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Adsorptive removal of Congo red from aqueous phase using graphene–tin oxide composite as a novel adsorbent

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Abstract

The main focus of this work was to prepare graphene tin oxide composite as a novel adsorbent for the removal of hazardous anionic dye, Congo Red, from aqueous systems. The composite was prepared by a simple solvothermal method. The adsorbent was characterized via scanning electron microscopic analysis, energy-dispersive spectroscopy, X-ray difraction, Fourier transform infrared spectroscopy and thermogravimetric analysis. The energy-dispersive spectra of graphene tin oxide composite showed a high percentage of tin (62.11%) with a reduction in the percentage of carbon (47.45 to 13.75%) and oxygen (39.37 to 23.71%) suggesting that the composite has been successfully prepared. Fourier transform infrared spectroscopic analysis showed that the intensity of some absorption peaks like C=O, C=O and OH decreased which support the efective reduction in graphene oxide to graphene in the composite. Removal of Congo red by graphene tin oxide composite was carried out as a function of pH, dye initial concentration, contact time, temperature and adsorbent dose in batch mode. Optimum adsorption was observed in the pH range of 2 to 4 with contact time of 60 min. Langmuir and pseudo-second order kinetic model ftted very well the isotherm and kinetic data, respectively. The maximum uptake capacity determined by Langmuir model was observed to be 359.71 mg/g at 318 K. Thermodynamic investigations have shown endothermic and spontaneous nature of Congo red adsorption. Regeneration studies revealed that graphene tin oxide composite could be a viable and potential adsorbent for detoxifcation of dyes bearing wastewater.

Keywords Adsorption · Anionic azo dye · Isotherm models · Kinetic models · Wastewater

Introduction

Water plays a key role in the existence of living organism. Generally, the quantity and quality of water is of main concern around the world. Rapid urbanization, industrialization and population growth have caused a serious problem of water pollution (Madan et al. [2019;](#page-14-0) Bhat et al. [2020](#page-14-1)). Various types of toxic substances like pesticides, pharmaceutical residues, heavy metals, drugs and dyes are continuously discharging in water bodies like ocean, lakes and rivers (Basheer [2018](#page-14-2)). Presently, dyes constitute the most adulterating agents in the effluents from textiles, cosmetic, plastic, rubber, leather, paper and pharmaceutical industries.

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Over 0.7 million tons of dyes are produced annually worldwide and almost 12–15% dyes are lost mainly from textile and other dyeing industries which are discharged as effluents in various aqueous environments without any handling (Mahmood et al. [2018;](#page-14-3) Parvin et al. [2019](#page-15-0)). The dyes containing effluents lead to many ecological complications. Owing to their intense color and high biological oxygen demand (BOD), dyes bearing effluents decline the photosynthetic activities of various phytoplankton and decrease the required oxygen level of water which leads to oxygen deprivation of aquatic fauna and fora and results in sufocation (Deng et al. [2018](#page-14-4); Naushad et al. [2019a\)](#page-15-1). Dyes, particularly azo dyes due to their recalcitrant molecules are high stable, non-biodegradable and exist for longer time in environment. Congo Red (CR) is an anionic azo dye, present in effluent from textile and other industries. It is highly toxic, causes allergies, skin irritation and is considered as carcinogenic and mutagenic for human beings (Aliabadi and Mahmoodi [2018;](#page-14-5) Wekoye et al. [2020](#page-15-2)). Therefore, there has been an

increasing demand for efective removal of these dyes from water bodies to safeguard human life and the aquatic biota.

Several treatment methods such as precipitation, focculation/coagulation, electro-dialysis, nano-fltration, photochemical degradation, chemical oxidation, aerobic and anaerobic degradation have been applied for the removal of azo dyes from aqueous systems (Golmohammadi et al. [2019](#page-14-6); Naushad et al. [2019b](#page-15-3); Dbik et al. [2020](#page-14-7)). Most of these technologies are less efective, have high operation cost, time consuming, and may leads to the formation of some intermediate toxic products which limit their prevalent applications in poor nations (Sun et al. [2011](#page-15-4); Yang et al. [2018](#page-15-5)). But, adsorption due to its simplicity, efectiveness, low cost and ability to purify large quantity of dyes bearing wastewater without production of any harmful by-products is the most promising and frequently used method around the world (Bharath et al. [2017](#page-14-8); Deng et al. [2018\)](#page-14-4). Until now, a variety of materials like biomass, silica, polymer gels, organic and inorganic composites, clays, metal–organic framework (MOF) and carbon-based adsorbents have been tested for removal of toxic dye from water bodies (Mahmood et al. [2017;](#page-14-9) Tang et al. [2020\)](#page-15-6). Recently, numerous carbon skeleton materials like carbon nanotubes, fullerene and graphene exhibited very good removal efficiency for different organic pollutants.

Graphene oxide (GO), a derivative of graphene, has twodimensional sheet-like carbon structure containing many oxygen functional groups such as carboxyl, hydroxyl, epoxy and carbonyl groups on edges and surface of its lattice (Liu et al. [2019a\)](#page-14-10). The unique physical and chemical structural of GO make it to be highly dispersed in aqueous mediums which can facilitate its interactions with solute molecules via hydrogen bonding and electrostatic interactions and hence make it as a good adsorbent for dyes removal in pollution control applications (Jiao et al. [2016](#page-14-11)). However, GO sheets due to their high specifc surface area have the tendency to agglomerate in liquid phase which leads to a reduction in the number of active sites available for adsorption. This behavior of GO restricts its direct application for pollutants removal from aqueous solutions. To overcome the problem of agglomeration of GO nano-sheets in liquid medium and improve its efficiency for dyes removal, the most convenient strategy is to make composite of GO with diferent metal oxides, polymers and ionic liquids (Mohammadi et al. [2018](#page-14-12); Abbasi [2020](#page-13-0)).

In the present study, graphene and tin (IV) oxide composites $(G/SnO₂)$ were synthesized and its adsorption capacity was evaluated for the removal of toxic anionic diazo dye, CR from aqueous solutions. Detailed literature survey showed that $G/SnO₂$ composite has not been used for the adsorption of CR from synthetic wastewater. This study attempts to assess the impact of major process variables such as pH, dye initial concentration, contact time, temperature and

adsorbent dose on CR adsorption by $G/SnO₂$ composite. Additionally, the correlation between the dye uptake capacity and adsorption mechanism was evaluated with diferent isotherm and kinetic models by performing systematic equilibrium and kinetic studies.

The research work was carried out in environmental science and Material Chemistry Laboratory at National Center of Excellence in Physical Chemistry, University of Peshawar, Pakistan, Dated 12th June 2019 to 28th December 2019.

Materials and methods

Chemical and reagents

Analytical grade chemicals/reagents were used in the present study without further purifcation. Graphite powder, potassium permanganate (99.0%), HCl (37%), hydrogen peroxide (30%), NaOH (99.99%) and acetone (99.90%) were purchased from Scharlau, Spain. Anionic dye Congo red (95%) and Tin (II) chloride dehydrate (99.99%) was purchased from Sigma Aldrich, Germany. Fresh double distilled water (DDW) was used all over the experimental work. The various characteristics and structure of CR are given in Table [1.](#page-2-0) CR dye solutions of desired initial concentration were prepared by diluting its stock solution (1000 mg/L) with DDW.

Adsorbent preparation

Synthesis of GO

GO was synthesized via modifed Hummers method (Alam et al. [2017](#page-13-1)). First 2.0 g graphite powder was put in 100 mL of concentrated H_2SO_4 at 0 °C. Then, 8.0 g of KMnO₄ was added slowly with continuous stirring for 2 h below 10 °C. The temperature of the reaction mixture was then raised to 35 °C and further stirred at this temperature for 1 h. DDW was then added to the reaction mixture below 100 °C and again stirred for 1 h which is then followed by addition of 300 mL DDW. After this 20 mL H_2O_2 was added to the mixture for the reduction in residual $KMnO₄$ which turned yellow. The resulting graphene oxide sample was washed frst with 5% HCl solution and then with 1 L of DDW for removing the acid. The GO was then dried in an oven at 60 °C for 24 h.

Synthesis of G/SnO₂ composite

Graphene tin oxide composite $(G/SnO₂)$ was prepared by Solvothermal method (Wu et al. [2010](#page-15-7)). In a typical procedure 0.04 g of GO, prepared by modifed Hummers method, was dispersed in 20 mL ethanol through ultra-sonication process for 90 min to get solution A. Solution B was obtained by **Table 1** Important physical properties and structure of Cong Red

dissolving 0.25 g tin chloride dihydrate in 20 mL absolute ethanol. Solution A and B were mixed and shifted to autoclave and kept in the oven for 10 h at 160 °C. The autoclave was then allowed to cool down and the product obtained was washed several times through centrifugation process followed by drying at 60 °C to get $G/SnO₂$.

Adsorbent characterization

GO and $G/SnO₂$ composite was characterized by various physicochemical techniques. Morphological examinations were carried out using a JEOL, JSM-5910 scanning electron microscope (SEM) with 20 kV accelerating voltage and resolution of 3.0 nm. Elemental compositions were evaluated by energy-dispersive spectroscopic (EDS) micro-analyzer (EDX Inca-200, UK) coupled with SEM analyzer. XRD analysis was performed to observe the crystalline nature of GO and $G/SnO₂$ using X-ray difractometer (JEOL, model JDX-3532) with Mn filtered Cu-K α radiations. XRD patterns were taken in the range of 10°–80° (2*θ*) with step size of 0.04° and a step time of 0.5 s. The applied current and voltage were kept at 30 mA and 40 kV, respectively. The chemical structure and surface functional groups were analyzed using Fourier Transform Infrared (FTIR) spectrophotometer (FTIR-8201PC 2000, Shimadzu) in the range of 500–4000 cm−1. Prior to FTIR analysis GO and $G/SnO₂$ were mixed with KBr powder and the mixture was homogenized thoroughly. Thermal stability of GO and $G/SnO₂$ was evaluated in the temperature range of 20–1000 °C at a heating rate of 10 °C/min using Perkin-Elmer Pyris1 analyzer, model 6300. Point of zero charge (PZC) was determined via a well-defined drift method (Ali et al. [2019\)](#page-13-2).

Adsorption studies

Adsorption of CR by $G/SnO₂$ composite was carried out in batch mode by considering the impact of various processes variables such as solution pH, dye initial concentration, contact time, temperature and adsorbent dose. A fxed amount of adsorbent (0.1 g) was put in 40 mL of dye solution of desired concentration taken in a series of polythene bottles (100 mL capacity) and agitated in a shaker bath (SHEL LAB, WS 17-2, USA) at 120 rpm at defnite temperature for a desired time interval. The pH of dye solution was adjusted via 0.1 M HCl or/and NaOH solution using a pH meter (Neo Met, pH 250 L, Korea). At the end of saturation point the dye solutions were fltered and analyzed for the left over concentration of CR at the wavelength of 498 nm using Vernier SpectroVis® Plus (SVIS-PL) spectrophotometer. The adsorption capacity q_e (mg/g) and removal efficiency (%*R*) were determined from the following equations:

$$
q_e = \frac{V(C_o - C_e)}{m} \tag{1}
$$

$$
\%R = \frac{(C_o - C_e)}{C_o} \times 100\tag{2}
$$

where C_o and C_e are the dye concentrations (mg/L) in solution before and after adsorption, respectively, *V* is the volume (L) and *m* (g) is the mass of adsorbent.

Equilibrium isotherm study

Adsorption isotherm experiments were performed by contacting 40 mL of CR dye solutions (20–1000 mg/L) with 0.1 g of adsorbent which were taken in a series of 100-mL bottles with their pH adjusted at 3.0 and shaken at constant temperature (298, 308 and 318 K) in a shaker bath at 120 rpm until the point of equilibrium is achieved. After fltration, the concentration of the residual dye solutions was measured spectrophotometrically at the wavelength of maximum absorption (λ_{max} =498 nm). In the current study the experimentally obtained isotherm data were analyzed via Freundlich, Langmuir and Temkin models.

Freundlich isotherm equation is an empirical model for adsorption on heterogeneous surfaces which assumes multilayer, reversible and non-ideal adsorption due to nonuniform distribution of adsorption sites. The linear form of Freundlich isotherm equation can be represented (Freundlich [1907](#page-14-13); Al-Othman et al. [2012](#page-14-14)) as:

$$
\ln q_e = \ln K_{\rm F} + \frac{1}{n} \ln C_e \tag{3}
$$

where K_F (mg/g (L/mg)^{1/n}) is Freundlich constants correspond to adsorption capacity, while n is known as heterogeneity factor that shows the adsorption intensity.

Langmuir isotherm model is based on the assumption that all the binding positions on adsorbent surface are fxed and homogeneous which leads to monolayer adsorption. The mathematical linear form of Langmuir isotherm equation is written (Langmuir [1916](#page-14-15)) as:

$$
\frac{C_e}{q_e} = \frac{1}{K_{\text{L}}q_m} + \frac{C_e}{q_m} \tag{4}
$$

where q_e and q_m refer to the amount of CR adsorbed per unit mass of adsorbent and monolayer adsorption capacity (mg/g), respectively, while K_L (L/mg) denotes the binding energy constant.

The favorability of Langmuir isotherm model for CR adsorption onto $G/SnO₂$ was further investigated by a dimensionless equilibrium parameter, named as separation factor (R_L) which can be expressed as follows as:

$$
R_{\rm L} = \frac{1}{1 + K_{\rm L} C_o} \tag{5}
$$

where C_o (mg/L) and K_L are the dye initial concentration and the Langmuir binding energy constant, respectively. In case, $0 < R_L < 1$ shows favorable adsorption, $R_L > 1$ unfavorable, $R_{\text{L}}=1$ linear and $R_{\text{L}}=0$ indicate irreversible adsorption process (Weber and Chakravorti [1974\)](#page-15-8).

Temkin isotherm model proposes that for all molecules adsorption energy decreases linearly with surface coverage due to adsorbate–adsorbent interactions. The general form

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of this isotherm model can be written (Temkin and Pyzhev [1940](#page-15-9)) as:

$$
q_e = \frac{RT}{b_{\rm T}} \ln K_{\rm T} C_e \tag{6}
$$

$$
q_e = \frac{RT}{b_{\rm T}} \ln K_{\rm T} + \frac{RT}{b_{\rm T}} \ln C_e \tag{7}
$$

$$
q_e = B_\text{T} \ln K_\text{T} + B_\text{T} \ln C_e \tag{8}
$$

where $T(K)$ is absolute temperature, $R(8.314 \text{ J mol}^{-1} \text{ K}^{-1})$ is universal gas constant, while $K_T(L/g)$ is the equilibrium constant, depicts the highest binding energy and b_T (J/mol) is associated with heat of adsorption.

Kinetic study

Adsorption kinetics tests were carried out to examine the impact of contact time and temperature on the CR uptake by $G/SnO₂$ and to find out the kinetic parameters. A known amount of adsorbent (0.1 g) was contacted with 40 mL of CR dye solution (700 mg/L) in an array of 100-mL polythene bottles at constants solution pH (3.0) and shaken in an isothermal shaker bath for certain time (5–240 min) at 120 rpm at fxed temperature (298, 308 and 318 K). Bottles were withdrawn at defnite time intervals from shaker bath, fltered and analyzed for the remaining concentration of CR in the fltrate.

In the present work, the kinetics and mechanism of CR were studied using pseudo-frst order (Corbett [1972](#page-14-16)), pseudo-second order (Ho [2006\)](#page-14-17) and intra-particle difusion (Weber and Morris [1963\)](#page-15-10) models. The linear form of pseudo-second order kinetic model is expressed as:

$$
\log\left(q_e - q_t\right) = \log q_e - \left(\frac{k_1}{2.303}\right)t\tag{9}
$$

where q_e and q_t denote the CR uptake capacities (mg/g) by $G/SnO₂$ at equilibrium and at any time t , respectively, while k_1 (1/min) signifies the pseudo-first-order rate constant.

Pseudo-second order kinetic models proposed by Ho and Mckay assume that adsorption of adsorbate species on adsorbent surface occurs by chemical interaction as a result of electron sharing between dye molecules and the functional groups on adsorbent surface. The linear form of pseudo-second order kinetic equation can be represented as follows:

$$
\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t
$$
\n(10)

where k_2 (g/mg min) is the rate constant for pseudo-second order kinetic model.

As many sorption processes are involved in the movement of adsorbate species from bulk solution into adsorbent surface. Therefore, Weber and Morris intra-particle difusion model was used to observe the effect of mass-transfer resistance on the adsorption of CR by $G/SnO₂$ and determine the rate controlling step. According to intra-particle difusion model, the sorption capacity varies with the square root of time. The linear form of this model can be expressed as:

$$
q_t = k_i t^{0.5} + C \tag{11}
$$

where k_i represents intra-particle diffusion model rate constant (mg/g min^{0.5}) at a given stage i , while the intercept *C* is related to the boundary layer thickness (mg/g). The adsorption kinetic data were further explained by Boyd model (Boyd et al. [1947](#page-14-18)) to confrm the rate determining step in the adsorption of CR. Boyd model equation can be represented as:

$$
F = 1 - \left(\frac{6}{\pi^2}\right) \sum_{m}^{1} \left(\frac{1}{m^2}\right) \exp\left(-m^2 B t\right)
$$
 (12)

$$
F = \frac{q_t}{q_e} \tag{13}
$$

Rearranging the above equation:

$$
Bt = -0.4977 - \ln(1 - F) \quad \text{when } F > 0.85 \tag{14}
$$

$$
Bt = \left[\sqrt{\pi} - \sqrt{\pi - (\pi^2 F/3)}\right]^2 \quad \text{when } F < 0.85 \tag{15}
$$

where '*F*' is the fraction of CR adsorbed at any time *t*, while *Bt* is a mathematical function of *F* and *m* is an integer which defnes the solution infnite series.

Thermodynamic investigations

To investigate whether the uptake of CR by $G/SnO₂$ composite is spontaneous process or not, various thermodynamic parameters such as Gibbs free energy change (Δ*G*°), enthalpy change (∆*H*°) and entropy change (∆*S*°) were calculated at 298, 308 and 318 K by using the following equations (Hassan et al. [2020](#page-14-19)).

$$
\ln K_{\rm L} = -\frac{\Delta H^0}{RT} + \frac{\Delta S^0}{R} \tag{16}
$$

$$
\Delta G^0 = \Delta H^0 - T\Delta S^0 \tag{17}
$$

where $T(K)$ is the solution temperature, $R(8.314 \text{ J/mol/K})$ is the universal gas constant, while K_L (L/mg) is equilibrium Langmuir constant. The ∆*H*° and ∆*S*° values were calculated from the slope and intercept of the linear plot of $\ln K_L$ versus 1/*T*.

Calculation of activation energy

Activation energy for the adsorption of CR onto the $G/SnO₂$ composite was determined using Arrhenius equation as follows (Li and Lin [2019\)](#page-14-20):

$$
\ln k_2 = \ln A - \frac{E_a}{RT}
$$
\n(18)

where E_a is activation energy (kJ/mol), k_2 is the pseudosecond-order rate constant, *A* is Arrhenius constant which is temperature independent and *R* is universal gas constant.

Desorption and regeneration studies

Desorption and regeneration tests were executed by contacting a known amount of dye loaded adsorbent (0.5 g) with desorbing medium (200 mL) followed by agitating for 2 h at room temperature (298 K) under the identical conditions as used in adsorption studies. Subsequently, the concentration of CR desorbed was measured spectrophotometrically and the adsorbent recovered was washed and used again in adsorption of CR in next adsorption–desorption cycle. Desorption efficiency was estimated via the equation as given below (Ali et al. [2021\)](#page-13-3):

Desorption efficiency =
$$
\frac{C_{\text{d}}}{C_0 - C_e} \times 100
$$
 (19)

where C_o and C_e are CR initial and equilibrium concentrations (mg/L), respectively, while C_d is the dye concentration (mg/L) after desorption.

Results and discussion

Adsorbent characterization

SEM and EDS analysis

The scanning electron microscope (SEM) images of GO and $G/SnO₂$ composite are presented in Fig. [1a](#page-5-0), b. The SEM image of GO (Fig. [1a](#page-5-0)) shows irregular porous morphology and un-exfoliated graphene sheets. SEM micrograph of $G/SnO₂$ composite indicates particles agglomeration and irregular particles morphology as evident from Fig. [1b](#page-5-0). Similar observations were made by Dhanabalan et al. [\(2013](#page-14-21)) in their study on graphene oxide/tin oxide composite. The percent amount of various elements examined in the EDS spectra of GO and $G/SnO₂$ composite are given in Fig. [2a](#page-6-0), b,

Fig. 1 SEM images of **a** GO and \mathbf{b} G/SnO₂ composite

respectively. The EDS spectrum of GO contains major peaks for carbon, oxygen and nitrogen and some minor peaks for Na, Mg, Si, Cl and S. The minor peaks indicate the presence of some impurities. The EDS spectrum of $G/SnO₂$ shows peaks only for carbon, oxygen, Cl and Sn, indicating that the synthesized material is free from impurity and was successfully prepared.

XRD analysis

X-Ray difraction (XRD) analysis is a worthwhile technique for studying the crystalline nature of solid materials. In the current work, degree of oxidation and crystallography of GO and $G/SnO₂$ composite was studied using XRD technique and the results obtained are shown in Fig. [3a](#page-7-0). In case of GO, a single sharp difraction peak was observed at 2*θ* value of about 11.5° which ratifes that the GO was successfully prepared. Same results were also observed by Alam et al. [\(2017\)](#page-13-1) in the XRD pattern of GO synthesized by modifed Hummers method. There are no distinctive peaks in the XRD pattern of $G/SnO₂$ composite which confirm the amorphous nature of the composite material at 160 °C temperature. The amorphous nature of $G/SnO₂$ composite at this temperature has been reported in the literature (Lin et al. [2012\)](#page-14-22).

FTIR analysis

Fourier transform infrared (FTIR) spectroscopic technique is commonly used to explore the structure of constituents and the variation in the chemical structure of materials. FTIR spectra of GO and $G/SnO₂$ composite are given in Fig. [3b](#page-7-0). FTIR spectrum of GO displays a wide peak in the range of 3000–3700 cm⁻¹ and a sharp peak at 1713 cm⁻¹, conforming the bending and stretching vibration of OH groups on GO surface. While the existence of absorption peaks, at 1615 cm−1 is due to the stretching vibration of C=O and C=C of carbonyl group and carboxylic acid which is present at the corner of GO. The peaks at the 1319 cm^{-1}

and 1053 cm−1 are matching to the stretching vibration of C–OH and C–O of alcohol and carboxylic acid, respectively. The presence of these oxygen containing groups shows the oxidation of graphite into GO (Lin et al. [2012\)](#page-14-22). The FTIR spectrum of $G/SnO₂$ composite shows shift in intensity of various absorption peaks corresponding to diferent oxygen containing groups like $C=O$, $C=O$ and OH, which confirm effective reduction in GO to graphene in $G/SnO₂$ composite (Zhang et al. [2012\)](#page-15-11).

FTIR spectra of $G/SnO₂$ composite displayed the occurrence of some new peaks after the adsorption of CR dye. The two sharp peaks that appeared at 1365 cm⁻¹ and 1045 cm⁻¹ were attributed to the stretching vibration of $-SO₃$ group and symmetric stretching of S=O, respectively. The new peaks at 1427 and 1180 cm−1 correspond to –N–H bending and aromatic ring of CR molecules, respectively (Hua et al. [2019\)](#page-14-23). The appearance of new peaks and shifting of some peaks (at 3370, 1574, 1218 and 1027 cm⁻¹) to higher wavenumber regions (3456, 1599, 1262 and 1045 cm⁻¹) affirming successful adsorption of CR by $G/SnO₂$ composite.

Thermal analysis

Thermogravimetric (TGA/DTA) study was carried out to find the weight loss of GO and $G/SnO₂$ composite with rise in temperature. The TGA/DTA plots of GO and $G/SnO₂$ composite are given in Fig. [3c](#page-7-0). As can be seen, GO shows weight loss in three steps. The initial weight loss (18.78%) was observed in the temperature range of 35–153 °C and is associated with the removal of water molecules adsorbed on the surface of GO. In the second step a high weight loss (23.63%) was noticed in the temperature of \sim 200 °C. This change is due to elimination of oxygen containing functional groups like OH, C=O and COOH as carbon monoxide, carbon dioxide and water produced during heat treatment. The third and lost weight loss (40.99%) which occurs in the temperature range of about 430–550 °C is associated with the combustion of carbon skeleton of GO. The present fnding

is in close agreement with those reported in the literature (Shahriary and Athawale [2014](#page-15-12)). The TGA plot of $G/SnO₂$ composite reveals that the decomposition of carbon skeleton occurred in the temperature range of 480–650 °C, which is much higher than that of graphene oxide. This confrms that $G/SnO₂$ composite is thermally more stable than GO.

Point of zero charge (pH_{PZC})

The pH at the point of zero charge pH_{PZC} for $G/SnO₂$ composite was found to be 6.0, obtained by plotting ΔpH versus initial pH values as shown in Fig. [3d](#page-7-0). The surface of composite was observed to be negatively charged above the pH_{PZC} (6.0) value. So, the adsorption of anionic dyes like CR by $G/SnO₂$ composite can be more efficient at lower pH, while cationic dyes can be adsorbed preferably at pH values higher than 6.0.

Adsorption protocol

Efect of pH

Solution pH is the most important parameter that could obviously afect uptake of adsorbate species on adsorbent surface. Solution pH can alter both, adsorbent surface charge and chemistry of adsorbate molecule (Ali et al. [2019\)](#page-13-2). In this study, removal of CR by $G/SnO₂$ composite was studied in the pH range of 2–12 at 298 K with initial CR dye

Fig. 3 a XRD pattern, **b** FTIR spectra before and after CR adsorption, **c** TGA/DTA curves of GO and G/SnO₂ composite and **d** plot of ΔpH versus pHi for the determination of pH_{PZC}

concentration of 50 mg/L as shown in Fig. [4](#page-8-0)a. It can be seen that CR removal efficiency decreases with increasing solution pH. In acidic conditions (pH 2–4) adsorption efficiency was highest (99.11–98.81%) and lowest (13.23%) in basic conditions (pH 12). This phenomenon can be explained on the basis of pH_{PZC} of $G/SnO₂$ which is 6.0. At pH value lower than 6.0, positive charges are more dominant on the surface of $G/SnO₂$ composite due to protonation which results in high adsorption of anionic dye CR, controlled by electrostatic interactions arising among negatively charged dye anions and the positive charges on $G/SnO₂$ surface. However, at pH value beyond pH_{PZC} , G/SnO₂ surface gets deprotonated leading to decrease in percent adsorption. Similar results have been reported by Bhat et al. ([2020](#page-14-1)) in the adsorption of CR by polyvinyl alcohol/melamine–formaldehyde composite.

Efect of CR initial concentration

The impact of initial concentration on the adsorption of CR by $G/SnO₂$ composite was scrutinized by varying dye

concentration from 20 to 1000 mg/L at pH 3.0 and the results acquired are given in Fig. [4](#page-8-0)b. It can be seen that the CR uptake capacity frst upsurges with rise in concentration of CR molecules from 20 to 1000 mg/L and fnally reaches the peak values which then level off after attaining equilibrium, where no more adsorption occurs. Initially, the increase in CR adsorption is associated with the development of driving force that overcomes all mass transfer resistance arising among the existing binding sites on $G/SnO₂$ surface and CR molecules in solution. The leveling and smoothing of the cures indicate that the available binding site on $G/SnO₂$ surface gets saturated with CR anions and no further adsorption could occur. Similar investigations were reported by Li and Lin [\(2019](#page-14-20)) and Zhao et al. ([2017\)](#page-15-13) for the adsorption of CR using La/MFA composite and nickel-based metal–organic framework/graphene oxide composites, respectively.

Efect of contact time and temperature

The influence of shaking duration and temperature on the uptake of CR (initial concentration 700 mg/L) by G/

Fig. 4 Effect of **a** dye solution pH, **b** initial concentration, **c** contact time and temperature and **d** adsorbent dose on CR adsorption by G/SnO₂ composite

 $SnO₂$ composite was studied at three different temperatures (298, 303 and 308 K) with dye solution pH 3.0. The results obtained (Fig. [4c](#page-8-0)) shows that shaking duration has a signifcant impact on the adsorption of CR. Initially the uptake was fast which then slowly decreased until saturation was achieved. The state of equilibirium was established in about 60 min, which was selected for all other adsorption studies. The enhanced uptake rate at initial intermezzos could be associated with availability of more binding positions on G/ $SnO₂$ surface. These binding positions then start decreasing swiftly with time which leads to slow adsorption rate and eventually attains a constant value. The slow uptake near the saturation point may be because of the electrostatic repulsion among the previously adsorbed CR anions and the dye anions in aqueous phase (Kataria and Garg [2017](#page-14-24); Madan et al. 2019). The effect of temperature (298, 308, and 318 K) on CR adsorption can also be seen in Fig. [4c](#page-8-0). It can be observed that uptake of CR by $G/SnO₂$ composite increases with mounting temperature from 298 to 318 K, signifying endothermic nature of CR adsorption. The increase in temperature may facilitate the CR molecules to reach the active sites on adsorbent surface by increasing its solubility. Also, at elevated temperature the interaction between dye molecule and adsorbent surface increases, leading to high adsorption capacity (Acemioğlu [2004](#page-13-4); Zhao et al. [2017\)](#page-15-13).

Efect of adsorbent dose

Adsorbent dose is a highly influential parameter in the adsorption of contaminants from aqueous systems. It explores the uptake capacity of a solid adsorbent material for a particular concentration of an adsorbate. Therefore, optimization of adsorbent dose is very essential for the removal of pollutants from aqueous environments. The impact of adsorbent dosage on the removal of CR with initial concentration of 700 mg/L was assessed by varying the amount of $G/SnO₂$ composite from 0.01 to 0.2 g at pH 3.0 and 298 K as depicted in Fig. [4](#page-8-0)d. It can be observed that adsorption efficiency of CR boosts from 42.41 to 99.64% with rising $G/SnO₂$ mass from 0.01 to 0.2 g. This behavior can be explained by the fact that with increasing adsorbent dose availability of binding sites on $G/SnO₂$ surfaces increases which leads to high adsorption efficiency. However, the uptake capacity (q_e) decreases with increase in adsorbent

dose due to aggregation of adsorption sites located on surface of adsorbent and reduction in adsorbent-to-adsorbate ratio. Similar results have been reported by other workers for the adsorption of anion and cationic dyes by various adsorbents (Ali et al. [2019;](#page-13-2) Dandil et al. [2019;](#page-14-25) Madan et al. [2019](#page-14-0)).

Equilibrium isotherm studies

To assess the performance of adsorbent during adsorption process and understand the sort of interactions between adsorbate and adsorbent, diferent adsorption isotherm models were used. In the current study Freundlich, Langmuir and Temkin isotherm models were employed for interpretation of experimentally obtained equilibrium data for CR adsorption on $G/SnO₂$ composite.

Freundlich isotherm model is one of the earliest known models that describe the sorption mechanism. The ftted plots of Freundlich isotherm model for CR adsorption by $G/SnO₂$ are given in Fig. [5a](#page-9-0). It can be observed from the fgure that the isotherms are linear but with very low regression coefficient value ($R^2 \le 0.67$), indicating that Freundlich model is not appropriate for describing the equilibrium data under the given experimental conditions. The Freundlich isotherm constants $(1/n$ and $K_F)$ calculated from the slope and intercept of ln C_e versus ln q_e plots (Table [2\)](#page-10-0) gives information about the nature and feasibility of sorption process. The value of K_F increases with rising temperature from 298 to 318 K, suggesting endothermic nature of CR adsorption onto G/SnO₂ composite. Furthermore, the $1/n$ values were smaller than 1.0 (Table [2\)](#page-10-0), signifying favorable adsorption process and high affinity of G/ $SnO₂$ composite toward the targeted dye molecules under the given conditions of temperatures.

Langmuir isotherm model plots are presented in Fig. [5b](#page-9-0), and the values of model parameters $(q_m$ and K_l) were calculated from the slope and intercept of the linear plots of C_e/q_e versus C_e as summarized in Table [2.](#page-10-0) The isotherms were linear with high R^2 values (\geq 0.99) than that of Freundlich model. In addition, the experimental and model predicted maximum uptake capacity $(q_m, mg/g)$ are in close agreement. This revealed that the CR dye adsorption by G/ $SnO₂$ composite can be described very well by the Langmuir

Fig. 5 Plots of **a** Freundlich, **b** Langmuir and **c** Temkin isotherms models for the uptake of CR onto G/SnO₂ composite

Table 2 Diferent isotherm model parameters for the adsorption of CR by $G/SnO₂$ composite at three different temperatures

Model	Parameters	Temperature (K)		
		298	308	318
Langmuir	Theoretical q_m (mg/g)	350.87	355.87	359.71
	Experimental q_e (mg/g)	338.07	343.27	347.28
	K_b (L/mg)	0.17	0.20	0.24
	R^2	0.99	0.99	0.99
Freundlich	$K_{\rm F}$ (mg/g(L/mg) ^{1/n})	50.19	51.62	55.12
	n	2.09	1.84	1.76
	R^2	0.48	0.60	0.67
Temkin	$B_{\rm T}$	59.15	63.51	64.25
	$b_{\rm T}$ (J/mol)	41.88	40.32	41.15
	A_T (L/mg)	3.89	3.57	4.32
	R^2	0.76	0.84	0.65

model, indicating homogeneous nature of $G/SnO₂$ surface and monolayer sorption process. The monolayer adsorption capacity (q_m) and binding energy constant $(K_L, L/mg)$ values increases from 350.87 to 359.71 mg/g and from 0.17 to 0.24 L/mg, respectively, with rising temperature from 298 to 318 K (Table [2](#page-10-0)), confrmed endothermic nature CR adsorption. The favorability of adsorption process and ftting quality of Langmuir isotherm model was further assessed using separation factor (R_L) . The values of R_L at all studied temperatures were found between zero and unity (Table [2](#page-10-0)), demonstrating feasible adsorption of CR onto $G/SnO₂$ composite that can be explained by Langmuir model very well. Similar fndings have been reported by Parida and Pradhan [\(2010](#page-15-14)) for the adsorption of phenolic compounds using manganese nodule leached residue as adsorbent.

The values of Temkin isotherm constants, K_T and b_T for the uptake of CR by $G/SnO₂$ were found from the intercept and slopes of q_e versus $\ln C_e$ plots, respectively (Fig. [5c](#page-9-0)), and the results are given in Table [2](#page-10-0). The smaller value of correlation coefficient ($R^2 \le 0.76$) showed that Temkin model did not ft the experimental data. With rising dye solution temperature from 298 to 318 K, b_T and K_T values were correspondingly increased from 40.32 to 41.88 J/mol and 3.89 to 4.32 L/mg. This phenomenon could be associated to the increase in surface courage due to adsorbate–adsorbent interaction and endothermic nature of CR adsorption (Jalil et al. [2012](#page-14-26)).

Kinetics study

The kinetic and mechanism of CR adsorption by $G/SnO₂$ was studied at 298, 308 and 318 K using pseudo-frst order, pseudo-second order, intra-particle difusion and Boyd's models. The plots for pseudo-frst order, pseudo-second order, intra-particle difusion and Boyd's models are shown in Fig. [6a](#page-11-0)–d and the calculated kinetic parameters are summarized in Table [3.](#page-11-1) Based on the lower R^2 values, the pseudo-frst order model did not ft well the experimental kinetic data of CR adsorption under the given conditions of temperature. However, the plots of t/q_t versus t for pseudosecond order model (Fig. [6](#page-11-0)b) are linear with very high value of correlation coefficient (equal to unity) fitted very well to the kinetic data points. Additionally, the closeness of model predicted adsorption capacities (*qe*, cal) based on pseudo-second order model and experimentally determined values (Table [3\)](#page-11-1) further verifed the good ftting quality of pseudo-second order kinetic model at all the studied temperatures. These results revealed that the uptake of CR may be accomplished by electron transfer among the functional groups on $G/SnO₂$ surface and CR anions via chemical interaction (Nayak and Pal [2017\)](#page-15-15). The pseudo-second order rate constant (k_2) values increases from 0.03 to 0.13 g/mg min, suggesting that the affinity of $G/SnO₂$ composite toward CR increases with rising temperature from 298 to 318 K, displaying endothermic nature of sorption process. The increase in $k₂$ values with temperature may be due to the quick transfer of CR molecules from solution to the adsorbent surface at elevated temperature. Other researchers have observed similar results for the adsorption of Congo red dye using $TiO₂$ nanoparticles and inorganic-and organic-modifed kaolinite as adsorbent materials (Shaban et al. [2018](#page-15-16); Rath et al. [2019\)](#page-15-17).

To get insight about the rate limiting step and difusion mechanism of CR adsorption onto $G/SnO₂$ composite, Weber–Morris intra-particle difusion model was employed for analyzing the kinetic data. The intra-particle difusion model parameters $(k_i$ and $C)$ were evaluated from the slope and intercept of linear plots of q_t versus $t^{0.5}$ (Fig. [6](#page-11-0)c) and are listed in Table [3.](#page-11-1) It can be observed from the fgure that the plot of q_t versus $t^{0.5}$ did not pass through the origin at all studied temperatures and have low regression coefficient values ($R^2 \le 0.91$), suggesting that only intra-particle diffusion is not the rate controlling step for CR adsorption (Abbas et al. [2017](#page-13-5)). The boundary layer thickness (*C*) values were increased from 275.28 to 279.31 mg/g with increasing temperature from 298 to 318 K, suggesting that boundary diffusion effect increases with rising dye solution temperature. The kinetic data were further analyzed via Boyd model to evaluate whether intra-particle difusion or flm difusion is the rate determining step. The Boyd model plots (Fig. [6d](#page-11-0)) were found to be linear but did not pass through the origin, confrming that both flm difusion and particle difusion control the rate of CR adsorption by $G/SnO₂$ composite.

Thermodynamic investigations

To further understand the impact of solution temperature on CR adsorption by $G/SnO₂$ composite thermodynamic studies

Fig. 6 a Pseudo-frst order, **b** Pseudo-second order, **c** Intra-particle difusion and **d** Boyd model plots for CR adsorption by G/SnO2 composite

were carried out at three diferent temperatures (298, 308 and 318 K). Diferent thermodynamic parameters like ∆*H°*, Δ*G°* and Δ*S°* were used to evaluate the intrinsic energetic changes associated with CR adsorption. The ∆*S°* and ∆*H°*

were found from the intercept and slopes of the linear plot of ln K_L versus $1/T$ (Fig. [7\)](#page-12-0) and the results achieved are compiled in Table [4](#page-12-1). The positive value of ∆*H°* has shown endothermic nature of sorption process, while positive value of ∆*S°* revealed increase randomness at solid–liquid interface due to high affinity of $G/SnO₂$ composite for CR dye in acidic pH ranges. Additionally, the negatively values of ∆*G°* have shown spontaneous and favorable adsorption of CR by $G/SnO₂$ composite at all the studied temperatures. The decrease in ∆*G°* value (Table [4\)](#page-12-1) with increasing temperature further verified that the feasibility of sorption process increases with temperature which is in agreement with results obtained from isotherm studies. Kumara et al. reported similar fndings for the adsorption crystal violet using TLAC/Chitosan composite (Kumari et al. [2017](#page-14-27)). Moreover, the magnitude of activation energy (E_a) also gives valuable information about the nature of adsorption process. For physical adsorption its range is from 4–40 kJ/mol and for chemisorption it is 40–800 kJ/mol (Kaur et al. [2015\)](#page-14-28). The E_a value calculated for CR adsorption onto $G/SnO₂$ at three diferent temperatures (298, 308 and 318 K) using Arrhenius equation was found to be 54.59 kJ/mol exposed that

Fig. 7 Plot of ln K_L versus 1/T for CR uptake by G/SnO_2 composite

Table 4 Various thermodynamic parameters for CR adsorption by G/ $SnO₂$ composite

			$T(K)$ ΔG° (kJ/mol) ΔH° (kJ/mol) ΔS° (J/mol K) E _s (kJ/mol	
298	-29.02	11.46	135.82	54.59
308	-30.37			
318	-31.73			

the adsorption process in the present case is chemisorption. Similar investigations have been reported by other workers for cationic and anionic dyes adoption using diferent adsorbents (Abbas et al. [2017](#page-13-5); Gemici et al. [2020\)](#page-14-29).

Desorption and adsorbent regeneration

Desorption and regeneration studies were carried out to assess the possible reuse of adsorbent and feasibility of the process. In regeneration experiments, choice of eluent is a top priority step as eluents can weaken the attractive forces among dyes molecules and adsorbent surface which is possible by a specifc eluent only. In the current study, HCl (0.1 M), DDW, ethanol and NaOH (0.1 M) were used as eluents and maximum desorption of CR (93.03%) from the surface of $G/SnO₂$ composite was achieved with 0.1 M NaOH solution as can be seen in Fig. [8a](#page-12-2). Hence, NaOH solution was selected for further regeneration studies. The highest desorption in alkaline medium may be due to the deprotonation of $G/SnO₂$ surface leading to a reduction in electrostatic interactions among dye anions and adsorbent surface.

Regeneration of dye loaded adsorbent was inspected in five consecutive adsorption–desorption cycles using NaOH (0.1 M) as desorbing medium and the results obtained are illustrated in Fig. [8b](#page-12-2). From the fgure it can be seen that the $G/SnO₂$ composite adsorption efficiency slightly fall after each cycle but is still higher than 75% even in the ffth cycle,

shown that $G/SnO₂$ composite could be recycled many times for dyes containing wastewater without any substantial loss in sorption efficiency. The slight reduction in uptake efficiency in the successive cycles may be due to loss of some active sites on $G/SnO₂$ composite surface (Hosseini et al. [2011](#page-14-30)).

Comparison with other adsorbent

The maximum monolayer uptake capacity of $G/SnO₂$ composite for CR was compared with many other already reported adsorbents, as illustrated in Table [5](#page-13-6). It can be perceived from the table that $G/SnO₂$ composite has considerably high uptake capacity for CR than many other previously reported adsorbents. This confirmed that $G/SnO₂$ composite synthesized by solvothermal method could be an efficient adsorbent for detoxification of highly toxic anionic dyes, such as CR from aqueous environment.

Fig. 8 a Impact of eluents type on CR desorption and **b** regeneration of $G/SnO₂$ composite in five consecutive cycles

of G/SnO₂ for CR with reported adsorbents

Table 5 Comparison of

Conclusion

Graphene tin oxide $(G/SnO₂)$ composite was successfully synthesized by a simple solvothermal method and was used efficiently for the removal of toxic anionic dye, CR, from aqueous environment. EDX analysis presented a high percentage of Sn (62.11%), accompanied by decrease in percentage of carbon (from 47.45 to 13.75%) and oxygen (from 39.37 to 23.71%) confirmed that $G/SnO₂$ composite has been successfully prepared which is also supported by FTIR analysis. TGA analysis has showed that $G/SnO₂$ composite is thermally more stable than GO as decomposition of its carbon skeleton occurred in the temperature range of 480–650 \degree C, which is much higher than that of graphene oxide (430–550 °C). The pH_{PCZ} (6.0) of G/ $SnO₂$ has shown that it can efficiently remove both anionic (below pH 6.0) and cationic (above pH 6.0) dyes from aqueous solutions. Highest adsorption of CR was observed in the pH range of 2–5. Adsorption of CR was explained very well by Langmuir isotherm model and pseudo-second order kinetic model with the maximum monolayer adsorption capacity 359.71 mg/g at 318 K which is quite high than many other adsorbent already reported adsorbents. Thermodynamic study has shown endothermic and spontaneous nature of CR adsorption onto $G/SnO₂$. Regeneration analyses shown that $G/SnO₂$ composite can be used many times for the adsorption of azo dyes from wastewater without any significant loss in sorption efficiency.

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Declarations

Conflicts of interest The authors declare that they have no competing interest.

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