

Finite-Time Adaptive Fuzzy DSC for Uncertain Switched Systems

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Abstract The finite-time adaptive fuzzy tracking control problem for a class of strict-feedback uncertain switched systems is investigated in this paper. Based on fuzzy approximation and adaptive dynamic surface control (DSC) technique, a finite-time adaptive state feedback fuzzy controller is developed via the common Lyapunov functions. Different from the existing works on uncertain switched systems, the DSC control scheme is developed based on a nonlinear filter to solve the "explosion of complexity" problem, and the structure of the proposed fuzzy controller is simple. Under the designed controller, all the signals of the closed-loop system remain semiglobally bounded, and within a finite-time interval, the system tracking error converges to an arbitrarily small region. That is, the semi-globally practical finite-time stability of the controlled system is guaranteed. To show the availability of the presented control scheme, a simulation example is given in this paper.

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1 Introduction

In the past decades, compared with asymptotic stabilization, the systems with finite-time convergence demonstrate some nice features, such as faster convergence, high accuracies and better robustness to uncertainties, and these benefits render that the method of finite-time stabilization becomes one of the most appealing tools in practical applications, lots of works have been obtained for a large variety of systems (e.g., see [1-11]). The fundamental research of the finite-time stability is proposed in [1]. Subsequently, a lot of finite-time control problems of linear/nonlinear systems have been solved. For the timevarying systems and impulsive dynamical systems, some sufficient conditions of the finite-time stability are established in [6, 7]. The finite-time control problems for timevarying linear systems are studied in [8, 9] using linear matrix inequalities (LMIs) method. For the disturbed system with mismatching condition, the problem of finite-time output regulation control is investigated based on a composite control design method in [10]. For a class of nonlinear time-varying interconnected systems, the decentralized control problem is studied in [12]. The finitetime stability problem of a class of homogeneous stochastic nonlinear systems modeled by stochastic differential equations is studied in [11] and it is shown that the finitetime stability of stochastic system can be ensured under some appropriate conditions.

In recent years, some significant results of finite-time control problems for different types of uncertain systems have been reported (e.g., see [13–27]). The authors in [14] study the problem of finite-time stabilization for nonlinear systems by Hölder continuous state feedback. For nonlinear systems with parametric and dynamic uncertainties, the non-smooth finite-time stabilization problem is investigated in [16]. For the SISO nonlinear systems, assume that the system of non-linear functions is unknown, and the adaptive practical finite-time control problem is addressed in [26] using backstepping design method. For the nonstrict feedback nonlinear systems, a finite-time tracking control scheme based on neural network is established in [27].

As a typical class of hybrid systems, lots of interesting control problems have been addressed for switched systems (e.g., see [28–34]), particularly in the finite-time stability research of the switched systems (e.g., see [35-50]). The stability analysis for uncertain nonlinear switched systems is reported in [35]. The authors in [41] study the problem of finite-time stabilization for a class of switched stochastic nonlinear systems in p-normal form, and it shows that the resulting closed-loop system is finite-time stable in probability. The problem of global adaptive finite-time stabilization for a class of switched nonlinear parameterized systems is studied in [42]. Furthermore, for uncertain nonlinear systems with unknown system functions, two effective control strategies are established using fuzzy logic systems [43, 44] or NNs [27] to approximate unknown nonlinear functions. Whereafter, some research results have been obtained via approximation-based adaptive fuzzy or NN control methods for the uncertain nonlinear switched systems, for instance, see [45–47, 51–53] for adaptive fuzzy control and [48-50, 54] for adaptive NN control.

Note that for the above-reported works on uncertain switched systems, the desired finite-time controller is developed by employing the traditional adaptive backstepping method which leads to the repeated differentiation of the virtual control variables in the design process, and the "explosion of complexity" problem occurs. To solve this issue, this paper studies the finite-time adaptive fuzzy tracking problem for a class of strict-feedback uncertain switched systems based on DSC technique. The main work of this paper is listed as following.

- (i) To our knowledge, this paper is the first work to address the finite-time adaptive DSC for uncertain switched systems to solve the "explosion of complexity" problem which widely exists in the reported results (e.g., see [45–50, 54]), and the adaptive fuzzy controller is developed with a simple structure.
- (ii) The fuzzy logic systems are employed to approximate the unknown common dominant functions of the considered systems, and the desired controller

is designed using the adaptive DSC method with a nonlinear filter based on the common Lyapunov functions. It proves that under the proposed controller, all the signals of the closed-loop system remain semiglobally bounded, and within a finite time interval, the system tracking error can converge to an arbitrarily small region.

The following is the organization of this paper. The problem statement and some preliminaries are introduced in Sect. 2. Next, adaptive dynamic surface controller design and stability analysis are presented in Sect. 3. Then, a simulation example is given in Sect. 4. A conclusion is drawn in Sect. 5.

2 Problem Statement and Some Preliminaries

Consider the uncertain strict-feedback nonlinear switched system as following

$$\begin{cases} \dot{x_i} = x_{i+1} + f_{i,\varrho(t)}(\bar{x_i}), i = 1, \dots, n-1\\ \dot{x_n} = u + f_{n,\varrho(t)}(\bar{x_n}),\\ y = x_1, \end{cases}$$
(1)

where $\bar{x_i} = [x_1, ..., x_i]T \in \mathbb{R}^i, i = 1, ..., n$ are the states of the system, $u \in \mathbb{R}$ is the control input, and $y \in \mathbb{R}$ is the system output. $f_i(\cdot) : \mathbb{R}^i \to \mathbb{R}$ are unknown continuously differentiable functions and $\varrho(t) : [0, \infty) \to \mathbb{N} = \{1, 2, ..., p\}$ is the switching signal.

The control objective for system (1) is to design a finitetime adaptive fuzzy controller such that the system output follows the appointed reference signal $y_r(t)$, and the boundedness of the other closed-loop signals is guaranteed.

Remark 1 The adaptive control problems have been widely reported for uncertain switched systems (e.g., see [45-50, 54, 55]). In this paper, the finite-time adaptive DSC problem is first addressed for uncertain switched systems and the proposed control scheme is developed to solve the "explosion of complexity" problem.

Definition 1 [56] The equilibrium position $\zeta = 0$ of the nonlinear system $\dot{\zeta} = f(\zeta, u)$ is semi-globally practical finite-time stable (SGPFS) if for all $\zeta(t_0) = \zeta_0$, there exist a scalar $\varepsilon > 0$ and a settling time $T(\varepsilon, \zeta_0) < \infty$ such that

$$\|\varsigma(t)\| \le \varepsilon, \forall t > t_0 + T.$$
⁽²⁾

Assumption 1 The reference signal $y_r(t)$ and its derivatives $\dot{y_r}(t)$ and $\ddot{y_r}(t)$ are bounded.

Lemma 1 [48] Let c_1 , c_2 and c_3 be positive constants. Then for any real variables χ and ζ , one has

$$|\chi|^{c_1}|\zeta|^{c_2} \le \frac{c_1}{c_1+c_2}c_3|\chi|^{c_1+c_2} + \frac{c_2}{c_1+c_2}c_3^{-\frac{c_1}{c_2}}|\zeta|^{c_1+c_2}.$$
 (3)

Lemma 2 [54] For $z_i \in R, i = 1, 2, ..., n$ and 0 < l < 1, one has

$$\left(\sum_{i=1}^{n} |z_i|\right)^l \le \sum_{i=1}^{n} |z_i|^l \le n^{1-l} \left(\sum_{i=1}^{n} |z_i|\right)^l.$$
(4)

Lemma 3 [27] Consider a nonlinear system $\dot{\zeta} = f(\zeta, u)$. Suppose that there exist a smooth positive definite function $V(\zeta)$ and scalars $a_0 > 0$, $0 < \lambda < 1$ and $b_0 > 0$ such that

$$\dot{V}(\varsigma) \le -a_0 V^{\lambda}(\varsigma) + b_0, t \ge 0, \tag{5}$$

then the nonlinear system $\dot{\varsigma} = f(\varsigma, u)$ is semi-globally practical finite-time stable (SGPFS).

Lemma 4 [57, 58] For any $\varepsilon > 0$ and $z \in R$, the following inequality can be obtained

$$0 \le |z| - \frac{z^2}{\sqrt{z^2 + \varepsilon^2}} < \varepsilon.$$
(6)

Lemma 5 [45–47] For any continuous function D(x) on a compact set Ω and an expected precision $\varepsilon > 0$, there exists an FLS $\theta^{*T}S(x)$ such that

$$\sup_{x\in\Omega} |D(x) - \theta^{*T} S(x)| \le \varepsilon.$$
(7)

By Lemma 5, for a given $\varepsilon^* > 0$ and any continuous function D(x) on the set Ω , there exists an FLS $\theta^{*T}S(x)$, such that

$$D(x) = \theta^{*T} S(x) + \varepsilon(x), \tag{8}$$

where $\varepsilon(x)$ represents the approximation error satisfying $|\varepsilon(x)| \le \varepsilon^*$, and $0 < ST(x)S(x) \le 1$.

3 Adaptive Controller Design and Stability Analysis

3.1 Adaptive Controller Design

The finite-time adaptive fuzzy DSC scheme is established based on the backstepping technique, and it contains *n* steps as follows. The error variables are defined as $\tilde{*} = * - \hat{*}$, where $\hat{*}$ is the estimate of *.

• Step 1: The first surface error is defined as $z_1 = x_1 - y_r$, and the time derivative of z_1 is presented as

$$\dot{z}_1 = \dot{x}_1 - \dot{y}_r = x_2 + f_{1,\varrho(t)}(\bar{x_1}) - \dot{y}_r.$$
 (9)

Then the Lyapunov function is designed as

$$V_1 = \frac{1}{2}z_1^2 + \frac{1}{2\gamma_1}\tilde{\theta}_1^2, \tag{10}$$

where $\tilde{\theta}_1$ is the error of estimate θ_1 , and $\gamma_1 > 0$ is a design parameter.

In view of Eqs. (12)–(13), the following equation can be obtained

$$\dot{V}_{1} = z_{1}(x_{2} + f_{1,\varrho(t)}(\bar{x_{1}}) - \dot{y}_{r}) - \frac{1}{\gamma_{1}}\tilde{\theta}_{1}\dot{\hat{\theta}}_{1}$$
$$= z_{1}(x_{2} + f_{1,\varrho(t)}(\bar{x_{1}}) - \dot{y}_{r} + \alpha_{1} - \alpha_{1}) - \frac{1}{\gamma_{1}}\tilde{\theta}_{1}\dot{\hat{\theta}}_{1}.$$
(11)

On the basis of $f_{i,\varrho(t)}$, we can obtain the following inequality

$$|f_{i,\varrho(t)}| \le \sqrt{\sum_{j=1}^{p} f_{i,j}^2}.$$
 (12)

Then let $D_i(\bar{x}_i) = \sqrt{\sum_{j=1}^p f_{i,j}^2}$, and according to Lemma 5, the following equation can be obtained

$$D_i(\bar{x}_i) = \theta_i^{*T} S(\bar{x}_i) + \varepsilon_i(\bar{x}_i).$$
(13)

Using the Young's inequality and based on Eq. (20), one has

$$z_{1}f_{1,\varrho(t)} \leq |z_{1}||f_{1,\varrho(t)}| \\\leq |z_{1}||D_{1}| \\\leq \frac{1}{2} + \frac{1}{2}z_{1}^{2}\theta_{1}S_{1}^{T}(\bar{x}_{1})S_{1}(\bar{x}_{1}) + \frac{1}{2}z_{1}^{2} + \frac{1}{2}\varepsilon_{1}^{2},$$
(14)

where $\theta_1 = \theta_1^{*T} \theta_1^*$.

In view of (9)-(14), the following inequality can be obtained

$$\dot{V}_{1} \leq \frac{1}{2} + \frac{1}{2}z_{1}^{2}\theta_{1}S_{1}T(\bar{x}_{1})S_{1}(\bar{x}_{1}) + \frac{1}{2}z_{1}^{2} + \frac{1}{2}\varepsilon_{1}^{2} + z_{1}(x_{2} + \alpha_{1} - \alpha_{1} - \dot{y}_{r}) - \frac{1}{\gamma_{1}}\tilde{\theta}_{1}\dot{\hat{\theta}}_{1}.$$
(15)

Design the first virtual control law α_1 as

$$\alpha_1 = -\left(\frac{1}{2} + k_1\right) z_1 + \dot{y_r} - \frac{1}{2} z_1 \hat{\theta}_1 S_1 T(\bar{x_1}) S_1(\bar{x_1}),$$
(16)

and design the update law of $\hat{\theta}_1$ as

$$\dot{\hat{\theta}}_1 = \frac{1}{2} z_1^2 S_1 T(\bar{x}_1) S_1(\bar{x}_1) - \eta_1 \hat{\theta}_1, \qquad (17)$$

where $k_1 > 0$ and $\eta_1 > 0$ are design parameters. In view of (15)–(17), one has

$$\dot{V_1} \le -k_1 z_1^2 + z_1 (x_2 - \alpha_1) + \frac{1}{2} + \frac{\eta_1}{\gamma_1} \tilde{\theta_1} \hat{\theta_1} + \frac{1}{2} \varepsilon_1^2.$$
(18)

In the backstepping design, the second error signal is designed as $x_2 - \alpha_1$ to avoid the "explosion of complexity" problem, and a filtered virtual controller s_1 can be obtained using the following novel nonlinear filter

$$\tau_1 \dot{s_1} = -e_1 - \frac{\tau_1 \hat{M}_1^2 e_1}{\sqrt{\hat{M}_1^2 e_1^2 + \sigma^2}} - \tau_1 z_1,$$

$$s_1(0) = \alpha_1(0),$$
(19)

where the first boundary layer error is presented as $e_1 = s_1 - \alpha_1$. \hat{M}_1 is used to estimate M_1 and the clarification will be provided later. σ is any positive constant. τ_1 is a filter constant and can be designed.

Step *i* (i = 2, ..., n - 1): The *i*th surface error is defined as $z_i = x_i - s_{i-1}$, then the following equation can be obtained

$$\dot{z_{i}} = x_{i+1} + f_{i,\varrho(t)} + \frac{\hat{M}_{i-1}^{2}e_{i-1}}{\sqrt{\hat{M}_{i-1}^{2}e_{i-1}^{2} + \sigma^{2}}} + z_{i-1} + \frac{e_{i-1}}{\tau_{i-1}}.$$
(20)

The Lyapunov function candidate V_i can be designed as

$$V_{i} = V_{i-1} + \frac{1}{2}z_{i}^{2} + \frac{1}{2\gamma_{i}}\tilde{\theta}_{i}^{2}.$$
(21)

Using the Young's inequality and based on Lemma 5, the following inequality is obtained

$$z_{i}f_{i,\varrho(t)} \leq |z_{i}||f_{i,\varrho(t)}| \\\leq |z_{i}||D_{i}| \\\leq \frac{1}{2} + \frac{1}{2}z_{i}^{2}\theta_{i}S_{i}T(\bar{x}_{i})S_{i}(\bar{x}_{i}) + \frac{1}{2}z_{i}^{2} + \frac{1}{2}\varepsilon_{i}^{2},$$
(22)

where $\theta_i = \theta_i^{*T} \theta_i^*$.

Then we can design the virtual control law α_i and the update law $\hat{\theta}_i$ as following

$$\alpha_{i} = -\left(\frac{1}{2} + k_{i}\right)z_{i} - 2z_{i-1} - \frac{1}{2}z_{i}\hat{\theta}_{i}S_{i}T(\bar{x}_{i})S_{i}(\bar{x}_{i}) - \frac{\hat{M}_{i-1}^{2}e_{i-1}}{\sqrt{\hat{M}_{i-1}^{2}e_{i-1}^{2} + \sigma^{2}}} - \frac{e_{i-1}}{\tau_{i-1}},$$
(23)

$$\dot{\hat{\theta}}_i = \frac{1}{2} z_i^2 S_i T(\bar{x}_i) S_i(\bar{x}_i) - \eta_i \hat{\theta}_i, \qquad (24)$$

where k_i and η_i are positive design parameters, $\hat{\theta}_i$ is the estimate of θ_i .

In view of (20)–(24), consider the time derivative of V_i as

$$\begin{split} \dot{V}_{i} &= V_{i-1}^{\cdot} + z_{i} \dot{z}_{i} - \frac{1}{\gamma_{i}} \tilde{\theta}_{i} \dot{\hat{\theta}}_{i} \\ &\leq -\sum_{j=1}^{i} k_{j} z_{j}^{2} + \sum_{j=1}^{i-1} z_{j} e_{j} + (x_{i+1} - \alpha_{i}) z_{i} + \frac{i}{2} + \sum_{j=1}^{i} \frac{1}{2} \varepsilon_{j}^{2} \\ &+ \sum_{j=1}^{i} \frac{\eta_{j}}{\gamma_{j}} \tilde{\theta}_{j} \hat{\theta}_{j}. \end{split}$$

$$(25)$$

The filtered virtual controller s_i can be obtained using the following nonlinear filter

$$\tau_{i}\dot{s_{i}} = -e_{i} - \frac{\tau_{i}\hat{M_{i}^{2}}e_{i}}{\sqrt{\hat{M_{i}^{2}}e_{i}^{2} + \sigma^{2}}} - \tau_{i}z_{i},$$

$$s_{i}(0) = \alpha_{i}(0),$$
(26)

and define

$$e_i = s_i - \alpha_i, \tag{27}$$

where the *i*th boundary layer error is e_i . \hat{M}_i is the estimate of M_i and the clarification will be presented later. τ_i is a filter constant.

• Step *n*: Consider the *n*th surface error as $z_n = x_n - s_{n-1}$, and the following equation holds

$$\dot{z}_{n} = u + f_{n,\varrho(t)} + \frac{\hat{M}_{n-1}^{2} e_{n-1}}{\sqrt{\hat{M}_{n-1}^{2} e_{n-1}^{2} + \sigma^{2}}} + z_{n-1} + \frac{e_{n-1}}{\tau_{n-1}}.$$
(28)

The Lyapunov function candidate V_n is designed as

$$V_n = V_{n-1} + \frac{1}{2}z_n^2 + \frac{1}{2\gamma_n}\tilde{\theta}_n^2, \qquad (29)$$

and consider the time derivative of V_n as

$$\dot{V}_{n} = \dot{V}_{n-1} + z_{n}(u + f_{n,\varrho(t)}) + \frac{\hat{M}_{n-1}^{2}e_{n-1}}{\sqrt{\hat{M}_{n-1}^{2}e_{n-1}^{2} + \sigma^{2}}} + z_{n-1} + \frac{e_{n-1}}{\tau_{n-1}}) - \frac{1}{\gamma_{n}}\tilde{\theta}_{n}\hat{\theta}_{n}.$$
(30)

By applying Young's inequality and on account of Lemma 5, the following inequality is obtained

$$z_{n}f_{n,\varrho(t)} \leq |z_{n}||f_{n,\varrho(t)}| \\\leq |z_{n}||D_{n}| \\\leq \frac{1}{2} + \frac{1}{2}z_{n}^{2}\theta_{n}S_{n}T(\bar{x}_{n})S_{n}(\bar{x}_{n}) + \frac{1}{2}z_{n}^{2} + \frac{1}{2}\varepsilon_{n}^{2},$$
(31)

where $\theta_n = \theta_n^{*T} \theta_n^*$. Design the actual control law *u* as

$$u = -\left(\frac{1}{2} + k_n\right)z_n - 2z_{n-1} - \frac{1}{2}z_n\hat{\theta}_n S_n T(\bar{x}_n)S_n(\bar{x}_n) - \frac{\hat{M}_{n-1}^2 e_{n-1}}{\sqrt{\hat{M}_{n-1}^2 e_{n-1}^2 + \sigma^2}} - \frac{e_{n-1}}{\tau_{n-1}},$$
(32)

and the update law for $\hat{\theta}_i$ is chosen as

$$\dot{\hat{\theta}}_n = \frac{1}{2} z_n^2 S_n T(\bar{x}_n) S_n(\bar{x}_n) - \eta_n \hat{\theta}_n, \qquad (33)$$

where k_n , η_n are positive design parameters, $\hat{\theta}_n$ is the estimate of θ_n .

In view of (28)–(33), we can obtain the following inequality

$$\dot{V_n} \le -\sum_{j=1}^n k_j z_j^2 + \sum_{j=1}^{n-1} z_j e_j + \frac{n}{2} + \sum_{j=1}^n \frac{1}{2} \varepsilon_j^2 + \sum_{j=1}^n \frac{\eta_j}{\gamma_j} \tilde{\theta}_j \hat{\theta}_j.$$
(34)

Remark 2 From the above subsection, it can be seen that the DSC method with a nonlinear filter [58] is introduced to overcome the "explosion of complexity" problem, and by introducing a novel estimated parameter, the nonlinear filter is developed. Then, the desired fuzzy controller is designed with a simple structure and the practical finitetime stability of the closed-loop systems is guaranteed. This is the main advantage of the proposed control method.

3.2 Stability Analysis

Based on the inequality (34), the main result of this paper is presented using the following theorem.

Differentiating the boundary layer errors $e_i = s_i - \alpha_i$ yields

$$\dot{e}_{i} = \frac{-e_{i}}{\tau_{i}} - \frac{\hat{M}_{i}^{2}e_{i}}{\sqrt{\hat{M}_{i}^{2}e_{i}^{2} + \sigma^{2}}} - z_{i} + B_{i}(z_{1}, \dots, z_{i},$$

$$e_{1}, \dots, e_{i}, \hat{\theta}_{1}, \dots, \hat{\theta}_{i},$$

$$\hat{M}_{1}, \dots, \hat{M}_{i}, y_{r}, \dot{y_{r}}, \dot{y_{r}}), i = 1, \dots, n - 1,$$
(35)

where

$$B_{1}(\cdot) = -\dot{\alpha}_{1}$$

$$= -\frac{\partial\alpha_{1}}{\partial x_{1}}\dot{x}_{1} - \frac{\partial\alpha_{1}}{\partial\dot{\theta}_{1}}\dot{\dot{\theta}}_{1} - \frac{\partial\alpha_{1}}{\partial y_{r}}\dot{y}_{r} - \frac{\partial\alpha_{1}}{\partial\dot{y}_{r}}\ddot{y}_{r},$$
(36)

$$B_{i}(\cdot) = -\alpha_{i}$$

$$= -\sum_{j=1}^{i} \frac{\partial \alpha_{i}}{\partial x_{j}} \dot{x}_{j} - \frac{\partial \alpha_{i}}{\partial \hat{\theta}_{j}} \dot{\hat{\theta}}_{j} - \frac{\partial \alpha_{i}}{\partial e_{i-1}} \dot{e}_{i-1}$$

$$- \frac{\partial \alpha_{i}}{\partial \hat{M}_{i-1}} \dot{M}_{i-1} - \frac{\partial \alpha_{i}}{\partial y_{r}} \dot{y}_{r} - \frac{\partial \alpha_{i}}{\partial \dot{y}_{r}} \ddot{y}_{r}$$
(37)

and the functions of B_i , i = 1, ..., n - 1 are continuous.

The Lyapunov function candidate is considered as following

$$V = V_n + \sum_{i=1}^{n-1} \frac{1}{2} e_i^2 + \sum_{i=1}^{n-1} \frac{1}{2\beta_i} \tilde{M}_i^2,$$
(38)

where β_i , i = 1, ..., n - 1 are positive design parameters.

Theorem 1 Consider the switched nonlinear strict-feedback system (1) including the nonlinear filters (19) and (26), the virtual control laws (16) and (23), the actual control law (32), and the update laws (17), (24), and (33). Under Assumption 1, there exit design parameters k_i , γ_i , β_i , η_i , i = 1, ..., n, τ_j , and ρ_j , j = 1, ..., n - 1 such that the following statements hold:

- (i) all the closed-loop signals are semi-globally bounded.
- (ii) the output $y_{(t)}$ can track the given signal $y_r(t)$ in finite time.

Proof The compact sets are defined as

$$\Omega_1 = \{ [y_r, \dot{y_r}, \ddot{y_r}] T : y_r^2 + \dot{y_r}^2 + \dot{y_r}^2 \le B_0 \},$$
(39)

$$\Omega_2 = \{ V(t) \le q \},\tag{40}$$

where B_0 and q are known positive constants. It is noted that set $\Omega_0 \times \Omega_1$ is also a compact in R^{4n+1} . As a consequence, the positive constants M_i can be obtained with $|B_i(\cdot)| \le M_i$ on $\Omega_1 \times \Omega_2$. It can be grasped quite clearly that the definitive values of M_i are unknown. Next, we will analyze the finite-time stability of the resulting closed-loop system.

The time derivative of V yields

$$\begin{split} \dot{V} &= \dot{V}_{n} + \sum_{i=1}^{n-1} e_{i}\dot{e}_{i} - \sum_{i=1}^{n-1} \frac{1}{\eta_{i}} \tilde{M}_{i}\dot{\hat{M}}_{i} \\ &\leq -\sum_{i=1}^{n} k_{i}z_{i}^{2} - \sum_{i=1}^{n-1} \frac{e_{i}^{2}}{\tau_{i}} - \sum_{i=1}^{n-1} \frac{\hat{M}_{i}^{2}e_{i}^{2}}{\sqrt{\hat{M}_{i}^{2}e_{i}^{2} + \sigma^{2}}} \\ &+ \sum_{i=1}^{n-1} M_{i}|e_{i}| - \sum_{i=1}^{n-1} \frac{1}{\beta_{i}} \tilde{M}_{i}\dot{\hat{M}}_{i} + \frac{n}{2} + \sum_{i=1}^{n} \frac{1}{2}\varepsilon_{i}^{2} + \sum_{i=1}^{n} \frac{\eta_{i}}{\gamma_{i}}\tilde{\theta}_{i}\hat{\theta}_{i}. \end{split}$$

$$(41)$$

Form Lemma 4, it follows that

$$M_{i}|e_{i}| = \hat{M}_{i}|e_{i}| + \tilde{M}_{i}|e_{i}| \\ \leq \frac{\hat{M}_{i}^{2}e_{i}^{2}}{\sqrt{\hat{M}_{i}^{2}e_{i}^{2} + \sigma^{2}}} + \sigma + \tilde{M}_{i}|e_{i}|,$$
(42)

then the following inequality can be obtained

$$\dot{V} \leq -\sum_{i=1}^{n} k_{i} z_{i}^{2} - \sum_{i=1}^{n-1} \frac{e_{i}^{2}}{\tau_{i}} - \sum_{i=1}^{n-1} \frac{1}{\beta_{i}} \tilde{M}_{i} (\dot{M}_{i} - \beta_{i} | e_{i} |) + (n-1)\sigma + \frac{n}{2} + \sum_{i=1}^{n} \frac{1}{2} \varepsilon_{i}^{2} + \sum_{i=1}^{n} \frac{\eta_{i}}{\gamma_{i}} \tilde{\theta}_{i} \hat{\theta}_{i}.$$

$$(43)$$

The update law for \hat{M}_i is considered as following

$$\hat{M}_{i} = \beta_{i}|e_{i}| - \rho_{i}\hat{M}_{i}, i = 1, \dots, n-1.$$
(44)

In view of (41)-(44), we can obtain the following inequality

$$\dot{V} \leq -\sum_{i=1}^{n} k_{i} z_{i}^{2} - \sum_{i=1}^{n-1} \frac{e_{i}^{2}}{\tau_{i}} + (n-1)\sigma + \sum_{i=1}^{n} \frac{\eta_{i}}{\gamma_{i}} \tilde{\theta}_{i} \hat{\theta}_{i} + \sum_{i=1}^{n-1} \frac{\rho_{i}}{\beta_{i}} \tilde{M}_{i} \hat{M}_{i} + \frac{n}{2} + \sum_{i=1}^{n} \frac{1}{2} \varepsilon_{i}^{2}.$$
(45)

By the definition of $\tilde{\theta}_i$ and \tilde{M}_i , the following inequalities can be obtained

$$\tilde{\theta}_i \hat{\theta}_i = \tilde{\theta}_i (\theta_i - \tilde{\theta}_i) \le \frac{1}{2} \theta_i^2 - \frac{1}{2} \tilde{\theta}_i^2, \tag{46}$$

$$\tilde{M}_{i}\hat{M}_{i} = \tilde{M}_{i}(M_{i} - \tilde{M}_{i}) \le \frac{1}{2}M_{i}^{2} - \frac{1}{2}\tilde{M}_{i}^{2}.$$
(47)

In view of inequalities (35)-(47), one has

$$\dot{V} \leq -\sum_{i=1}^{n} k_{i} z_{i}^{2} - \sum_{i=1}^{n-1} \frac{e_{i}^{2}}{\tau_{i}} - \sum_{i=1}^{n} \frac{\eta_{i}}{2\gamma_{i}} \tilde{\theta}_{i}^{2} - \sum_{i=1}^{n-1} \frac{\rho_{i}}{2\beta_{i}} \tilde{M}_{i}^{2} + (n-1)\sigma + \sum_{i=1}^{n} \frac{\eta_{i}}{\gamma_{i}} \theta_{i}^{2} + \sum_{i=1}^{n-1} \frac{\rho_{i}}{2\beta_{i}} M_{i}^{2} + \frac{n}{2} + \sum_{i=1}^{n} \frac{1}{2} \varepsilon_{i}^{2}.$$

$$(48)$$

By applying Lemma 1 and taking $x = \sum_{i=1}^{n} (\frac{1}{2}z_i^2)$, y = 1, $c_1 = \lambda$, $c_2 = 1 - \lambda$ and $c_3 = \lambda^{-1}$ into account, the following inequality can be obtained

$$\sum_{i=1}^{n} \left(\frac{1}{2} z_{i}^{2}\right)^{\lambda} \leq \sum_{i=1}^{n} \frac{1}{2} z_{i}^{2} + (1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}}.$$
(49)

Then, the following inequality can be obtained using Lemma 2

$$-\sum_{i=1}^{n} \left(\frac{1}{2}z_{i}^{2}\right)^{\lambda} \leq -\left(\sum_{i=1}^{n} \frac{1}{2}z_{i}^{2}\right)^{\lambda}.$$
(50)

In view of (49)–(50), one has

$$-\sum_{i=1}^{n} \frac{1}{2} z_i^2 \le -\left(\sum_{i=1}^{n} \frac{1}{2} z_i^2\right)^{\lambda} + (1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}}.$$
 (51)

Similarly, we can also obtain the following inequalities

$$-\sum_{i=1}^{n} \frac{1}{2\gamma_i} \theta_i^2 \le -\left(\sum_{i=1}^{n} \frac{1}{2\gamma_i} \theta_i^2\right)^{\lambda} + (1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}},\tag{52}$$

$$-\sum_{i=1}^{n-1} \frac{1}{2} e_i^2 \le -\left(\sum_{i=1}^n \frac{1}{2} e_i^2\right)^{\lambda} + (1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}},\tag{53}$$

$$-\sum_{i=1}^{n-1} \frac{1}{2\beta_i} \tilde{M}_i^2 \le -\left(\sum_{i=1}^n \frac{1}{2\beta_i} \tilde{M}_i^2\right)^{\lambda} + (1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}}.$$
 (54)

In view of inequalities (48)–(54), one has

$$\dot{V} \leq -a_0 \left(\sum_{i=1}^n \frac{1}{2} z_i^2\right)^{\lambda} - a_0 \left(\sum_{i=1}^n \frac{1}{2\gamma_i} \tilde{\theta}_i^2\right)^{\lambda} - a_0 \left(\sum_{i=1}^{n-1} \frac{1}{2} e_i^2\right)^{\lambda} - a_0 \left(\sum_{i=1}^{n-1} \frac{1}{2\beta_i} \tilde{M}_i^2\right)^{\lambda} + b_0,$$
(55)

i.e.,

$$\dot{V} \le -a_0 V^{\lambda} + b_0, \tag{56}$$

where

$$a_{0} = \min\{2k_{1}...2k_{n}, \frac{2}{\tau_{1}}, ..., \frac{2}{\tau_{n-1}}, \\\eta_{1}, ..., \eta_{n}, \rho_{1}, ..., \rho_{n-1}\},$$
(57)

$$b_{0} = (n-1)\sigma + \frac{n}{2} + \sum_{i=1}^{n} \frac{1}{2}\varepsilon_{i}^{2} + \sum_{i=1}^{n} \frac{\eta_{i}}{\gamma_{i}} \left(\frac{1}{2}\theta_{i}^{2}\right) + \sum_{i=1}^{n-1} \frac{\rho_{i}}{\beta_{i}} \left(\frac{1}{2}M_{i}^{2}\right) + 4(1-\lambda)\lambda^{\frac{\lambda}{1-\lambda}}.$$
(58)

Let $T^* = \frac{1}{(1-\lambda)\xi a_0} [V^{1-\lambda}(0) - (\frac{b_0}{(1-\xi)a_0})^{\frac{1-\lambda}{2}}]$, where V(0) means the initial value of V(t). On the basis of Lemma 3, for $\forall t \ge T^*$, $V^{\lambda} \le \frac{b_0}{(1-\xi)a_0}$, that is, all the signals of the closed-loop system are SGPFS. Furthermore, based on the definition of V(t), for $\forall t \ge T^*$, we have

$$|y - y_r| \le 2 \left(\frac{b_0}{(1 - \xi)a_0} \right)^{\frac{1}{2\epsilon}},\tag{59}$$

which implies that after the finite time T^* , the tracking error will be in a small neighborhood of the origin. This completes the proof.

4 Simulation Example

To show the availability of the presented control scheme, the switched RCL circuit system is presented in this paper, and it is shown in Fig. 1. According to [57], we describe the switched RCL circuit system as

$$\begin{cases} \dot{x}_1 = x_2 + f_{1,\varrho(t)}(x_1) \\ \dot{x}_2 = u + f_{2,\varrho(t)}(\bar{x_2}) \\ y = x_1, \end{cases}$$
(60)

where $\varrho(t): R \to \{1,2\}, \quad f_{1,1} = f_{1,2} = (1/L)x_2 - x_2,$ $f_{2,1} = -(1/C_1)x_1 - (R/L)x_2, f_{2,2} = -(1/C_2)x_1 - (R/L)x_2,$ $x_1 = q_c$ means the charge in capacitor, $x_2 = \phi_L$ stands for the flux in the inductance for this circuit, C_i denotes the *i*th capacitor, *L* is the inductance, *R* shows the resistance, *u* represents the voltage, which also means the system input. The related parameters are selected as R = 1, L = 0.5, $C_1 = 60$ and $C_2 = 100$. The control objective is that within a finite time interval, the system tracking error can converge to an arbitrarily small region, and the reference signal y_r is chosen as $y_r = 0.25 \sin(2t)$.

Nine fuzzy sets are defined over [-2, 2] for all state variables by choosing the partitioning points as -2, -1.5, -1, -0.5, 0, 0.5, 1, 1.5, 2 and the fuzzy membership functions are presented as follows

$$\begin{split} \mu_{F_i^1}(x_i) &= \exp(-0.5(x_i+2)^2), \quad \mu_{F_i^2}(x_i) = \exp(-0.5(x_i+1.5)^2), \\ \mu_{F_i^3}(x_i) &= \exp(-0.5(x_i+1)^2), \quad \mu_{F_i^4}(x_i) = \exp(-0.5(x_i+0.5)^2), \\ \mu_{F_i^5}(x_i) &= \exp(-0.5(x_i+0)^2), \quad \mu_{F_i^6}(x_i) = \exp(-0.5(x_i-2)^2), \\ \mu_{F_i^7}(x_i) &= \exp(-0.5(x_i-1.5)^2), \quad \mu_{F_i^8}(x_i) = \exp(-0.5(x_i-1)^2), \\ \mu_{F_i^9}(x_i) &= \exp(-0.5(x_i-0.5)^2). \end{split}$$

According to (8), S_i can be constructed for i = 1, 2. Following Theorem 1, we can have adaptive fuzzy controller (32) with n = 2, the virtual control α_1 (16), and adaptive laws $\dot{\hat{\theta}}_i$, i = 1, 2 to control system (60).

The design parameters are selected as $k_1 = 30$, $k_2 = 0.3$, $\eta_1 = 3$, $\eta_2 = 5$, $\beta_1 = 0.5$, $\rho_1 = 0.3$, $\tau_1 = 0.2$ and $\sigma = 0.3$. The initial conditions of this switched system are presented as $x_1(0) = 0.01$, $x_2(0) = 0.1$, $\hat{\theta}_1(0) = 0.02$, $\hat{\theta}_2(0) = 0.1$ and $\hat{M}_1(0) = 0.01$.

According to the above analysis, the simulation results are displayed in Figs. 2, 3, 4, 5, 6, 7. Figure 2 gives the switched signal. Figure 3 shows the output tracking performance. Figure 4 shows the tracking error. From Figs. 3, 4, we can find that the control objective of this paper has been achieved. The control signal *u* is presented in Fig. 5. Figure 6 expresses the curves of adaptive laws of $\hat{\theta}_1$ and $\hat{\theta}_2$. Figure 7 shows the adaptation of parameter \hat{M}_1 . It is obvious that the boundedness of all the signals in this closed-loop system can be achieved.

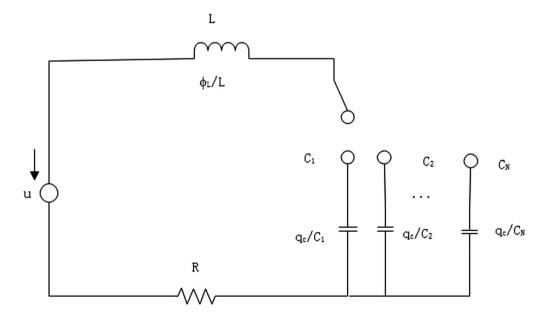


Fig. 1 Switched RCL circuit

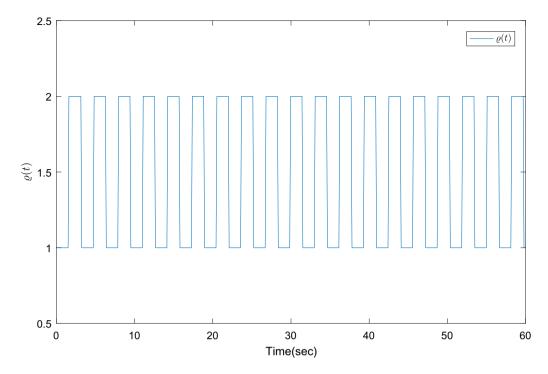


Fig. 2 Switched signal

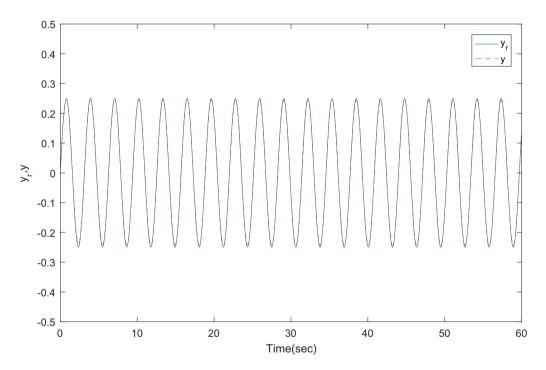


Fig. 3 The reference trajectory y_r and the output signal y

5 Conclusions

This paper studies the finite-time adaptive fuzzy tracking problem for a class of strict-feedback uncertain switched systems. The unknown system functions are approximated online using FLS. In addition, the common Lyapunov functions are presented to deal with the switched signals of this system. According to a nonlinear filter, a DSC method is presented to overcome the problem from "explosion of complexity". The boundedness of all the signals in the closed-loop system can be guaranteed under the designed controller and adaptive laws. Furthermore, it shows that the

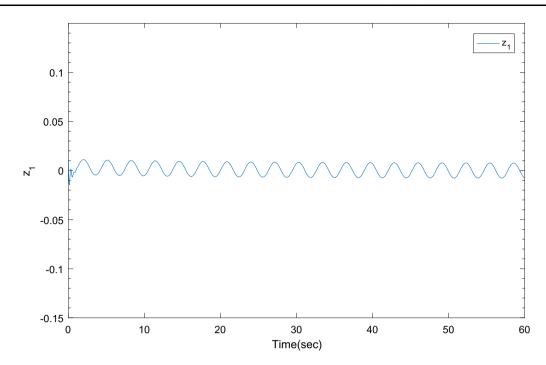


Fig. 4 Tracking error z_1

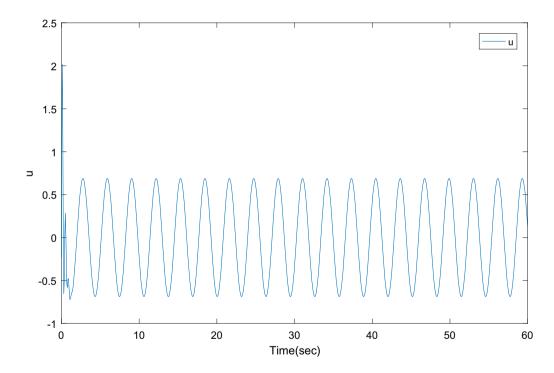


Fig. 5 The control signal u

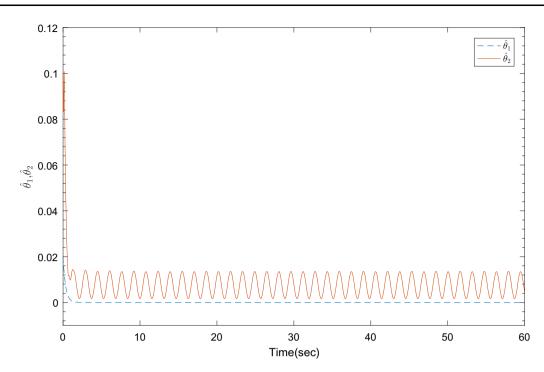


Fig. 6 Adaptive laws for $\hat{\theta}_1$, $\hat{\theta}_2$

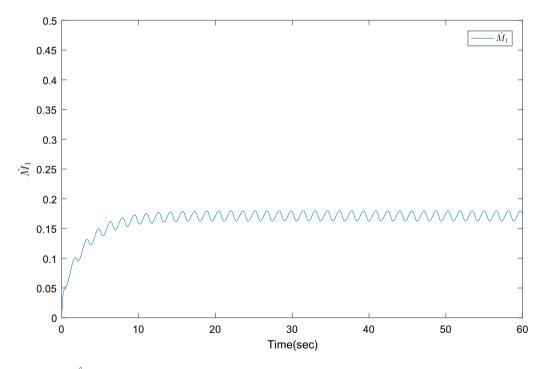


Fig. 7 Adaptive parameter \hat{M}_1

output signal can track the reference signal to a small compact in finite time.

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Compliance with Ethical Standards

Conflicts of Interest The authors declare that they have no conflict of interest.

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