**ORIGINAL ARTICLE**



# **Application of SWAT model and SWAT‑CUP software in simulation and analysis of sediment uncertainty in arid and semi‑arid watersheds (case study: the Zoshk–Abardeh watershed)**

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### **Abstract**

This research aimed to appraise the performance of the Soil and Water Assessment Tool (SWAT) model in sediment fow simulation and also to investigate the uncertainty of the model in the watershed areas of arid and semi-arid regions. In this survey, we used the Sequential Uncertainty Fitting ver.2 (SUFI-2) algorithm to assess the uncertainty and calibrate the model. Diferent factors of water resources are simulated, and we consider the crop yield and water quality at the Hydrological Response Units (HRU) level. Besides, to quantify the water resources, we implemented monthly time intervals. Also, we used monthly time intervals to quantify the water resources. The results showed that in a 3-year validation period (2007–2010), the *P*-factor and the *r*-factor were 0.28 and 0.38 respectively, while in the 7-year calibration period (2000–2006), these two factors were 0.29 and 0.39, respectively. The fndings of this study proved that in the validation period, statistical indicators of model evaluation comprise  $R^2$ ,  $bR^2$ , and the Nash–Sutcliffe efficiency (NSE) coefficients were 0.85, 0.23, and 0.47, respectively, while in the calibration period, these coefficients were 0.46, 0.14, and 0.37, respectively. The results of uncertainty and calibration analysis were acceptable, but in the validation phase, the model has been more applicable and useful. These results show the acceptable efficiency of the SWAT model in simulating the sediment load of the study area. To assess the sensitivities of 22 input parameters, we used SWAT Calibration Uncertainties Program (SWAT-CUP) and achieved three of the most sensitive parameters comprising CN2, SOL\_BD, and USLE\_P. In contrast, the parameters with the least sensitivity were SLSUBBSN, GW\_DELAY, and ESCO. We can use the calibrated model as inputs for SWAT, to assess the impact of climate change on soil erosion.

**Keywords** SWAT · SUFI-2 · Calibration · Uncertainty analysis · Zoshk–Abardeh watershed

# **Introduction**

In many parts of Iran, the quality and quantity of groundwater have settled and water levels have drawdown, resulting in indiscriminate depletion of water and its potential unfavorable environmental impacts (Gholami et al. [2016;](#page-8-0) Alizadeh et al. [2018\)](#page-8-1). However, according to some researchers such as Raneesh and Santosh [\(2011](#page-9-0)) and also Abbaspour et al.  $(2015)$  $(2015)$ , the trend and phenomenon of climate change create a new level of uncertainty about freshwater resources; to understand the role of rainfall-runoff and sediment processes and quantify them in watershed areas the use of simulation models in costume (Khaleghi et al. [2011](#page-9-1), [2014;](#page-9-2) Alizadeh et al. [2017;](#page-8-3) Varvani and Khaleghi [2018;](#page-9-3) Kargar et al. [2020](#page-8-4)). Recently many approaches have implemented for estimating suspended sediment load of river systems (Olyaie et al. [2015\)](#page-9-4). Despite the progress of technology in recent decades, an increasing trend in implementing distributed models, the lack of data, and another issue such as the high cost of data provision in Iran, implementing semi-distributed models such as soil and water assessment tool (SWAT), are unavoidable. Investigations in this area show the high performance of these models to the sustainable use of water resources to meet diferent water demands (Abbaspour et al. [2015](#page-8-2)). SWAT, as a hydrological model to calculate the basin hydrological response accurately, was formed by integrating a hydrological and basinscale model with Geographic Information System software

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(ArcGIS 10.3). Investigations in these regards (Ang and Oeurng [2018\)](#page-8-5) show the improvement in the accuracy of the simulated results of the basin hydrological response (discharge fow). This semi-distributed and process-based model (Tobin and Bennett [2009](#page-9-5)) also play a considerable role in assessing the efect of land-use changes in the watershed area (Li et al. [2010](#page-9-6)). Arnold et al. [\(1998\)](#page-8-6) developed this model for the frst time and then widely used around the world (Arnold et al. [1998](#page-8-6), [2012](#page-8-7)). Abbaspour et al. [\(2007\)](#page-8-8) extracted SWAT-CUP (SWAT Calibration Uncertainty Procedures) by connecting three programs to the hydrologic simulator SWAT (Arnold et al. [1998\)](#page-8-6). These three programs, which have been interconnected with SWAT (Hallouz et al. [2018](#page-8-9)), are Sequential Uncertainty Fitting Ver.2 (SUFI-2) (Abbaspour et al. [2007](#page-8-8)), ParaSol (Van Griensven and Meixner [2006](#page-9-7)), and Generalized Likelihood Uncertainty Equation (GLUE) (Beven and Binley [1992;](#page-8-10) Saleh and Du [2004](#page-9-8); Chen and Chau [2019](#page-8-11)). SWAT-CUP is developed for the calibration of SWAT (Abbaspour et al. [2015](#page-8-2)). Recently, many types of studies have been implementing the SWAT model (Xiaobo [2008;](#page-9-9) Setegn et al. [2010;](#page-9-10) Thampi et al. [2010;](#page-9-11) Phomcha et al. [2011](#page-9-12); Mbonimpa et al. [2012](#page-9-13); Havrylenko et al. [2016\)](#page-8-12). Hassen et al. ([2016](#page-8-13)) implemented the SWAT model and earned favorable results concerning flood hydrograph calculation. Ang and Oeurng ([2018](#page-8-5)) used the SWAT model to simulate daily and monthly streamfow in the Stung Pursat River catchment and accessed to highefficiency results. To find a good model performance for discharges, Hallouz et al. ([2018\)](#page-8-9) used the SWAT model to assess the results of implementing the SWAT model in the Upper Tana Basin, and Nkonge et al. ([2014](#page-9-14)) used the GLUE and SUFI-2 calibration-uncertainty methods and found SUFI-2 as the best method. Recently, the SWAT model has implemented widely in Iran to assess uncertainty and optimize model parameters and to simulate food hydrograph (Hosseini et al. [2018\)](#page-8-14) and sediment discharge (Khaleghi and Varvani [2018a,](#page-9-15) [b](#page-9-16); Varvani and Khaleghi [2019a,](#page-9-17) [b;](#page-9-18) Varvani et al. [2019](#page-9-19)). Faramarzi et al. ([2009\)](#page-8-15) used SWAT to calculate streamfow hydrology for Iran. Also, Faramarzi et al. ([2013\)](#page-8-16) implemented the African SWAT model to investigate the impact of climate change in variations of food and sediment in Africa.

Above-mentioned literature and feedbacks indicate the successful implementation of the SWAT model in simulation and calculation of the water resource and the features of hydrologic processes. Also, the SWAT-CUP and the SUFI-2 method were selected to calibrate and validate the SWAT model by providing sufficient results. We conducted this study to investigate the efficiency of the SWAT model in estimating and simulating runoff, and investigate the uncertainty of hydrologic parameters in arid and semi-arid regions.

#### **Methods and materials**

#### **Case study**

The Zoshk–Abardeh Watershed with an area of 9225.5 hectares is located in the west of Mashhad in Khorasan Razavi Province, Iran. The studied area was located in the eastern longitude 59°4′39″ to 59°16′13″ and northern latitude 36°15′16″ to 36°23′12″. We present the location of the study area in Fig. [1](#page-1-0). The area is under a temperate climate with cool summers and freezing winters. The average annual rainfall and temperature are about 404 mm and 12 °C, and the climate of the region based on the Emberger method is cold semi-humid and based on the De Martonne method is the Mediterranean.

#### **Study method**

In this study, we implemented the SWAT model to simulate the efects of diferent climate change scenarios. Data required for SWAT model simulation include digital elevation model (DEM), drainage network map, land use, soil data, and meteorological data. The meteorological data required include rainfall, minimum and maximum temperatures, relative humidity, solar radiation, and wind speed daily for stations within and around the basin. We divide the simulation process in the SWAT model into two phases: the land phase and water for routing phases (Neitsch et al. [2005\)](#page-9-20). Land phases control the loading of the amount of water, sediment, and nutrients, and the second phase defnes the movement of water, sediment, and nutrients through the streams of the sub-basins or the Hydrological Response Units (HRU) to watershed outlets. SWAT allows users to defne management practices taking place in every HRU (Fig. [2](#page-2-0)). For ease of simulation, reducing inhomogeneity and increasing accuracy, the basin should be subdivided into sub-basins and then into the hydrological response unit



<span id="page-1-0"></span>**Fig. 1 L**ocation of Zoshk–Abardeh Watershed



<span id="page-2-0"></span>**Fig. 2** Principle of discretization of Hydrological Response Units (Briak et al. [2016\)](#page-8-18)

(Robert et al. [2008](#page-9-21)). The minimum threshold level method was used to determine HRU to remove land uses, soils, and slope within each sub-basin. In this study, 10% of thresholds were set for each slope, soil, and land-use class to include the most detail. Based on the threshold value, we simulated diferent variables for each HRU and then weighted for the total sub-basins, and after summing, we calculated the total value for that basin (Di Luzio and Arnold [2004\)](#page-8-17). It shows the conceptual process of the SWAT model in Fig. [3](#page-2-1).

The SWAT model simulates surface runoff using two alternative methods: the method of the Curve Number (CN) of the Soil Conservation Service (SCS) of the USDA and the method of Green and Ampt. In the SWAT model, erosion caused by rainfall and runoff is calculated using the modified

relationship of the Modifed Universal Soil Loss Equation (MUSLE) presented by Wischmeier and Smith ([1978](#page-9-22)):

$$
\text{Sed} = 11.8 \left(Q_{\text{surf}} q_{\text{peak}} \text{area}_{\text{hru}}\right)^{0.56} K_{\text{USE}} C_{\text{USE}} P_{\text{USE}} \text{LS}_{\text{USE}} \text{CFRG},\tag{1}
$$

where Sed is sediment rate (ton/day),  $Q_{\text{surf}}$  is runoff (mm in hectare),  $q_{\text{peak}}$  is the maximum runoff (m<sup>3</sup>/s), area<sub>hru</sub> is the area of each HRU (hectare),  $K_{\text{USLE}}$  is the soil erodibility factor,  $C_{\text{USLE}}$  is the cropping management factor,  $P_{\text{USLE}}$  is a factor of protective methods,  $LS_{\text{USLE}}$  is the topographic factor, and CFRG is the coefficient of coarse-grained particles.

The sediment routing model consists of two decomposition and sedimentation components that operate simultaneously. In this model, the maximum sediment that can be transported along the route is considered a function of the maximum fow rate:

$$
Conc_{\text{eded},\text{ch},\text{mx}} = C_{\text{sp}} v_{\text{ch},\text{pk}}^{\text{sp} \exp},\tag{2}
$$

where  $Conc_{\text{sed},ch,mx}$  is the maximum sediment concentration that can be traversed (ton/m<sup>3</sup>).  $v_{\text{ch},pk}$  is the maximum flow rate (m/s), and spexp and  $C_{sp}$  are empirical coefficients and spexp varies between numbers 1 and 2. If the sediment concentration exceeds the maximum calculated sediment concentration, the sediment is deposited in the path and the sediment content is calculated from the following relation:

$$
\text{Sed}_{\text{dep}} = (\text{conc}_{\text{sed,ch,i}} - \text{conc}_{\text{sed,ch,mx}})V_{\text{ch}}.
$$
 (3)

If the sediment concentration in the path is lower than the calculated maximum sediment concentration, the decomposition process occurs and the amount of sediment decomposed is calculated from the following relation:

<span id="page-2-1"></span>

$$
\text{Sed}_{\text{deg}} = \left(\text{conc}_{\text{sed},\text{ch},\text{mx}} - \text{conc}_{\text{eded},\text{ch},i}\right) V_{\text{ch}} K_{\text{CH}} C_{\text{CH}},\tag{4}
$$

where  $K_{\text{CH}}$  is erosion factor (cm/h/Pascal) and  $C_{\text{CH}}$  is channel coverage factor. The amount of sediment is obtained from the following relation:

$$
\text{Sed}_{\text{ch}} = \text{Sed}_{\text{ch},i} - \text{Sed}_{\text{deg}} + \text{Sed}_{\text{deg}},\tag{5}
$$

where  $\text{sed}_{\text{ch}}$  is the amount of suspended sediment (ton),  $\text{sed}_{\text{ch},i}$  is the amount of sediment suspended at the beginning of the time step (ton), and  $V_{ch}$  is the volume of water suspended in the track (cubic meters). Finally, the amount of sediment that gets out of the way is calculated from the following equation:

$$
\text{sed}_{\text{out}} = \text{sed}_{\text{ch}} \frac{V_{\text{out}}}{V_{\text{ch}}}.
$$
 (6)

#### **Statistical indicators of model evaluation**

To evaluate the model,  $R^2$ ,  $bR^2$ , and the Nash–Sutcliffe efficiency (NSE) coefficients (Nash and Sutcliffe [1970\)](#page-9-24) are used:

$$
R^{2} = \frac{\left[\sum_{i=1}^{n} \left(\text{Simulated}_{i} - \text{Simulated}_{avg}\right) \left(\text{Measured}_{i} - \text{Measured}_{avg}\right)\right]^{2}}{\sum_{i=1}^{n} \left(\text{Simulated}_{i} - \text{Simulated}_{avg}\right)^{2} \sum_{i=1}^{n} \left(\text{Measured}_{i} - \text{Measured}_{avg}\right)^{2}},\tag{7}
$$

$$
bR^{2} = \begin{cases} |b|R^{2} & \text{if } |b| \leq 1 \\ |b|^{-1}R^{2} & \text{if } |b| > 1 \end{cases},
$$
 (8)

$$
E_{\text{NS}} = 1 - \frac{\sum_{i=1}^{n} (\text{Measured}_i - \text{Simulated}_i)^2}{\sum_{i=1}^{n} [\text{Measured}_i - \frac{1}{n} \sum_{i=1}^{n} \text{Measured}_i]^2},
$$
(9)

where Simulated<sub>avg</sub> and Measured<sub>avg</sub> are average simulated and measured values, respectively.

## **The SWAT model uncertainty analysis, calibration, and validation**

In this study, because of high potential and efficiency of the SUFI-2 program for time-consuming large-scale models, it was implemented for sensitivity analysis, model calibration and validation, and uncertainty analysis in the SWAT-CUP program (Abbaspour et al. [2007](#page-8-8); Yang et al. [2008](#page-10-0); Abbaspour et al. [2015;](#page-8-2) Ang and Oeurng [2018;](#page-8-5) Shamshirband et al. [2019](#page-9-25)). To perform the calibration and validation processes, it was used from runoff data. To perform the sensitivity analysis based on linear approximation and uncertainty, we used it from two factors called the *R*-factor and *P*-factor. The *P*-factor is the percentage of observation

data covered equal to the estimated 95% uncertainty band (PPU95). The R-factor is the average PPU95 bandwidth divided by the measured standard deviation (Khalid et al. [2016\)](#page-9-26). The 95PPU has calculated at 2.5% and 97.5% levels of the cumulative distribution of an output variable got through Latin hypercube sampling (Memarian et al. [2013a](#page-9-27)). The closer the *P*-factor to 100% and the *R*-factor to zero, the more accurate is the simulation (Shimelis et al. [2008](#page-9-28)). To analyze the quantity and quality of calibration, validation, and sensitivity assessment, we implemented three measures: (a) the percentage of data excluded by the 95% prediction uncertainty (95PPU) (*P*-factor); (b) the ratio of the band 95PPU's medium thickness (Hallouz et al. [2018](#page-8-9)). Using the SUFI-2 program allows us to implement ten diferent aim functions such as mean square error (MSE), Nash–Sutclif (NS), and  $r^2$ . So long as most observational data are in the 95% uncertainty band and the band thickness is as small as possible, the process of computations in the SUFI-2 algorithm continues (Memarian et al. [2013b\)](#page-9-29).

#### **Results**

## **Sensitivity analysis of parameters afecting sediment load**

We used SUFI2 software only for sensitivity analysis. In the first step, we considered 22 potential and effective parameters in the production of watershed sediment. We introduced these parameters in the model along with their permissible range of variation and we performed 300 simulations to optimize the model outputs. For each of these parameters, a *t*-stat value was provided by the SUFI2 program, and based on them, the sensitive parameters were determined. The higher the *t*-stat values, the greater the relative sensitivity. *P* values are used to determine the signifcance of the sensitivity, so that the closer the *P* values to zero, the more important the parameters become. The outcomes of *t*-stat and the *P* values for each of the parameters afecting sediment outfow are presented in Figs. [4](#page-4-0) and [5](#page-4-1), respectively.

Table [1](#page-5-0) shows these values for the various parameters. Analyzing and the analogy of the obtained *t*-stat values for each parameter show that the parameters CN2, SOL\_BD, and USLE\_P have the highest relative sensitivity, and SLSUBBSN, GW\_DELAY, and ESCO have the least relative sensitivity. Based on this algorithm, about 22 efective parameters in the sediment have been investigated, which have been tried to be selected based on the results of previous research and the suggestions of researchers in other countries.

<span id="page-4-0"></span>





<span id="page-4-1"></span>

## **Model calibration and validation**

We performed the calibration and validation of the SWAT model to amend the simulation results of the sediment load. 7-year (2000–2006) and 3-year (2007–2010) monthly sedimentation statistics were implemented to perform calibration and validation processes, respectively. The *P*-factor and the *r*-factor values for the calibration period calculated 0.29 and 0.39, respectively, while the validation period was 0.28 and 0.38, respectively. The fndings of this study proved that in the validation period, the coefficients of  $R^2$ ,  $bR^2$ , and Ns were 0.85, 0.23, and 0.47, respectively, while in the calibration period, these coefficients were 0.46, 0.14, and 0.37, respectively. The results of uncertainty and calibration analysis were acceptable, but in the validation phase, the model has been more applicable and useful. These results show the acceptable efficiency of the SWAT model in simulating the sediment load of the study area. The results of optimal

values of the efective parameters on sediment load, *t*-stat, and *P* value are presented in Table [2](#page-6-0).

#### **Runoff calibration and validation results**

Statistical indicators of model evaluation include  $R^2$ ,  $bR^2$ , and NS coefficients were implemented to evaluate model performance. The results of these indices in the calibration and validation steps have been presented in Table [3.](#page-6-1)

As shown in Figs. [6](#page-6-2) and [7](#page-7-0), during the calibration and validation periods, diagrams of observed and simulated daily (Spruill et al. [2000](#page-9-30)) sediment load values were drawn to simulate minimum and maximum sediment loads and also to check their temporal compliance with real data. The analysis of these diagrams shows that the model well-simulated maximum and minimum deposition times. The average rates of simulated monthly sediment load during the calibration and validation period are 14,790 and 13,597 tons, respectively,

	$t$ -stat	P value			Minimum Maximum Parameter acronym	Parameters
1	$-0.01$	0.99	$-0.2$		$r$ CN2.mgt	Curve number
2	1.41	0.16	$\theta$		v_ALPHA_BF.gw	Groundwater Reaction Factor
3	$-2.1$	0.04	$\mathbf{0}$	500	v_GW_DELAY.gw	Delay time of groundwater supply flow
4	$-1.28$	0.2	$\mathbf{0}$	1	v ESCO.bsn	Compensation factor for evaporation from soil
5	0.71	0.48	$\Omega$	$\mathbf{1}$	v_EPCO.bsn	Plant water harvesting factor
6	3.19	$\mathbf{0}$	$-0.5$	0.5	$r\_SOL_K($ ).sol	Saturated hydraulic conductivity of soil (mm/h)
7	$-0.2$	0.84	$-0.5$	0.5	r_SOL_AWC().sol	Available water capacity in the soil layer
8	5.73	$\mathbf{0}$	$-0.5$	0.5	$r$ SOL BD $($ ).sol	Density of soil mass
9	0.12	0.9	$-0.5$	0.5	$r\_SOL$ $ALB()$ .sol	Wet soil albedo coefficient
10	$-2.42$	0.02	$-0.5$	0.5	r_SLSUBBSN.hru	Average slope length (m)
11	1.65	0.1	$-0.5$	0.5	r_OV_N.hru	Coefficient of roughness of range
12	0.94	0.35	$-5.0$	5.0	v SFTMP.bsn	Degree of snowfall $(^{\circ}C)$
13	0.09	0.93	$\overline{0}$	10	v SMFMX.bsn	Degree of melting snow $(^{\circ}C)$
14	$-0.74$	0.46	$\Omega$	10	v SMFMN.bsn	Degree of melting snow $(^{\circ}C)$
15	0.95	0.34	$\Omega$	10	v TIMP.bsn	Snow mass temperature delay coefficient
16	$-1.02$	0.31	$\mathbf{1}$	24	v SURLAG.bsn	Surface flow delay coefficient
17	1.95	0.05	$-0.5$	0.5	r_CH_N2.rte	Manning coefficient in the main channel
18	$-0.01$	0.99	0.0	150	v_CH_K2.rte	Hydraulic conductivity in the main channel
19	4.79	$\mathbf{0}$	0.0	1	v_USLE_P.mgt	Factor related to soil conservation operations in the USLE equation
20	0.45	0.65	0.5	2	v_ADJ_PKR.bsn	Peak rate adjustment factor for sediment routing in sub-basin
21	0.4	0.69	$\mathbf{0}$	1	v_CH_ERODMO().rte	Channel erodibility coefficient
22	$-0.12$	0.91	$\mathbf{1}$	1.5	v_SPEXP.bsn	Exponential re-entrainment coefficient for channel sediment routing

<span id="page-5-0"></span>**Table 1** Parameters entered into the model and the minimum, maximum and results of *t*-stat and *P* value values after sensitivity analysis

*v* means replacing existing parameter values with a given value and *r* means multiplying existing parameter values by (+1 given value)

while these values for real data are 6124 and 17,463 tons, respectively.

#### **Uncertainties in simulating sediment load**

After performing the calibration process, we calculated the probability of data uncertainty between 92.5% and 97.5% and the runoff uncertainty band showed that in this graph, both simulated and observed discharges were determined within the 95% uncertainty band. However, Fig. [8](#page-7-1) shows that the outputs of the model were not accurately and favorably got.

# **Conclusion and discussion**

In this study, we implemented the SWAT model and integrated it with the spatial variability of ArcGIS 10.3 to appraise the performance of the SWAT model in sediment flow simulation and also to investigate the uncertainty of the model in the watershed areas of arid and semi-arid regions. The results of the statistical indicators of model evaluation  $(R<sup>2</sup>$  and NS) illustrate the efficiency of the SWAT model in simulating the sediment load of the study area which is acceptable. Also, analysis of related graphs of the calibration

and validation periods of the sediment load shows the high capability of the model in the maximum's modeling and minimum sediment load occurrences. This fnding is consistent with the results of the study by Abbaspour [\(2005](#page-8-19)) and Abbaspour et al. [\(2015](#page-8-2)) about the high capability of the SWAT model in simulating the seasonal changes of sediment. Another ability of this model is in simulating water phenomena and sediment transfer processes. This fnding is consistent with the results of the study by Ang and Oeurng ([2018\)](#page-8-5) and Hallouz et al. [\(2018\)](#page-8-9).

Also, the results of the uncertainty diagrams show that after the calibration and validation processes, there was a high diference in simulated and observed values. This high uncertainty, particularly in the results of sedimentation, is observed in studies that can be attributed to several reasons. First, there are no exact statistics for sedimentation. Second, there are no statistics on the amount of water harvested in gardens and upstream of the basin. Third, there are a lot of wells in upstream of the basin that does not have any statistics on discharge. In general, several factors are involved in the accuracy of modeling results. One group of these factors was related to the climatic and geological conditions of the basin (Gholami et al. [2017](#page-8-20); Khaleghi [2018](#page-9-3)) and the information collected, and the other group was related to the weaknesses of the model in the simulation. In terms of geology,

<span id="page-6-0"></span>**Table 2** Efective parameters on sediment load and their optimal values, *t*-stat, and *P* value



*v* means replacing existing parameter values with a given value and *r* means multiplying existing parameter values by  $(+1$  given value)

<span id="page-6-1"></span>**Table 3** Values of the model evaluation index in the calibration and validation steps

Evaluation indicators and stages of model implementation	Calibration step	Validation step
Coefficient of determination $(R^2)$	0.46	0.85
Nash-Sutcliffe coefficient (NS)	0.37	0.47
$Br^2$ coefficient	0.140	0.23
P-factor	0.29	
$r$ -factor	0.39	

it seems that most of the sedimentation load of this basin is related to the bed load, which will increase the possibility of increasing the error due to the lack of collected statistics and data reconstruction.

Evaluation of SWAT\_CUP and SWAT model for simulation of sediment load variable of the Zoshk–Abardeh watershed shows that uncertainty about sediment is higher. This result is consistent with the results of Xu et al. ([2009\)](#page-10-1) and Khalid et al. ([2016\)](#page-9-26). These results show the acceptable efficiency of the SWAT model in simulating the sediment



<span id="page-6-2"></span>**Fig. 6** Comparison of monthly values of runoff observed and simulated after calibration

<span id="page-7-0"></span>



<span id="page-7-1"></span>

load of the study area. To assess the sensitivities of 22 input parameters, we used SWAT-CUP and achieved three of the most sensitive parameters comprising CN2, SOL\_BD, and USLE P. In contrast, the parameters with the least sensitivity were SLSUBBSN, GW\_DELAY, and ESCO. We can use the calibrated model as inputs for SWAT, to assess the impact of climate change on soil erosion. To the validation of the modeling results, many factors are involved. Some of them are linked to climatic and geological conditions of the basin and the collected data, and other factors are related to model weaknesses in the simulation. We can implement the outcomes of this research to predict the efects of climate change on the hydrological patterns of watersheds and also the management practices needed to deal with them in the region (as a scenario in the proposed model).

In general, the SWAT model, as a comprehensive model for natural resource studies, can be a powerful tool in macro planning and management. The multifunctionality, or in other words, the prediction of diferent goals for this model, including hydrological processes, water quality, soil erosion, rangeland management, and climate change efects, and the greater accuracy of the model's results on a large scale, confrms this model. The compatibility of the model with diferent software environments such as Arc View and Arc GIS has increased the efficiency of this model. The results of research conducted in diferent parts of the world also show that this model can be introduced as a standard model in the world. However, it should be noted that compared to other models, this model requires a lot of input information, which is one of the weaknesses of the model.

Finally, model validation and validation have been introduced as a key factor in reducing uncertainty and increasing user confdence in simulation and more efective forecasting and as a factor to help watershed models in developing the SWAT model to achieve watershed management goals. The calibrated model can be used to simulate the efects of climate change and land use, as well as various management scenarios on runoff and soil erosion.

Due to the proper performance of the SWAT model in stimulating the flow of runoff and sediment load of Zoshk–Abardeh basin as well as its extensive capabilities, other study felds in this basin are suggested as follows:

- Comparison of SWAT efficiency with other models about the simulation of diferent basin variables.
- Simulation of river flow basins with natural and climatic conditions similar to the Zoshk–Abardeh basin in terms of data access limitation using the SWAT weighed model.
- Using a calibrated model to study the effects of climate change, land use, vegetation, and various management scenarios on runoff and soil erosion of the basin to determine the best land-use pattern and allocate water resources.
- Investigating the effects of climate change on water resources using the SWAT model to reduce and compensate for the harmful efects of climate change.
- Prioritization of sub-basins based on soil loss ratios to take protective measures.
- Analysis of parameter sensitivity assessment in diferent climatic conditions and time scales.
- Determining the importance of baseline flow and surface runoff as important components of total discharge and determining the number of watershed losses due to evaporation and transpiration.
- According to the required information of the SWAT model, this model can be used to simulate discharge and sediment load in Iran's watersheds, although the lack of accurate meteorological statistics and land-use maps with appropriate accuracy and appropriate to the similar period hurts the accuracy of results.

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