**ORIGINAL PAPER**



# **Recovery of gold ions from wastewater using a three‑compartment electrodialysis separation system**

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## **Abstract**

Gold can be extracted from gold plating baths, printed circuit boards, and goldsmithing wastes by sodium hypochlorite leaching. However, the leach liquor should be purifed to remove other metallic ions and recover the gold from the mixture. While most metals form cations in solutions, gold occurs in anionic complexes. This property makes it possible to separate gold from other ions by the electrodialysis method. In this research, a three-compartment batch electrodialysis setup consisting of an anion-exchange membrane and a cation-exchange membrane is developed on a laboratory scale for this purpose. The impact of three parameters, namely applied voltage, Au concentration in the feed solution, and fow rate, is investigated in gold recovery using the response surface methodology. The results indicate that voltage has the highest and Au concentration in the feed solution has the lowest impact on gold recovery by electrodialysis. The optimal condition to achieve the highest percentage of Au recovery (95%) was found to be a voltage of 32.51 V, 4.1 ppm gold concentration in the feed solution, and a fow rate of 0.32 L/min. Electrodialysis ofers an innovative, environmentally friendly route for gold recovery and helps to reduce the loss of valuable metal ions.

**Keywords** Gold · Electrodialysis · Membrane · Response surface methodology · Recycling

# **Introduction**

Gold-coated particles are widely used in various industries due to their excellent electrical and thermal conductivity, coupled with high corrosion resistance (Habashi [2005](#page-10-0)). Electrochemically deposited gold particles have numerous functions in diferent areas, such as the electronics industry (to produce connectors, printed circuit boards and etc.), the aerospace industry, dentistry, decorative purposes, and jewelry (Lambrechts and Lall [2021](#page-10-1); SI et al. [2020\)](#page-10-2). The electroplating process is considered one of the main methods of Au-coating gold particles, while cyanide-based gold reagents are the most common electrolytes (Shacham-Diamand et al. [2015](#page-11-0)). Given the considerable economic value

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 $\boxtimes$  S. Ghassa Sina.ghassa@ut.ac.ir of gold, the metal-fnishing industry uses almost every gram of gold in the plating bath to avoid waste (Hannapel and Richter [2004](#page-10-3)). During the plating process, using an insuffcient amount of solution or low discharge of the plating solutions into the plating bath may lead to a signifcant loss of metal ions (Meng et al. [2020\)](#page-10-4). Even if great care is taken to make optimal use of gold in the plating bath, the bath may reach a point where it loses its initial ability to produce the desired deposits (Van Grieken et al. [2005\)](#page-11-1). In such cases, the efficiency of the bath decreases and, eventually, it must be discarded. In the wastewater, which contains 6 to 8% of the total initial gold, Au occurs in the form of  $[Au(CN)<sub>2</sub>]<sup>-</sup>$  and [Au  $(CN)_4$ ]<sup>-</sup> complexes (Wilkinson [1986](#page-11-2)); where [Au  $(CN)_2$ <sup>-</sup> is the more common ion in electrodeposition (Reid [1973\)](#page-11-3). Removing plating solutions from the process leads to signifcant fnancial loss, especially when using precious metals (Heights [1983](#page-10-5)).

Formation of a layer of gold in the gold plating tanks and cables is a common phenomenon. Removing this layer is essential to avoid decreasing the process efficiency and increasing gold consumption. The gold layer can be removed with cyanide or hypochlorite/chloride-based reagents. When CN− is used for gold plating washing, wastewater containing



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signifcant concentrations of gold-cyanide complexes is generated (Johnson [2015\)](#page-10-6). Treating this wastewater is necessary not only to recycle the Au, but also to remove its toxic cyanide content (Van Grieken et al. [2005\)](#page-11-1). However, using conventional oxidation technologies for cyanide degradation is extremely difficult due to the high stability of these complexes (Sousa et al. [2021](#page-11-4)). Hypochlorite/chloride-based reagents are suitable alternatives for gold dissolution. The gold makes a stable complex with Cl based on Eq. [1](#page-1-0).

$$
4Au + 16NaOCl + 12HCl \rightarrow 4NaAuCl_4 + 12NaCl + 6H_2O + 5O_2
$$
  
(1)

The wastewaters from the washing of gold plating baths contain a mixture of Au and other metals. Recycling gold from this wastewater is important from economic and environmental points of view. The separation of Au ions from other metallic ions is important to recycle gold. Membranes can be employed for gold ions separation in hypochlorite/ chloride-based solutions. Membranes have been used to separate ions from solutions and to purify water for decades (Han et al. [2019](#page-10-7)). However, they are known to be inefective in dealing with metallic ions due to membrane fouling and the metal precipitations formed on the membrane surface (Wang et al. [2019](#page-11-5)). Extensive research has been carried out to solve this problem, resulting in methods such as chemical modifcation of membrane surfaces and synthesis of new membranes (Bazrgar Bajestani et al. [2020;](#page-10-8) Mubita et al. [2020](#page-10-9)).

Electrodialysis (ED), a relatively new method introduced by (Chaudhary et al.  $2000$ ), increases the separation efficiency of membranes and mitigates their disadvantages. In this electrochemical membrane separation technique, an external electric feld is applied as a driving force for ions to transfer through selective ion-exchange membranes from one solution to another (Song and Zhao [2018\)](#page-11-6). Although the main target of the ED process is water desalination, it is also regarded as a highly promising technology in hydrometallurgical processes and may be implemented to remove ions from solutions (Gmar and Chagnes [2019\)](#page-10-11). Another application of ED is in the enrichment of ions in cathodic or anodic solutions based on the charge of the available ions in the solutions and the depletion of ions in the feed solution (Golubenko and Yaroslavtsev [2020](#page-10-12)). In other words, ED is an efficient method of separating ions from wastewater and metallurgical leach liquors.

ED has several advantages over conventional activated carbon extraction methods and selective precipitation, such as minimal energy expenditure (Chan et al. [2022\)](#page-10-13), low waste rejection (Generous et al. [2021](#page-10-14)), and high modularity (Seyedhakimi et al. [2018](#page-11-7)). This method is economical and environmentally friendly because additional reagents are not required in the ED process, which will lower the severe environmental impacts and decrease operational costs



(Kavitha et al. [2022](#page-10-15); Vineyard et al. [2020](#page-11-8)). Moreover, since the system's primary operational cost is electricity usage, the process would be favorable in countries using low-price industrial electricity like Iran, Qatar, Russia, and Kyrgyzstan (Tonner and Tonner [2004](#page-11-9)). Consequently, it can be used to concentrate and purify metallic solutions (Affah et al. [2018\)](#page-10-16). However, ED is associated with a number of limitations, including limited selectivity in solutions containing a variety of metallic ions with similar valences (Zafari et al. [2022\)](#page-11-10). Few papers have addressed electromembrane techniques or attempted to identify factors that infuence the separation of ions from multi-metallic mixtures (Babilas and Dydo [2018](#page-10-17)).

<span id="page-1-0"></span>In the present study, we investigate the possibility of recovering gold from solutions with a 3-compartment ED cell with the goal of minimizing the loss of gold and reducing waste generation through a technically and economically feasible process. The central objective of this study is to develop an electrochemical method of recovering gold from electroplating baths. We investigate the effects of three parameters including applied voltage (25 to 35 V), gold concentration in the feed solution (2 to 5 ppm) and circulating solution flow rate (0.24 to 0.48 L/min) on the recovery of gold from hypochlorite solutions by ED. The results of this research can be used to improve processes of separating and recycling gold ions from wastewater. The low investment cost and remarkable safety of ED make it an ideal technique, both in small- and large-scale plants. This manuscript's results are also important from an environmental point of view. The current manuscript investigates gold recycling to avoid Au release in nature. Releasing heavy metals (like Au) in the environment can cause severe environmental impacts and afect human and animal health.

# **Materials and methods**

## **Leach liquor solution preparation**

In order to synthesize the gold plating wastewater, the leach liquor was prepared by dissolving high-purity metallic gold in a leaching reagent containing 2% sodium hypochlorite, 1% hydrochloric acid and 1 g/L sodium chloride (Merck-Germany). The initial rate of gold dissolution was extremely rapid. Nearly, 90% of the gold was dissolved in only 30 min, according to reaction [1](#page-1-0) (Yen and Pindred [1989](#page-11-11)).

The leaching experiment was carried out in a 500-mL fask, installed inside a temperature-controlled water bath (IKA, Germany), raising the leach solution temperature to about 55 °C with an agitation rate of 500 rpm. The obtained 300 mL leach liquor with a gold concentration of 365 ppm was used for all ED experiments after dilution. The gold content of solutions was determined with atomic absorption spectroscopy (AAS, Varian 220, Australia).

# **Electrodialysis cell**

A three-compartment ED cell was developed and made to carry out the gold separation experiments. The cell diameters were  $7.5 \times 16 \times 9$  cm<sup>3</sup>, as shown in Fig. [1a](#page-2-0). The dimensions of the cathodic and anodic solutions compartment were  $5 \times 12 \times 1$  cm<sup>3</sup>, and the feed solution compartment volume was  $60 \text{ cm}^3$ .

The cathodic and anodic solutions were separated from the feed solution by the cathodic and anodic solid membranes (Fig. [1b](#page-2-0)). The solid cation and anion exchange membranes were Ionsep-AM-C and Ionsep-AM-A models, respectively (Ionsep, Zhejiang, China). These membranes were selected due to their high permselectivity, low electric resistance, broad pH range resistance and high mechanical strength (Table [1\)](#page-2-1). The mixed metal oxide (MMO)-coated titanium plates (DSA® plate electrode, Ionsep, China) with a surface area of  $5 \times 12$  cm<sup>2</sup> were used as electrodes. The distance between the electrodes and their membrane was 1 cm. As shown in Fig. [1c](#page-2-0), the spaces between the membranes (the deionized and the concentrated flow paths) were flled with inert (electrically non-conducting) net-like spacers, which mainly provided the stack with mechanical support and specifed the geometry of the fow channel between the membranes. These spacers made of low-density polypropylene were placed between the membranes in the membrane stack to create independent flow branches. Using plate flow spacers increases the fluid flow, which can decrease the processing time. Another function of the spacer net is to make a turbulent fow in the solution. The solution fowing through the net-flled channel follows the so-called zig-zag flow, leading to increased mass transfer toward the membrane surface. Therefore, concentration polarization phenomena that might occur in the difusion layer at the membrane surface were minimized since the fuid undergoes irregular fuctuations or mixing, in contrast to laminar fow, in which the fuid moves in smooth paths or layers. In addition, the precipitation of fne particles and ions can block the



<span id="page-2-0"></span>**Fig. 1** The three-compartment ED cell was used for separation tests; **a** ED cell, **b** cell parts, **c** spacer

Thickness	Water content	Ion exchange capacity	Burst strength	Water permeating	Diffusion coefficient	Permselectivity	Electric resistance
(mm)	$(\%)$	(mol/kg)	(Mpa)	(min)	(cm <sup>2</sup> h mol/L)	$(\%)$	$(\Omega$ cm <sup>2</sup> )
Cation exchange membrane							
0.4	< 40	>2.5	0.6	>125	< 2.6	> 96	< 6
Anion exchange membrane							
0.4	<30	> 2.1	0.6	>120	< 0.4	> 97	< 6

<span id="page-2-1"></span>**Table 1** Specifcations of the ion-exchange membranes



flow passes in the membrane surface. Using spacers reduces the blocking of fow passes (Tanaka [2015](#page-11-12)).

The solid membranes were soaked in water for 24 h before cell assembly. This action prevents the membranes from deforming, caused by its expansion after contact with the solution inside the cell. The direct electric current was supplied to the plane electrodes with a DC power supply (Tetaelectronic PS1203, Iran). Voltage was measured by a digital voltmeter. Semi-transparent silicone connection hoses and 4 containers were used for transmission and storing solutions. One-way pump and fow control valves were also used to circulate and control the cell fow rate.

## **Gold recovery experiments**

The effect of three different parameters, including applied voltage, feed solution concentration and circulating solutions flow rate, were investigated on gold recovery. These factors were chosen because they are technically controllable on laboratory and industrial scales. The central composite design (CCD) method combined with response surface methodology (RSM) was employed to study the efect of the three mentioned parameters and statistical modeling of results. The response surface methodology is an optimization method determining the relationship between several variables with one or several response variables. CCD investigates the efect of parameters in 5 levels, including two factorial points (high level and low level), two axial points (plus and minus the alpha) and one central point (center of low and high levels) (Sina et al. [2022\)](#page-11-13). The high and low levels for gold concentration in feed solution were 2 and 5 ppm, as actual values of the plating process wastewater effluents for voltage were 25 and 35 V and for flow rate were 0.24 and 0.48 L/min. The studied voltage and flow rate ranges were selected based on preliminary experiment results and previous studies (Kang et al. [2017;](#page-10-18) Korolev et al. [2018](#page-10-19)). The center point experiment was repeated 6 times to study the experiment's repeatability and calculation of errors. The detailed experimental conditions are listed in Table [2.](#page-3-0)

1 L of the solution was fed into the cell compartments after preparing the feed solution by diluting the gold leach liquor to operate the experiments. The solution flow rate in the ED system for each experiment was adjusted based on the specifc values in the design of the experiments. The specifed voltage was applied after adjusting the fow rate, which is the beginning of the process. ED tests were continued for 4 h. The approximate time of experiments was selected based on preliminary experiments. The gold ionfree leaching solution was circulated as an electrolyte at the rear part of the cell, with the previously mentioned volume, to decrease the cell temperature. During this process, the solutions were constantly circulated inside the device

<span id="page-3-0"></span>

Anodic solution De-ionized solution cathodic solution



<span id="page-3-1"></span>**Fig. 2** The ions fow paths in an ED cell

(shown in Fig. [2\)](#page-3-1) and passed through the desired membranes under the applied voltage.

The feed solution exchanged some of its ionic content in each cycle inside the cell in a batch process; therefore, the anodic and cathodic solutions get rich in ions. At the end of the process, when the feed solution attained a defnite value, the solution was withdrawn from the cathode compartment and gold concentration was measured with atomic absorption spectroscopy (AAS). The results showed that the change

in the volume of working solutions during the ED process was negligible. Also, the pH value of each compartment and current intensity changes was measured regularly during the experiments.

The gold recovery efficiency is calculated based on Eq. [2](#page-4-0):

$$
R = \frac{C}{C_0} \times 100\tag{2}
$$

where *C* denotes the metal concentration (in g/l) in the cathode compartment, and  $C_0$  represents the feed solution's metal concentration (in g/l).

# **Results and discussion**

## **Statistical modeling and process optimization**

Electrodialysis is a membrane method to separate the ions in the aqueous environment. By using this method, selected ions (Au in our research) will migrate to the cathodic chamber, and a pure solution with a high concentration of gold ions (in the form of  $[AuCl_4]$ <sup>-</sup> complexes) will be provided. This solution can then be used to produce pure gold with metal production methods, such as electrowinning or cementation.

Statistical analysis is an efficient technique to study parameters' efects and interactions. In addition, it can be used to predict a response based on investigated factors. Among statistical analysis methods, analysis of variance (ANOVA) is a robust tool for predicting a response based on independent variables. Design expert 7 (DX7) was employed for the statistical modeling of the obtained data. The following second-order polynomial (quadratic) equation was proposed based on ANOVA for predicting the gold recovery based on the investigated parameters and their interactions:

$$
R_{Au} = -566.97 + 31.65A + 51.84B + 408.45C
$$
  
- 0.37AB + 3.02AC - 11.46BC (3)  
- 0.49A<sup>2</sup> - 4.71B<sup>2</sup> - 723.13C<sup>2</sup>

where  $R_{Au}$  is a gold recovery  $(\%)$ , *A* is voltage (V), *B* is feed concentration (ppm), and *C* is fowrate (L/min). The statistical indexes for the model are listed in Table [3.](#page-4-1) With a *p* value lower than 0.05, the model was signifcant. The *p* value shows that there is only a 3.69% chance that the model occurs due to noise. Adequate precision is a statistical index that shows the ratio of the efect of investigated parameters (signal) to not-investigated parameters (noise) (Rezaei et al. [2022\)](#page-11-14). The model's adequate precision is 5.39, which shows that the selected parameters were highly effective in the process.

<span id="page-4-1"></span>**Table 3** The ANOVA for gold concentration (A: voltage (V), B: feed concentration (ppm), C: fowrate (L/min))

<span id="page-4-0"></span>

	Sum of squares	Mean square	$F$ -value	<i>p</i> value
Model	6816.16	757.35	3.34	0.0369
A	1064.81	1064.81	4.70	0.0554
B	381.98	381.98	1.68	0.2235
$\mathsf{C}$	748.29	748.29	3.30	0.0993
AB	63.28	63.28	0.28	0.6088
AC	26.28	26.28	0.12	0.7406
BC	34.03	34.03	0.15	0.7066
$A^2$	2200.78	2200.78	9.71	0.0110
B <sup>2</sup>	1616.17	1616.17	7.13	0.0235
$C^2$	1562.66	1562.66	6.89	0.0254
Residual	2267.54	226.75	434.37	< 0.0001

As mentioned, a test at the center points was repeated six times (Table [1\)](#page-2-1) to study the repeatability and calculate the standard error. The population standard deviation for gold recoveries in repeated tests was 1.28%. The low quantity of standard deviation shows a high degree of experiment repeatability (Rafee et al. [2021](#page-10-20)). The sample standard deviation was divided by the sample size's square root (number of repeating tests) to calculate the standard error. The standard error of 0.52% also shows the high repeatability of experiments.

The optimal condition for the highest gold recovery was obtained at voltage 32.51 V, gold concentration of 4.1 ppm and flow rate of 0.32 L/min. This condition was suggested by Design Expert 7 software based on Eq. [3](#page-4-2). According to the software calculations, the gold recovery reaches 96% at optimal conditions. A test was carried out at the optimal conditions to validate the optimization results. The validation experiment results showed that the gold recovery reached 94.9% at the actual test.

<span id="page-4-2"></span>The kinetics of gold (III) transportation from the feed solution and metal accumulation in the cathodic solution is shown in Fig. [3.](#page-5-0) More than 94.5% of gold (III) was transported from the feed solution at optimal condition into the cathodic solution within 4 h of ED separation. It has been found that without electric feld application, only 29% of gold (III) was transferred across the membrane from the feed solution.

## **Parameter's infuence**

The effect of each parameter was comprehensively investigated. The ANOVA was employed for this purpose. ANOVA is a method that is mainly used to determine the critical parameters afecting the response by analyzing the total variance of the appropriate components and measuring the efect between each of them. The *F*-ratio represents the mean



<span id="page-5-0"></span>



square error ratio to the residual error and is usually used to determine the efect of a parameter on the results. The higher the *F*-value, the greater the efect of that parameter. The lower the *p* value of a parameter, the greater the importance and impact of that parameter on the results (Ghassa et al.  $2021$ ). Therefore, in determining the recovery efficiency, the parameters such as applied electrical voltage, input current flow, and finally, the feed concentration were of operational importance, respectively.

The main reaction that takes place with the application of the electric current is the electrolysis of water during the ED process. Reactions for anode and cathode are shown in Eqs. [4](#page-5-1) and [5.](#page-5-2)

$$
2H_2O \to O_2(g) + 4H^+ + 4e^-(anode)
$$
 (4)

$$
4H_2O + 4e^- \rightarrow 2H_2(g) + 4OH^- (cathode)
$$
 (5)

As can be seen from Eqs.  $(2)$  $(2)$  and  $(3)$  $(3)$ , while anode reactions produce acid, cathode reactions produce a base. The pH change was related to the anode and cathode reactions and the ionic composition change in the solutions (as shown in Fig. [4\)](#page-5-3). A reasonable explanation for the increase of pH in the anodic solution could be the production of OH− ions in the cathode compartment. Also, the production of  $H^+$  ions in the anode compartment decreased the cathodic solution pH. The results showed that the process pH range does not affect membrane efficiency.

## **Voltage**

<span id="page-5-2"></span><span id="page-5-1"></span>The electrolyte solution continuously rotated in the vicinity of the electrodes to exchange the heat produced at the electrodes in the ED system. This solution does not contain valuable ions and has no role in the ion exchange process. However, the current fowing through the device was a function



<span id="page-5-3"></span>



of the voltage applied by the rectifer, and either of these two factors can be considered. Due to safety issues, the ED unit's operation at constant voltage (potentiostatic mode) was preferable to a constant current state (galvanostatic mode). During the ED process, the ions content and, consequently, the solution's electrical conductivity in the feed region decrease. As a result, the electrical resistance of the ED unit increased. In the case of the galvanostatic mode, this causes an uncontrollable increase in voltage applied to the ED unit and, in some cases, causes damage to the electrical current source. Besides, the membrane stack heats up in many cases due to the heat generated by the solution's resistance and impaired function. For the reasons mentioned above, the voltage was controlled by the rectifer to be constant during tests.

According to the ANOVA table (Table [3\)](#page-4-1), the voltage had the lowest *p* value (0.0554) and highest *F*-value (4.7). As a result, this parameter had the highest effect on gold recovery with the ED technique, which means that the electric feld represented the main driving force of the process. The applied electric feld induced migration movement of all ions dissolved in the process solutions and contained in the membranes so that the cations move toward the cathode, while the anions move toward the anode.

Figure [5](#page-6-0) demonstrates the effect of changes in the electric voltage in the operating range of 25 to 35 V (at a fow rate of 0.36 L/min and a feed concentration of 3.5 ppm) on gold recovery. As can be seen, by increasing the electric current above 32 V, the process efficiency decreases. The reason for this can be considered as the thermal flow created by this increase in electrical voltage in the electrodes and its transfer to the whole system, thus reducing the permeability

<span id="page-6-0"></span>**Fig. 5** The effect of voltage on gold recovery (at a fow rate of 0.36 L/min and a feed concen-

tration of 3.5 ppm)

performance of ion-exchange membranes (Sadyrbaeva [2012](#page-11-15); Tanaka [2015\)](#page-11-12). Figure [5](#page-6-0) clearly shows the importance of considering the heat fow generated in the electrodes of the ED system and shows the existence of a limitation in the use of the applied voltage in this system. It is always expected that due to the signifcant efect of the voltage on the ED process, increasing its value will improve the performance of the process, but increasing the voltage reduces the efficiency due to the efect on the system temperature as a harmful factor (Benneker et al. [2018\)](#page-10-22), which is consistent for all scales due to the effects on the electrolyte and membrane efficiency (Vizserálek et al. [2014](#page-11-16)).

The current density changes during the test with optimum conditions are shown in Fig. [6](#page-7-0). Regardless of the initial current (which depends on the applied voltage and, to some extent, the concentration of soluble ions), the general trend of changes in the passing current was decreasing. The current was reduced by passing of time due to an increase in the resistance of the medium resulting from the reduction in concentration of existing ions and increasing of the temperature of the solution (Strathmann [2010\)](#page-11-17).

#### **Gold concentration in the feed**

The metal concentration is a controllable parameter in the pilot and industrial scales. As the ANOVA table shows, with the highest *p* value (0.2235) and lowest *F*-value (1.68), the gold concentration in feed solution had the lowest efect among all investigated parameters. The effect of gold concentration in feed solution (at a flow rate of 0.36 L/min and a voltage of 30 V) is depicted in Fig. [7.](#page-7-1) The gold recovery





<span id="page-7-0"></span>



<span id="page-7-1"></span>Fig. 7 The effect of feed concentration on gold recovery (at a fow rate of 0.36 L/min and a voltage of 30 V)

increased by increasing in gold concentration from 2 to 3.5 ppm. The gold recovery was in direct relation with Au concentration in solution because the current intensity at a constant voltage increased by increasing the ions concentration. Therefore, higher current intensity stimulates the movement of ions and reduces the resistance of the device.

It should be noted that the gold concentration range in this research was selected based on the actual values from industrial plating process wastewater effluents that were between 2 and 5 ppm (Sadyrbaeva [2012](#page-11-15)). Although gold concentration has little effect in this range, it may significantly afect the process in the higher ranges. Generally, the ED system shows inefficiency in dealing with a high concentration of ions available in feed solution due to precipitations that may form on the membrane surface when a high voltage is applied. This could occur due to the small effective area of the membrane in the laboratory-scale ED cell, which limits the initial concentration of metal ions. The highest



amount of metallic ions in the feed solution reported in previous researches was around 450 ppm (Chan et al. [2022](#page-10-13)). However, the metal concentration in the current study was remarkably lower than the maximum capacity of the ED systems; therefore, this parameter has an insignificant effect on the process.

## **Flow rate**

The effect of feed flow rate changes on gold recovery (at a feed concentration of 3.5 ppm and a voltage of 30 V) is shown in Fig. [8](#page-8-0). As can be seen, by increasing the feed flow rate up to 0.32 L/min, the Au recovery increased. This occurred due to turbulence in the fow and reduced mass transfer boundary layer at the membrane surface. It reduced the thickness of the layer formed around the membrane, which increased the penetration of ions and, as a result, the efficiency of the process. On the other hand, the gold

<span id="page-8-0"></span>



recovery decreased at flow rates higher than the optimum condition due to the drop in the solution residence time on the membrane's efective surface. Furthermore, unspecifc flow geometry and consequently increment in the cell's electrical resistance as a consequence of high fow rate explain recovery decreases (Długołęcki et al. [2010\)](#page-10-23). Although increasing the flow rate increased the setup capacity, deterioration or rupture of the membrane surface could occur at high flow rates (Aytaç and Altın [2017\)](#page-10-24).

## **Experiment with gold plating bath wastewater**

The gold plating tanks and cables are covered by a layer of gold. This layer should be removed regularly to increase the plating process efficiency and avoid gold overuse. Cleaning gold plating baths with hypochlorite and chloride-based solutions is a standard method in the industry. An experiment was carried out with actual wastewater containing gold ions obtained from gold plating bath washing to evaluate the application of ED method on an industrial scale. The gold plating bath was washed with a reagent containing 2% sodium hypochlorite, 1% hydrochloric acid and 1 g/L sodium chloride. The wastewater was used to run an experiment at the optimum condition obtained from optimization tests (voltage =  $32.51$  V and a flow rate of 0.32 L/min). The metal concentration of the feed, cathodic, and anodic solution was measured after 3 h (Table [4\)](#page-8-1).

As it is concluded from Table [4](#page-8-1), the recovery of gold in the cathode compartment is approximately 91% which is 4% less than the gold recovery when using a pure gold solution. This decrease in recovery can be caused due to membrane fouling. Membrane fouling in almost all membrane processes is commonly caused by the precipitation of ions on the membrane surface or membrane pores. As can be seen in SEM images (Fig. [9](#page-9-0)), some particles were deposited on the surface of the anodic membrane. The energy-dispersive X-ray spectroscopy (EDS) indicated that deposited particles were made from iron. Despite its low concentration, iron is considered to be one of the most common inorganic pollutants that generate oxides and hydroxides, causing membrane fouling (Melliti et al. [2022](#page-10-25), [2019\)](#page-10-26). The X-ray difraction analysis confrms the presence of iron oxide on the membrane surface in the form of goethite (Fig. [10](#page-9-1)).

<span id="page-8-1"></span>**Table 4** The chemical analysis of the plating bath waste stream before and after ED separation

Components	Au	Fe	€u	Ni
The initial concentration of metals in the feeding compartment	4.31	3.4	241	139
The final concentration of metals in the feeding compartment	$201$ ppb	$3.3$ ppm	Negligible	$104$ ppb
The final concentration of metals in the cathode compartment	$3.92$ ppm	negligible	Negligible	Negligible
The final concentration of metals in the anode compartment	97 ppb	Negligible	$218$ ppb	Negligible



<span id="page-9-0"></span>



<span id="page-9-1"></span>





# **Conclusion**

In this research, a three-compartment electrodialysis (ED) cell was used for gold recovery from hypochlorite liquors. The effect of three different parameters, including the applied voltage, gold concentration in solution and fow rate, were investigated in gold recovery. The gold was efectively recovered during the potentiostatic mode in an optimum condition, including voltage 32.51 V, the gold concentration of 4.1 ppm and a flow rate of 0.32 L/ min. The results indicated that voltage had the highest impact on gold recovery, while the Au concentration in feed solution had the most negligible impact. The gold extraction percent of 95% was achieved during 3 h, representing the electromembrane process used in this research as an appropriate technique for recovering and purifying the remaining gold in waste plating bath reagent. A test also was carried out with wastewater obtained from washing gold plating bath with hypochlorite and chloride-based



solutions, at optimum conditions. The results indicated that this method could also be used to efficiently separate ions from industrial wastewater.

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**Availability of data and materials** Not applicable.

**Code availability** Not applicable.

## **Declarations**

**Conflict of interest** There are not any conficts of interest.

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