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Evolution of Outrigger Structural System: A State‑of‑the‑Art Review

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Abstract

This paper presents the development of the outrigger structural system from the conventional outrigger to damped outrigger concepts. Outrigger structural system development from the conservative design as a rigid connection to a virtual connection with passive control, active control system, semi-active control system to hybrid control system is deliberated. Following brief overviews on history of outriggers, types of the outrigger, analysis of tall buildings without outriggers, formulation of equations for outrigger structure to simplify analysis are elaborated. Diferent approach to locate optimum positioning of outriggers in tall structure is elucidated. Analysis of outrigger to study its behavior in high-rise buildings using diferent methods is stated, and review on the damped outrigger system is explicated. This paper tries to highlight the advantages of outrigger structure with semi-active control and performance enhancement of the outrigger system with the efective devices, and enhanced results are also depicted. This review also paves a way for the new area of research in structural control with the incorporation of smart devices and smart technology.

Keywords Outrigger · Tall building · Dampers · Controllers · Structural response · Semi-active

1 Introduction

Today, increase in the worldwide population and the present trend of people moving toward cities has increased the scarcity of living space within cities which in turn demands the small space occupancy with a large population. This stimulates the demand for the ratio of small space to the large tenancy and triggering the construction of tall slender skyscrapers. In modern cities, tall buildings are a common prospect, as they proffer a high ratio of floor space per area of land, especially in those countries where land is inadequate. Tall buildings are also, arguably, a sign of a city's economic loftiness, and these structures are always prone to lateral forces like wind and earthquake. Unpredictable wind action can cause oscillatory activities and infuence an extensive range of responses in building occupants, mild discomfort to acute nausea, buildings become undesirable is elucidated by Smith [\[1](#page-15-0)]. The risk associated with tall buildings for seismic ground motion is very high since all tall buildings often accommodate thousands of occupants, and because of the unpredictable nature of earthquakes, particular attention has to be given to the design. It is conceivable that the structural collapse of such buildings can lead to disasters of unacceptable proportions. Preliminary analysis to fnd the natural frequency, mode shapes, and primary structural parameters is important in design, where most of the time the approximate methods are used like continuum method by considering Euler–Bernoulli or Timoshenko beam theory. Rahgozar [[2\]](#page-15-1) has introduced the novel approximate method in mathematical modeling of structure to fnd the preliminary structural parameter based on the energy method and Hamilton's principle. There is a need to introduce novel and simplifed methods for the preliminary design approaches in structural system. Another important topic is the resistance of lateral forces that includes wind and earthquake forces that are dominantly considered in design of structures. Various structural systems have been introduced in tall buildings to overcome the lateral and vertical loads. These structural systems are divided into exterior and interior structural systems. The exterior structural systems such as the tube, framed tube, braced tube, bundled tube, tube-in-tube, diagrid, space truss,

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super-frame, and exoskeleton are explicated by the author in the article $[3, 4]$ $[3, 4]$ $[3, 4]$ $[3, 4]$ as shown in Fig. [1](#page-1-0).

The interior structural systems are the moment-resisting frame, braced frames, concentrically braced frames, shear walls, rigid frame, frame tube, braced tube, bundled tube, and outrigger systems that can be used to enhance the lateral resistance in tall buildings as presented by Choi et al. [\[5](#page-15-4)] as shown in Fig. [2](#page-2-0). Because of innovation of new design concepts and construction technologies, massive structures are being constructed across countries in their major cities, such as Taipei 101 in Taiwan, Shanghai's World Finance Center in China, Petronas Twin Towers in Malaysia, and the ultimate skyscraper, Burj Dubai, with a fnal projected height of more than 800 m is presented by the article [[6\]](#page-15-5) including the antenna is presented by the article [[7\]](#page-15-6), Fig. [3](#page-3-0) represents world's tallest building with the height and name of the building [\[8](#page-15-7)]. Alhaddad et al. [\[9](#page-15-8)] has given a comprehensive introduction on outrigger usage in the tall building; detailing about building name, location, height, material, and outrigger usage is tabulated in the study.

Modernization toward the gigantic structures toward sky and preference to the most lightweight structure have increased risk of fexibility and probably diminished damping can lead the structure to become more susceptible to wind action [[4\]](#page-15-3). To meet this requirement, the structure is designed to meet the requirements of ultimate strength and serviceability drift, but the structure is not free from levels of motion that can cause serious discomfort to its occupants. Therefore, there is a need to control the structure for structural safety and its occupants.

Rigorous research has been carried out to use smart systems for smart structures to quantify a building's acceleration to ensure that the building remains serviceable without causing disturbing motions to its occupants is presented in the article [\[10](#page-15-9)]. Simple methods for the structural analysis are needed; so Alavi et al. [[11\]](#page-15-10) developed a framework for combined structural and control optimization considering structural mass and linear quadratic regulator performance index as objectives. This approach combined structural and control variables as a single objective function linearly,

Conjoined Towers

Fig. 1 External structural system [\[4](#page-15-3)]

Fig. 2 Interior structures [\[4\]](#page-15-3)

and the variable neighborhood search (VNS) metaheuristic method was adopted because of complexity. This combined method adopted by the authors in [[11\]](#page-15-10) delivers superior dynamic performance compared to the sequentially optimized cases. Research needs to be developed for fnding the structural forms and efective ways to reduce uncontrolled lateral forces.

Some of the research has the core wall system that performs efectively in the reduction in structural responses like story drift, displacement, acceleration, etc., for the wind and earthquake loads as stated by authors in [\[12](#page-15-11)]. The core systems themselves offer enough confrontation to the overturning, but drift increases approximately to the cube of the height of the building $[12]$ $[12]$. Therefore, the height of the building makes the core wall system inefficient, and when the building height increases, stifness of the core decreases, becomes insufficiently stiff to the wind load, and fails to bring down the wind drift to an acceptable limit [[13](#page-15-12)]. To stabilize the tall structure, the concept of outriggers was introduced which was earlier used in canoes to stabilize it; so that the same behavior is mimicked in tall structural control. Outriggers are the stif beam that connects the core of the structure to the perimeter column which has the advantage of mitigating the movement of the core, in turn, reduces the drift at the top floor in comparison with the structure without outriggers as stated in [[5\]](#page-15-4). Ho [[14\]](#page-15-13) has provided a review on the concept of the outrigger system, optimum topology in construction, and its application in structural control. So in

Fig. 3 Comparative heights of world's tallest buildings [[8\]](#page-15-7)

this study, a brief evolution of the outrigger structure over the period is discussed in Sect. [2](#page-3-1), and developments of outrigger structural systems from tall buildings to the recent concept of damped outrigger in the structural control involving smart devices are explicated in Sect. [3](#page-5-0).

2 Overview of Outrigger Structure

The concept of the outrigger started from its use in canoes. The archeological evidence shows that Austronesia's migrated from Southeast Asia sometime between 40,000 and 30,000 years ago. This was during the last ice age of the Pleistocene Era, which started 70,000 years ago and ended 10,000 years ago. This outrigger was introduced for rollover stabilization of canoes, and its concept is explained in terms of feedback mechanism. The feedback mechanism criteria are satisfed, i.e., it enhances the roll stability of the canoe, it provides negative feedback, it is a separate element from the canoe. Figure [4](#page-3-2) shows canoes with outriggers. The main hull of the canoes with outrigger will be narrow compared to the plank-built vessel as stated in the article [[15](#page-15-14)]. This concept of outrigger present in canoes system also can be used for other systems which require the roll stability. Thus, outrigger can be used for the tall slender structural system where the core with the outrigger will mitigate the top drift and stabilize the overturning moment.

Historically, outriggers are used for the slimmer system as in the case of canoes to resist wind, it can be considerably used in skyscrapers which are having a slender and tall core that is afected by the wind. The use of outriggers in highrise buildings started about 5 decades ago as stated in the article [[15\]](#page-15-14). Smith and Salim [\[16](#page-15-15)] stated that the frst outrigger building was designed by Barbacki which was 47 stories, Place Victoria Building in Montreal Canada, completed in 1962. This outrigger braced structure acts as a single structure in a combination of outriggers connected to the core wall and perimeter column when excited by lateral loads

like wind and earthquake. Likewise, in the cases where the core of tall buildings cannot handle the lateral load alone, outriggers reduce the moment in the core by transferring part of it to the outer columns in the form of axial forces consisting of compression-tension couples as stated in the article [[3\]](#page-15-2). Eventually, the core will no longer act as a pure cantilever. A belt truss can be used to help to distribute the forces to a larger number of columns and to reduce the differential corners that can support the outriggers as well. Even though outriggers are internal structures, the contribution to belt trusses and mega columns represents a large planner spread of the building stresses. Another advantage of an outrigger structure is that closely spaced columns are not needed which allows fexibility in meeting building functional requirements as presented in an article [[17\]](#page-15-16). Previous studies demonstrate a possibility that designing the belt truss is not only to resist the lateral load but to mitigate possible disproportionate collapse caused by extreme events. Other research works state the usage of buckling restrained bracing members in an outrigger to increase the energy dissipation besides the extra stifness as explained in [[18](#page-15-17)]. Since outriggers are added to the dual structural system (shear walls and frames) aiming for extra stifness, the location of those outriggers will have a major impact on the whole building behavior as stated by authors in the article [\[19\]](#page-15-18). Therefore, most of the studies were oriented toward fnding the optimal location of the outriggers in the tall building against applied loads using all possible approaches as stated in [\[19](#page-15-18)]. Taranath [\[20\]](#page-15-19) stated that by the introduction of outriggers in the structure, its stifness increases by 20 to 30 percent. Thus, in the massive structures, outriggers have been introduced which can be constructed out of reinforced concrete or steel-braced core which are linked to the perimeter column by a flexural stiff horizontal beam at an optimal location. The introduction of these outriggers increases the lateral fexural resistance to the building, it does not increase the shear stifness and the core itself will carry all the lateral shear forces as illustrated in [\[21](#page-15-20)]. The advantages of outriggers are presented in article [\[22\]](#page-15-21), they will decrease the lateral moment of the structure, the overturning moment of the core is reduced which will reduce the uplifting of the core, which will decrease foundation cost. In a rectangular plan of the structure, the outrigger adds the interior gravity column as lateral load resisting elements intern the economy of the structure can be achieved. Also, the outrigger can be in many structural forms like the tube-in-tube, frame tube, core wall, and shear wall system with the outer column. The addition of an outrigger in the system will increase the stifness of the system; will also make axial stress distribution in a column that leads to a decrease in shear lag efect as stated in the article [[9\]](#page-15-8). Damped outrigger concept also has advantages like reducing force induced in the component of control elements in the structure and involves in reducing material usage in construction adding to the economy. Article [\[9](#page-15-8)] states few discomforts like diferential shorting and no repetitive construction sequence because of the outrigger at the diferent levels and construction practice sluggish down. As the number of outriggers increases in tall buildings, its construction cost increases with the difficulty of the construction sequence. There are some other disadvantages like irregular stifness is distributed within the foors of the structure because of outrigger that produces weak stories near the outrigger levels.

Considering all advantages and disadvantages of outrigger structure, there are diferent types of outrigger depending on the structural material used, the connection of external and internal systems, and depending on its response [[9](#page-15-8)]. Depending on structural material, there are steel outrigger, concrete outrigger, and composite outrigger. Depending on the connection and response of the outrigger, there are rigid (conventional) outrigger, fexible outrigger, damped outrigger, yielding outrigger, offset outrigger, and virtual outrigger [\[9\]](#page-15-8). Article [[23\]](#page-15-22) states that the conventional outrigger concept is based on the planar concept with the interactions between the core walls, the outrigger arms, and the exterior columns. In this system, outriggers are directly connected to the core shear wall or braced frames at the core and the perimeter column at the exterior end. This system when imposed with lateral loading acts along the plane of the outrigger bent, the bending of the core rotates the stif outrigger arms that cantilever from it, inducing tension in the upwind column and compression in the downwind column. These column forces, acting at the extremities of the outrigger arms, form a couple that restrains the bending and defection of the core. Article [\[23](#page-15-22)] states that when outriggers are not placed in the plane with the core walls, but it adopts all the advantages, and by reducing some of the disadvantages of conventional outriggers a new type of outrigger is produced, called an offset outrigger. The offset outrigger states that the offset is taken from the core wall, and the outrigger is placed horizontally within the floor plan. Eom et al. [[24\]](#page-15-23) analyzed the virtual outrigger as distributed belt wall system to comprehend the behavior of the structure. The article [\[24](#page-15-23)] has made a study on belt walls made of the reinforcing method using high-strength pre-stressing strands subjected to high shear demand, and compression feld theory was used to fnd the shear strength of pre-stressing strands. The authors concluded that the drift of the structure is reduced as efectively as conventional belt and outrigger systems with the correct arrangement and number of belt walls. The output recommends that the shear design of the pre-stressing strands belt walls depends on the cracking strength; its shear resistance can be increased by using an increased pre-stressing and reinforcing ratio [\[24](#page-15-23)]. Figure [5](#page-5-1) shows a typical floor plan of the conventional outrigger, ofset outrigger, and alternative offset outrigger.

Fig. 5 Plan of **a** Typical foor plan, **b** Conventional outrigger, **c** Ofset outrigger, **d** Alternative offset outrigger [\[23\]](#page-15-22)

Fig. 6 Virtual outrigger system using belt trusses [\[25\]](#page-15-24)

As seen in conventional outrigger, there is a direct connection between the core, outrigger, and peripheral column, this direct connection is not seen in the virtual outrigger concept but a diaphragm is used to transfer overturning moment from the core, which is usually very sturdy and stiff in their plane, to transfer moment in the form of a horizontal couple from the core to trusses or walls that are not connected directly to the core. This is achieved by providing belt trusses or belt walls for full depth, continuously, around the perimeter of an outrigger level as stated in [[25\]](#page-15-24) and act together with the top and bottom structural diaphragm of the outrigger level as shown in Fig. [6](#page-5-2).

Virtual outriggers provide an advantage because the direct connection between the core and outrigger is eliminated as stated in [\[23\]](#page-15-22). The outrigger structural evolution is briefy elaborated by the diferent researchers in Sect. [3](#page-5-0).

3 Development of Outrigger Structural System from Tall Buildings

A tall structure with the outrigger and belt trusses has proved to be adequate in mitigating the story drift, base shear, and base moment of the core. Therefore, research has been undertaken, the study of outrigger structural behavior under lateral load. As per the study undertaken by diferent researchers, the review on outrigger structural system can be broadly classifed as

- Analysis of tall building without outriggers by diferent approaches
- The empirical formulation for outrigger structural system
- Optimum positioning of outriggers by various methods
- Analysis of outrigger structure by different techniques
- Damped outrigger concept

Tall buildings came into existence in the late nineteenth century, which was the economic symbol of the city. These tall buildings development from a small- and medium-sized structure has taken place in the cities because of the population to the foor area ratio. The evolution of tall buildings and the technology behind the development of tall buildings are briefy discussed in the introduction. Review on tall buildings is a vast topic with the inclusion of the tall building evolution, classification of building structural system, the material used for construction, height criteria, advantage and disadvantage of the tall structural system. Ali and Moon [\[3\]](#page-15-2) illustrated all above consideration of building with damping strategy for a structural system like an active system which includes an active mass damper, active liquid column damper, and passive system which includes tuned mass damper further subdivided as pendulum type, sliding type, bearing mounted type and tuned liquid damper further subdivided as tuned sloshing damper, tuned liquid column damper. The authors also described the implementation of these devices in the tall structural system and further explained the new contemporary structural forms and their concept, their advantages, and disadvantages, their material, topology and size, number of stories, and scale of real example buildings that are coated for all the classifcation of structures with the location, and specifcation is also presented by the article [[26,](#page-15-25) [27\]](#page-15-26). The shortcoming of the tall building led to structural control practice to safeguard the skyscrapers battered by uncertainty. Soong and Spencer [\[28](#page-15-27)] presented state-of-the-art and state-of-the-practice review, alongside article [\[29](#page-15-28), [30](#page-15-29)] presented a state-of-the-art review on structural control systems including implementation of the passive and active control system in all real structural details with name, location, year, the scale of the building, control system, number and mass of control system and actuation mechanism is specifed. This is the general review which includes the passive, active, and semi-active structural control with a description of semi-active dampers like variable orifce fuid dampers, variable stifness devices, controllable friction devices, smart tuned mass dampers, and tuned liquid dampers, controllable fuid dampers, and controllable impact dampers. Initially, tall buildings are stabilized by a passive protective system by using the bracing systems of diferent combinations for the mitigation of structural response like displacement, inter-story drift, shear response, etc. To illustrate the passive control, article [\[31](#page-15-30)] adopted a genetic algorithm to determine optimum bracing system, by using *X*, *V*, and *Z* bracings with constraints as strength and serviceability. Authors proved with a design example that *V* and *Z* bracing do not show much lateral stifness as *X* bracing. As the height of the building increases, the bracing system shows sluggish resistance to lateral loading, therefore, for tall building response control, alternative methods are presented by a diferent researcher. So to improve the tall structural resistance toward lateral load, the stifness parameter and damping of the structure were studied in [[32\]](#page-15-31); presented a novel probabilistic damping model to explain amplitudedependent damping of tall buildings. This method showed that height is not a good parameter to decide to damp instead it is lateral deformation response; hence, the structural response of the tall building is important in deciding the damping capacity of tall buildings. Initially, to increase the damping of the structure, the passive damping system was designed, its mechanism depends on structural response. A passive system does not require an external power source for its works and it is easy to maintain which makes it reliable and economical. The passive damping also includes the dampers like viscous dampers, tuned mass dampers, friction devices, metallic yield devices, tuned sloshing dampers, and tuned column dampers, these dampers are expounded in the article [[10\]](#page-15-9). Many researchers studied tuned liquid damper (TLD) but article [[33\]](#page-15-32) studied the sloping bottom TLD with the slope of the bottom end at 200, 300 and 450 for a diferent type of structure, mass ratio, and depth ratio. The author found that the slope in the bottom of TLD will reduce the

structural response more than a fat bottom TLD. Another passive device exercised in the article [[34\]](#page-15-33) was tuned mass damper (TMD) in multi-story buildings which were analyzed for time history analysis in ETABS with TMD and without TMD which are excited about earthquake ground motion, and the performance comparison is made by placing it at the top of the building. Results depict that TMD reduces structural response better when placed at the top of the building. Giaralis and Petrini [\[35](#page-16-0)] further used a tuned mass-damper–inerter to upgrade the performance of existing TMD in benchmark buildings without changing the attached mass to reduce displacement. These passive devices provide control to a building to a certain extend which cannot adapt to all the uncertainty because its behavior cannot be manipulated, as it is installed permanently to the structure. TMD has some disadvantages like the requirement of huge mass and more space for installment and requires an adjustment of the frequency to fne-tune its performance in agreement with a natural frequency of the structure. To overcome the limitations of the passive system, semi-active control has been adapted instead of active control because of its reliability like passive and adaptability like active devices. A set of semi-active dampers is used in the article [[36\]](#page-16-1) for a comparative study to reduce the response of the structure by using diferent control laws and dampers like magnetorheological (MR) dampers and variable stifness tuned mass dampers. The author used optimal static output feedback control, linear quadratic Gaussian, and Passive-on controllers to actuate dampers and performance is compared in reducing seismic response mitigation. Another semi-active device stated in [\[37\]](#page-16-2), modeled a 76-story benchmark building (as described in detail by the article [[38](#page-16-3)]) with a semiactive tuned mass damper (STMD), consists of MR damper controlled by a multi-objective genetic algorithm which is optimized by the fuzzy logic controller (FLC) based on nondominated sorting genetic algorithm version II (NSGA-II) (detailed description of the fuzzy controller is given by article [[39\]](#page-16-4)). The modeling is done in MATLAB and Simulink to get peak response of the structure, and this result was compared with sky-ground hook algorithm and observed that the designed controller in this study performed better which involves numerical simulation only. Figure [7](#page-7-0) represents the physical block diagram of structural control system involving all the practical devices such as controllers and dampers with feedback and feed forward loop [[37\]](#page-16-2).

To overcome the limitation of passive control, active control, and semi-active control, a hybrid control system is adopted by the researchers to increase the efficiency of the protective system by mitigating the response of the structure presented in [[40\]](#page-16-5). The study on the response of the building is important by increasing the damping and stifness of the building. Inter-story drift is an important parameter that addresses structural behavior; Zhou et al. [\[41\]](#page-16-6) stated

Fig. 7 Physical block diagram of structural control system [\[37\]](#page-16-2)

harmful and harmless methods of calculation of inter-story drift. Cruz and Miranda [[42\]](#page-16-7) determined the damping ratio of the building considering 14 buildings in California with more than 20 stories by adopting the parametric least squares system identifcation technique. This method concluded with the result that as the height of the building increases, the damping ratio decreases, and steel structures have less damping ratio in comparison with concrete structures. This real-time building dynamic study prejudiced [\[43](#page-16-8)] to present a dynamical analysis of super tall structure Taipei 101 for earthquakes and strong typhoons; an experimental shake table test was conducted to determine the constitutive relationships between structural parameters. The time history analysis and response spectrum analysis were conducted to get lateral displacement and distributions of interior column forces, the result showed that Taipei 101 has relatively high earthquake resistance capacity and could safeguard structure during a moderate seismic event. These are some of the analyses of a tall building with diferent protective systems and various technical approaches to mitigate the response of the buildings without outriggers. In mitigating the response of the structure due to lateral load, outrigger structural systems are designed for better performance than the normal tall buildings without outriggers. Thus, the structure with the outrigger system is concentrate in the further section.

Analysis of outrigger in a tall building is complicated; thus, outrigger structural parameters are formulated to understand the behavior of outrigger structural systems and complicated analysis of the tall buildings can be done

effortlessly. Therefore, many studies are undertaken to understand the actions of tall structures with outriggers excited for lateral load, and one of the study is presented in [\[44\]](#page-16-9). Alavi et al. [[45\]](#page-16-10) proposed the new stifness-based method for the preliminary design of outrigger structure based on uniform distribution of deformation by keeping curvature of the beam constant. This proposed method was presented through a simplifed hand calculation algorithm considering only the lateral loads and output of the novel method gave normal stress distribution uniform along with building height that was lower than permissible value [\[45](#page-16-10)]. Alavi et al. [\[45](#page-16-10)] considered only the lateral load but the vertical load was not considered in the proposed method that provides a research gap in improving the stifness-based method for the tall building considering all the parameters in the analysis including a programing based output for preliminary and fnal parametric analysis. The author in paper $[16]$ $[16]$ found that the equation for core rotation, restraining moment, top drift, the optimal location of outrigger to reduce the drift, and non-dimensional parameter Ω to understand the behavior of an idealized multi-outrigger structure which is the function fexural rigidity ratio was also formulated to simplify the analysis. Figure [8](#page-8-0) shows the outrigger structural response to lateral loading and moment in the core.

The above structure is analyzed approximately by continuum approach in which the set of outriggers is smeared over the height to get closed-form solution which facilitates in producing generalized design curve as stated in the article [\[46](#page-16-11)]. This generalized design curve helps in producing

Fig. 8 a Outrigger braced structure **b** Response to lateral loading **c** Resultant bending moment in core [[16](#page-15-15)]

a reasonably accurate result for a small or large number of the outrigger. By taking lateral load as constraining, a simple mathematical model is developed to optimally locate the outrigger and belt truss with the reduction in lateral load on the structure as presented in the article [[47](#page-16-12)]. This simple mathematical model projected was applied for a numerical structure to obtain the result and was compared with the same model developed in SAP 2000 and found that the results are approximately equal and comparison is represented as when belt truss is located at *H*/6, *H*/2, 3*H*/4 error in displacement at the top of the building is 1.2%, 2%, 3%. A closed-loop analytical solution is a new method addressed in [[48\]](#page-16-13) to formulate the equation for the most advantageous location of the outrigger, damping coefficient of the damper, and the maximum damping ratio. Outrigger with the single shear wall was studied in the common but auxiliary study has been undertaken by considering a pair of the coupled shear wall by taking into account the suitability of outrigger placement at the top by [[49](#page-16-14), [50](#page-16-15)]. This coupled shear wall is analyzed by continuous medium technique and additionally studied for its stifness which is infuenced by the type of loading, column-to-wall areas ratio, and external spans of the outrigger. After the coupled shear wall, a diferent approach of analyzing the outrigger is planned by authors in the article $[51]$ $[51]$, by considering the outrigger as a spring and its stifness depends on bending and racking shear in the outrigger truss and axial lengthening or shortening of the exterior columns. This approximate method of analysis relates the natural frequencies of the structure to the top defection and rotation when the self-weight is taken as a distributed horizontal load, this method of analysis is compared with fnite element analysis. An optimized analytical model is developed by Netzer and Lavan [\[52](#page-16-17)] using Maxwell model in connection with equation of equilibrium considering fexibility of perimeter column and outrigger excited for stochastic seismic excitations. To reduce the computational effort and number of design parameters, a novel damping distribution function is developed; consideration of fexibility in the column has shown signifcantly improved the performance in article [[52](#page-16-17)]. There is no specifc code or design guideline for the seismic response reduction by the outrigger system. But the council of tall buildings and urban habitat formed a design guide for the outrigger system with the historic overview, which provides benefts of an outrigger system, challenges for an outrigger design system, suitable condition for outrigger system, design consideration for outrigger system, organization of outrigger, and core system is illustrated in [[53\]](#page-16-18).

When an outrigger is introduced in a structure, it reduces the structural response but when this outrigger location is at the optimum position, the structural response is minimized to a maximum. Thus, many studies are undertaken to formulate an equation for the optimum positioning of outrigger, diferent approaches to fnd the optimum positioning, the diferent algorithms proposed to fnd the optimum positioning with reduction in the response of the structure as stated in the previous paragraph. Once the optimum position of the outrigger is found, the light weightiness of the structural system and construction cost can be calculated. Consequently, Mousleh and Batikha [[54](#page-16-19)] found the optimum position of the outrigger in a structure, and then, the weight of the steel and volume of reinforced concrete are calculated according to the model without outrigger and outrigger in a diferent position. The authors found that an outrigger placed in optimum position gives less weight to the structural element, and therefore, the material cost decreases; hence,

cost-efectiveness is liable for the outrigger structure. The position of the outrigger is very signifcant in the reduction in lateral defection at the top of the building; thus, a graphical method is presented in [\[55](#page-16-20)]. The authors in this paper show a graphical method to fnd optimum positioning of outrigger as shown in Fig. [9](#page-9-0) by knowing two non-dimensional characteristic parameters of structure like *ω* and *γH* by considering the bending stifness and fexibility of shear wall, outrigger, and exterior column.

Most of the time graphical method does not interpret the exact result, so Zhou et al. [\[19](#page-15-18)] have illustrated that the program can be coded on the theoretical method to fnd the optimum positioning of outriggers in structure. A MATLAB program was coded by authors to analyze optimum positioning of outrigger for a 240 m tall 60-foor building based on the theoretical method of inter-story drift parameter. The authors simulated single to three outrigger placement in this structure to fnd its optimal positioning excited for wind and earthquake loading by varying ratio of core wall area to foor area. Genetic algorithm and decision frameworks are the other solutions to fnd the optimum positioning of outrigger depending on some constraints, and this procedure is taken up by [\[56–](#page-16-21)[58\]](#page-16-22). The further optimal position of the outrigger (one to four in numbers) was determined by changing the position of the outrigger in the tall building by the two constrain of reducing lateral displacement at the top level and maximum bending stress at the bottom level presented in [\[44](#page-16-9)]. The fnite element method also can be used to locate the optimal position of the outrigger as analyzed by [[59](#page-16-23)]. Optimum positioning of outrigger can be found out by analyzing an outrigger structure in diferent available software with response reduction has constrained by trial and error method, and many studies have been carried out as stated in the article $[60]$ $[60]$.

Analysis of outrigger to study its behavior for the diferent confgurations of the building, loading type, dampers, and bracing connections is studied using diferent numerical software. There are many studies undertaken using ETABS and SAP 2000 software for regular and irregular structures with a linear and nonlinear pushover analysis and time history analysis to observe the behavior under earthquake loading or wind loading as presented by [\[61,](#page-16-25) [62\]](#page-16-26). Amoussou et al. [\[63](#page-16-27)] proposed a simplifed analysis method considering super-element (interval in the column and core taken as a single element) and degrees of freedom as fnite element analysis. The results of the simplifed analysis method were compared with the same model developed in ETABS and found that the approximate result in comparison was obtained. The study of the single and multi-outrigger system with additional features like infll wall, eccentrically bracing, conventional slab, fat slab, bare frame shear wall, connections (bolting and welding) is analyzed for the responses like displacement, base force, inter-story drift for the further enhancement of the outrigger structural system is elucidated by using the numerical software presented in [[64,](#page-16-28) [65\]](#page-16-29). The previous study explained is further varied for diferent loading conditions like static and dynamic loading by varying relative fexural rigidity is presented by [[66\]](#page-16-30). A similar study in Midas Gen and ETABS is undertaken to fnd optimum outrigger geometry by the typical Maxwell–Mohr method, adopting optimal angles for three sets of height to width of a given outrigger space as stated by [\[67](#page-16-31)]. The study is further advanced by the addition of the viscous damper connected between the column and outrigger mainly excited for earthquake forces by [[68](#page-16-32), [69\]](#page-16-33). The diferent approach of strut

Fig. 9 Optimum location of outrigger [\[55\]](#page-16-20)

and tie method is introduced in [\[70\]](#page-16-34) to study the general structural behavior comparing with conventional analysis of the outrigger. The outrigger trusses of various confgurations were discussed and another numerical method based on fnite element analysis software like ETABS and SAP 2000 was also referred to. A special type of connection called fshbone-shaped beam-column connection is modeled in [[71\]](#page-17-0) to represent the composite joint in a steel outrigger structure to transfer the large axial tensile forces from outrigger to concrete wall through concrete-flled steel tube column and double skinned steel plates. It is verifed with a fnite element model with shell and solid element, and it was found that it reasonably refects the load distribution and enables accurate prediction of both the axial force ratio and horizontal displacement of the joint. Lu et al. [[72](#page-17-1)] studied a collapse mechanism and failure mode of mega-braced frame-core tube building model based on fber-beam and multiple layer shell model. After numerical investigation, the behavior of outriggers was tested experimentally by [\[73](#page-17-2), [74](#page-17-3)] for retroftted and non-retroftted specimen that were mainly tested for their torsional strength, ductility, and energy dissipation capacity and found that after retroftting, all the capacity increased because of plastic hinge formation in the gap. Following the literature survey done on optimum positioning of the outrigger, a few kinds of literature are shown in Table [1](#page-10-0) for the optimum location of the outrigger in the diferent types and height of building excitement for a diferent type

of loading with the structural response parameter for optimum positioning.

By finding the optimal location of the outrigger, the response of the structure can be reduced to a considerable range than an outrigger place elsewhere as shown by several literature addresses in the previous paragraphs. But this does not facilitate a decrease in the number of outriggers which will reduce the structural size and economy of the building by increasing the damping of the structure itself. When the outrigger structure is excited for lateral loads, a large amount of force induces between the outrigger and perimeter column because of redistribution of the moment. So there is a need to increase the building damping, where this limitation can be overwhelmed by using extra devices like dampers, actuators, and some other control devices. The addition of these devices in an outrigger structure between the perimeter column and end of the outrigger constitutes a structure called a damped outrigger which is an efective way to satisfy the requirement, which is explained in the further course.

Smith and Willford [[77](#page-17-4)] and O'Neill [[78](#page-17-5)] introduced a new concept for outrigger structural systems in tall building dynamic response and intrinsic damping called damped outrigger. The methods to mitigate the dynamic response by increasing stifness, by the installation of tuned mass damper, viscous damper, and similar devices are illustrated with the comparison to conventional design approaches in [[79,](#page-17-6) [80\]](#page-17-7). This damped outrigger review is provided by [\[81](#page-17-8)],

Table 1 Optimum position of outrigger for diferent buildings

	Reference Height and no. of stories in structure	Type of structure	Type of loading	Structural response param- eter for optimum position		Optimum position (single) outrigger)
$[55]$	87 m (27 stories)	Outrigger braced shear wall	Wind load	Horizontal deflection and displacement		0.33 times its height from the top
[60]	187.5 m (50 stories)	Outrigger with shear core	Earthquake load	Story drift index		$0.44 - 0.48$ times its height from bottom
$[19]$	240 m (60 stories)	Outrigger with shear core	Wind and Earthquake load	Inter-story drift		0.63 and 0.67 times its height from the bottom
[44]	400 m (100 stories)	Outrigger with shear wall	Wind load	Top displacement		0.39 times its height from the bottom
$[59]$	280 m (80 stories)	Outrigger with shear core	Wind load	Drift at top		0.375 times its height from top
$\left[75\right]$	201 m (67 stories)	Outrigger and belt truss with shear core	Wind load	Top displacement		0.31 times its height from the bottom
						More than one outrigger
[76]	a) 70 m (20 stories)	Outrigger with shear wall with belt truss	Earthquake load	a)	Drift	6, 12, 16 floor
						Weight 12 floor
	b) 105 m (30 stories)			b) $\mathbf{c})$	Drift	6, 12, 18, 24 floor
						Weight $8, 15, 24$ floor
	c) 140 m (40 stories)				Drift	12, 20, 26, 34 floor
						Weight 12, 20, 32 floor
	d) 175 m (50 stories)			d)	Drift	12, 26, 34, 42 floor
						Weight 12,18, 30, 42 floor

he stated the mechanism of damped outrigger where the dampers are installed between the outrigger end and perimeter column, calculation methods for damping, the external force effect on the outrigger structure, the methods to optimize damping system, an example of three building which uses damped outrigger system is elaborated. In damped outrigger systems, the column performance is neglected in dynamics of the structural equation of motion and the performance is observed, building damping calculation is done and also practical design consideration with design example is presented in [\[82](#page-17-11)]. Figure [10](#page-11-0) shows the mechanism of the damped outrigger concept which considers the involvement of the column dynamic condition in the outrigger structural equation of motion stated by the article [[83\]](#page-17-12).

Variables in Fig. [10](#page-11-0) represent material properties and structural dimensions. *E* represents Young's modulus, *I* moment of inertia, *ρ*—density of the material used for the structure, *h*—total height of the building, *e*—span of outrigger, α is the ratio of total height of the core where outrigger is placed, *A* is the area of the core, and *f*—force produced by the damper.

A new approach of structural dynamics of the damped outriggers is studied by compatibility equations and boundary conditions; but article [[84\]](#page-17-13) adapted dynamic stifness method to formulate the governing equation for three-parameter such as damper coefficient installed stiffness ratio of core to the column and location of the damped outrigger. The authors found that the damping ratio of the structure is signifcantly persuaded by the stifness ratio of the core and column. The passive protective system like a TMD, TLD, the viscous damper is used to reduce the response as passive dampers in damped outriggers as

Fig. 10 Mechanism of outrigger system [\[83\]](#page-17-12) engineering applications.

stated in [[85\]](#page-17-14). To study viscous damper, article [[86](#page-17-15)] presented performance variation in the real-time tall buildings installed in it for wind and earthquake forces. The authors illustrated the examples of the twin St. Francis Shangri-La Towers in Manila, Philippines, and the Taipei 101 in Taipei, Taiwan, which is considered to explain the technology involved and wide laboratory testing campaign aimed at verifying their behavior during both wind and earthquake. Taipei 101 is a practical example of a skyscraper that uses TMD that is spherical with mass of 660 metric tons suspended with cables as a single-stage pendulum with primary viscous damper connected in resisting acceleration of the structure induced by the wind as a state by the article $[87]$. Figure [11](#page-12-0) shows general configuration of TMD and viscous damper integrated with TMD.

To improve the performance of the viscous damped outrigger, Wand et al. [\[88](#page-17-17)] introduced a negative stifness device using a pre-compressed spring and a pivot lever is installed along with the viscous damper between the perimeter column and outrigger as shown in Fig. [12.](#page-12-1) A parametric study is conducted introducing negative stifness in transcendental characteristic equations of the structure to get improved damping capacity and reduce the structural responses as in the article [\[89](#page-17-18)].

After the real structural application observation of tall buildings, there are some shortcomings for every tall structural form and the outrigger structural system limitations like diferential shortening, the disproportionate collapse of structure with outrigger, toppling of building structures; all these issues are addressed by [[90,](#page-17-19) [91](#page-17-20)]. To overcome the limitation of a TMD of supplemental mass, article [[92](#page-17-21)] introduced tuned viscous mass damper for outrigger structure excited for particularly earthquake rather than wind load. In tuned viscous mass damper, apparent mass is realized by an inertial mass through a ball screw mechanism which acts better than a TMD. Luo et al. [\[93\]](#page-17-22) studied dynamic cyclic tests and numerical analysis of amplifed viscous damped outrigger (AVDO) achieved by adding steel devices to improve the performance of the passively working damper. In Fig. [13,](#page-13-0) a viscous damper connected to the outrigger truss and the column is shown as viscous damped outrigger (VDO); this VDO connection is then modifed with the addition of toggle-brace and lever arm to produce togglebraced viscously damped outrigger (TBVDO) and leverarmed viscously damped outrigger (LAVDO) to enhance the performance of the structural response. θ_1 , θ_2 , θ_3 are the arrangement angles of brace in TBVDO, and l_h , l_v are the horizontal and vertical length of the lever arm amplifying device. A study on AVDO concludes that there is greater dissipation of input seismic force and hysteresis curve of LAVDO is symmetric and full in comparison with TBVDO. So authors have concluded that LAVDO is more suitable for

Fig. 11 a General confguration of TMD b) Viscous damper integrated with TMD

Fig. 12 Mechanism of outrigger system [\[88\]](#page-17-17)

As observed in earlier paragraphs, the passive dampers are not very prominent in structural control, thus the article [[21\]](#page-15-20) studied damped outriggers with a combination of a protective system like passive dampers and active dampers to produce hybrid damping and comprehend the outrigger behavior. The author found that the hybrid damped outrigger reduces the displacement up to 20–30% in comparison with the passively damped outrigger. Another semi-active damper which has proved to be a promising device in structural control is magneto-rheological fuid damper, which has a wide application in all the control system including building used as semi-active damper as stated by [\[94](#page-17-23), [95\]](#page-17-24) and as elastomer for base isolation as elucidated by articles [[96](#page-17-25), [97](#page-17-26)]. Considerably, Wang et al. [[98](#page-17-27)] presented a study on semi-active control strategy employed in St. Francis Shangri-La Palace in Manila, Philippines, by using a MR damper with clipped optimal control algorithm combined with linear quadratic Gaussian acceleration feedback control algorithm. The clipped optimal control algorithm is compared with viscous damper placement in place of MR damper, which showed better performance than viscous damper in the response control of the outrigger structure. This study was further evaluated for the damper size and location by the article [[83](#page-17-12)]. St. Francis Shangri-La Palace in the Philippines is further studied for tuned inertial mass electromagnetic transducer as a damper, and the performance of the structure was observed by the article [[99\]](#page-17-28). This intended damper by authors is compared with electromagnetic transducers and found that the designed damper system is efective in vibration reduction for time history analysis. As MR damper has proved to be a promising device in structural control, in the article [[100](#page-17-29)], a fuzzy logic algorithm is combined with genetic algorithm optimization for reducing the outrigger structural response. From this study, the displacement of the structure excited for an earthquake is shown in Fig. [14.](#page-13-1)

A novel energy dissipation system is designed by Tan et al. [[101](#page-17-30)] considering the interaction between perimeter columns and the dampers in damped outriggers. By this designed method outrigger location, stifness ratio of core to the outrigger, damping coefficient of the damper were

Fig. 13 Integrated steel amplifcation devices with viscous damper [[93](#page-17-22)]

Fig. 14 Displacement of structure without and with outrigger and semi-active outrigger [\[100](#page-17-29)]

found, and this model is evaluated by comparing it with the finite element model. Lin et al. [\[102](#page-17-31), [103](#page-17-32)] presented buckling restrained brace in place of the damper in between the perimeter column and outrigger end for single and multiple outriggers and formulated the dynamics of the structure with buckling restrained brace, shear wall, perimeter column, and outrigger to mitigate the response of the structure. Zhou et al. [[104\]](#page-17-33) developed a combined damped outrigger system with the viscous damper in a combination of the buckling restrained braces with the novel frequency-based analysis. A simplifed model developed in the time domain is then converted to the frequency domain to fnd the amplitude, phase, and variance. The combined damped outrigger system shows a better energy dissipation, and in practical situations, the buckling restrained braces outrigger placement

above viscously damped outrigger is recommended for better performance [[104](#page-17-33)]. Another numerical method was executed in the article $[105]$ $[105]$, which applied the separation of the variable method to convert the partial diferential equation of motion to an ordinary diferential equation. The authors used three numerical examples with diferent stepped discontinuities in their cross sections that are been studied to demonstrate the reliability of this method. The theoretical study presented earlier has no experimental validation; hence, to validate this theory, a real-time hybrid simulation (RTHS) is taken up in which damping devices are tested experimental, whereas remaining structural models are numerically simulated as presented by articles [\[106–](#page-17-35)[109\]](#page-18-0) and presented a study which adopted St. Francis Shangri-La Palace in the Philippines for RTHS with experimental setup MR damper driven by a hydraulic actuator, where the numerical model of the structure was simulated in MATLAB and Simulink as shown in Fig. 15 , where f_{MR} is the MR damper force measured by the load cell, *x* is the displacement measured by the linear variable displacement transducer, and *i* is the control current sent to the hydraulic actuator as stated by the article [\[110\]](#page-18-1).

The damped outrigger analysis is done by a stochastic optimization procedure by Fang et al. [\[111](#page-18-2)], where the earthquake is modeled as fltered white noise following the Kanai-Tajimi spectrum. The author modeled the core the structure using Timoshenko beam, a Kelvin model of the damper, and the genetic algorithm was used to determine the damper placement and associated parameters to minimize structural responses. There is a need to improve the performance of damped outriggers by using the hybrid

Fig. 15 Schematic diagram of real-time hybrid simulation [\[110\]](#page-18-1)

damping system and semi-active dampers regulated by different control algorithms to enhance the outrigger structural behavior.

4 Conclusion

This review paper introduces a concept of outrigger which was historically started as use in canoes, then gradually usage extended to the tall building and skyscrapers in mitigating the structural response and to add stability. The literature survey done on the outrigger structural proves its signifcance in the tall building response control and shows it is efficient in high-rise buildings as a lateral load resistant technique by mitigating the vibration response of the building. An optimum outrigger structure is being developed to make this technology economic and many studies are done, respectively. The introduction of novelist concepts of damped outrigger has accounted for more advantage by reducing the vibration of the building with the addition of reduction in lateral design forces. Because of the reduction in lateral design forces, there is an increase in structural damping, which has also led to the reduction in structural member size and construction cost. Although damped outrigger with a controller is still an upcoming design and relatively new methodology in structural control and monitoring, it has enormous untapped potential in the structural design and construction sector. Based on the state-of-the-art review, it can be summarized that there is a need for a more precise semi-active and hybrid control techniques to make the outrigger structural system perform better and more economically feasible.

5 Future Scope

This paper discusses the evolution of the outrigger from the history of its usage in canoes to the new concept of the damped outrigger with novel control system concepts. This review paper paves the way for real-time hybrid simulation of the novel control system with the novel dampers which are recently developed with the adoption of simplifed preliminary design concepts. There is a new area of research in the damped outrigger structural control by incorporating adaptive control, robust control, and stochastic control. The outrigger structural system can also be studied for the stochastic optimal control which resembles the randomness in the structural control. So randomness can be considered in structural dynamical properties, feedback control randomness, lateral load excitation distributed through the appropriate filter, randomness in actuator dynamical behavior, and randomness in the design of outrigger including the topology, energy dissipation, diferential shorting, the construction pattern, etc. As the construction sector is a complex data management system, the big data technology can be incorporated in processing, storage, and databases in the enhancement of the structural response mitigation. As vibration control of the structural system is upcoming technology and is a new innovative area in research, this has a huge potential in construction industries.

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