# The Effect of Nb<sub>2</sub>O<sub>5</sub>-Ni Coatings on the Microstructural and Corrosion **Behavior on Carbon Steel for Marine Application**

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#### **Abstract**

In this study, we developed  $Nb_2O_5-Ni$  composite coatings on carbon steel by DC sputtering technique. The effect of  $Nb_2O_5$ particulate on the Ni coating properties was investigated. The weight percents of  $Nb_2O_5$  in Ni coating were 0, 12, 15, and 30 wt%. The structural properties of the composite coatings were characterized using scanning electron microscope equipped with energy-dispersive spectrometer. The microhardness and thickness of composite coatings were measured, in addition to examine the corrosion properties in 3.5% NaCl using MLab 200 potentiostat/galvanostat with linear polarization technique. The results showed that hardness value increased to 164 HV for 30 wt% Niobia compared with 155 HV for Ni coating and the thickness increased slightly for  $Nb_2O_5-Ni$  composite coatings. The corrosion performance improved to obtain efficiencies better than Ni coating alone.

**Keywords**  $Nb_2O_5-Ni$  coatings  $\cdot$  Microstructure  $\cdot$  Microhardness  $\cdot$  Corrosion behavior

# **1 Introduction**

Nickel coating is resistant to dry gases, oil, soaps, and petrol. Nickel coating increases resistance to many corrosion types in diferent media, but not to nitric acid and environments containing chloride. The life of nickel coatings may be further increased by a thin overlay of microcracked chromium because corrosion would not penetrate the nickel directly, but will spread laterally. Nickel is generally plated as a part of multilayer coating system. The coating system consisting of the dull nickel, bright nickel, and chromium layer is called the composite nickel coating. Nickel coatings are commonly applied to zinc, steel, and other metals to provide protection against corrosion. Incorporating other materials (metals or ceramics) with nickel coating can also be referred to

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as composite coating. On the other hand, applying ceramic coatings on metal surfaces gives protection against corrosion and erosion with some disadvantages. In this work,  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni composite coatings were investigated. There are many works focused on  $Nb<sub>2</sub>O<sub>5</sub>$  coating using different techniques  $[1-10]$  $[1-10]$ .

# **2 Experimental Procedures**

# **2.1 Materials Preparation and Co‑deposition**

Structural steel (AISI 1015) with the dimensions of  $(20 \text{ mm} \times 20 \text{ mm} \times 2 \text{ mm})$  were used as the substrate, its chemical composition (wt%) was as follows: C 0.161, Si 0.271, Mn 0.425, P 0.0073, S 0.0049, and balance of Fe. Before the coating test, the substrate was in turn ground with SiC abrasive papers of 400, 600, 800, and 1000 in water, rinsed with alcohol, dried in the air, and sandblasted with alumina grit.

DC sputtering technique was achieved in a low-pressure gas discharge device consisting of an evacuated chamber, a target (cathode), and anode disk of stainless steel. The cathode was placed opposite the anode and provided the gas discharge of electrical feld with 4 KV DC power supply. The cathode electrode insulated with diameter of



14.5 cm, while the diameter of target electrode was 7.5 cm and the distance between them was 3.5 cm.

The gas source-fow controller system is responsible for supplying the feedstock at the desired fow rate and gas pressure to the plasma chamber. It is consists of dual-stage regulators, tubing, and fttings for the gas storage cylinders (Argon). Dual-stage needle valve regulated the fow pressure to the plasma chamber.

The vacuum system consists of a turbo pump (Variant, V-1000HT) assisted by a hydraulic rotary pump (60 m<sup>3</sup>/h, Balzer). The installation of penning (Edward CP25-K with controller 1102) and pirani gauges (LH-Thermovac with Combitron CM350) in the plasma chamber was required



<span id="page-1-0"></span>

<span id="page-2-0"></span>**Fig. 2** AFM images of uncoated steel (**a**) and  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni composite coatings with diferent percents: **b** 0 wt%, **c** 12 wt%, **d** 15 wt%, and **e** 30 wt%



to monitor the actual pressure and the partial pressure of the discharge gases.

#### **2.2 Characterization Methods**

The morphologies and chemical compositions of the obtained coating were analyzed using scanning electron microscope (SEM) and its confgured energy-dispersive spectrometer (EDS). This test was performed at University of Sanity Sherif Tehran-Iran. The phases were analyzed by X-ray difraction (XRD), type (Angstrom Advanced Inc model ADX 2700) at Ministry of Science and Technology, Iraq.

The coating roughness was measured using an image analysis from AFM (Model AA3000 Scanning Probe Microscope), at College of Science – University of Baghdad.

The electrochemical test was conducted using WINKINK MLab 200 Potentiostat/Galvanostat from Bank Company at 303 K. The classical three-electrode confguration was composed of platinum rod, saturated calomel electrode (SCE), and steel sample, which were used as the counter electrode, reference electrode, and working electrode, respectively. The working electrode with an area of  $1 \text{ cm}^2$  was immersed into the solution for 30 min to attain the stable state of open circuit potential (OCP); the potentiodynamic polarization test was conducted with scanning rate of 10 mV/s.

# **2.3 Microhardness and Thickness**

Microhardness values were calculated for coated specimens with load of 9.8 g for 15 s. The average readings were taken for three measurements. Optical method for determining flm thickness is commonly used because it refers to both opaque and transparent flm and typically yields high-precision thickness value. These tests were performed at the Department of Material Engineering-University of Technology, Iraq.

# **3 Results and Discussion**

# **3.1 Morphological Studies**

Figure [1](#page-1-0) shows the morphological structure of  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni composite coatings 0, 12, 15, and 30 wt% of total weight of target, from this Figure can be seen crystallite particles growth distributed on the steel surface within nickel layer. Also, it is clearly showing a perfect incorporation of  $Nb<sub>2</sub>O<sub>5</sub>$ within the nickel-rich region. The incorporation of  $Nb<sub>2</sub>O<sub>5</sub>$ 

particles increased with increasing wt% of  $Nb<sub>2</sub>O<sub>5</sub>$  addition due to microstructural bonding and increasing nucleation process in Ni metal as carrier for  $Nb<sub>2</sub>O<sub>5</sub>$ .

EDS pattern of deposited  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni layers shows combined elemental composition of the deposited composite coating with indication of Ni, Nb, and O present as major components.

Figure [2](#page-2-0) shows the AFM images. These images indicate a smooth surface for uncoated surface with very small roughness equal to (2.97 nm) due to atmospheric corrosion with random distribution of particles with highest average diameter (148.06 nm). Ni-coated surface shows some summits and valleys due to deposition of Ni particles and nickel oxide with roughness average (9.52 nm) and more ordered distribution of particles with average diameters equal to (81.14).

The  $Nb_2O_5-Ni$  composites-coated surfaces gave smoother surface and the smoothness increases with increasing the weight percent of  $Nb<sub>2</sub>O<sub>5</sub>$  in composite as shown in Table [1.](#page-3-0) The decrease in surface roughness can be attributed to the  $Nb<sub>2</sub>O<sub>5</sub>$ -incorporated Ni film which enhanced grain growth to obtain a larger particle size as shown in Fig. [3](#page-4-0).

#### **3.2 Microhardness and Coating Thickness**

The microhardness measurement was done for coated specimens and the results are shown in Fig. [4](#page-5-0). These data show the higher hardness for Ni-coated surface (155 HV) compared with uncoated surface (132 H.V). Adding  $Nb_2O_5$  with 12 and 15 wt% to Ni coating decreased the hardness to (139) and (148), respectively, because of the presence of some pores within the coating. While adding the higher weight percent (30 wt%) of  $Nb<sub>2</sub>O<sub>5</sub>$  led to increasing the hardness to (164 HV) due to flling of the pores within Ni layer.

The incorporation of  $Nb<sub>2</sub>O<sub>5</sub>$  within Ni coating led to slight increases in thickness of coating by  $\approx 1$  µm because of flling of the gaps as shown in Fig. [4](#page-5-0).

## **3.3 Corrosion Characteristics**

The results of the corrosion progression in 3.5 wt% NaCl at 303 K from the linear potentiodynamic polarization

<span id="page-3-0"></span>





<span id="page-4-0"></span>**Fig.** 3 Distribution chart of particles of uncoated steel (a) and  $Nb_2O_5$ -Ni composite coatings with different percents: **b** 0 wt%, **c** 12 wt%, **d** 15 wt%, and **e** 30 wt%

study are shown in Fig. [5](#page-5-1) and Table [2](#page-5-2). The Tafel data were extrapolated to obtain  $E_{\text{corr}}$ ,  $i_{\text{corr}}$ , and Tafel slopes. From the polarization curves of the  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni composite coatings on carbon steel, it can be seen that corrosion potential  $(E_{\text{corr}})$  was shifted toward more noble value due to attaining passivity. The corrosion current density  $(i_{\text{corr}})$  was decreased with increasing wt% of  $Nb<sub>2</sub>O<sub>5</sub>$  in Ni coating confrming the role of protection of applied coatings. Tafel slopes  $(b_c \& b_a)$  deceased referring to reducing the reactions at cathodic and anodic sites.

Polarization resistance  $(R_p)$  can be calculated by the following formula [[11](#page-6-2)]:



<span id="page-5-0"></span>**Fig. 4** Microhardness and thickness of  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni-coated specimens



<span id="page-5-1"></span>**Fig. 5** Tafel plots of uncoated and coated specimens at 303 K

$$
R_{\rm p} = \frac{(b_{\rm c} \times b_{\rm a})}{2.3 \times i_{\rm corr}(b_{\rm c} + b_{\rm a})}.
$$
 (1)

The data of  $R_p$  as listed in Table [3](#page-5-3) indicate that the polarization resistance increased with increasing  $Nb<sub>2</sub>O<sub>5</sub>$  percent in Ni coating because of flling of the pores within the Ni layer.

Other parameters can be calculated from corrosion data such as protection efficiency ( $PE\%$ ) from corrosion current density of coated sample ( $i_{\text{corr,coated}}$ ) and corrosion current density of uncoated sample  $(i_{\text{corr,uncoded}})$  as follows [[12\]](#page-6-3):

PE% = 
$$
\left[1 - \frac{i_{\text{corr, coated}}}{i_{\text{corr,uncoded}}}\right] \times 100.
$$
 (2)

The protection efficiency increases with increasing  $wt\%$ of  $Nb<sub>2</sub>O<sub>5</sub>$  in coating composite to get the best efficiency equal to 80.826% for 30%  $Nb<sub>2</sub>O<sub>5</sub>$ -Ni mixture. The porosity percentage (PP%) can be calculated from the polarization

<span id="page-5-2"></span>**Table 2** Corrosion data of uncoated and coated steel at 303 K

Coating type	$-E_{\rm corr}$ mV	$l_{\rm corr}$ $\mu$ A cm <sup>-2</sup>	$-bc$ $mV$ dec <sup>-1</sup>	$+b_{\alpha}$
Uncoated steel	656	15.49	571.5	89.8
Ni coating	552	5.72	177.3	80.2
$12\%Nb2O5$ -Ni coating	517	4.51	184.2	73.4
$15\%Nb2O5$ -Ni coating	509	3.67	154.3	89.5
$30\%Nb2O5$ -Ni coating	490	2.97	151.8	71.5

<span id="page-5-3"></span>**Table 3** Protection properties of uncoated and coated steel at 303 K



resistance of uncoated ( $R_{p,\text{uncoded}}$ ) and coated ( $R_{p,\text{coated}}$ ) sample using the following equation [[13\]](#page-6-4):

$$
PP\% = \frac{R_{p,\text{uncoated}}}{R_{p,\text{coated}}} 10^{\frac{-\Delta E_{\text{corr}}}{b_{\text{a}}}} \times 100. \tag{3}
$$

The porosity percentage increases with increasing wt% of  $Nb<sub>2</sub>O<sub>5</sub>$  in nickel layer to get the best value of 0.433% for  $30\%$  Nb<sub>2</sub>O<sub>5</sub>-Ni composite coating due to incorporation of  $Nb<sub>2</sub>O<sub>5</sub>$  with Ni layer.

# **4 Conclusions**

 $Nb<sub>2</sub>O<sub>5</sub>$ -Ni composite coatings were successfully fabricated using DC sputtering.

The structural properties indicate the presence of  $Nb<sub>2</sub>O<sub>5</sub>$ within Ni coating by SEM/EDS and AFM.

Good corrosion resistance was attained for all deposited coatings as against the as-received specimen.

The signifcant performance improvement in the protection efficiency and porosity percentage was found as a result of physical barriers produced by  $Nb_2O_5$  particles by flling of the pores within the Ni layer.

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