Mechanical and Thermal Properties of Waterborne Polyurethane Films Modified by CaCO₃@TiO₂ Particles with UV Absorption Activity

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Abstract CaCO₃@TiO₂ particles were synthesized through a direct carbonation method, which can be used as the substitutes of TiO₂ in pigments and coatings. To improve the dispersion in waterborne polyurethane(WPU) suspensions, CaCO₃@TiO₂ particles were modified by stearic acid. SEM tests of the fractured surfaces of the composites films showed that the CaCO₃@TiO₂ particles were well embedded in the WPU matrix. And the mechanical properties, thermal stability and water resistance of the composites films were improved by the introduction of CaCO₃@TiO₂ particles.

Keywords Waterborne polyurethane; CaCO₃@TiO₂ particle; In situ polymerization

1 Introduction

Waterborne polyurethane(WPU) owns excellent features of non-pollution and non-toxicity, and is widely applied in coatings, adhesives, paper, textile, wood or glass fiber, and biodegradable materials^[1—3] instead of the conventional organic solvent-borne polyurethane(SPU). Compared to SPU, WPU still has some drawbacks such as lower thermal stability, water-resistance, photostability and mechanical strength^[4]. To improve the performance of WPU, powder composition methods have been used as an effective strategy, such as the introduction of $CaCO_3^{[5]}$, $SiO_2^{[6]}$, $TiO_2^{[7]}$, $clay^{[8]}$, $ZnO^{[9]}$, $Ag^{[10]}$, graphene^[11,12] in WPU dispersions^[13].

Yao *et al.*^[5] had prepared stable WPU/CaCO₃ hybrids with good dispersion of CaCO₃ by gas-diffusion mineralization method, and the thermal stability, water penetration and chemical resistance of the hybrid films were improved. Che *et al.*^[7] obtained Nano-TiO₂/PU emulsions *via in situ* RAFT(reversible addition-fragmentation chain transfer) polymerization of HEA-end capped PUM emulsions(HEA=hydroxyethyl acrylate). The tensile strengths of the composite films were significantly enhanced and the nano-TiO₂/PU emulsions were stable enough not to precipitate in at least three months^[6]. Therefore, the interaction between the fillers and PU chains should be considered before the composition process^[14].

We had reported two routes to prepare WPU/CaCO₃ and WPU/SiO₂ composites films, which only focus on the basic synthesis method, not the specific properties derived from the fillers^[15].

Core-shell structured CaCO3@TiO2 particles could be

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considered as the potential substitute of commercial TiO₂, for its outer layer was composed of TiO₂ nano-sheets to exhibit most properties of TiO₂, which leads to lower the consumption of TiO₂^[16]. Various methods have been reported for the synthesis of CaCO₃@TiO₂ composite, including template method^[12], liquid deposition method^[13], sol-precipitation routes^[14,15], and mechanochemical method^[14].

In this study, CaCO₃@TiO₂ particles were prepared by bubbling CO₂ gas into Ca(OH)₂-TiO₂ slurry as reported before^[17]. WPU/CaCO₃@TiO₂ composites were obtained by *in situ* polymerization method^[18,19]. The properties of WPU/ CaCO₃@TiO₂ composites films were studied by scanning electron microscopy(SEM), thermogravimetric analysis(TGA), UV-Visible spectrometry, mechanical testing and water swelling testing^[20]. WPU/CaCO₃@TiO₂ composites can be potentially applied in coatings and textiles fields^[21].

2 Experimental

2.1 Materials

CaO was supplied by Menghe Chemical Reagent Factory. Rutile-type TiO_2 treated by silica and aluminia was supplied by Panzhihua Iron and Steel Group. polypropylene glycol (PPG, Yantai Wanhua Polyurethanes Co., Ltd.) was dried for 12 h at 80 °C under vacuum to eliminate the inner moisture before use. 2,2-Bishydroxymethyl propionic acid(DMPA), which was purchased from Alfa Aesar, America was dehydrated at 80 °C under vacuum for 24 h. Toluene diisocyanate (TDI), stearic acid(SA), dibutyltin dilaurate(DBTDL), trimethylamine(TEA) and acetone were all of analytical grade.

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2.2 Preparation of CaCO₃@TiO₂ Particles

Firstly, 60 g of CaO was put in distilled water to form 10%(mass fraction) Ca(OH)₂ slurry. Then, a certain amount of commercial TiO₂ powder was added to the above Ca(OH)₂ slurry in a vessel, and homogenized by ultrasonic vibration for 30 min. The carbonization reaction monitored by pH value of the slurry was carried out under 40 °C in water bath. The gas mixture(CO₂/N₂, volume ratio 1:2) was bubbled into the suspension through a quartz tube at a flow rate of 1 L/min until the pH value of the slurry reached 7. The precipitates were separated from the liquor by filtration and washed five times with distilled water, then dried at 120 °C for 12 h in an oven.

2.3 Surface Modification of CaCO₃@TiO₂ Particles

Firstly, 8 g of CaCO₃@TiO₂ particles were dispersed in water with mechanical stirring at 90 °C. Then, 0.2 g of SA and 0.014 g of NaOH dissolved in 10 mL of ethanol were added to the above-mentioned solution under continuous stirring. The final products(SA-CaCO₃@TiO₂) were obtained by filtration, washed and dried at 120 °C for 24 h.

2.4 Synthesis of WPU/ CaCO₃@ TiO₂ Composites Films

A 500 mL round-bottom, 4-necked glass flask with a mechanical stirrer, a nitrogen inlet and a condenser was used as the reactor for the preparation of WPU/CaCO₃@TiO₂ composites. The synthesis procedures of the composite are shown as follows: 20 mL of acetone mixed with 0.73 g of CaCO₃@TiO₂ particles were added to 22.2 g of PPG in the flask, which was kept at room temperature for 10 min under stirring. Excess TDI was charged into the flask, and the suspension was heated at 70 °C for 2 h. Then certain amounts of DMPA and DBTDL were added and the mixture was heated at 60 °C for another 2 h. During the above process, extra acetone was used to adjust the viscosity of the WPU prepolymers. When the reaction mixture was cooled to 40 °C, TEA was added and agitated for 30 min to neutralize the carboxylic groups of DMPA. Finally, an aqueous emulsion was obtained by adding 120 mL of distilled water to the mixture with vigorous stirring. The WPU/CaCO₃@TiO₂ composites film was prepared by casting the emulsion onto Teflon mold under heating in a vacuum oven at 60 °C for 24 h. The process is shown in Scheme 1.



 $Scheme \ 1 \quad Flow chart \ of \ the \ preparation \ of \ WPU/CaCO_3 @TiO_2 \ composites$

2.5 Characterization and Property Measurements

Fourier transform infrared(FTIR) spectra of CaCO₃@TiO₂ particles and WPU/CaCO₃@TiO₂ composites were identified in the wavenumber range of 4000—400 cm⁻¹ at a resolution of 4 cm⁻¹ using a JIR-5500(JEOL) spectrophotometer at room temperature. UV-visible transmission spectra of particles were obtained on a UV-2550(Shimadzu) UV-visible spectrometer. X-ray powder diffraction(XRD) data of CaCO₃@TiO₂ particles and composites films were collected on a Rigaku2400 X-ray diffractometer(Cu $K\alpha$ radiation, λ =0.15418 nm). Thermogra-

vimetric analysis(TGA) was carried out on a DTG-60H (Shimadzu) analyzer at a heating rate of 20 °C/min under nitrogen atmosphere. Scanning electron microscope(SEM, XL30 ESEMFEG) was used to observe the dispersion of Ca-CO₃@TiO₂ powders in WPU films. Mechanical properties of the casting films were measured at 25 °C by a universal mechanical testing machine(Shimadzu AGS-J) in accordance with GB1040-79 at a crosshead speed of 50 mm/min. For each data point, five specimens were tested and the average value was reported. Water swelling values of the hybrid films were collected as follows: pre-weighed dry samples(20 mm×20 mm) were totally immersed in distilled water at 25 °C for 12 h. Water swelling was expressed as the mass percentage of water in the swollen sample and calculated by the following equation:

Swelling(%) =[$(m_2-m_1)/m_1$]×100% (1) where m_1 and m_2 are the mass of the original dry sample and the swollen sample, respectively.

3 Results and Discussion

3.1 Morphology Characterization

Fig.1 shows the SEM images of the CaCO₃(prepared under the same conditions as CaCO₃@TiO₂), commercial TiO₂, CaCO₃@TiO₂ and the fractured surface of WPU/CaCO₃@TiO₂ composites films. From Fig.1(A) we can observe that the CaCO₃ particle is spindle-shaped, and its diameter and length are about 200 and 600 nm, respectively. Fig.1(B) shows that commercial TiO₂ particle was spherical with an average diameter of about 200 nm. As shown in Fig.1(C), the as-synthesized core-shell structured CaCO₃@TiO₂ particles are also spindle-shaped, but the size become bigger and the particles' surface grow coarser after being coated by TiO₂

nano-sheets. In addition, no extra TiO2 particles can be observed, indicating that the commercial TiO₂ particles were converted into slice layer on CaCO₃ particles surface, attributed to the disaggregation of original TiO2 particles under alkaline conditions during mechanical stirring. The combination of CaCO₃ and TiO₂ particles was chiefly physical adsorption of electrostatic attraction^[18]. In Fig.1(D), the fractured section of pristine WPU showed a smooth surface, different from that of the WPU/CaCO₃@TiO₂ composites films. In Fig.1(E), the particles aggregates obviously because of their high surface energy and low surface reactive capacity. In contrast, a homogeneous distribution of SA-CaCO₃@TiO₂ in the WPU matrix is observed without large aggregates or agglomeration[Fig.1(F)], which demonstrates that the particles were well adhered to the WPU matrix. Therefore, the adhesion between the particles and WPU matrix became better due to the active surface originated from the treatment by SA^[21]. Such a good distribution of the additives in the WPU matrix could play an important role in improving the thermal and mechanical properties of the resulting composite films^[15].



Fig.1 SEM images of CaCO₃(A), commercial TiO₂(B), CaCO₃@TiO₂(C), pure WPU(D), WPU/CaCO₃@TiO₂(E) and WPU/SA-CaCO₃@TiO₂(F)

3.2 XRD Analysis

Fig.2 shows the XRD patterns of the $CaCO_3$, TiO_2 , $CaCO_3@TiO_2$ particles, WPU and WPU/CaCO_3@TiO_2 composites. The diffraction peaks of pure calcite phase $CaCO_3$



[Fig.2(A) pattern *a*, JCPDS No. 47-1743] is presented in the patterns of those samples expect TiO₂ and WPU. And the diffraction peaks of TiO₂ correspond with those of the rutile phase^[19][Fig.2(A) pattern *b*, JCPDS No. 4-0551]. From Fig.2 pattern *c*, it can be seen clearly that this composites is



Fig.2 XRD patterns of CaCO₃(*a*), TiO₂(*b*), CaCO₃@TiO₂(*c*)(A) and pure WPU(*a*), WPU/CaCO₃@TiO₂(*b*) and WPU/SA-CaCO₃@TiO₂(*c*)(B)

composed of CaCO₃ and TiO₂. As shown in Fig.2(B), the XRD pattern indicates that the pure WPU is amorphous, and the WPU/CaCO₃@TiO₂ or WPU/SA-CaCO₃@TiO₂ has similar diffraction peaks, which proves that there is no change on the structure of WPU matrix by the addition of particles. However, there is a weak peak at around 2θ of 44° corresponding to the characteristic peaks of CaCO₃, which proves that the particles has successfully embedded into the WPU solid films.

3.3 FTIR Analysis

Fig.3(A) shows the FTIR spectra of CaCO₃@TiO₂, CaCO₃@TiO₂ modified by SA and the pure SA, respectively. In Fig.3(A) spectrum *b*, new absorption bands belonged to SA is presented at 2920 and 2860 cm⁻¹(stretching vibration of the —CH₂)^[20], which suggests that SA molecular has grafted on the surface of CaCO₃@TiO₂ successfully, although the powder sample was extracted by alcohol several times. Fig.3(B) shows the representative FTIR spectra of WPU, WPU/CaCO₃@TiO₂ and WPU/SA-CaCO₃@TiO₂, respectively. All the samples exhibited the characteristic peaks of WPU^[2,5,7], proving that the main structure of the WPU/CaCO₃@TiO₂ composites remains the same as that of the pure WPU.



4000 3500 3000 2500 2000 1500 1000 500 $\tilde{\nu}/cm^{-1}$

Fig.3 FTIR spectra of CaCO₃@TiO₂(*a*), SA-CaCO₃@TiO₂(*b*), SA(*c*)(A) and pure WPU(*a*), WPU/CaCO₃@TiO₂(*b*) and WPU/SA-CaCO₃@TiO₂(*c*)(B)

3.4 UV-visible Diffuse Reflectance Spectra Analysis

From Fig.4, it is found that the UV-Vis diffuse reflectance spectra(DRS) of both commercial TiO_2 and $CaCO_3@TiO_2$ present the absorption regions from 200 nm to 400 nm, but the intensity of $CaCO_3@TiO_2$ composite decreases because $CaCO_3$ as the template of TiO_2 layers has no contribution on UV absorption. However, such materials with perfect UV absorption

ability can also prevent the light degradation of polymer films^[19].



Fig.4 UV-Vis diffuse reflectance spectra of commercial TiO₂(*a*) and CaCO₃@TiO₂(*b*)

3.5 Thermal Properties

Fig.5 exhibits the thermal decomposition behaviors of the pure WPU and WPU/CaCO3@TiO2 composites under a nitrogen atmosphere. Two stages of decomposition appear at the TGA curves of all samples. The first mass loss step is the decomposition of the soft segment of WPU and the second stage is of the hard segment of WPU^[4,20]. In Fig.5 curve b, the decomposition temperature of the hard segment increases by 11 °C due to the incorporation of unmodified particles, but it has no effect on the decomposition stage of soft segment. While the adding of SA-CaCO₃@TiO₂ altered the decomposition temperature remarkably, the decomposition temperature of hard segment is changed from 264 °C of pure WPU to 296 °C. It could be explained that the formation of the physical crosslinking between the particles and WPU matrix could limite the movement of the WPU chains due to the good dispersion of the particles in the WPU matrix.



Fig.5 TGA curves of pure WPUWPU(*a*), WPU/CaCO₃@ TiO₂(*b*) and WPU/SA-CaCO₃@TiO₂(*c*)

3.6 Tensile Properties

The stress-strain curves of WPU/CaCO₃@TiO₂ composites are shown in Fig.6. It is found that pure WPU displays a nonlinear elastic behavior and possesses a low tensile strength of 4.5 MPa and a high elongation at break of 1659% because of its amorphous nature. The tensile strength of WPU/ CaCO₃@TiO₂ composites increases to 6.67 MPa, while that of WPU/SA-CaCO₃@TiO₂ composites increases to 7.98 MPa. The introduction of CaCO₃@TiO₂ particles also improves the tensile modulus of the composites due to the enhancement of the interfacial interaction between particles and WPU^[21]. But the elongation at break of the WPU/SA-CaCO₃@TiO₂ decreases to 813%. This is primarily because of the enhance of interfacial strength between WPU matrix and particles from possible physical cross-linking effect^[5—9].



3.7 Water Resistance

In Table 1, the water swelling of WPU/CaCO₃@TiO₂ composites film is lower than that of pure WPU(from 68.65% to 26.24%), and for WPU/SA-CaCO₃/TiO₂ composites film, it decreases to 13.11%. One possible reason is that the chain densification of WPU is improved by the addition of particles^[4], the other reason may be that a mesh structure is formed between the additives and WPU matrix which prevents the water entrance^[17]. The water resistance of the composites films was modified remarkably, which indicates that such materials could be applied as functional films in the coatings and textiles fields.

Table 1 Water swelling behavior of WPU/CaCO₃@TiO₂ composites

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Sample	m_1/g	m_2/g	Water swelling(%)
WPU	0.0992	0.1673	68.65
WPU/CaCO3@TiO2	0.1246	0.1573	26.24
WPU/SA-CaCO ₃ @TiO ₂	0.1289	0.1458	13.11

4 Conclusions

In this work, $CaCO_3@TiO_2$ particles have been successfully prepared by a facile carbonation method. The results of SEM demonstrated that the CaCO₃ particles were

coated by TiO₂ nano-sheets, and the CaCO₃@TiO₂ presented specific characters of both CaCO₃ and TiO₂. While the composite tended to aggregate together since the CaCO₃@TiO₂ had large specific surface and high surface tension. SEM images proved that the CaCO₃@TiO₂ modified by SA had a good dispersion in WPU. The thermal stability and mechanical properties could be effectively improved by the addition of SA-CaCO₃@TiO₂ into WPU matrix, which means this novel materials may be applied in coatings and textiles fields.

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