

Stabilization of Asynchronous Switched Systems with Constrained Control

Yong Zhang¹ · Jingjing Hu¹  · Ning Wang²

Received: 18 April 2017 / Revised: 23 July 2017 / Accepted: 4 September 2017 / Published online: 11 September 2017
© Brazilian Society for Automatics–SBA 2017

Abstract This paper investigates the method on stabilizing asynchronous switched linear systems with constrained inputs. Firstly, asynchronous systems mean the asynchronization between the system modes and state feedback controllers. Usually, it takes a period of time to identify which one of the state feedback controllers should be activated in practical application. Next, in consideration of the saturation effect of the controllers, this paper is aimed at stabilizing the systems with constrained inputs by mode-dependent average dwell time method. Besides, unstable subsystems are considered in this paper.

Keywords Stabilization · Switched systems · Mode-dependent average dwell time · Constrained input · Asynchronization

1 Introduction

The past decades have witnessed the fast growing interest in switched systems, which consist of many subsystems and a switching law (Zhao et al. 2015). Switched systems are used in practical applications widely, such as electrical networks (Cong 2016), sampled-data systems (Hetel et al. 2011) and sliding mode control systems (Ullah et al. 2016). Meanwhile, many theories of switched systems have been well established, such as reachability (Chao and Yu 2015), adaptive controller design (Niu et al. 2017) and output tracking control (Niu and Zhao 2013).

Till now, the stability analysis of switched systems is still a hot field. The mode-dependent average dwell time (MDADT) (Zhao et al. 2012) based on multi-Lyapunov functions has been verified to be a very valid and flexible method. The results get by MDADT are much less conservative than those get by average dwell time. While using MDADT to analyze the stability of switched systems, every subsystem must be Hurwitz stable. Otherwise, a state feedback controller should be designed for the unstable subsystem. Fiacchini and Jungers (2014) and Minh et al. (2011) have studied the method on stabilizing the unstable subsystems. Besides, their researches are based on the assumption that the switching of system modes and state feedback controllers is simultaneous. However, in practical application, it usually takes a period of time to identify which subsystem is activated. And then the certain state feedback controller can be chosen (Liu et al. 2016). This causes the inaccuracy while applying the established theories to practice. Next, when a state feedback controller is designed, the control input is supposed to be set arbitrarily or infinitely. However, the controllers with saturation effect in practice limit this assumption. Over the past two decades, the stabilization study of control system (not switched system) was very abundant. Many excellent theories were established, such as Hu and Lin (2001) and Hu et al. (2002). In the book Hu and Lin (2001), the authors had introduced the solutions to stabilization of control systems with constrained input in detail. After several years, these theories were generalized to switched systems. In Chen et al. (2012), the authors studied stability condition of switched systems based on minimum dwell time method. In Remark 1 of Chen et al. (2012), the authors presented that “we cannot employ average dwell time approach”. In fact, it is incorrect. We can use not only average dwell time approach but also MDADT approach by choosing appropriate initial states. Via this way, we can design a switching signal more flexibly.

✉ Jingjing Hu
hu_589@163.com

¹ College of Information and Control Engineering, China University of Petroleum (East China), Qingdao, China

² Sinopec YuJi Natural Gas Pipeline Branch, Jinan, China

Although there are some researches toward stabilization of switched systems with constrained input, to the best of the authors' knowledge, no one considers asynchronous switching and constrained input jointly. For instance, authors in [Ding et al. \(2015\)](#) and [Chen et al. \(2012\)](#) studied the stability of switched systems with constrained input, but they all failed to analyze the asynchronous switching. Next, in [Benzaouia et al. \(2010\)](#), the arbitrary switching condition was studied. However, the results were restrictive to some extent because of the arbitrary switching law. Considering these, we aim at stabilizing the asynchronous switched linear systems with constrained inputs. It should be pointed out that all the subsystems may be unstable. Based on multi-Lyapunov functions, the mode-dependent average dwell time is obtained to guarantee that the system is exponentially stable. Furthermore, a Euclidean ball is found to limit the system states within it. By this method, the system can be stabilized with the constrained input. Moreover, most of the researchers assumed that each subsystem could be stabilized while analyzing the stability of switched systems with constrained input, such as [Ding et al. \(2015\)](#) and [Wang and Zhao \(2015\)](#). In fact, it is not impeccable. Because if certain subsystem state diverges quickly, the subsystem may not be stabilized by controllers with constrained input. In view of this, we present another two theorems (Theorems 2, 3). In the two theorems, the asynchronous switched systems with unstable subsystems can be exponentially stable with constrained control. Finally, while analyzing asynchronous switched systems, most of the researchers suppose that the delay time of state feedback controllers is a constant and equal. In this paper, the delay time of state feedback controllers can be different in different subsystems.

Notations Throughout this paper, the symbols used are quite standard. \mathbb{R}^n and $\mathbb{R}^{n \times n}$ represent the n -dimensional Euclidean space and the space of $n \times n$ matrices with real entries, respectively. $\|\cdot\|$ denotes the Euclidean vector norm. For a matrix P_i , $\lambda_i^{\max}(P_i)$ and $\lambda_i^{\min}(P_i)$ are the maximal and minimal eigenvalue of P_i , respectively. λ_{\min} is the minimum of λ_i^{\min} . For two vectors $x, y \in \mathbb{R}^n$, $x \leq y$ denotes $x_i \leq y_i$, $i = 1, 2, \dots, n$. $R(\cdot)$ denotes the range of a matrix. Δt^s is the total running time of stable subsystems while Δt^u denotes the total running time of unstable subsystems. Next, Δt_i denotes the total running time of the i th subsystem. In this paper, \max means the maximum. For example, T_{\max} , α_{\max} , μ_{\max} and β_{\max} denote the maximum of T_i , α_i , μ_i and β_i , respectively.

2 Preliminary

Consider the switched linear system

$$\dot{x} = A_{\sigma(t)}x + B_{\sigma(t)}u_{\sigma(t)} \quad (1)$$

where $x \in \mathbb{R}^n$ is the system state, $\sigma(t) : [0, \infty) \rightarrow \mathbb{Z} = \{1, 2, \dots, N\}$ is the switching law, N is the number of subsystems. For a switching sequence $t_0 < t_1 < \dots < t_k < \dots$, $\sigma(t)$ is continuous from right everywhere. Throughout this paper, $\sigma(t_k) = i$, $\sigma(t_k^-) = \sigma(t_{k-1}) = j$, $i \neq j$ and $\sigma(t) \in \mathbb{Z}$. So when $t \in [t_k, t_{k+1})$, we say the i th subsystem is activated. $A_i \in \mathbb{R}^{n \times n}$, $B_i \in \mathbb{R}^{n \times m_k}$.

Definition 1 ([Liberzon 2003](#)) The equilibrium $x = 0$ of system (1) is globally uniformly exponentially stable (GUES) under certain switching signal if for initial conditions $x(t_0)$, there exist constants $\eta_1 > 0$, $\eta_2 > 0$ such that the solution of the system satisfies

$$\|x(t)\| \leq \eta_1 e^{-\eta_2(t-t_0)} \|x(t_0)\|, \quad \forall t \geq t_0.$$

Definition 2 ([Zhao et al. 2012](#)) For a switching signal σ and any $t_2 > t_1 > t_0$, let $N_{\sigma i}(t_1, t_2)$ be the switching numbers of the i th subsystem over the interval $[t_1, t_2)$. If $N_{\sigma i}(t_1, t_2) \leq N_{0i} + (t_2 - t_1)/\tau_{ai}$ holds, then τ_{ai} is mode-dependent average dwell time and N_{0i} is mode-dependent chatter bound.

Definition 3 ([Xie et al. 2013](#)) For a switching signal σ and any $t_2 > t_1 > t_0$, let $N_{\sigma}^u(t_1, t_2)$ be the switching numbers of unstable subsystems over the interval $[t_1, t_2)$. If $N_{\sigma}^u(t_1, t_2) \geq N_0^u + \Delta t^u/\tau_a^u$ holds, then τ_a^u is average dwell time of unstable subsystems and N_0^u is called chatter bound.

Remark 1 To introduce the three definitions and the following lemma, the asynchronization between system modes and state feedback controllers is not considered. Besides, Definition 3 is used to analyze the stability of fast switched systems, which means the average dwell time cannot exceed an upper bound value.

Next, a method to stabilize linear systems (not switched linear system) is introduced.

Consider a linear system

$$\dot{x} = Ax + Bu \quad (2)$$

where $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times m}$, $\text{rank}(B) = m \leq n$, $u \in U \subset \mathbb{R}^m$, U is the admissible control set which is defined by $U = \{u \in \mathbb{R}^m \mid -u_{\min} \leq u \leq u_{\max}\}$, besides, $u_{\min}, u_{\max} \in \mathbb{R}^m$ are two vectors only with positive components. Set $K \in \mathbb{R}^{m \times n}$ such that $A - BK$ is Hurwitz matrix. Then the closed-loop system becomes

$$\dot{x} = (A - BK)x \quad (3)$$

Define

$$D = \{x \in \mathbb{R}^n \mid -u_{\min} \leq Kx \leq u_{\max}\} \quad (4)$$

Lemma 1 (Ni and Cheng 2012) For the system matrix A , using Schur unitary triangularization Theorem (Bhatia 1991), there exists an orthogonal matrix $Q \in \mathbb{R}^{n \times n}$ such that

$$Q^T A Q = \begin{pmatrix} A_0 & A_2 \\ 0 & A_1 \end{pmatrix} \tag{5}$$

where A_0 has all negative real part eigenvalues and A_1 has all nonnegative real part eigenvalues.

Consider the linear system (2). Suppose A has r non-negative real part eigenvalues. Q is an orthogonal matrix satisfying (5), besides,

$$Q^T B = \begin{pmatrix} (B_0)_{(n-r) \times r} & * \\ (B_1)_{r \times r} & * \end{pmatrix}$$

where $*$ is the element we do not concern. Let $H = (h_{ij})_{n \times n}$ be a Hurwitz matrix such that

$$\begin{pmatrix} H^+ & H^- \\ H^- & H^+ \end{pmatrix} (u_{\max}^T \ u_{\min}^T)^T \leq 0$$

where

$$H^+(i, j) = \begin{cases} h_{ij} & \text{if } i = j \\ \max(h_{ij}, 0) & \text{if } i \neq j \end{cases}$$

$$H^-(i, j) = \begin{cases} 0 & \text{if } i = j \\ \max(-h_{ij}, 0) & \text{if } i \neq j \end{cases}$$

Then there exists a unique solution to the equation

$$A_1 X - X H = -B_1 \tag{6}$$

Moreover, if $R(B_1) \subset R(X)$, system (2) with

$$K = - \begin{pmatrix} 0 & X^{-1} \\ 0 & 0 \end{pmatrix} Q^T$$

is asymptotically stable for all $x_0 \in D$. The control input $u = Kx$ is admissible and domain D in (4) is positively invariant.

Remark 2 Lemma 1 is used to stabilize linear systems with constrained inputs. We can stabilize all the subsystems according to Lemma 1, firstly, switched system may not be stable with all subsystem stable (the mode-dependent average dwell time must exceed a constant), secondly, how to choose an appropriate initial state? Thirdly, what if the switched system is with asynchronous switching? Finally, what if some of the subsystem cannot be stabilized? So this paper is aimed at solving the four problems.

In what follows, the method of stabilizing switched linear systems with constrained inputs will be presented.

3 Main Results

Consider system (1). $u_i = [u_i^1, u_i^2, \dots, u_i^{m_i}]^T \in \mathbb{R}^{m_i}$ is the control inputs, besides,

$$-u_i^{\min} \leq u_i \leq u_i^{\max}, \quad i \in \mathbb{Z} \tag{7}$$

where u_i^{\min} and u_i^{\max} are only with positive elements. Suppose that system (1) is controllable. According to Lemma 1, feedback matrices K_i and admissible region $D_i = \{x \in \mathbb{R}^n \mid -u_i^{\min} \leq K_i x \leq u_i^{\max}\}$ can be obtained. Assume that the switched controllers lag behind system modes for T_i , besides, $T_i < (t_{k+1} - t_k)$. Then system (1) becomes

$$\dot{x} = (A_{\sigma(t)} - B_{\sigma(t)} K_{\sigma(t-T_i)})x \tag{8}$$

Because of asynchronous switching, time interval $[t_k, t_{k+1})$ is divided into matched period (denoted by T_i^+) and mismatched period (denoted by T_i). It should be pointed out that during all the mismatched periods, the system is supposed to be divergent. Let Ω be the biggest Euclidean ball which is centered at the origin and inside the intersection of D_i , $i \in \mathbb{Z}$. For any $z \in \Omega$,

$$d = \max(\|z\|).$$

In what follows, the main results of this paper will be presented.

Theorem 1 Consider system (8), let K_i be obtained in Lemma 1, if there exist constants $\alpha_i > 0$, $\beta_i > 0$, $\mu_i \geq 1$ and two class κ_∞ functions κ_1, κ_2 such that (9), (10), (11), (12) and (13) hold, then system (8) is exponentially stable by admissible control input $u_i = K_i x, \forall i \in \mathbb{Z}$.

$$\|x(t_0)\|^2 \leq d^2 / \psi_1 \tag{9}$$

$$\kappa_1(\|x(t)\|) \leq V_i(x(t)) \leq \kappa_2(\|x(t)\|) \tag{10}$$

$$\dot{V}_i(x(t)) \leq \begin{cases} -\alpha_i V_i(x(t)) & t \in [t_k + T_i, t_{k+1}) \\ \beta_i V_i(x(t)) & t \in [t_k, t_k + T_i) \end{cases} \tag{11}$$

$$V_i(x(t)) \leq \mu_i V_j(x(t)) \tag{12}$$

$$\tau_{ai} > \frac{T_i(\alpha_i + \beta_i) + \ln \mu_i}{\alpha_i} \tag{13}$$

where

$$\psi_1 = \frac{\lambda_{\sigma(t_0)}^{\max}}{\lambda_{\min}} \cdot \exp\{\beta_{\max} T_{\max}\} \cdot \prod_{i=1}^N \mu_i^{N_{0i}} \cdot \exp\{T_i(\alpha_i + \beta_i) N_{0i}\}.$$

Proof Denote $g_i(t) = e^{\alpha_i t} V_i(t)$. Then

$$\frac{dg_i(t)}{dt} = e^{\alpha_i t} [\dot{V}_i(t) + \alpha_i V_i(t)] \tag{14}$$

From the first inequality in (11), it can be obtained that $g_i(t)$ is decreasing when $t \in [t_k + T_i, t_{k+1})$. Thus,

$$V_{\sigma(t_k)}(x(t_{k+1})) \leq e^{-\alpha_i(t_{k+1}-t_k-T_i)} V_{\sigma(t_k)}(x(t_k + T_i)) \tag{15}$$

From the second inequality in (11), when $t \in [t_k, t_k + T_i)$, by using the same method, the following can be got

$$V_{\sigma(t_k)}(x(t_k + T_i)) \leq e^{\beta_i T_i} V_{\sigma(t_k)}(x(t_k)) \tag{16}$$

Combine (15) and (16), it follows that

$$V_{\sigma(t_k)}(x(t_{k+1})) \leq e^{-\alpha_i T_i^+ + \beta_i T_i} V_{\sigma(t_k)}(x(t_k)) \tag{17}$$

Multiply both sides of (17) by $\mu_{\sigma(t_{k+1})}$ and then apply (12) to it, we can get

$$V_{\sigma(t_{k+1})}(x(t_{k+1})) \leq e^{-\alpha_i T_i^+ + \beta_i T_i} \mu_{\sigma(t_{k+1})} V_{\sigma(t_k)}(x(t_k)) \tag{18}$$

It follows from (18) that,

$$\begin{aligned} V_{\sigma(t_{k+1})}(x(t_{k+1})) &\leq e^{-\alpha_i(T_i^+ + T_i)} \frac{e^{\beta_i T_i^-}}{e^{-\alpha_i T_i^-}} \mu_{\sigma(t_{k+1})} V_{\sigma(t_k)}(x(t_k)) \\ &= e^{-\alpha_i(t_{k+1}-t_k)} e^{T_i(\alpha_i + \beta_i)} \mu_{\sigma(t_{k+1})} V_{\sigma(t_k)}(x(t_k)) \\ &\leq e^{-\alpha_i(t_{k+1}-t_k)} e^{T_i(\alpha_i + \beta_i)} \mu_{\sigma(t_{k+1})} \mu_{\sigma(t_k)} V_{\sigma(t_{k-1})}(x(t_k)) \\ &\vdots \\ &\leq \prod_{i=1}^N \mu_i^{N_{\sigma_i}} e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i) N_{\sigma_i}} V_{\sigma(t_0)}(x(t_0)) \\ &< \exp\{\beta_{\max} T_{\max}\} \end{aligned} \tag{19}$$

$$\prod_{i=1}^N \mu_i^{N_{\sigma_i}} e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i) N_{\sigma_i}} V_{\sigma(t_0)}(x(t_0)) \tag{20}$$

Then Lyapunov functions are set as

$$V_i(x(t)) = x^T P_i x \tag{21}$$

According to the Rayleigh theorem,

$$\lambda_{\min}(P) \leq \frac{x^T P x}{x^T x} \leq \lambda_{\max}(P) \tag{22}$$

the following can be got from (19) and (22)

$$\begin{aligned} \|x(t_{k+1})\|^2 &\leq \frac{\lambda_{\max}^{\sigma(t_0)}}{\lambda_{\min}^{\sigma(t_{k+1})}} \cdot \exp\{\beta_{\max} T_{\max}\} \\ &\cdot \prod_{i=1}^N \mu_i^{N_{\sigma_i}} e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i) N_{\sigma_i}} \|x(t_0)\|^2 \end{aligned} \tag{23}$$

Because $N_{\sigma_i}(t_1, t_2) \leq N_{0i} + \frac{\Delta t_i}{\tau_{ai}}$ in Definitions 2 and (13) hold, (23) can be simplified to

$$\begin{aligned} \|x(t_{k+1})\|^2 &\leq \psi_1 \\ &\exp\left\{ \sum_{i=1}^N \Delta t_i \cdot \left[\frac{\ln \mu_i}{\tau_{ai}} - \alpha_i + \frac{T_i(\alpha_i + \beta_i)}{\tau_{ai}} \right] \right\} \|x(t_0)\|^2 \end{aligned} \tag{24}$$

Denote $\xi_1 = \max_{i \in \mathbb{Z}} \left(\frac{\ln \mu_i}{\tau_{ai}} - \alpha_i + \frac{T_i(\alpha_i + \beta_i)}{\tau_{ai}} \right)$, then (24) becomes

$$\|x(t_{k+1})\|^2 \leq \psi_1 \exp\{\xi_1(t - t_0)\} \|x(t_0)\|^2 \tag{25}$$

From Definition 1, it can be obtained that system (8) is exponentially stable under condition (13). Next, since (9) holds and Ω is an Euclidean ball, besides, $D_i, i \in \mathbb{Z}$, are positively invariant, then for any $\sigma(t_k) \in \mathbb{Z}$, state response $x(t) \in \Omega$. Thus, the control input $u_i = K_i x$ is admissible. In conclusion, the system is exponentially stable with constrained control. \square

Remark 3 To solve τ_{ai} , the Lyapunov function can be chosen as $V_i(x(t)) = x^T P_i x$, then, (11) and (12) become (26) and (27), respectively.

$$\begin{cases} (A_i - B_i K_i)^T P_i + P_i (A_i - B_i K_i) \leq -\alpha_i P_i, & t \in [t_k + T_i, t_{k+1}) \\ (A_i - B_i K_j)^T P_i + P_i (A_i - B_i K_j) \leq \beta_i P_i, & t \in [t_k, t_k + T_i) \end{cases} \tag{26}$$

$$P_i \leq \mu_i P_j \tag{27}$$

By using LMI toolbox in Matlab, α_i, β_i and μ_i can be got. Then τ_{ai} can be solved.

Remark 4 As has been supposed that the system is divergent during all the mismatched periods (the divergence speed can be described by β_i) and the delay time (T_i) of state feedback controllers can be different and variable. With β_i and T_i getting larger, ψ_1 is getting larger simultaneously. This means the feasible initial states that can be chosen are shrunken.

As has been assumed that all the subsystems can be stabilized by Lemma 1, but what if some of the subsystems cannot be stabilized? Besides, in practice, it is usually difficult to design some state feedback controllers. Considering this, we suppose that only the subsystems $i \in [1, M]$ can be stabilized, $\Omega \subset \bigcap_{i=1}^M D_i$ is the biggest Euclidean ball centered at the origin and the rest of subsystems ($i \in [M+1, N]$) are without state feedback controllers. For any $z \in \Omega, d = \max(\|z\|)$. Besides, $V_i^s(x(t))$ and $V_i^u(x(t))$ are Lyapunov functions for stable subsystems and unstable subsystems, respectively. τ_{ai}^s and τ_{ai}^u are MDADT of stable subsystems and unstable subsystems, respectively. Moreover,

$$\Delta_{\max} = \max_{M+1 \leq \sigma(t_k) \leq N} (t_{k+1} - t_k).$$

Now we will give another two theorems where there are unstable subsystems without state feedback controllers.

Theorem 2 Consider system (8), let $K_i, i \in [1, M]$ be obtained in Lemma 1 and $u_i = 0, \forall i \in [M + 1, N]$. If there exist constants $\alpha_i > 0, \alpha^u > 0, \beta_i > 0, \beta^u > 0, \mu_i \geq 1, 0 < \mu^u < 1$ and two class κ_∞ functions κ_1, κ_2 such that (28), (29), (30), (31) and (32) hold, then system (8) is exponentially stable by admissible control input $u_i = K_i x, i \in [1, M]$.

$$\|x(t_0)\|^2 \leq d^2/\psi_2 \tag{28}$$

$$\begin{cases} \kappa_1(\|x(t)\|) \leq V_i^s(x(t)) \leq \kappa_2(\|x(t)\|) \\ \kappa_1(\|x(t)\|) \leq V_i^u(x(t)) \leq \kappa_2(\|x(t)\|) \end{cases} \tag{29}$$

$$\begin{cases} \dot{V}_i^s(x(t)) \leq \begin{cases} -\alpha_i V_i^s(x(t)), & t \in [t_k + T_i, t_{k+1}) \\ \beta_i V_i^s(x(t)), & t \in [t_k, t_k + T_i) \end{cases} \\ \dot{V}_i^u(x(t)) \leq \begin{cases} \alpha^u V_i^u(x(t)), & t \in [t_k + T_i, t_{k+1}) \\ \beta^u V_i^u(x(t)), & t \in [t_k, t_k + T_i) \end{cases} \end{cases} \tag{30}$$

$$\begin{cases} V_i^s(x(t)) \leq \mu_i V_j^s(x(t)) \\ V_i^s(x(t)) \leq \mu_i V_j^u(x(t)) \\ V_i^u(x(t)) \leq \mu^u V_j^s(x(t)) \end{cases} \tag{31}$$

$$\begin{cases} \tau_{ai}^s > \frac{T_i(\alpha_i + \beta_i) + \ln \mu_i}{\alpha_i} \\ \tau_a^u < \frac{-\ln \mu^u}{\gamma} \end{cases} \tag{32}$$

where $\psi_2 = \frac{\lambda_{\sigma(t_0)}^{\max}}{\lambda_{\min}} \cdot \mu_{\max} \exp\{\gamma \Delta_{\max} + \beta_{\max} T_{\max}\} (\mu^u)^{N_0^u} \cdot \prod_{i=1}^M \mu_i^{N_{0i}} \cdot \exp\{T_i(\alpha_i + \beta_i)N_{0i}\}$ is a constant, τ_a^u is the average dwell time (except MDADT) of unstable subsystems and $\gamma = \max(\alpha^u, \beta^u)$.

Proof The proof of Theorem 2 is similar to that of Theorem 1. So some part of the proof which has been appeared in Theorem 1 is omitted. It follows from (18) that

$$\begin{aligned} V_{\sigma(t_{k+1})}(x(t_{k+1})) &\leq e^{-\alpha_i T_i^+ + \beta_i T_i} \mu_{\sigma(t_{k+1})} V_{\sigma(t_k)}(x(t_k)) \\ &\vdots \\ &\leq e^{\gamma \Delta t^u} \mu_u^{N_\sigma^u} \cdot \prod_{i=1}^M e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i)N_{\sigma_i}} \mu_i^{N_{\sigma_i}} V_{\sigma(t_0)}(x(t_0)) \end{aligned} \tag{33}$$

The Lyapunov functions are set as $V_i(x(t)) = x^T P_i x$ then the following can be got.

$$\|x(t_{k+1})\|^2 \leq \frac{\lambda_{\sigma(t_0)}^{\max}}{\lambda_{\min}} e^{\gamma \Delta t^u} (\mu^u)^{N_\sigma^u} \cdot \prod_{i=1}^M e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i)N_{\sigma_i}} \mu_i^{N_{\sigma_i}} \|x(t_0)\|^2 \tag{34}$$

$$\begin{aligned} &< \frac{\lambda_{\sigma(t_0)}^{\max}}{\lambda_{\min}} \mu_{\max} \exp\{\gamma \Delta_{\max} + \beta_{\max} T_{\max}\} e^{\gamma \Delta t^u} (\mu^u)^{N_{\sigma^u}} \\ &\cdot \prod_{i=1}^M e^{-\alpha_i \Delta t_i} e^{T_i(\alpha_i + \beta_i)N_{\sigma_i}} \mu_i^{N_{\sigma_i}} \|x(t_0)\|^2 \end{aligned} \tag{35}$$

From Definitions 2, 3 and inequality (32), (34) can be simplified to

$$\|x(t_{k+1})\|^2 \leq \psi_2 \exp\left\{\sum_{i=1}^M \left[\frac{\ln \mu_i + T_i(\alpha_i + \beta_i)}{\tau_{ai}^s} - \alpha_i\right] \cdot \Delta t_i + \left(\frac{\ln \mu^u}{\tau_a^u} + \gamma\right) \cdot \Delta t^u\right\} \|x(t_0)\|^2 \tag{36}$$

Denote $\xi_2 = \max\left(\frac{\ln \mu_i + T_i(\alpha_i + \beta_i)}{\tau_{ai}^s} - \alpha_i, \frac{\ln \mu^u}{\tau_a^u} + \gamma\right)$ Then (36) becomes

$$\|x(t_{k+1})\|^2 \leq \psi_2 \exp\{\xi_2(t - t_0)\} \|x(t_0)\|^2 \tag{37}$$

Compared with Definition 1, it can be concluded that system (8) is exponentially stable under condition (32). Next, since (28) holds, and D_i is positively invariant, then from (36), for any $\sigma(t_k) \in \mathbb{Z}$, state response $x(t) \in \Omega$. Thus the control input $u_i = K_i x, i \in [1, M]$ is admissible. In conclusion, the system is exponentially stable with constrained control. \square

Remark 5 As has been stated, both τ_{ai} and τ_a^u can be calculated by using the LMI toolbox in Matlab. Next, from (31), it should be noticed that once the unstable subsystem is activated, then the following subsystem must be a stable subsystem. In what follows, another theorem is presented where the unstable subsystems can be activated one by one. But its total running time must be limited.

Theorem 3 Consider system (8), let $K_i, i \in [1, M]$ be obtained in Lemma 1. If there exist constants $\mu_i \geq 1, \beta_i > 0, \alpha_i$ and two class κ_∞ functions κ_1, κ_2 such that (38), (39), (40), (41) and (42) hold, then system (8) is exponentially stable by admissible control input $u_i = K_i x, i \in [1, M]$.

$$\|x(t_0)\|^2 \leq d^2/\psi_3 \tag{38}$$

$$\kappa_1(\|x(t)\|) \leq V_i(x(t)) \leq \kappa_2(\|x(t)\|) \tag{39}$$

$$\dot{V}_i(x(t)) \leq \begin{cases} -\alpha_i V_i(x(t)), & t \in [t_k + T_i, t_{k+1}) \\ \beta_i V_i(x(t)), & t \in [t_k, t_k + T_i) \end{cases} \tag{40}$$

$$V_i(x(t)) \leq \mu_i V_j(x(t)) \tag{41}$$

$$\begin{cases} \tau_{ai}^s > \frac{T_i(\alpha_i + \beta_i) + \ln \mu_i}{\alpha_i} \\ \tau_{ai}^u \geq 0 \\ \frac{\Delta t^s}{\Delta t^u} > \frac{\zeta^* - \zeta_2}{\zeta_1 - \zeta^*}, (\zeta_1 < \zeta^* < 0) \end{cases} \tag{42}$$

where $\zeta_1 = \max_{1 \leq i \leq M} \left(\frac{T_i(\alpha_i + \beta_i)}{\tau_{ai}^s} - \alpha_i + \frac{\ln \mu_i}{\tau_{ai}^s}\right)$ is a negative constant, $\zeta_2 = \max_{M+1 \leq i \leq N} \left(\frac{T_i(\alpha_i + \beta_i)}{\tau_{ai}^u} - \alpha_i + \frac{\ln \mu_i}{\tau_{ai}^u}\right)$ is

a positive constant and $\psi_3 = \frac{\lambda_{\sigma(t_0)}^{\max}}{\lambda_{\min}} \mu_{\max} \exp\{\gamma \Delta_{\max} + \beta_{\max} T_{\max}\} \prod_{i=1}^N \exp\{T_i(\alpha_i + \beta_i) N_{0i} + N_{0i} \ln \mu_i\}$ is a positive constant.

Proof The proof of Theorem 3 is similar to that of Theorem 1. So some part of the proof which has been appeared in Theorem 1 is omitted. It follows from (18) that

$$V_{\sigma(t_{k+1})}(x(t_{k+1})) \leq e^{-\alpha_i T_i^+ + \beta_i T_i} \mu_{\sigma(t_{k+1})} V_{\sigma(t_k)}(x(t_k)) \leq e^{-\alpha_i T_i^+ + \beta_i T_i} \mu_{\sigma(t_{k+1})} \mu_{\sigma(t_k)} V_{\sigma(t_k^-)}(x(t_k)) \quad (43)$$

$$\begin{aligned} & \vdots \\ & \leq \prod_{i=1}^M \mu_i^{N_{\sigma i}} \exp\{-\alpha_i \Delta t_i + T_i(\alpha_i + \beta_i) N_{\sigma i}\} \\ & \quad \cdot \prod_{i=M+1}^N \mu_i^{N_{\sigma i}} \exp\{-\alpha_i \Delta t_i + T_i(\alpha_i + \beta_i) N_{\sigma i}\} \quad (44) \end{aligned}$$

$$\begin{aligned} & < \mu_{\max} \exp\{\gamma \Delta_{\max} + \beta_{\max} T_{\max}\} \\ & \prod_{i=1}^M \mu_i^{N_{\sigma i}} \exp\{-\alpha_i \Delta t_i + T_i(\alpha_i + \beta_i) N_{\sigma i}\} \\ & \quad \cdot \prod_{i=M+1}^N \mu_i^{N_{\sigma i}} \exp\{-\alpha_i \Delta t_i + T_i(\alpha_i + \beta_i) N_{\sigma i}\} \quad (45) \end{aligned}$$

The Lyapunov functions are set as $V_i(x(t)) = x^T P_i x$ then the following can be got,

$$\|x(t_{k+1})\|^2 \leq \psi_3 \exp\{\Delta t^s \zeta_1 + \Delta t^u \zeta_2\} \|x(t_0)\|^2 \quad (46)$$

Because $\zeta_1 < \zeta^* < 0$ holds, (46) becomes,

$$\|x(t_{k+1})\|^2 \leq \psi_3 \exp\{\zeta^*(t - t_0)\} \|x(t_0)\|^2 \quad (47)$$

So (42) can verify exponential stability of the system. Besides, (38) makes the control input admissible. This completes the proof of the theorem. \square

Remark 6 In Theorem 1, ψ_1 will get larger with T_i and β_i getting larger. In Theorems 2 and 3, ψ_2 and ψ_3 not only have a relationship with T_i and β_i , but also have a relationship with Δ_{\max} and γ . In this way, the trajectory of state response with unstable subsystems can remain in the feasible region all the time.

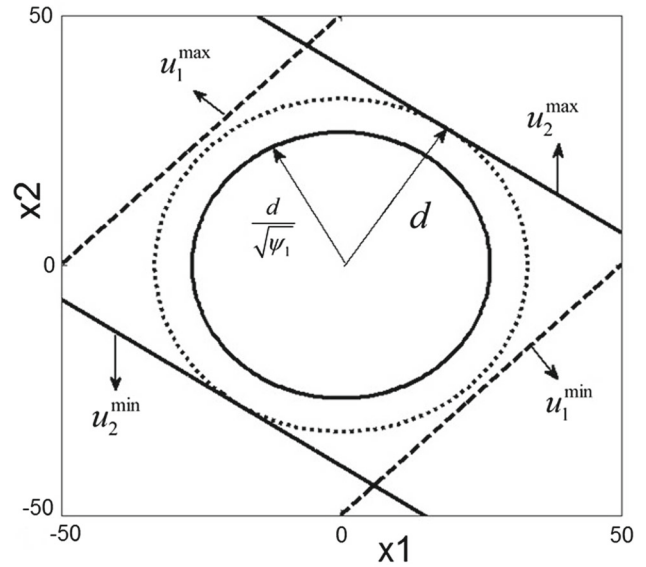


Fig. 1 The feasible region of initial states

4 Numerical Examples

Example 1 Consider system (8) with

$$A_1 = \begin{bmatrix} -1.4402 & -3.36 \\ -3.52 & -1.28 \end{bmatrix}, B_1 = \begin{bmatrix} -3.36 \\ 3.52 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} -2.928 & 2.88 \\ 2.24 & -1.488 \end{bmatrix}, B_2 = \begin{bmatrix} 1.92 \\ 2.24 \end{bmatrix}$$

$T_1 = T_2 = 0.1$ s. $N_{01} = N_{02} = 0$. According to Lemma 1, feedback matrices can be chosen as: $K_1 = [-1 \ 1]$, $K_2 = [1 \ 1.5]$.

By solving the LMIs in (26) and (27), we can get $\alpha_1 = 9.5999$, $\beta_1 = 0.224$, $\mu_1 = 1.4455$, $\alpha_2 = 9.6938$, $\beta_2 = 0.3198$, $\mu_2 = 1$ (μ_2 is smaller than one so it is enlarged to one.), $\psi_1 = 1.7211$. According to (13), $\tau_{a1} > 0.1023$, $\tau_{a2} > 0.1033$. The control input is constrained with $-50 \leq u_1 \leq 50$ and $-40 \leq u_2 \leq 40$. Because $u_i = K_i x$, we can get the biggest Euclidean ball, which is plotted in a dotted line in Fig. 1. The circle plotted in a solid line illustrates the feasible region of initial states. We choose $x(t_0) = [-20 \ 17.5601]$, $\tau_{a1} = 0.12$ s, $\tau_{a2} = 0.13$ s. Figure 2 illustrates the state responses, while Fig. 3 is the switching signal. Next, we choose $\tau_{a1} = 0.19$ s, $\tau_{a2} = 0.2$ s, Fig. 4 illustrates the state responses, while Fig. 5 is the switching signal.

Example 2 Consider system (8) in Example 1 with the same subsystems and another subsystem:

$$A_3 = \begin{bmatrix} 0.048 & 0 \\ 0 & 0.048 \end{bmatrix}, B_3 = \begin{bmatrix} 0.16 \\ 0.32 \end{bmatrix}$$

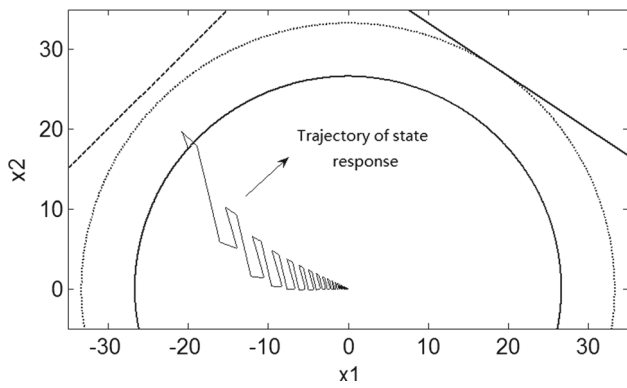


Fig. 2 State responses of Example 1 with shorter MDADT

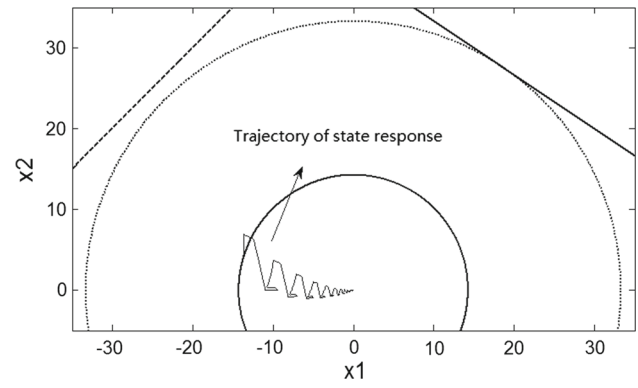


Fig. 6 State responses of Example 2 with shorter MDADT

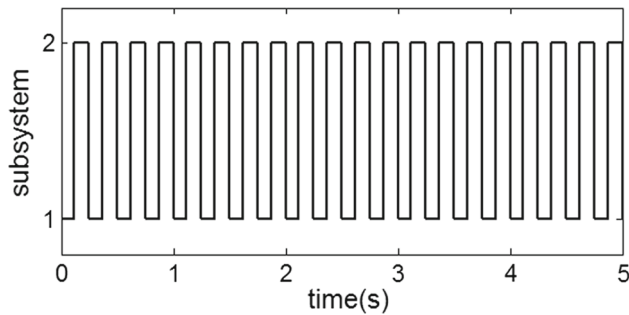


Fig. 3 Switching signal of Example 1 with shorter MDADT

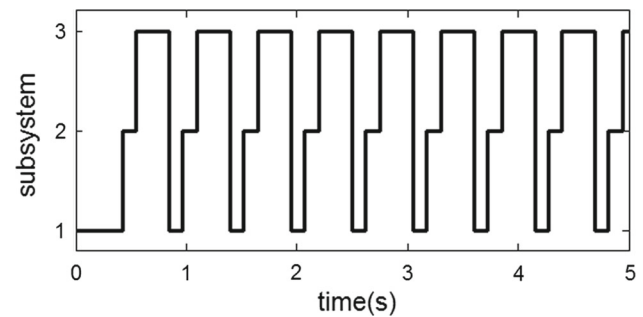


Fig. 7 Switching signal of Example 2 with shorter MDADT

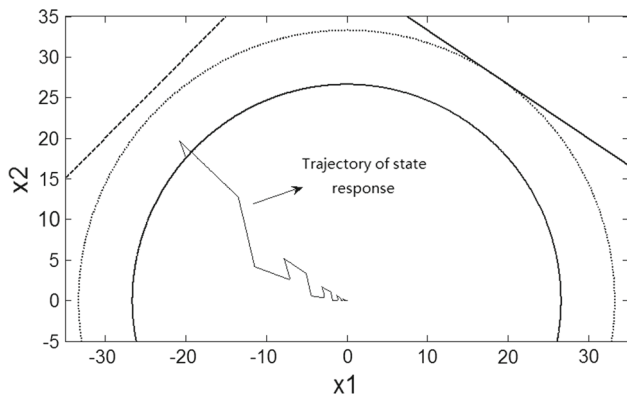


Fig. 4 State responses of Example 1 with longer MDADT

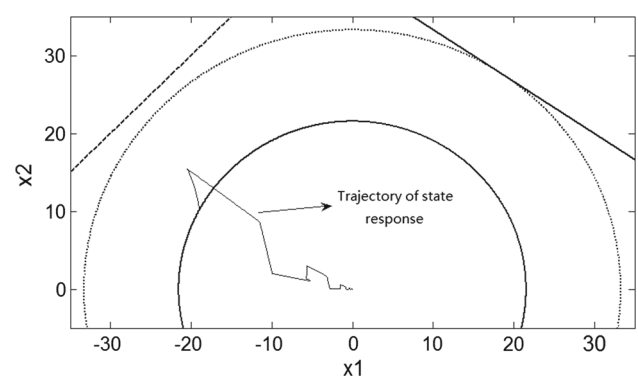


Fig. 8 State responses of Example 2 with longer MDADT

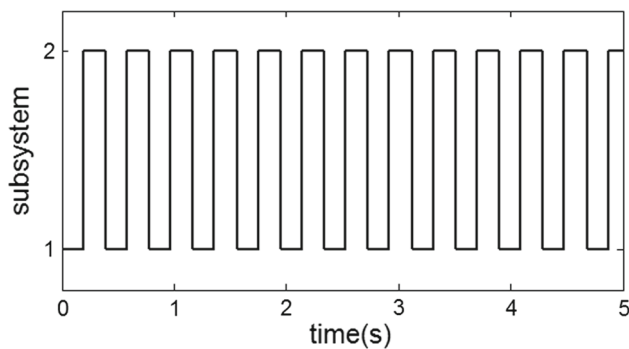


Fig. 5 Switching signal of Example 1 with longer MDADT

Suppose subsystem 3 cannot be stabilized and $N_{03} = 0$, $T_3 = 0.1$ s. By solving the LMIs in Theorem 2 we can get $\alpha_1 = 9.5999$, $\beta_1 = 0.224$, $\mu_1 = 1$, $\alpha_2 = 9.6838$, $\beta_2 = 0.96$, $\mu_2 = 1$, $\gamma = 3.8398$. $\mu^u = 0.207$. According to (32), we can get $\tau_{a1} > 0.102$ s, $\tau_{a2} > 0.110$ s, $\tau_{a3} < 0.400$ s. Then we choose $\tau_{a1} = 0.12$ s, $\tau_{a2} = 0.13$ s, $\tau_{a3} = 0.3$ s, then $\psi_2 = 5.446$, we choose $x(t_0) = [-14 \ 2.7184]$. Figures 6 and 7 illustrate the state responses and switching signal, respectively. Next, we choose $\tau_{a1} = 0.22$ s, $\tau_{a2} = 0.23$ s, $\tau_{a3} = 0.2$ s, then $\psi_2 = 2.386$, we choose $x(t_0) = [-19 \ 10.1601]$. Figures 8 and 9 illustrate the state responses and switching signal, respectively.

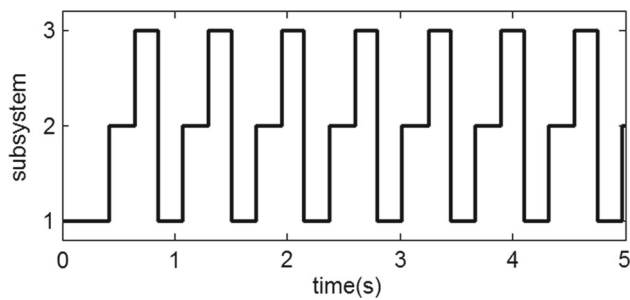


Fig. 9 Switching signal of Example 2 with longer MDADT

From the two examples, it can be noticed that by choosing the appropriate initial states and MDADT, the asynchronous switched system is exponentially stable. Besides, although there may be unstable subsystem, the trajectory of state responses can also remain in the feasible region all the time. The example for Theorem 3 is omitted. The advantage of Theorem 3 is that unstable subsystems can be activated one by one. But the total running time of stable and unstable subsystems must be calculated.

5 Conclusion

This paper provides three theorems which can be used to stabilize asynchronous switched systems with constrained inputs and unstable subsystems. The mode-dependent average dwell time can guarantee that the system is exponentially stable. Even if there are unstable subsystems, the restriction of the running time of unstable subsystems can also guarantee the system is exponentially stable. Furthermore, choosing the initial states within a specific Euclidean ball makes the control inputs admissible all the time.

Acknowledgements This work is supported by National Nature Science Foundation under Grant 51777215, the Fundamental Research Funds for the Central Universities under Grant 16CX02035A and the Applied Basic Research Plan Project of Qingdao City under Grant 16-5-1-1-jch.

References

Benzaouia, A., Akhrif, O., & Saydy, L. (2010). Stabilisation and control synthesis of switching systems subject to actuator saturation. *International Journal of Systems Science*, 41(4), 397–409.

Bhatia, R. (1991). Matrix analysis. *Graduate Texts in Mathematics*, 169(8), 1–17.

Chao, D. Y., & Yu, T. H. (2015). Computation of control related states of bottom kth-order system (with a non-sharing resource place) of Petri nets. *Transactions of the Institute of Measurement and Control*, 37(3), 382–395.

Chen, Y., Fei, S., Zhang, K., & Fu, Z. (2012). Control synthesis of discrete-time switched linear systems with input saturation based on minimum dwell time approach. *Circuits Systems and Signal Processing*, 31(2), 779–795.

Cong, S. (2016). On almost sure stability conditions of linear switching stochastic differential systems. *Nonlinear Analysis Hybrid Systems*, 22, 108–115.

Ding, X., Xiang, Z., & Yang, C. (2015). Robust stabilization and disturbance rejection of positive systems with time-varying delays and actuator saturation. *Mathematical Problems in Engineering*, 2015, Article ID 125343. doi:10.1155/2015/125343.

Fiacchini, M., & Jungers, M. (2014). Necessary and sufficient condition for stabilizability of discrete-time linear switched systems: A set-theory approach. *Automatica*, 50(1), 75–83.

Hetel, L., Daafouz, J., Richard, J. P., & Jungers, M. (2011). Delay-dependent sampled-data control based on delay estimates. *Systems and Control Letters*, 60(2), 146–150.

Hu, T., & Lin, Z. (2001). *Control systems with actuator saturation: Analysis and design (control engineering)*. Boston: Birkhauser.

Hu, T. S., Lin, Z. L., & Chen, B. M. (2002). Analysis and design for discrete-time linear systems subject to actuator saturation. *Systems and Control Letters*, 45(2), 97–112.

Liberzon, D. (2003). *Switching in systems and control*. Berlin: Birkhauser.

Liu, J., Wang, D., Wang, W., & Zhuang, Y. (2016). Positive stabilization for switched linear systems under asynchronous switching. *International Journal of Robust and Nonlinear Control*, 26(11), 2338–2354.

Minh, V. T., Awang, M., & Parman, S. (2011). Conditions for stabilizability of linear switched systems. *International Journal of Control Automation and Systems*, 9(1), 139–144.

Ni, W., & Cheng, D. (2012). Stabilization of switched linear systems with constrained inputs. *Journal of Systems Science and Complexity*, 25(1), 60–70.

Niu, B., Karimi, H. R., Wang, H., & Liu, Y. (2017). Adaptive Output-feedback controller design for switched nonlinear stochastic systems with a modified average dwell-time method. *IEEE Transactions on Systems Man Cybernetics Systems*, 47(7), 1371–1382.

Niu, B., & Zhao, J. (2013). Barrier Lyapunov functions for the output tracking control of constrained nonlinear switched systems. *Systems and Control Letters*, 62(10), 963–971.

Ullah, N., Han, S., & Khattak, M. I. (2016). Adaptive fuzzy fractional-order sliding mode controller for a class of dynamical systems with uncertainty. *Transactions of the Institute of Measurement and Control*, 38(4), 402–413.

Wang, J., Zhao, J., & Dimirovski, G. M. (2015). Stabilization and L-1-gain analysis of switched positive system subject to actuator saturation by average dwell time approach. In *34th Chinese control conference (CCC), Hangzhou, Peoples Republic of China, 2015 Jul 28–30 2015* (pp. 59–62, Chinese Control Conference).

Xie, D., Zhang, H., Zhang, H., & Wang, B. (2013). Exponential stability of switched systems with unstable subsystems: A mode-dependent average dwell time approach. *Circuits Systems and Signal Processing*, 32(6), 3093–3105.

Zhao, X., Yin, S., Li, H., & Niu, B. (2015). Switching Stabilization for a class of slowly switched systems. *IEEE Transactions on Automatic Control*, 60(1), 221–226.

Zhao, X., Zhang, L., Shi, P., & Liu, M. (2012). Stability and stabilization of switched linear systems with mode-dependent average dwell time. *IEEE Transactions on Automatic Control*, 57(7), 1809–1815.