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Quantifying the greenhouse gas emissions abatement cost of biomass co‑fring in coal‑powered electricity generation

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Abstract

This paper analyzes the abatement costs associated with greenhouse gas reductions achievable by co-fring corn stover with coal at 71 coal-fired, utility-scale power plants in the Midwestern USA. The cost per metric ton of abated CO₂-equivalents is estimated using facility-specifc supply functions for corn stover assuming best carbon management practices, county-level corn production data, a life cycle inventory tool for calculating biomass feedstock emissions, and simplifed cost models for coal and co-fred capital and operating costs. Abatement costs vary substantially across the power plants modeled: mean costs were \$123.71 per metric ton CO_2 -eq at a 5% co-firing rate, \$64.43 for 10% co-firing, and \$49.20 for 20% co-firing, with coefficients of variation of 26%, 38%, and 48%, respectively. Lower abatement costs are primarily associated with high co-fring rates and high estimated unit costs for coal. The local corn yield and collection radius do not appear to have a substantial impact on estimated abatement costs. This advances our understanding of the abatement costs associated with co-fring biomass and coal, and the drivers of variability in abatement costs, by modeling feasible production scenarios using actual power plant and corn production data instead of idealized scenarios.

Keywords Biomass co-fring · Climate change mitigation · Corn stover · Emissions abatement · Greenhouse gas emissions

Introduction

Electricity generation in coal-fred power plants is responsible for approximately one-quarter of greenhouse gas (GHG) emissions in the USA; in 2016, coal produced one-third of the country's electricity but two-thirds of the GHG emissions associated with power generation (US Environmental Protection Agency [2018](#page-11-0)). Several studies have explored the potential cost-efectiveness of co-fring biomass in existing

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coal-fred plants to reduce their emissions profle, identifying a wide range of abatement costs over varied scenario assumptions (Ortiz et al. [2011;](#page-10-0) Wilson et al. [2012](#page-11-1); McGlynn et al. [2014](#page-10-1); Schakel et al. [2014;](#page-10-2) Djomo et al. [2015](#page-10-3)). Many policies, such as the Clean Power Plan and federal Renewable Fuel Standards, have identifed biomass as a potential source of emissions reductions in the electricity and transportation fuels sectors. As of 2020, 30 states have developed their own Renewable Portfolio Standards, many of which address the potential for utilizing biomass to reduce GHG emissions (National Conference of State Legislatures [2020](#page-10-4)).

However, the life cycle emissions associated with biomass can vary greatly. They depend on factors such as the choice of biomass feedstock, prior land use, geographic location, and indirect land use change implications (Farrell et al. [2006;](#page-10-5) Curtright et al. [2012](#page-10-6); Johnson et al. [2013](#page-10-7)). With respect to the cost of abating emissions, incremental capital and operating costs are needed to repower boiler systems and process biomass for co-fring. Resource availability also plays a major role in determining the cost of co-fring; in addition to direct feedstock expenditures, a larger collection area increases transportation costs.

As a result, there is signifcant scenario uncertainty in the abatement costs associated with co-fring GHG emissions reductions. Abatement costs may vary substantially by individual power plants due to diferences in local resource availability and boiler capacity, even for the same feedstock and co-fring rate. This study estimates abatement costs associated with co-fring corn stover for 71 coal-fred Midwestern power plants in the Midcontinental (MISO) power region. The location and size (net MWh produced in 2016) are shown in Fig. [1.](#page-1-0) Estimated abatement costs are based on integration of spatially explicit supply curves for biomass available for sourcing to each power plant, a life cycle inventory tool to estimate GHG emissions, and a simplifed model of non-fuel co-fring costs.

This analysis is intended to identify the key factors driving variation in the abatement cost associated with biomass co-fring and to provide estimates of the average abatement costs suitable for high-level planning. The results would also be useful for comparing the approximate abatement cost for co-fring technology with estimates of the social cost of carbon or estimates of abatement costs for other emissions mitigation technologies. While the analysis utilizes 2016 data reported by the US Energy Information Administration (EIA) for the MISO region at the individual power plant scale, a design-level analysis of individual power plants interested in analyzing their own abatement costs would of course rely on more detailed information than is employed here for a regional analysis.

Materials and methods

The set of power plants included in the analysis consists of 71 utility-scale facilities in the MISO region. Power plants with signifcant utilization of non-coal fuel sources were excluded from the analysis. Smaller plants owned and operated by universities or private industry were also excluded. The geographic distribution and sizes of the plants are summarized in Table [1](#page-1-1).

Table 1 Number of included power plants and annual net generation by state (2016)

State	Number of power plants	Median genera- tion (MWh)	Average generation (MWh)
Illinois	11	2.347.827	3,749,487
Indiana	14	1.918.654	3.724.339
Iowa	6	1,475,253	1,815,930
Kentucky	3	2.092.403	2,159,054
Michigan	16	780,677	2,498,416
Minnesota	4	1.609.641	2,718,759
Missouri	4	5,471,617	6,836,244
North Dakota	4	1,755,131	2,078,884
Wisconsin	9	3,756,559	3,654,989
Grand total	71	2,066,768	3,241,732

Fig. 1 Location and annual net electricity generation of 71 coal-fred power plants in the study region (as of 2016)

Abatement cost analysis

This analysis is restricted to the use of corn stover, as an agricultural residue, for co-fring with coal at a rate of 5%, 10%, or 20% (by energy content). Conceptually, the estimated abatement cost is equal to the diference in costs associated with co-fring biomass with the coal, divided by the diference in GHG emissions (measured in metric tons of $CO₂$ -equivalents).

Calculation of the diference in costs associated with cofring accounts for the diference in fuel costs, incremental capital and operating costs from repowering to co-fre and processing the feedstocks, and lost revenues associated with parasitic load and lost efficiency from utilization of biomass. Emissions are calculated using life cycle values. A simplifed emissions model for coal incorporates emissions from combustion, fuel transport, and methane produced at the mine. For the biomass, emissions estimates come from a version of the Calculating Uncertainty in Biomass Emissions model (Curtright et al. [2011](#page-10-8)), modifed to use county-level corn yield values and generate GHG emissions using the power plants as the unit of analysis. Additional details about each component of the abatement cost equation are provided in the following sections.

Estimation of biomass utilization and coal displacement by Co‑fring rate

Production data for each power plant were obtained for the year 2016 from the US EIA (US Energy Information Administration [2018\)](#page-11-2). This dataset includes the quantity of fuel consumed, electricity generation (kWh), and tons of $CO₂$ emissions, broken out by plant and coal type (subbituminous, bituminous, refned, and lignite). The total annual power generation was summed over all coal types and multiplied by the assumed 5%, 10%, or 20% co-fring rate to obtain the energy content that must be replaced by the cofred biomass. A lower heating value of 16.8 MJ per kg of corn stover was used to calculate the quantity of biomass required (International Renewable Energy Agency [2012](#page-10-9)). While baled stover is estimated to have little impact on boiler efficiency due to its low moisture content (Ortiz et al. [2011](#page-10-0)), further refnements adjust the heat rates of co-fring following Tillman (Tillman [2000\)](#page-10-10).

The quantity of coal displaced by the biomass is assumed to be proportionally distributed across all coal types utilized by a plant. For example, if a plant utilizes both bituminous and subbituminous coal, the 5% co-fring scenario assumes a reduction of 5% in fuel consumption from both types. This is a simplifying assumption and may not align with actual practice if fuel costs vary substantially on an energy basis, or for other reasons.

Estimation of biomass supply functions

Feedstock costs represent a major variable cost of biomass co-fring. This study considers the cost of obtaining corn stover, specifically the harvest and transportation costs (Langholtz et al. [2016\)](#page-10-11). While the harvest location of biomass does signifcantly afect harvest costs, transportation costs rise with the increase in distance between harvest locations and power plants. Power plants located in areas with richer availability of local biomass pay lower transportation costs compared to power plants located in areas with low biomass density to obtain the same amount of biomass. Even in areas of high agricultural production, transportation costs constitute a large portion of total feedstock costs (Langholtz et al. [2016](#page-10-11)). Given the variation in transportation costs, the total feedstock costs to collect the same quantity of biomass are diferent across power plants; at a given level of feedstock cost, the supplied biomass quantities are heterogeneous across power plants. Further, heterogeneity in the electricity production at each plant means that diferent quantities of biomass are required to reach the same co-fring rate.

The total quantity of corn stover biomass available within a specifed distance of a power plant depends on the proportion of local land being used for corn production, as well as the yield. To estimate a separate supply function for each power plant, we measure the available quantity of biomass within different radii from each plant. Specifically, we draw 80 supply circles centered on each power plant in 5 km increments for the radius (Fig. [2](#page-2-0)) and calculate the total quantity of available biomass within each circle. The feedstock cost for biomass in each circle is the total cost of harvesting and transporting biomass located at the boundary of the circle, the furthest locations with the highest transportation cost. With 80 circles, we collect 80 sets of data on biomass quantity and cost and estimate a unique biomass supply function for each power plant. We denote supply circles from smallest to largest, such that circle *r* is defned as the circle, centered on the power plant, with a radius of 5*r* kilometers.

Corn stover is considered an ideal feedstock for co-fring (International Energy Agency, International Renewable Energy Agency [2013\)](#page-10-12). Most power plants in the MISO

Fig. 2 Illustrative supply circles around a power plant

region are located in the US Corn Belt and surrounded by intense production of corn and corn residues, making the region a good study area. The total available quantity of corn stover residue within each supply circle is measured using the Cropland Data Layer dataset (CDL) from the US Department of Agriculture (National Agriculture Statistics Service [2010](#page-10-13)). CDL data show the crops planted on each grid cell at a 30 m resolution. The land area of all corn-producing grid cells is aggregated to calculate the total production area of corn within each circle. The total quantity of corn stover available for co-fring within each supply circle is calculated by combining the yield data for corn and corn stover and a stover harvest rate of 33% (Thompson and Tyner [2014](#page-10-14)). Yields were calculated using a six-year moving average of harvested bushels per acre from 2010 to 2015 (National Agriculture Statistics Service [2018\)](#page-10-15). In county-year combinations where yield data are unavailable, yields are imputed using a linear model based on methods from Schlenker and Roberts (Schlenker and Roberts [2009\)](#page-10-16), as implemented by Haqiqi and Hertel (Haqiqi et al. [2018](#page-10-17)). The yield within each circle was assumed to equal these average yields, except in a handful of cases of urban power plants in counties with no agricultural production. In these cases, yields from adjacent counties were used instead.

The feedstock cost of corn stover includes harvest costs and transportation costs. Harvest costs are obtained from Thompson and Tyner (Thompson and Tyner [2014\)](#page-10-14), which include the costs of equipment, labor, fuel, processing, storage, and replacement of nutrients removed by residue harvest. Transportation cost data are from the US Department of Energy Billion-Ton Report (2016). The data include logistics costs (which do not depend on transportation distance) and other transportation costs that are calculated based on the travel distance, laden and unladen transport costs per mile, and travel time value of money (Langholtz et al. [2016\)](#page-10-11). Transport distances are calculated as the geodesic straight-line distance between a grid cell and the power plant, multiplied by an average tortuosity factor to account for roads deviating from straight lines. Specifc values for the data used are reported in Table [2.](#page-3-0) The marginal cost *cr* of obtaining the marginal quantity q_r of corn stover available within supply circle *r* (i.e., the biomass contained in circle *r* but not circle $r - 1$) is

$$
c_r = q_r (P + 3.107 \bar{r} \tau ((D_l + D_u) + T/v))
$$

where q_r is the dry tonnage of biomass collected from all corn-producing grid cells within circle *r* but outside of circle $r - 1$, \bar{r} is the average distance of those corn-producing grid cells to the power plant, *P* is the sum of harvest and logistics costs per dry ton, D_l and D_u are the laden and unladen transport costs per dry ton per mile, τ is the tortuosity factor, *T* is the time cost of transport per dry ton per hour, and ν is the average velocity of transport in miles per hour. The constant factor converts the average distance \bar{r} from kilometers to miles $(5 \text{ km} = 3.107 \text{ miles})$.

Midwestern states in the MISO region are major corn producers. Availability of corn stover is high, and we assume that stover is treated as a residue not used for other purposes such as production of cellulosic ethanol. However, stover plays a role in soil replenishment, so the analysis assumes a cost for nutrient replacement after its removal (as noted in the previous paragraph). Under this assumption, the collection radius required for each plant and co-fring rate very rarely exceeds 100 km, as shown in Fig. [3](#page-4-0). This distance is well below the radius beyond which densifcation for transport (i.e., pelletization) becomes economically advantageous (Ortiz et al. [2011\)](#page-10-0). As such, the calculations of life cycle GHG emissions, processing costs, and transport costs assume the corn stover is simply baled.

This analysis focuses on the variability in abatement costs associated with each power plant if they were to

¹\\$46.43/Mg in the literature, converted with 1 Mg = 1.1023 US ton

Table 2 Parameters used to calculate quantities and costs of corn stover

Radius of Collection Area (km)

Fig. 3 Frequency distribution of collection radius size by co-fring rate

choose to co-fre biomass, independent of other plants' actions. Thus, geospatial proximity between some of the plants is ignored; if multiple power plants acted simultaneously, potential overlap in collection areas could impact resource availability and prices.

The calculated feedstock cost is the sum of harvest and transportation costs for the biomass harvested on the boundary of each circle, representing the highest cost within the circle. It can also be understood as the price that a power plant needs to pay to purchase the last unit of biomass available within a given supply circle. This approach yields 80 values defning the relationship between the quantity and price, specifc to each power plant, associated with sourcing biomass from within a radius of 0 to 400 km (in practice, all plants are able to satisfy their biomass tonnage requirements at distances well less than 400 km). Because the supply circles are concentric, the marginal tonnage available at the price associated with each supply circle is calculated. The total costs to obtain the biomass required for a given plant and co-fring rate are calculated by summing over the marginal costs associated with each supply circle until the required tonnage is met. Equivalently, we multiply the total tonnage required by the average supply cost over each supply circle utilized; as such, rents do not accrue to infra-marginal producers.

Estimation of coal costs

As noted previously, the analysis assumes that the tonnage of coal displaced by biomass co-fring is distributed proportionally across all fuel types, in accordance with the specifed co-fring rate. These quantities are then multiplied by assumed costs for each coal type (as summarized in Table [3](#page-4-1)). The costs from the table are adjusted for transportation costs, assuming that transportation represents approximately 25% of the total delivered price (US Energy Information Administration [2015\)](#page-11-3).

Estimation of incremental costs

Co-fring biomass with coal can require additional capital expenditures for biomass-specifc equipment. It also incurs incremental operating expenses related to the storage,

handling, and processing of biomass before fring. Finally, parasitic load associated with processing and handling, and the minor decrease in efficiency associated with use of corn stover both represent opportunity costs in the form of lost revenue.

Costs for each of these categories are adopted from the baled herbaceous feedstock scenario in Ortiz, et al. (Ortiz et al. [2011\)](#page-10-0), infated to the year 2018. Values for the 20% co-fring rate are extrapolated from the 2%, 5%, and 10% scenarios presented in that report. These are summarized in Table [4;](#page-5-0) all values are given in terms of dollars per kWh of production.

Estimation of life cycle coal emissions

GHG emissions associated with the coal-fred electricity life cycle are dominated by combustion emissions of carbon dioxide (Jaramillo et al. [2007](#page-10-22); Whitaker et al. [2012\)](#page-11-4). Emissions from combustion in 2016 are reported by the US EIA, specifc to each plant and coal type (US Energy Information Administration [2018](#page-11-2)). As noted in Sect. [2.2,](#page-2-1) the specifed co-fring rate scenario determines the quantity of each coal type displaced by biomass. For each plant, the reduction in GHG emissions from coal combustion is therefore calculated by reducing the EIA-reported emissions for each coal type by the same proportion as the reduction in fuel tonnage. This approach accounts for the fact that diferent power plants have diferent emissions factors.

As concluded by Whitaker et al. [\(2012\)](#page-11-4), transportation emissions are assumed to be 3% of combustion emissions on average. The vast majority of GHG emissions from coal production are attributable to coal mine methane emissions; this analysis assumes the median value of 63 g $CO₂$ –eq/kWh from Whitaker, et al. ([2012](#page-11-4)). These three categories—combustion, transportation, and production—collectively represent over 99% of the life cycle emissions for coal-based electricity generation.

Estimation of life cycle biomass emissions

GHG emissions associated with the co-fred corn stover are calculated using the Calculating Uncertainty in Biomass Emissions (CUBE) model, a life cycle inventory tool developed by analysts at RAND Corporation for the US Department of Energy's National Energy Technology

Laboratory (Curtright et al. [2011](#page-10-8)). CUBE estimates the life cycle GHG emissions associated with production of seven diferent biomass feedstocks over a wide range of production scenarios driving diferences in emissions, including production on diferent prior land use types, over diferent lengths of time, and in diferent geographic locations (Johnson et al. [2013\)](#page-10-7). Full details on the methods, data sources used, and validation for estimating life cycle biomass emissions are available in Curtright, et al. (Curtright et al. [2011](#page-10-8)). The original version of the model calculated "farm-to-gate" emissions agnostic of the end use of the biomass (i.e., electrifcation or conversion to liquid fuels for transportation). This analysis adds combustion emissions for the biomass based on the carbon content of corn stover (Kumar et al. [2008](#page-10-23)). The CUBE model has also been modifed to utilize county-specifc yields and to report estimates of emissions associated with the tonnage needed for each combination of power plant and co-fring rate.

The system boundary of CUBE excludes indirect land use change. This exclusion is reasonable when considering emissions attributable to corn stover, an agricultural residue, for individual power plants acting in isolation (Taheripour and Tyner [2013](#page-10-24)). The system boundary does include GHG sources such as $N₂O$ release from volatilization of fertilizer; direct emissions from agrochemical production and application, cultivation, transportation, and processing; and other minor sources such as emissions due to storage losses.

Assumptions about the production scenario within CUBE are harmonized with the supply function analysis where required (e.g., harvest ratio, yield). Because resource availability was derived from actual corn production acreages in the supply curve analysis, it is assumed that all production occurs on existing row crop land when assessing GHG emissions from soil and root carbon storage. This includes carbon from emissions associated with nutrient replacement (Anderson-Teixeira et al. [2009\)](#page-10-25). If future renewable energy policies strongly incentivize land use change for production of biomass for electrifcation, this assumption should be revisited. Other management practices impacting GHG emissions, such as passive feld drying and low-loss storage methods (e.g., covered bales), are taken from the default production scenarios prescribed by the CUBE model.

Table 4 Incremental costs associated with co-fring biomass (\$ per kWh). Source: Ortiz et al. [\(2011](#page-10-0))

Results and discussion

Figure [3](#page-4-0) presents an intermediate result, the collection radius required to source the necessary quantity of biomass to achieve a 5%, 10%, or 20% co-fring rate. Even under the 20% co-fring rate scenario, the clear majority of power plants are able to source sufficient biomass from within a 50 km radius. This may be an artifact of using the MISO region as the study domain, which overlaps heavily with major corn-producing states. In other parts of the world where corn is not the dominant crop (or in the case of analyzing other biomass feedstocks), a larger collection radius may be required.

Table 5 Summary of abatement costs by co-fring rate

Co-Firing rate	Median	Average	Standard Deviation
5%	\$119.94	\$123.71	\$31.63
10%	\$56.85	\$64.43	\$24.73
20%	\$41.29	\$49.20	\$23.37

The estimated abatement costs (\$ per metric ton CO_2 –eq) are provided in Table [5](#page-6-0) (median, average, and standard deviation), as summarized over all 71 power plants in the data set.

Abatement costs decrease substantially for higher co-fring rates, due to incremental capital costs that decline on a per-kWh basis when co-fring greater quantities of biomass. The full distribution of abatement costs over the 71 power plants is shown in Fig. [4,](#page-6-1) with the same values mapped geospatially along with the size of the plant in Fig. [5](#page-7-0).

As noted in the Introduction section, many diferent factors could lead to variation in the abatement costs by power plant, such as power plant characteristics (e.g., average fuel costs, production capacity), or geospatial variation in feedstock yields or corn production density. To examine this, further analysis of the abatement costs as a function of explanatory variables such as these is necessary.

Figure [6](#page-8-0) shows the estimated abatement cost for each power plant at co-fring rates of 5%, 10%, and 20%, as a function of the local corn yield. As suggested visually, the relationship between corn yield and the cost of reducing GHG emissions through co-fring is insignifcant when controlling for the co-fring rate (Pearson correlation values of

Fig. 4 Histogram of abatement costs by co-fring rate

Fig. 5 Abatement costs (\$ per metric ton CO_2 -equivalent) by power plant and co-fring rate. The size of each dot indicates the net generation (MWh) of the plant in 2016

−0.11, −0.08, and −0.07 at co-fring rates of 5%, 10%, and 20%, respectively).

Similarly, abatement costs appear to have little correlation with the size of the required collection radius (after controlling for the chosen co-fring rate). Perhaps this is not surprising, as the collection radius is partially determined by the local corn yield and the co-fring rate (in addition to the production density of corn and the size of the power plant). Further refnement of the analysis could develop a better measure of local corn production density to test whether it can explain more of the variance in abatement costs. However, this may not be the case,

as production density is likely to be somewhat correlated with local yields.

Figure [7](#page-8-1) examines the relationship between the size of the power plant and the estimated abatement costs. The trend lines for each co-fring rate are ft using a cubic polynomial; they all have F statistics with p values less than 0.0001.

The key fndings from Fig. [7](#page-8-1) are that abatement costs are generally an increasing function of the power plant size. This is intuitive, given that larger plants would require larger quantities of biomass for a specifed co-fring rate, resulting in a larger collection area and transportation costs associated with feedstock sourcing. Visually, it appears that there may be a slight decline in abatement costs for the very largest power plants; this seems plausible if greater electricity production is correlated with marginally more expensive average fuel costs.

Figure [8](#page-9-0) portrays the relationship between abatement cost, co-fring rate, and the unit cost of coal fuel (\$ per kWh, where variation stems from the plants' fuel mixes among the four coal types reported by EIA). The trend lines in Fig. [8](#page-9-0) are also ft using cubic polynomials. Again, all three lines have F statistics with *p* values less than 0.0001, indicating a statistically signifcant relationship between the abatement cost and the unit cost of coal fuel. Abatement costs should clearly be a decreasing function of average unit fuel costs, and this is indeed observed.

Estimated Average Coal Fuel Cost (\$ per kWh)

Table 6 Regression statistics from a linear model of abatement costs

	Estimate	SE	<i>p</i> value
5% Co-fire			
(Intercept)	$1.69E + 02$	$2.34E + 01$	6.48E-10
Generation (kWh)	3.49E-09	$6.65E-10$	1.76E-06
Coal unit cost (\$/kWh)	$-1.44E + 03$	$1.55E + 02$	1.27E-13
Corn yield (bu/acre)	$-6.84E-02$	1.52E-01	6.53E-01
Collection radius (km)	$-8.07E-03$	8.33E-02	9.23E-01
10% Co-fire			
(Intercept)	$1.05E + 02$	$1.24E + 01$	4.09E-12
Generation (kWh)	1.90E-09	3.55E-10	1.16E-06
Coal unit cost (\$/kWh)	$-1.42E + 03$	$8.25E + 01$	$< 2.00E - 16$
Corn yield (bu/acre)	$-1.64E-02$	8.10E-02	8.40E-01
Collection radius (km)	2.78E-02	3.90E-02	4.78E-01
20% Co-fire			
(Intercept)	$8.81E + 01$	$9.91E + 00$	6.85E-13
Generation (kWh)	1.48E-09	$2.83E-10$	1.89E-06
Coal unit cost (\$/kWh)	$-1.42E + 03$	$6.49E + 01$	$< 2.00E - 16$
Corn yield (bu/acre)	$-3.80E-04$	6.45E-02	9.95E-01
Collection radius (km)	3.94E-02	2.76E-02	1.59E-01

Putting the various covariates together in a simple linear model, instead of plotting them separately from one another, yields similar fndings. Table [6](#page-9-1) presents the regression coefficients, standard errors, and *p* values associated with net electricity generation, unit coal costs, corn yields, and the size of the collection radius. For all co-fring rates, the electricity generation and coal unit costs are both highly statistically signifcant; conversely, the corn yield and collection radius are not statistically signifcant at the 0.05 level for any co-fring rate.

The marginal efects indicate that, *ceteris paribus*, a

Conclusion

This study examines the abatement costs associated with co-fring corn stover at existing coal-fred power plants in Midwestern states of the MISO electricity transmission region. Key fndings include considerable variability in the estimated costs of using corn stover to reduce GHG emissions. The co-fring rate, average cost of coal, and size of the power plant are the key determinants of the abatement costs, which do not appear to be particularly sensitive to variability in corn yields or the size of the collection area. While these results are specifc to co-fring corn stover with coal in the American Midwest, the conceptual model presented here is easily transferrable to other regions of the world or other biomass feedstock, provided that data are available. One should consider, however, whether other potential feedstocks should be treated as a residue or whether harvest for electrifcation would generate appreciable indirect land use change.

This work advances knowledge about real-world abatement costs for the electric power sector by incorporating spatial heterogeneity in resource availability and existing plant characteristics into integrated models of co-fring costs and life cycle GHG emissions. Future study is needed to explore additional determinants of variability and validity of the fndings to other regions and feedstocks. For example, sensitivity of the abatement cost to the feedstock yield of corn may be greater in other regions outside of the American Corn Belt due to greater variability in yield and production density. Further analysis could also be done regarding estimates of how the co-fring scenarios described here could contribute to meeting policy targets set by state renewable portfolio standards, how competition for biomass resources would impact feedstock costs, and whether renewable energy credits would be efective incentives for co-fring adoption in existing coal plants.

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Data availability Data underpinning the analysis come from publicly available sources (e.g., USDA Cropland Data Layer, US EIA). Data related to the life cycle inventory analysis come from a wide range of journal articles and technical reports, as documented in Wilson et al. ([2012](#page-11-1)).

Code availability Scripts used to generate the analysis are available upon request.

Declarations

Conflict of interest The authors have no conficts of interest to declare that are relevant to the content of this article.

Ethical approval This article does not contain any studies with human participants or animals performed by any of the authors.

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