



Investigation of Corrosion Behavior of SiC-Reinforced Al 6061/SiC Metal Matrix Composites Using Taguchi Technique

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Abstract

In the present work, the statistical investigation on corrosion behaviour of Silicon Carbide-reinforced Al6061 Aluminium metal matrix (AMMCs) composites using Taguchi technique has been reported. Stir casting technique was adopted for synthesizing Al/SiC composites containing 0%, 2%, and 4% weight percentages of SiC. The corrosion studies were carried out for test variables—wt% of SiC, normality of solution, and corrosion duration for the as-cast composite specimens. The specimens were tested in NaCl solutions of normality 1.0, 1.5, and 2 and the exposure period ranging from 40 to 80 days. Corrosion characteristics of the composites were statistically analyzed by employing the design of experiments approach using Taguchi technique. Influence of various parameters on corrosion behavior of composites were investigated by Signal-to-noise ratio and analysis of variance. Result of the research determines that greater corrosion resistance was obtainable by composites when compared to monolithic aluminium 6061 alloy in the chosen corrosion media. This phenomenon of decrease of corrosion rate with exposure time was attributed to possible passivation of matrix alloy with the formation of protective layer formed on the specimen exposed to NaCl protecting the base metal from aggressive environment. The corrosion morphology was studied by scanning electron microscopy (SEM).

Keywords Aluminium · Stir casting · Corrosion · Metal matrix composites · Design of experiments · Taguchi technique

1 Introduction

Aluminum is the extreme prevalent matrix material for the Metal Matrix Composites (MMCs). Aluminum alloys are more attractive materials owing to their lower density, superior resistance for corrosion, high electrical and thermal conductivity, and higher damping capacity [1]. Composite materials based on Aluminium alloy are attractive prospective materials suitable for engineering applications as they exhibit outstanding blend of properties such as high strength-to-weight ratio, superior stiffness, thermal and electrical conductivities, low thermal expansion coefficient, and resistance for wear. By virtue of their exceptional mixture of

properties, Aluminium alloy-based composites find varieties of applications such as automobile, aerospace, mineral and mining, defense, and additional associated segments [2–5].

The reinforcement and matrix interface shows a vital role in defining the properties of composites based on metal matrix. Physical and mechanical characteristics of the MMCs such as ductility, strength, toughness, stiffness, creep resistance, fatigue resistance, coefficient of thermal expansion, thermal conductivity, and resistance for corrosion are reliant on the interfacial characteristics [5]. The foremost apprehension is the high corrosion affinity of Aluminium alloys, deteriorated by the galvanic corrosion among the metallic matrix and functionally important particle or fiber reinforcement. Consequently, it is imperative to understand the corrosion characteristics of composites to make them suitable for a variety of applications.

AMMCs are widely used in engineering applications, and therefore, it is important to understand the corrosion behaviour of AMMCs [6, 7]. The foremost drawback of the reinforced metal matrix composites is the effect of reinforcement on the corrosion rate as it declines the shielding film of oxide layer in composites of aluminum alloy, however,

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formation of particle interfaces in the matrix influences the corrosion characteristics [8–10]. Composites are subjected to a number of corrosive atmospheres through the processes like pickling, cleaning, and many other. Materials made of aluminum and its alloys demonstrate high corrosion rates in corrosive medium [11–14].

The corrosion studies on composites reinforced with various types of ceramic particulates, such as SiC, Al₂O₃, and TiC, have been carried by Deuis et al. [15] in 3.5 wt% NaCl (sodium chloride) medium. They have concluded that the corrosion rate increases in the following order: Al₂O₃ < SiC < TiC. The corrosion resistance of composites were superior than their matrix alloys when the test was conducted in NaCl medium. The interfaces found to be preferred sites for passive film breakdown (pitting initiation sites), that produces voids, resulting in an easier breakdown of the oxide layer [16–18]. Pitting in composites has been observed at the reinforcement matrix interface [10–12]. Although several researches have been carried out by many researchers on the corrosion behaviour of MMCs, but there exist ambiguity and lack of understanding of corrosion behavior of 6061 Al-based MMCs as it is not reported significantly.

The objective of the present work is to carryout corrosion studies on Silicon Carbide-reinforced Al metal matrix composites fabricated by stirr casting technique under the as-cast condition, with reinforcement content of 0%, 2%, and 4% weight percentages of SiC by using Taguchi method. The corrosion studies were carried out for test variables—normality of solution, wt% of SiC and corrosion duration on the as-cast composite specimens. The specimens were tested in NaCl solutions of normality of the 1.0, 1.5, and 2 and the exposure period ranging from 40 to 80 days.

2 Experimentation

2.1 Composite Preparation and Experimentation

Al6061 alloy was used as the matrix metal. The composition of Al6061 alloy is given in Table 1.

Silicon carbide (SiC) particles with particle size ranging from 25 to 30 µm were used as a reinforcement. Before mixing in molten aluminium, matrix particles were pre-heated by an electric oven. Different percentages of SiC (0, 2, and 4% by weight) were used for mixing with Al 6061 matrix alloy to fabricate composites.

The Al/SiC composite materials were synthesized by adopting stir casting method. In stirr casting process, the

ingots of 6061 aluminium were placed in the electric furnace in graphite crucible, and gradually the temperature was raised above the melting point 800 °C. After continuously heating for about 2–3 h, the aluminium completely melted. For proper mixing of aluminium melt and SiC particle, the aluminate-coated stirrer was used to form the “Vortex.” Stirrer was rotated at speed of 450 rpm to form “vortex” for about 5 min. Then desired calculated quantity of SiC particulates as per weight percentage which were already pre-heated to 350 °C were transferred to the “vortex” formed in aluminium melt and stirring was continued for about 2 min. After the stirring operation was completed, the molten mixture of Al/SiC was poured into a permanent metallic mould made up of cast iron of dimensions having diameter 60 mm and length of 180 mm. Composite castings were taken out from the moulds after solidification.

2.2 Corrosion Tests on the Prepared Specimens

Weight loss method was employed for corrosion test. The specimens for corrosion tests were prepared by machining to the required sizes and were weighed. Samples prepared were of as-cast Al SiC composite of 0%, 2%, and 4% weight percentages of SiC. All the samples prepared were immersed in NaCl solution with varying normality of 1.0, 1.5, and 2 and the exposure period ranging from 40 to 80 days in the increments of 10 days. The samples after the specific duration were taken out, wiped, and weighed to check for the weight loss. Further, the samples were subjected to macroscopic investigation using SEM.

2.3 Taguchi Technique

Taguchi technique [19, 20] is a effective tool which facilitates the performance improvement of the process, design, and product with substantial estimate of time and cost. Various studies have been carried out successfully by using this technique to optimize the different processes [21–30]. Taguchi technique is a systematic methodology used to optimize the design and hence confirm both performance and quality with the help of Taguchi orthogonal array concept that delivers much condensed inconsistency or fluctuations for the experiments with an optimal setting of design parameters that control the process. It presents a combined methodology that is modest and effective to discover the preminent choice of designs for performance, quality, and cost. The orthogonal array (OA) requires minimum experimental set. Three factors (wt% of SiC, Normality of solution

Table 1 Chemical composition of Al6061 aluminium alloy

Al	Mg	Si	Cr	Mn	Ti	Cu	Fe	Zn
95.8–98.6	0.8–1.2	0.4–0.8	0.04–0.4	0.15	0.015	0.15–0.4	0.7	0.25

Table 2 Levels for various control factors

Control factors	Level I	Level II	Level III
C: composition	0	2	4
N: normality	1	1.5	2
D: duration of test	40	60	80

and duration of test) with three levels were selected and are shown in Table 2. The influence of parameters were studied by analyzing means and variance of experimental results. A mathematical equation was established to forecast the corrosion rate of the as-cast composites by multiple linear regression. Thus, the main aim of the current study is to analyze the effect of parameters like wt% of SiC, Normality of solution, and duration of test on corrosion behaviour of Al-SiC metal matrix composites using Taguchi technique.

2.4 Experimental Design

The experiments were carried out according to the customary orthogonal array. The choice of the orthogonal array is created on the complaint that the degrees of freedom for the orthogonal array have to be more than, or at minimum equal to, the sum of those corrosion rate controlling or governing parameters/factors. The corrosion rate factors (control parameters) selected for the experiment were wt% of SiC, i.e., Composition (*C*), Normality of solution (*N*), and duration of test (*D*). Various factors along with their levels are as presented in Table 2. In the current research, an orthogonal array L27 was selected, which has 6 columns and 27 rows, as presented in Table 3. Each row in the L27 orthogonal array represents individual experiment and the columns were allocated to different factors or parameters [21, 22].

In the Taguchi technique, the experimental outcomes are converted into a S/N ratio (signal-to-noise ratio), which are used to compute the quality characteristics. In the present investigation, ‘the-lower-the-better’ quality characteristic was implemented for analysis of the corrosion rate of the aluminium composites as smallest values of corrosion rate are necessary. The S/N ratio for every level of the process factors was calculated based on the S/N analysis. Additionally, a statistical analysis of variance (ANOVA) was implemented to ascertain the statistically substantial parameters. The optimal mixture of the test factors can thus be anticipated [23].

The signal-to-noise ratio (S/N ratio) for corrosion rate by means of ‘the-lower-the-better’ characteristic, specified by Taguchi, is as given below:

$$S/N = -10 \log (1/n) \{y_1^2 + y_2^2 + \dots + y_n^2\}, \quad (1)$$

Table 3 Experimental design using L27 (33) orthogonal array

Experiment number	Wt% SiC	Normality	Number of days	Corrosion weight loss (mg)	S/N ratio (db)
1	0	1	40	2.529	- 8.0590
2	0	1	60	3.567	- 11.0461
3	0	1	80	4.04	- 12.1276
4	0	1.5	40	2.714	- 8.6722
5	0	1.5	60	4.007	- 12.0564
6	0	1.5	80	3.977	- 11.9911
7	0	2	40	2.859	- 9.1243
8	0	2	60	4.165	- 12.3923
9	0	2	80	4.559	- 13.1774
10	2	1	40	2.313	- 7.2835
11	2	1	60	3.22	- 10.1571
12	2	1	80	3.517	- 10.9234
13	2	1.5	40	2.451	- 7.7869
14	2	1.5	60	3.554	- 11.0143
15	2	1.5	80	3.728	- 11.4295
16	2	2	40	2.254	- 7.0591
17	2	2	60	3.34	- 10.4749
18	2	2	80	4.023	- 12.0910
19	4	1	40	1.808	- 5.1440
20	4	1	60	2.862	- 9.1334
21	4	1	80	3.297	- 10.3624
22	4	1.5	40	1.949	- 5.7962
23	4	1.5	60	2.888	- 9.2119
24	4	1.5	80	3.1	- 9.8272
25	4	2	40	1.496	- 3.4986
26	4	2	60	2.526	- 8.0487
27	4	2	80	3.051	- 9.6888

where y_1, y_2, \dots, y_n are the response of corrosion rate and n is the number of observations. The ‘lower-the-better’ characteristics along with the S/N ratio conversion are appropriate for minimization of corrosion rate. A statistical analysis of variance (ANOVA) is performed to identify the statistically significant control parameters. ANOVA in addition to S/N ratio make it conceivable to forecast the optimal mixture of corrosion factors to a satisfactory level of precision [24–26].

Table 3 shows that the response for signal-to-noise ratios displays the average of particular characteristics for each level of the factor. This table comprises the ranks depending upon the delta statistics, which matches the relative values of the effects. S/N ratio is a response which combines recurrences and the influence of noise levels into a particular data point.

Minitab 17 software was used to plot Mean-response graphs, and the ANOVA analysis was employed to find out the percentage of contribution of test parameters.

3 Results and Discussion

The elementary objective of the apprehended experiment was to determine the supreme dominant factors and the mixture of factors which have extreme effect on the corrosion rate, in order to decrease its value to a least. Experiments were carried out depending upon the orthogonal array, which relate the effect of the composition (*C*), Normality (*N*), and test duration in Number of days (*D*). It is these factors which influence the corrosion process and outline the corrosion characteristics of composites.

With the aim of establishing the influence of specific factor, experimentally obtained values were converted into the S/N ratio. Also analyzed were effects of the corrosion rate control factors that is the composition (*C*), Normality (*N*), and test duration (*D*) in Number of days on the corrosion rate with the intention of obtaining the S/N ratio. Ranking of factors, depending upon the S/N ratio for the corrosion rate for the different levels of those factors, is shown in Table 4. It can be followed from Table IV that, depending on the S/N ratio, the governing factor which effects the corrosion rate, is the number of days, followed by composition and lastly by the normality.

3.1 ANOVA and the Effect of Factor

Taguchi technique cannot critic the influence of individual factors and hence the experimental results were analyzed by employing Analysis of Variance (ANOVA). The ANOVA is

Table 4 Response table for signal-to-noise ratios—the smaller is the better (corrosion rate)

Level	Wt% SiC	Normality	Number of days
1	3.602	3.017	2.264
2	3.156	3.152	3.348
3	2.553	3.141	3.699
Delta	1.049	0.135	1.435
Rank	2	3	1

Table 5 Analysis of variance (ANOVA) for means for the corrosion rate

Source	DF	Seq SS	Adj SS	Adj MS	F	P	Pr
Wt% SiC	2	44.282	44.2825	22.1412	298.16	0.000	29.79
Normality	2	0.715	0.7153	0.3576	4.82	0.042	0.48
Number of days	2	95.166	95.1664	47.5832	640.78	0.000	64.02
Wt% SiC × normality	4	4.630	4.6301	1.1575	15.59	0.001	3.11
Wt% SiC × number of days	4	1.561	1.5608	0.3902	5.25	0.023	1.05
Normality × number of days	4	1.698	1.6982	0.4246	5.72	0.018	1.14
Residual error	8	0.594	0.5941	0.0743			0.40
Total	26	148.647					100.00

applied to investigate the effect of parameters, like the composition (*C*), Normality (*N*), and test duration in Number of days (*D*) as well as their optimal level.

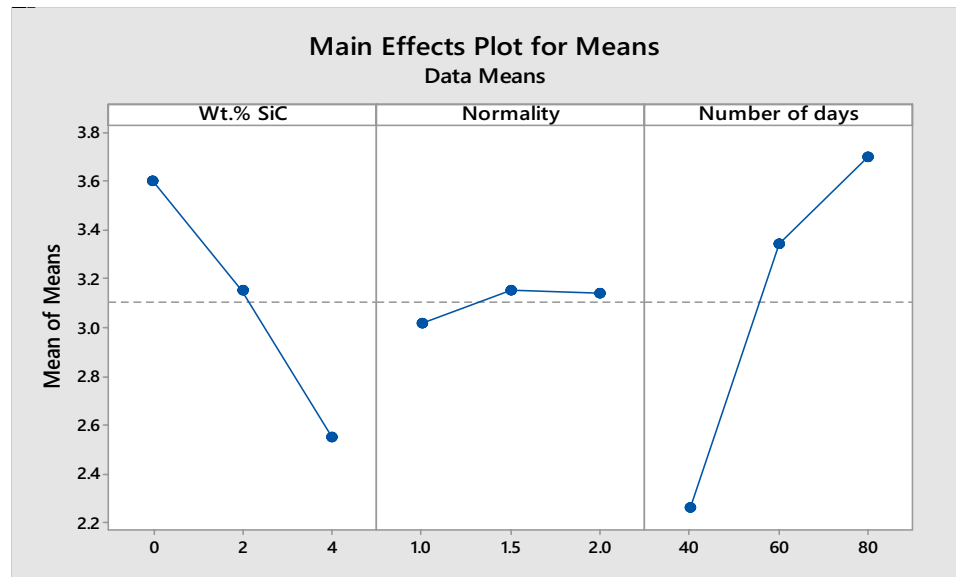
By performing the ANOVA, it is likely to decide the effect of the specific factors on the corrosion rate and also the percentage of that influence, for each of its values. The results of the ANOVA tests are represented in Table 5 for the corrosion rate and for the three analyzed factors that vary over their levels, as well as their mutual interactions. This analysis is performed for a significance level of $\alpha = 0.05$, i.e., for a confidence level of 95%. Sources with a *P* value less than 0.05 were considered to have a statistically substantial influence to the performance measures. Also presented is the % influence for individual factors as well as the degree of their effect on the overall result.

Table 5 displays the results of the ANOVA of composites in terms of the corrosion rate in this research. From Table 5, it can be observed that the most influencing factor on the corrosion rate is enforced by the number of days ($P = 64.02\%$). The second most influence is offered by the composition ($P = 29.79\%$). The least specific effect on the corrosion rate is demonstrated by the normality ($P = 0.48\%$). The highest influence has the interaction between composition normality and no. of days ($N \times D$) and it sums to $P = 3.11\%$. Significance of interaction between the no of days and normality ($C \times N$) is $P = 1.14\%$, while the modest influence has the interaction between the composition and no. of days ($C \times D$) and is $P = 1.05\%$. The residual error connected in the ANOVA Table was nearly about 0.40%.

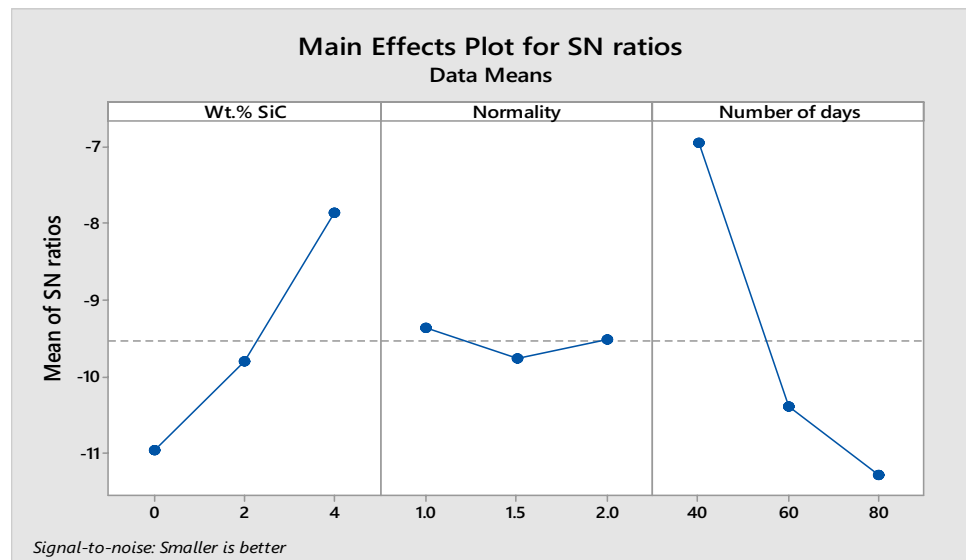
3.2 Influence of Testing Parameters on Corrosion Rate

Figure 1a, b displays the plots of the main effects for means and S/N ratio of the different testing factors on the corrosion rate, respectively. In the main effect plot, if the line for a particular factor is near flat, then the factor has no substantial influence. On the other hand, a factor for which the line has the maximum inclination has the greatest substantial effect. Also, if the slope of plot is positive it indicates corrosion rate is more and vice versa. It is apparent that the most

Fig. 1 a Main effect plots for means-corrosion rate of Al/SiC composites. **b** Main effect plots for S/N ratio-corrosion rate of Al/SiC composites. Gr hybrid composites



(a)



(b)

substantial influence on the corrosion rate is offered by the no. of days, whereas the other factors demonstrate slighter effects. The corrosion rate declines with composition as the slope is negative in the mean plot, while it rises with no. of days. The lowest corrosion rate appears at the highest composition and lowest no. of days. Figure 2 shows related interactions of all the analyzed factors and their effect on the corrosion rate.

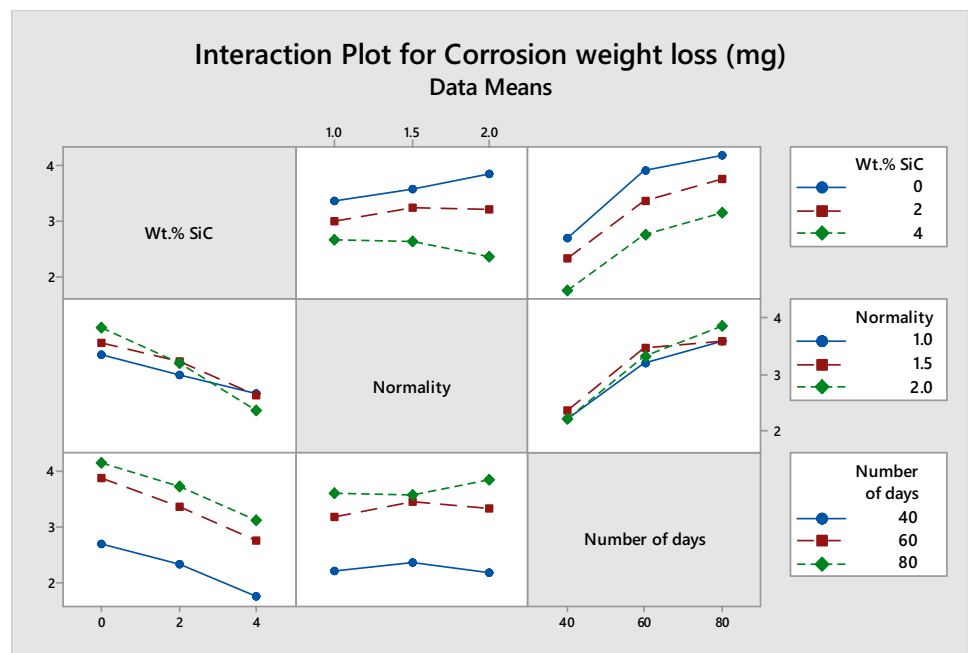
3.3 Multiple Linear Regression Models

The multiple linear regression model was developed for the corrosion rates of composites with the help of MINITAB

17 statistical software program. Established model provides the linear dependency of the unidentified variable on the identified variables. In the current investigation, the linear dependency of the corrosion rate from the composition (C), normality (N), and no. of days (D) can be noticed. The linear regression equation was acquired with the help of ANOVA analysis and the given values of the composition, normality, and no. of days.

The established regression linear equation for the corrosion rate is as given below:

Fig. 2 Interactions plots for means-corrosion rate of Al/SiC composites



$$\begin{aligned} \text{Corrosion weight loss (mg)} = & 1.288 - 0.2622 \text{ wt\% SiC} \\ & + 0.124 \text{ normality} + 0.03589 \\ & \text{number of days} \end{aligned}$$

The expressions that are statistically important are involved in the model, and the above equation is appropriate for a specified corrosion regime. When the experimentally obtained values are substituted for the variables in Eq. (1), the corrosion of the composite can be computed. From the equation, it can also be observed that the corrosion rate rises with normality and no. of days, while it declines with composition. (From + and – signs present in the equation.) The acceptability of the model characterized by Eq. (1) was confirmed using the normal probability plot of the residuals, as presented in Fig. 3. The points are very nearby to the normal probability line; thus, there is considerable confirmation that the model is acceptable. Thus, the model framed for the calculation of the corrosion rate of the aluminium based composite, as characterised by Eq. (1), is acceptable as validated by several other researchers [27, 28].

3.4 Corrosion Morphology

Figure 4 shows the SEM micrographs corroded surfaces of the as-cast unreinforced monolithic specimens and composites containing 2 wt% and 4 wt% SiC reinforcement after test duration of 80 days in a corrosion media NaCl with normality 1 N. It can be decided from these SEM micrographs that the quantity of surface degradation decreased with increase in SiC content. Severe pitting was noticed for unreinforced

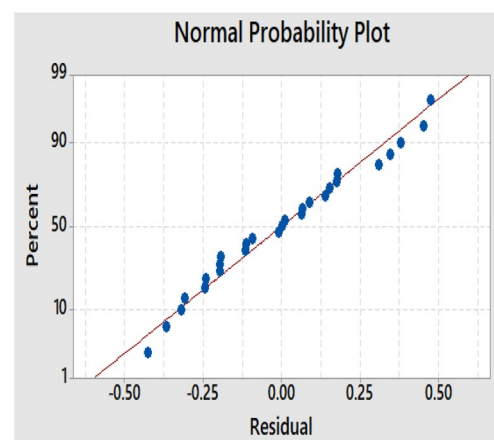


Fig. 3 Normal probability plots of residuals for corrosion rate of Al composites

monolithic aluminium specimen compared to composites containing SiC.

The justification of greater corrosion resistance of the composite in 3.5 wt% NaCl solution could be owing to discontinuity of the matrix material in the composites. Subsequently intermetallics, particularly Mg_2Si , is located at the juncture of the SiC particulates, it possibly restricted the link of the matrix material through the internal regions of the composite. Considering a small pit established at the composite surface, the pit will spread into the matrix through the inner part of the channel till it meets nearby SiC particulate in the matrix. Owing to the existence of

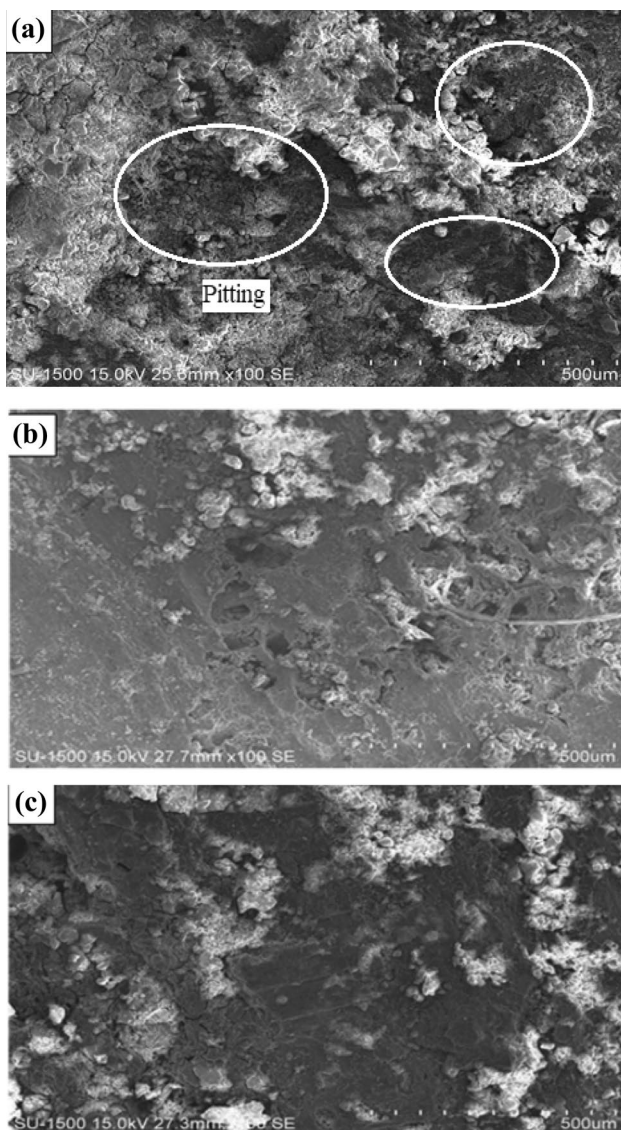


Fig. 4 Shows corroded surface of the Al alloy **a** as-cast, **b** 2 wt% SiC-reinforced, and **c** 4 wt% SiC-reinforced composites exposed for 80 days in NaCl at 1 N solution

Mg_2Si phase at the juncture of the SiC particulates, matrix channels will get narrower or transform to almost closed, and consequently, spreading of the pit will be constrained or terminated due to noble characteristics of the Mg_2Si phase [31, 32].

4 Conclusions

- Al/SiC-based MMCs, when reinforced with varied weight percentage of SiC from 0 to 4% were successfully fabricated by the stirr casting liquid metallurgical technique.

- From the studies it is observed that, though the weight loss was severe in initial stages, there is an appreciable decrease of the corrosion rate and weight loss per unit area with increase of time.
- Composites exhibited superior corrosion resistance when compared to monolithic unrienforced matrix alloy.
- The corrosion by weight loss of the composite decreased with the increase in the weight percentage of the reinforcement.
- Linear Regression equation developed for the current study was used to calculate the corrosion rate and it is reasonably in well agreement with the experimental data.

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