ORIGINAL RESEARCH

Electrospun polyvinylidene fuoride/polyacrylonitrile composite fbers: fabrication and characterization

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Abstract

The purpose of this study is to make use of the advantages of both polyvinylidene fuoride (PVDF) and polyacrylonitrile (PAN) to fabricate a fexible electronic device. Polyvinylidene fuoride (PVDF)/polyacrylonitrile (PAN) composite fbrous mats with diferent blend ratios were fabricated using electrospinning. The efects of PVDF and PAN mass ratio on fber morphology, chemical structure, thermal stability, and piezoelectric properties of the produced composite fbers were investigated by scanning electron microscopy (SEM), X-ray difractometry (XRD), Fourier transform infrared spectroscopy (FTIR), thermogravimetry (TG), and piezoelectric tester. The SEM images showed that the PVDF/PAN composite nanofbers were fabricated successfully and fber diameters increased with the increase of PVDF content. The FTIR and XRD analyses showed that both the α - and β -crystal phases existed in PVDF/PAN composite fibers. The thermal stability of PVDF/PAN fibrous mats was less than that of neat PVDF fibers. The piezoelectric properties of PVDF/PAN fibrous mats were significant and a function of PVDF content. The output voltage of PVDF/PAN fbrous mats increased from 1.2 to 5.0 V as PVDF content increased from 20 to 100%. The piezoelectric voltages of PVDF/PAN composite nanofbers also increased with the increase of impacting force. Tensile and contact angle testing indicated that the PVDF/PAN fbrous mats were more fexible and hydrophilic than neat PVDF membrane. PVDF/PAN nanocomposite fber mats were observed suitable for potential application in fexible electronic devices.

Keywords PVDF · PAN · Nanocomposites · Electrospinning · Piezoelectricity

Introduction

Polymer piezoelectric material such as polyvinylidene fuoride (PVDF) was discovered in 1970s. Because of the strong polarity of C–F bond in PVDF and the combination of two fuorine atoms with one carbon atom at the same time, a great dipole moment can be formed in PVDF monomer and there are at least fve crystalline phases of alpha, beta, gamma, delta, and epsilon in this semi-crystalline PVDF polymer [[1,](#page-9-0) [2](#page-9-1)]. In general, it is just a non-polar alpha-crystal phase which exists in PVDF, which does not possess piezoelectric properties. By means of drawing or stretching [[3,](#page-9-2) [4](#page-9-3)], the incorporation of nanoparticles and other polymers [\[5,](#page-9-4) [6](#page-9-5)] and other methods [\[7](#page-9-6)], the PVDF with beta-crystal phase can be obtained, which has good piezoelectric properties. Compared with traditional piezoelectric materials, PVDF has the advantages of wide frequency response, light weight, good fexibility, and impact resistance. At present, various types of PVDF piezoelectric sensors have been developed and used in many felds such as energy converters [[8\]](#page-9-7), motion recognition [\[9](#page-9-8)], and human health monitoring [[10,](#page-9-9) [11\]](#page-9-10). However, the preparation process of PVDF piezoelectric flms is complex and costly, and the flm has high hardness and poor permeability. In contrast, electrospinning has the advantages of simple operation and low cost, and the electrospun fbers have fne diameter, and continuous and complex porous structures. Thus to fabricate soft and light PVDF membranes with good air permeability, electrospinning method is an ideal choice. At the same time, the electrospinning process integrates polarization and tension, which is beneficial to the fabrication of beta-phase PVDF piezoelectric membrane [[12](#page-9-11), [13\]](#page-9-12). In addition, considering pure PVDF membranes cannot meet the special application requirements, many efforts have been devoted to improve

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the performance of the membranes by blending diferent polymer components [\[14](#page-9-13), [15\]](#page-9-14). Among them, polyacrylonitrile (PAN) polymer is a good choice for co-electrospinning. PAN has many unique characteristics: low density, thermal stability, high strength, good chemical and microbial resistance, compatibility with DMF and DMSO, and especially good spinnability. These properties have let PAN to play a role in the production of functional electrospun materials

The main objective of this work is to present fabrication and characterization of composite nanofbers electrospun from PVDF and PAN system, and provide important basis for the selection of suitable piezoelectric material. The reports on the production of PVDF and PAN blend composite fbers by single-nozzle co-electrospinning and their piezoelectric properties and other characters are presented. The effect of PVDF and PAN mass ratio on the structure of the electrospun composite nanowebs and the resulting piezoelectric properties were studied in detail. The results can provide useful information for the development of fexible piezoelectric sensors.

Experimental

based on PAN [\[16](#page-9-15), [17\]](#page-9-16).

Materials and chemicals

Polyvinylidene fluoride (PVDF, $M_w = 1,000,000$) powder was purchased from Shanghai Sanfuai New Material Co. Inc., China. *N*,*N*-Dimethylformamide (DMF) was the analytical reagent and was purchased from Shanghai Chemical Reagent Co. Inc., China. Polyacrylonitrile (PAN, M_{w}) 50,000) powder was obtained from Shanghai Plastics Co. Ltd. (Shanghai, China).

Fabrication of PVDF/PAN composite nanofbers

Six gram of PVDF and PAN mixed powder (mass ratio of PAN to PVDF: 0:10, 2:8, 5:5, 8:2 and 10:0, respectively) was added to DMF and the mixture was stirred magnetically until the blend was dissolved completely to obtain a 12 wt% solution. Electrospinning set-up consisted of high-voltage power generator, extrusion pump, syringe (20 mL) with stainless steel needle (0.5 mm inner diameter) on the tip, and fber collector. Electrospinning of the blended solution was performed at an ambient temperature with an applied voltage of 15 kV, pumping rate of 0.8 mL/h, tip-to-collector distance of 15 cm, and collector rotational speed of 80 rpm. The nanofbers were collected on an aluminum foil wrapped on the collector. After spinning for 12 h, the fbrous mats were collected and kept at an ambient condition for further characterization.

Characterization

Scanning electron microscope (Jeol, JSM-6510LV, Japan) was used to observe surface morphology and microstructure of the electrospun fbrous mats with an accelerated voltage of 30 kV. All the samples were sputter-coated with a thin layer of gold under vacuum before the measurement.

The crystalline phase of PVDF, PAN, and PVDF/PAN nanofiber was analyzed using an X-ray diffractometer (XRD, Dmax-RA, Japan). XRD measurement was carried out at 40 kV per 40 mA with Bragg's angle 2*θ* from 10° to 90° by a step size of 0.02°.

The chemical structure was confrmed further by Fourier transform infrared (FTIR) spectra of PVDF, PAN, and PVDF/PAN fbrous mats using Avtar360 (TENSOR 27X, Bruker, German). FTIR spectrum of all samples was collected from wavenumber 400 to 4000/cm with a resolution of 4/cm within 32 scans.

Thermal decomposition property of PVDF, PAN, and PVDF/PAN fbrous mats was characterized by thermal gravimetric analysis (NETZSCH STA409PC, German). The TG and DTG curves were recorded starting from the ambient temperature to 800 °C with a heating rate of 20 °C/min. The fowing rate of protective nitrogen was 50 mL/min.

To evaluate the piezoelectric performance of the PVDF/ PAN electrospun mats, a self-made free-falling sphere device was used to connect the oscilloscope to form a piezoelectric testing device. The testing device is schematically shown in Fig. [1.](#page-1-0) The fibrous mats were cut into 1×1 cm² pieces and connected on both the sides with the oscilloscope electrode wire. The nanocomposite was mechanically impacted by a small steel hammer with adjustable mass. When the small steel ball falls freely from the catheter onto the surface of the sample, the positive and negative poles of the oscilloscope will transmit the electric signal to the oscilloscope for processing and analysis. The initial position of the small ball is 10 cm from the base and the whole reaction process lasts for 7 ms. The measurement was repeated three times for each sample and the average value was obtained.

Fig. 1 Schematic representation of the piezoelectric test device

Mechanical properties were determined by a dynamometer (Instron 5566, United States). The tests were performed with a fxed gauge of 20 mm at a loading velocity of 10 mm/ min at ambient.

The contact angle of PVDF/PAN composite fber membrane was measured by a contact angle meter (SL200C, Shanghai Shenrui Instrument Co., Ltd., China) with stationary droplet method. The measurement was repeated three times for each sample and the obtained average values of measurements were reported.

Results and discussion

SEM observation

SEM imaging was used to characterize the nanofiber morphology and structure. The SEM images of electrospun PVDF, PAN, and PVDF/PAN mats are shown in Fig. [2.](#page-3-0) These images were also analyzed using Image Pro Plus measurement tool to determine the average of fber diameters. It can be clearly seen that continuous nanofbers were produced and fbers are cylindrical and fne with a relative smooth surface. Several beads can be seen in the webs of the composite fber with a mass ratio of 8:2 (PAN:PVDF). The density of PVDF/PAN composite fber with a mass ratio of 5:5 appeared greater, with rougher fber surfaces compared to the other two composite fber webs. SEM images were used to obtain the average fber diameter by analyzing at least 100 fbers using Image Pro Plus. As it can be seen in Fig. [2,](#page-3-0) the diameters of all fber samples centered in the nanoscale. Pure PAN (Fig. [2](#page-3-0)a) has the narrowest fber diameter distribution and the fnest fbers, most of the fber diameters are in the range of 400–500 nm. As Fig. [2b](#page-3-0)–d shows, the diameter distribution of PVDF/PAN composite fbers becomes broader and there is an increasing trend in the average values as PVDF content increased. The diferences may be caused by the changes of the concentration and viscosity of the blended solution.

XRD analysis

An X-ray difraction measurement was used to obtain more insight into the structure of the composite nanofbers. The XRD patterns of the composites nanofbers containing different PVDF mass ratio are shown in Fig. [3.](#page-5-0)

PVDF belongs to polycrystalline polymer and has three different crystalline phases $(\alpha, \beta, \text{ and } \gamma)$. As shown in Fig. [3](#page-5-0)a, pure PAN has one wide peak at $2\theta = 16$, and pure PVDF (Fig. [3](#page-5-0)e) has three distinct peaks in its spectrum. It is known from the literature that the difraction peaks of 2*θ* in the range of 10–45 correspond to the crystal plane from small to large in tahe order of *α*(100), *α*(020), *α*(110), *β*(110,200),

α(021), *α*(130), *α*(210) [\[18\]](#page-9-17). Thus the peaks in the pattern of pure PVDF have been centered at $2\theta = 14.1$, 16.9, and 20.5 corresponding to reflections of $\alpha(100)$, $\alpha(020)$, and β [(110),(200)] PVDF crystalline phases, respectively [[19](#page-9-18)]. This is consistent with the previous report that the beta-crystalline PVDF fbers can be obtained directly from PVDF solution by electrospinning [[20\]](#page-9-19). It is also proved that the electrospinning is a simple and efective method for producing beta-crystalline PVDF fber membranes. As shown in Fig. [3d](#page-5-0), the composite mat with mass ratio of 2:8 (PAN:PVDF) displays strong peaks located at 2*θ*=13.9° and 16.7° and two weak peaks at 20.0° and 25.6°, implying the dominance of α phase and coexist with a small quantity of *β* phase. As shown in Fig. [3](#page-5-0)c, after enlargement, it can be seen that the PVDF/PAN composite mat with mass ratio of 5:5 displays two peaks: one broad peak at 2*θ*=17.2° and one clear peak at $2\theta = 20.4^{\circ}$, which may be due to the amorphous halo of PAN and *β* phase of PVDF, respectively. Whereas, the peak for β -crystalline phase is hard to see in Fig. [3b](#page-5-0). The composite mat with PAN and PVDF mass ratio 8:2 just shows strong reflections located at $2\theta = 14.1^\circ$ and 16.9° and a weak peak at 25.5°, implying the dominance of α phase. The change of PVDF-crystalline phase type in the composite fiber was due to the introduction of PAN, affecting the formation of large-sized crystalline grains in polymer blends.

FTIR study

FTIR is sensitive to the conformation and changes in the molecular region of polymers. Diferent crystalline phases absorb diferent infrared wavelengths; thus, FTIR can be used to analyze the structure of crystalline polymers. Typical FTIR spectra of PAN, PVDF/PAN, and PVDF fbrous mats are presented in Fig. [4.](#page-6-0) Figure [4](#page-6-0)a shows that the typical peaks of PAN spectrum have been centered at about 2240, 2942, and 1448/cm, corresponding to –C≡N bond stretching vibration, $-CH₂$ bond asymmetric and symmetric bending vibrations, respectively. The PAN characteristic peaks have also been displayed in the spectrum of PVDF/PAN fbrous mats (Fig. [4b](#page-6-0)). The characteristic peaks in PVDF/PAN samples spectra at 1401 and 1178/cm are strengthened, ascribing to the C–H bond bending vibration and C–F bond stretching vibration, respectively. Spectrum results indicated that the PAN and PVDF structures are reserved in the composite fber, and PAN and PVDF have a good adaptation.

According to the literature $[21]$ $[21]$ $[21]$, the characteristic peaks at 1383, 976, 853, 796, 762, 612, and 530/cm correspond to the *α* crystal form of PVDF, and those at 1278, 839, 510, and 471/cm correspond to the *β* crystal form. As shown in Fig. [4](#page-6-0)c, the peak observed at wavenumber 769/ cm is assigned to α phase with chain conformations of short trans-sequences. The peaks appearing at wavenumbers 1275, 836, 509, and 475/cm correspond to the *β* phase with long

Fig. 2 SEM images of electrospun webs: **a** PAN; **b** PAN:PVDF=8:2; **c** PAN:PVDF=5:5; **d** PAN:PVDF=2:8; **e** PVDF

Fig. 2 (continued)

trans-sequences. The FTIR spectra of PVDF/PAN composites (Fig. [4](#page-6-0)d) exhibited almost the same spectral features as PVDF, regardless of the PAN content. By observation of the relative intensity of the beta peaks, there is an increasing trend with the increase of PVDF content. The results indicate a good consistency between those of the FTIR and X-ray difraction testing. It is known that the piezoelectric properties come from the β phase of the PVDF. The results from XRD and FTIR measurement indicate that the PVDF/ PAN composite mats have potential piezoelectric functions.

Thermal stability

The relationship between mass residues and temperature was measured to investigate the thermal stability of neat PAN, PVDF/PAN nanocomposites and neat PVDF by means of TG and DTG as displayed in Fig. [5](#page-7-0). As it is evident in Fig. [5](#page-7-0), there are two main thermal degradation areas with about 50% weight loss for neat PAN and $PAN: PVDF = 8:2$ composite fibers: the minor one between 280 and 330 °C and the major one between 370 and 460 °C, which was attributed to the volatilization of gaseous compounds during the heating process. For PVDF/PAN composite fber with mass ratio of 5:5 and 2:8, a major wide mass degradation peak happened between 280 and 460 °C. For neat PVDF, one major sharp mass degradation peak was observed between 410 and 500 °C. The decomposition of all samples was nearly completed at 500 °C. Thermal stability can be judged by the initial decomposition temperature and thermal degradation temperature at 5% mass loss [\[22\]](#page-9-21). Considering these two parameters, the composite fber with higher PVDF content shows better thermal stability than neat PAN nanofber.

Fig. 3 XRD patterns of electrospun fbrous mats: **a** PAN; **b** PAN:PVDF=8:2; **c** PAN:PVDF=5:5; **d** PAN:PVDF=2:8; **e** PVDF

Mechanical properties

The mechanical properties of the nanofiber mats were measured and the tensile stress–strain curves of the electrospun mats are presented in Fig. [6.](#page-7-1) It can be seen that the PVDF, PAN, and PVDF/PAN mats show typical thermoplastic behavior. Comparing them with a neat PAN fber mat, PVDF and PVDF/PAN composites present stifening characteristics such as greater elastic modulus and less elongation-at-break. Compared with polyvinylidene fuoride (PVDF), the fexibility of PAN is more prominent. The mechanical properties of the electrospun mats are a result of the complex efect of many parameters such as average fber diameter value, diameter distribution, porosity, and the degree of polymer

Fig. 4 FTIR spectra of electrospun PVDF/PAN fbers: **a** PAN; **b** PVDF/PAN composite mats; **c** PVDF; **d** enlargement of spectra of PVDF/PAN composite mats

crystallinity, thus PVDF/PAN composite nanowebs have complex mechanical behavior. Generally, though the addition of PAN may decrease the piezoelectric function, the fexibility of the composite mats can be improved and the obtained composites could be more suitable for applying in polymer electrolytes in self-power devices.

Hydrophilicity

The water contact angles measured for all samples are presented in Fig. [7.](#page-7-2) Since the molecular chains of PVDF are composed of hydrocarbon bonds and CF bonds, the hydrophilicity of pure PVDF fbrous mat is poor due to the absence of hydrophilic groups. The measured water contact angle is as high as 133. While the cyanogen group with hydrophilicity exists in PAN molecule, with the increase of PAN content, the contact angle begins to decrease till 116 when the mass ratio of PAN and PVDF reaches 8:2. Therefore, the hydrophilicity of PVDF/PAN nanocomposites can be adjusted by the addition of PAN.

Piezoelectricity

A steel ball of 5.61 g was used to impact the PVDF and PVDF/PAN nanocomposite fibrous mats between two metal electrodes, and the output voltage measured by the oscilloscope is shown in Fig. [8](#page-8-0). When the fbrous membrane was impacted by the small steel ball, the elastic deformation caused the change in dipole of the beta crystal of the fber and produced the piezoelectric efect. The voltage curve corresponds to three states of impacting process: original state, compression state, and rebound

Fig. 5 Thermograms of electrospun PVDF/PAN fbers: **a** thermogravimetric (TG) analysis, **b** derivative thermogravimetric (DTG) curves

Fig. 6 Mechanical stress–strain curves of electrospun fbrous mats

Fig. 7 Contact angle of electrospun PVDF/PAN composites

state. Before the sphere reaches the surface of the fbrous mat, there is no potential diference between the two ends of the fbrous mat and the voltage value is zero. When the sphere contacts the surface of fbrous mat, the fbrous mat is impacted by a small ball and begins to compress downward, resulting in a negative voltage. Since the deformation of the fbrous mat belongs to elastic deformation, when the velocity of the ball decreases to zero, the fbrous mat begins to rebound and the voltage signal turns into a positive voltage. As the deformation rate increases gradually, the positive voltage gradually increases to the maximum value. It is obvious that the output voltage of the generators increases from 1.2 to 5.0 V with the increase of PVDF content in the fbrous mats from 20 to 100%. These outputs can be compared to the voltage output of previous literature $[23]$ $[23]$. The more efficient electrical outputs can be interpreted by higher *β*-phase crystallinity in PVDF/PAN composite fber.

To investigate the efect of impact pressure on the piezoelectricity, the steel ball with diferent masses was used on the PVDF/PAN composite fber with a mass ratio of 2:8 (PAN:PVDF). The results are shown in Fig. [9](#page-8-1). The increase of ball mass resulted in a greater compression force and rebound force on the nanofbrous mat; therefore, the negative voltage during the compression process and output positive voltage during rebound process increase correspondingly. The piezoelectric response process also becomes longer. When the mass of the small ball is 14 g, the maximum voltage value reaches 9 V. Excellent piezoelectricity can produce micro-current efect, which indicates that the PVDF/PAN composites can be used as a potential electrical generator and to charge portable electronic devices.

Fig. 8 Piezoelectric voltages of PVDF/PAN fbrous mats

Fig. 9 Efect of small ball mass on piezoelectric voltages

Conclusion

PVDF has displayed an effective approach towards textile fexible sensor. Electrospinning of PVDF and other polymers with good spinnability provides a new method for fabrication of piezoelectric membrane. Based on these, PVDF/PAN nanocomposites were fabricated using electrospinning successfully. Performance characterizations indicated that the addition of PAN reduced the toughness and water repellency of the nanocomposites. The thermal stability of PVDF/PAN fbers was similar to that of neat PAN nanofbers. XRD and FTIR analyses showed that the electrospun PVDF and PVDF/PAN fibrous mats possessed β-phase crystalline structure. Neat PVDF and PVDF/PAN nanocomposites demonstrated good piezoelectricity. The piezoelectric properties of PVDF/PAN nanocomposites could be adjusted through PVDF and PAN mass ratio. The electrical outputs of PVDF/ PAN were related to the impact force. Electrospun PVDF/ PAN nanocomposite fber mats demonstrate a promise for potential application in fexible wearable electronic devices.

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References

- 1. Ruan L, Yao X, Chang Y, Zhou L, Qin G, Zhang X (2018) Properties and applications of the β-phase poly(vinylidene fuoride). Polymers 10:1–27
- 2. Gregorio R (2006) Determination of the α, β , and γ crystalline phases of poly(vinylidene fuoride) flms prepared at diferent conditions. Proteomics 100:3272–3279
- 3. da Silva AB, Wisniewski C, Esteves JVA, Gregorio R (2010) Efect of drawing on the dielectric properties and polarization of pressed solution cast beta-PVDF flms. J Mater Sci 45:4206–4215
- 4. Du CH, Zhu BK, Xu YY (2007) Efects of stretching on crystalline phase structure and morphology of hard elastic PVDF fbers. J Appl Polym Sci 104:2254–2259
- 5. He LH, Qun X, Hua CW, Song R (2010) Efect of multi-walled carbon nanotubes on crystallization, thermal, and mechanical properties of poly(vinylidene fluoride). Polym Compos 31:921–927
- 6. Sun J, Yao L, Zhao QL, Huang J, Song R, Ma Z, He LH, Huang W, Hao YM (2011) Modifcation on crystallization of poly(vinylidene fuoride) (PVDF) by solvent extraction of poly(methyl methacrylate) (PMMA) in PVDF/PMMA blends. Front Mater Sci 5:388–400
- 7. Song R, Liu X, Wang HF, Xia GM, He LH, Wang Y, Huang W, Zhao QL (2014) Enhanced beta phase of polyvinylidene fuoride with addition of polyamide 6: role of interfacial interactions. Colloid Polym Sci 292:817–828
- 8. Zabek D, Taylor J, Le Boulbar E, Bowen CR (2015) Micropatterning of fexible and free standing polyvinylidene difuoride (PVDF) flms for enhanced pyroelectric energy transformation. Adv Energy Mater 5:1401891
- 9. Dong WT, Xiao L, Hu W, Zhu C, Huang YA, Yin ZP (2017) Wearable human–machine interface based on PVDF piezoelectric sensor. T I Meas Control 39:398–403
- 10. Lopes AC, Gutierrez J, Barandiaran JM (2018) Direct fabrication of a 3D-shape flm of polyvinylidene fuoride (PVDF) in the

piezoelectric beta-phase for sensor and actuator applications. Eur Polym J 99:111–116

- 11. Fu YM, He HX, Zhao TM, Dai YT, Han WX, Ma J, Xing LL, Zhang Y, Xue XY (2018) A self-powered breath analyzer based on PANI/PVDF piezo-gas-sensing arrays for potential diagnostics application. Nano Micro Lett 10:1–12
- 12. Motamedi AS, Mirzadeh H, Hajiesmaeilbaigi F, Bagheri-Khoulenjani S, Shokrgozar M (2017) Effect of electrospinning parameters on morphological properties of PVDF nanofbrous scafolds. Prog Biomater 6:113–123
- 13. Gee S, Johnson B, Smith AL (2018) Optimizing electrospinning parameters for piezoelectric PVDF nanofber membranes. J Membr Sci 563:804–812
- 14. Xing J, Ni QQ, Deng BY, Liu QS (2016) Morphology and properties of polyphenylene sulfde (PPS)/polyvinylidene fuoride (PVDF) polymer alloys by melt blending. Compos Sci Technol 134:184–190
- 15. Sun D, Yue DM, Li BB, Zheng ZS, Meng XC (2019) Preparation and performance of the novel PVDF ultrafltration membranes blending with PVA modified $SiO₂$ hydrophilic nanoparticles. Polym Eng Sci 59:E412–E421
- 16. Sidorina AI, Druzhinina TV (2016) Macrostructure of polyacrylonitrile nanofbers produced by electrospinning. Fibre Chem 47:362–366
- 17. Choi S, Kim HR, Jeong YK (2018) Mechanism of electrospinning for poly(amic acid)/polyacrylonitrile fber fabrication. J Macromol Sci Part B Phys 57:222–230
- 18. Guo ZW, Nilsson E, Rigdahl M, Hagström B (2013) Melt spinning of PVDF fbers with enhanced β phase structure. J Appl Polym Sci 130:2603–2609
- 19. Hossein F, Mohammad MA, Parastoo S, Nima Z, Li QX, Minoo N (2016) Morphological changes towards enhancing piezoelectric properties of PVDF electrical generators using cellulose nanocrystals. Cellulose 23:3625–3637
- 20. Neppalli R, Wanjale S, Birajdar M, Causin V (2013) The efect of clay and of electrospinning on the polymorphism, structure and morphology of poly(vinylidene fuoride). Eur Polym J 49:90–99
- 21. Layek RK, Samanta S, Chatterjee DP, Nandi AK (2010) Physical and mechanical properties of poly(methyl methacrylate)-functionalized graphene/poly(vinylidine fuoride) nanocomposites Piezoelectric beta polymorph formation. Polymer 51:5846–5856
- 22. Gaur MS, Indolia AP, Rogachev AA, Rahachou AV (2015) Infuence of $SiO₂$ nanoparticles on morphological, thermal, and dielectric properties of PVDF. J Therm Anal Calorim 122:1403–1416
- 23. Wang G, Liu T, Sun XC, Li P, Xu YS, Hua JG, Yu YH, Li SX, Dai YZ, Song YX, Lv C, Xia H (2018) Flexible pressure sensor based on PVDF nanofber. Sens Actuator A Phys 280:319–325