-healing properties of Cu-DOU-CPU_{0.3}-T (Fig. 3c and d). The relative recovery rate (%) was defined as the ratio of the toughness of the original and healed samples. The Young's modulus, tensile strength, maximum elongation and toughness of the original samples were (4.79 ± 0.09), (7.43 ± 0.92) MPa, $(677.41 \pm 22.61)\%$, and (20.99 ± 1.60) MJ m⁻³, respectively. The Young's modulus, maximum elongation and toughness of healed samples restored to 0.08) MPa, (668.56 (4.77)± \pm 44.11)%, and (19.68 ± 1.20) MJ m⁻³, respectively, without statistical difference to the original samples (Fig. 3d and Figs S5-S7). The healed tensile strength was (5.97 \pm 0.32) MPa, slightly lower than the original one. The relative recovery

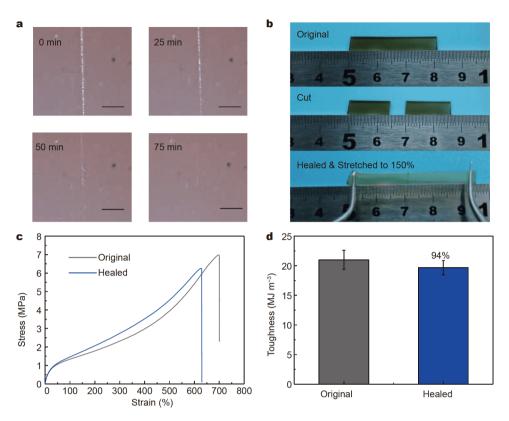


Figure 3 Self-healing properties of the Cu-DOU-CPU_{0.3}-T polymer (room temperature). (a) Optical microscopy photographs of the healing of the scratch on the Cu-DOU-CPU_{0.3}-T film. Scale bar: 150 μ m. (b) Photographs of the original, cut, and healed Cu-DOU-CPU_{0.3}-T specimens under ambient conditions. The healed specimen was stretched to 150%. (c, d) Mechanical recovery of the healed Cu-DOU-CPU_{0.3}-T strips including the tensile stress-strain curves (c) and toughness (d).

rate reached 94%. These results confirmed the spontaneous self-healing capability of Cu-DOU-CPU $_{0.3}$ -T without any external stimulus.

Free assembly of 3D-printed objects via self-healing

While printing complex architectures such as overhangs using FDM, temporary support structures are indispensable. The introduction of the additional support results in waste of sacrificial support material and increase of printing complexity and duration. The support removal process may even damage the printed structures [20]. Moreover, being limited by the size of the 3D printer, it is difficult to print large objects.

Inspired by Lego bricks, we split a complex geometric digital model into simple parts that could be easily fabricated by 3D printing, without support structures. Then, the complete complex architectures would be assembled from these parts (Fig. 1e). We fabricated three different structures to demonstrate this design principle, including the Eiffel Tower, a Chinese building, and a ship anchor. First, Cu-DOU-CPU_{0.3}-T was 3D-printed into small

simple parts, which were assembled by hand into large complex objects, and then seamlessly fused together *via* the room-temperature self-healing. Accordingly, the sophisticated architectures were efficiently produced without additional support structures (Fig. 4a and b, and Fig. S8), and the self-healed joints of the ship anchor could sustain a weight of 50 g, which proved the strong bonding between the assembled components (Fig. 4c). This strategy of dividing the whole into parts and then assembling the parts into a whole *via* spontaneous selfhealing is a powerful means to fabricate large sophisticated support-free 3D-printed objects that are not limited in size by the dimensions of the 3D printer.

Mechanical isotropy of 3D-printed objects

The mechanical properties of the 3D-printed objects at different printed orientations were compared to evaluate the anisotropy of the objects. We prepared three print patterns, X, Y, and Z, where the print variation X consisted of a 45° alternating infill layer pattern, and the print variations Y and Z consisted of linear layer patterns

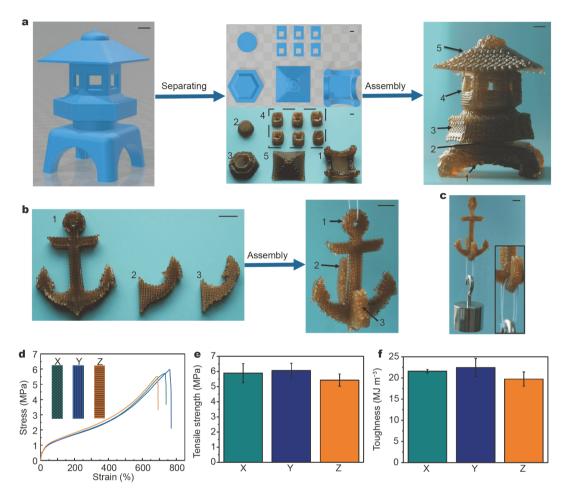


Figure 4 Free assembly of 3D-printed parts into sophisticated objects and mechanical isotropy properties of the 3D-printed objects. (a) Digital model (left and upper middle) and photographs (lower middle and right) of 3D-printed small simple parts, and assembled large complex Chinese building model (scale bar, 5 mm). (b) Photographs of the 3D-printed parts and assembled ship anchor (scale bar: 10 mm). The numbers in the photographs represent the assembly sequence. (d–f) Mechanical properties of X, Y, and Z pattern samples printed with Cu-DOU-CPU_{0.3}-T, including the tensile stress–strain curves (d), tensile strength (e), and toughness (f).

parallel to the *y*-axis and *z*-axis of the machine coordinate system, respectively (Fig. 4d). Isotropy was calculated according to the ratios of ultimate strength and toughness along the X and Z patterns compared with that of the Y pattern. Tensile stress-strain curves of the objects with different print directions were similar, which demonstrated reduced anisotropy of the mechanical properties for different print directions (Fig. 4d). The tensile strengths of the X, Y, and Z print patterns were (5.89 \pm 0.62), (6.06 \pm 0.48), and (5.43 \pm 0.40) MPa, respectively (Fig. 4e). The X and Z printing patterns exhibited 97.19% and 89.60% isotropic behavior relative to the Y printing pattern. Toughness values for the X, Y, and Z patterns were (21.60 \pm 0.40), (22.47 \pm 2.14), and (19.74 \pm 1.69) MJ m⁻³, respectively (Fig. 4f). The X and Z patterns showed 96.13% and 87.85% isotropic behavior relative to the Y pattern, respectively. The isotropic behaviors were comparable to those (80%–96%) of previously reported 3D printed objects strengthened *via* high-temperature Diels-Alder reactions [19,37,38]. Here, the printed objects without any post-treatment showed excellent isotropic properties that confirmed the feasibility of increasing the layer-to-layer adhesion *via* spontaneous recombination of dynamic hydrogen bonds, Cu(II)-DOU coordination bonds, and covalent DOU bonds (Fig. 1d). This provides a facile and efficient way to improve the mechanical properties of resultant 3D printing objects.

Repair of damage to 3D printed objects *via* **self-healing** Owing to the integral forming process, customized 3D printing objects cannot be easily repaired by replacing broken parts. Thus, the entire 3D objects have to be discarded after damage, causing abundant waste [30]. The room-temperature self-healing property of Cu-DOU- $CPU_{0.3}$ -T could effectively solve this problem. As an example, a 3D-printed mesh was locally cut by a scissor. The two broken cross sections were brought back into contact under ambient conditions without external treatment. The fracture could heal spontaneously, and the healed object could resist stretching by tweezers without breaking (Fig. S9). Accordingly, the room-temperature self-healing property could significantly enhance the longevity of 3D-printed objects and reduce resource dissipation.

Wide applicability of print-healing strategy

It is worth noting that all raw reagents used for synthesizing the Cu-DOU-CPU_{0.3}-T polymer are common inexpensive industrial chemicals, and the one-step polycondensation process is simple and can be readily scaled up. Thus, Cu-DOU-CPU_{0.3}-T could be readily produced at a large scale for a wide range of applications. Furthermore, various self-healing materials including silicone, polyamide, polyetherimides, diolefine rubber, and polyurethane materials have been recently developed [39– 49]. Applying the print-healing strategy to these materials would facilitate the 3D printing of diverse objects with various properties for a wide range of applications.

CONCLUSIONS

In summary, we have established a new Print-Healing strategy based on an emerging spontaneously self-healing polymer ink to address a series of key challenges of FDM 3D printing. These include avoiding support structures, inducing strong interlayer adhesion, enabling large-size fabrication, and self-healing of subsequent damage. The key to realizing this strategy is the newly designed polymer ink with a suitable combination of a mobile molecular chain, dynamic bonds, and stable networks. This strategy significantly enhances the achievable complexity, size, and performance of FDM 3D printed objects. The entire fabrication process can be performed using common FDM 3D printers without additional treatment. The 3D printing ink developed here can readily be synthesized from inexpensive commercially available chemicals in one step, which could easily be made available in large quantities. Many self-healing materials can be used with this strategy to produce objects with diverse properties. Overall, this study provides a simple, practical, powerful way based on emerging dynamic chemistry to tailor 3D

objects with sophisticated architectures and outstanding performance, will widen the capability of 3D printing technology, and enable new applications in various fields.

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Author contributions Zuo H, Wu Q and You Z conceived the idea and designed the experiments. You Z directed the entire project. Zuo H performed the experiments (with involvement of Liu Z, Zhang L, Liu G and Ouyang X). Zuo H, Liu Z, Zhang L, Guan Q and Wu Q contributed to data analysis and interpretation. Zuo H and You Z wrote the manuscript. All authors commented on the manuscript.

Conflict of interest The authors declare that they have no conflict of interest.

Supplementary information Supporting data are available in the online version of the paper.

ARTICLES



Han Zuo is a PhD student at the State Key Laboratory for Modification of Chemical Fibers and Polymer Materials at Donghua University. From 2016 to now, she has been conducting her master and doctoral research at Donghua University. Her current research involves biomaterials, 3D printing and self-healing polymers.



Zhengwei You is a professor and the chair of the Department of Composite Materials at Donghua University. He serves as the director of Research Base of Textile Materials for Flexible Electronics and Biomedical Applications, China Textile Engineering Society. He received his PhD degree from Shanghai Institute of Organic Chemistry and conducted research at Georgia Institute of Technology, University of Pittsburgh, and Bayer MaterialScience. His current research involves elastomers, biomaterials, 3D printing, and stretchable electronics.



Qilin Wu received her PhD degree from Donghua University in 2002. As a visiting scholar, she worked at the University of California, Davis for one year from 2006 to 2007. Now she is a full professor of Donghua University. Her research focuses on composite materials.

自愈合材料实现自支撑各向同性3D打印

左涵¹, 刘增贺¹, 张璐之¹, 刘庚鑫^{1,2}, 欧阳希凯^{1,2}, 管清宝¹, 吴琪琳^{1*}, 游正伟^{1*}

摘要 3D打印已经在诸多领域产生了重要影响,其中熔融沉积成型(fused deposition modeling, FDM)是最通用和最经济的3D打印技术.然而,FDM通常需要支撑结构,这大大增加了加工的复杂性和成本.此外,层间结合力差极大地影响了FDM 3D打印制品的机械稳定性.本文提出了一种新的打印-愈合策略来解决上述挑战.采用了三重动态键设计,研制了一种具有良好的打印性能和室温自愈能力的聚合物.利用简便紧凑型的3D打印机打印出了各种形状的物体,并通过自修复便捷地将它们组装成大型复杂的三维结构. 三重动态键显著提升了打印制品层与层之间的结合力.此外,损坏的打印品可以自我修复,这大大延长了它们的使用寿命.这项工作为解决FDM 3D打印的关键瓶颈问题提供了一种简单有效的方法,有望在多个领域获得应用.