RESEARCH ARTICLE-MECHANICAL ENGINEERING

Impact of Nonlinear Rosseland Approximation on Flow of Newtonian Fluid with Unequal Difusivities of Chemically Reactive Species

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Abstract

This investigation studies the fow of a Newtonian fuid close to stagnation point past a stretching/shrinking plate embedded in a porous media. Heat transfer analysis with nonlinear thermal radiation (TR) is also carried out. Homogeneous-heterogeneous reactions with unequal difusivities of reactants take place in the fuid. The controlling partial diferential equations (DEs) of the existing model are reduced to dimensionless ordinary DEs through similarity transformations. These subsequent equations are numerically tackled with the guide of the shooting procedure. The velocity, temperature and concentration's behaviour has been inspected for specifc estimations of the including parameters. The viscous fuid (VF) temperature increases with nonlinear TR. The change in the concentration profile due to the diffusion coefficient rate δ is more prominent in the concentration of specie D compared to specie C. Heterogeneous reaction parameter intensity is very helpful in reducing the concentration of bulk fluid $\phi_1(\eta)$ as well as increasing the surface catalyst concentration $\phi_2(\eta)$

Keywords Viscous fuid · Chemically reactive species · Nonlinear thermal radiation · Unequal difusivity of species *C* and *D*.

List of Symbols

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1 Introduction

Boundary layer flow due to a stretchable surface is essential as it is benefcial in many application and engineering processes, i.e. extrusion produced materials, melt-spinning, wire drawing, manufacture of plastics, hot rolling, production of glass fbre, extrusion process, in production of polymer sheets and the association of biological fuids. BL flow in two dimensions for a viscous, laminar, as well as incompressible fuid due to a stretchable fat plate was first studied by Crane [[1\]](#page-7-0). The liquid flowed at a speed that was proportional to a distance from a fxed point. Parhi and Nath [\[2\]](#page-7-1) discussed the stability of BL flow of viscous liquid past a stretching plate. Kumaran et al. [\[3\]](#page-7-2) examined the transition consequence of the magnetic feld on the flow of VF due to a stretched wall. Yirga and Tesfay [[4\]](#page-7-3) numerically inspected the magnetohydrodynamic (MHD) flow of VF over an expanded wall. Hassan [[5\]](#page-7-4) applied the Lie group method to analyse the heat transfer on VF infuenced by the magnetic feld over an expanding surface. Sheikh and Abbas [\[6](#page-7-5)] looked into the consequence of thermophoresis on MHD flow of Newtonian liquid having chemically reactive species with heat transmission over an oscillatory stretched wall. Sigh et al. [[7](#page-7-6)] explored the efects of nonlinear MHD on the fow of viscous fuid over a porous stretchable sheet with mass transpiration. Reddy and Reddy [[8\]](#page-7-7) dealt with heat and mass characteristics on BL fow of a VF because of an exponential inclined stretching sheet. On the other hand, Wang [[9\]](#page-7-8) frst studied the problem in the reverse case, i.e. the fow caused by the shrinking sheet. In this article, he discussed the fow of a fuid over a shrinking sheet near stagnant point where the speed of a fuid is zero. Lok et al. [\[10](#page-7-9)] considered stagnant point flow of a Newtonian fluid past a contracting/expanding sheet and also discussed the existence and multiplicity of solutions of the fow. Rosila and Ishak [\[11\]](#page-7-10) performed an analysis for SP fow in the presence of porous media past a SS sheet and obtained numerical results. By applying partial velocity slip and Joule heating, Yasin et al. [[12\]](#page-7-11) considered the VF flow in the vicinity of stagnant point. Nasir et al. [[13](#page-7-12)] numerically examined the viscous liquid flow near SP past a quadratically SS plate. By considering viscous dissipation along with magnetic field effects, Alarif et al. [[14](#page-7-13)] studied the fow of VF past a vertical stretching sheet near SP.

Efects of thermal radiation (TR) on heat and mass transfer fuid have many signifcant practical applications, for example in solar power technology, electric power generator, space vehicle re-entry, radioactive waste disposal, chemical pollutants dispersal by water-saturated soil and much more. Many authors studied linear and nonlinear heat radiation efects. By using linear Rosseland

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approximation (RA), Magyari and Pantokratoras [[15](#page-7-14)] studied heat transfer features of different BL flows. Later, Pantokratoras [[16](#page-7-15)] investigated the flow along the vertical plate by considering both linear and nonlinear RA. Laxmi and Shanker [\[17](#page-7-16)] considered the VF flow caused by a stretching sheet with nonlinear TR and suction/injection. The effects of thermal radiation on Carreau-Yasuda nanofuid in the presence of chemical reactions were discussed by Waqas et al. [\[18](#page-7-17)], and it was observed that thermal radiation raises Carreau-Yasuda nanofuid temperature. Raiz et al. [[19](#page-7-18)] studied the heat transfer through the rectangular channel of the Eyring–Powell fluid flow. Hashim et al. [[20](#page-7-19)] presented the numerical investigation of non-Newtonian fuid fow with nonlinear TR and nanoparticles. Pattnaik et al. [\[21\]](#page-7-20) conducted a heat transfer study of nanofuid fow and found that when nanofuid was considered, there was a rapid decline in the temperature profle. Zhang et al. [[22\]](#page-7-21) looked at the infuence of heat transfer with generalized magnetic Reynold number on the 3D nanofuid fow and observed that with the increase in the squeeze Reynolds number, temperature drops signifcantly.

Chemical reactions may be categorized as heterogeneous or homogeneous. This classifcation is based upon the occurrence of reactions whether the reactions happen at a single-phase volume reaction or they happen at a boundary. Food processing, development and difusion of fog, design of chemical managing equipment, moisture above agricultural felds and fruit tree groves are some areas of concern where joined mass and heat transfer occurs with a chemical reaction. Various chemical reacting structures possess both heterogeneous as well as homogeneous reactions. The interaction between both reactions happening on some catalytic surfaces is exceptionally complicated, which could be integrated at diferent rates in the manufacturing as well as usage of reactant species either inside the fuid or on catalytic surfaces. Chaudhary and Merkin [\[23](#page-8-0), [24\]](#page-8-1) originally formulated a basic HH reactions model in the BL fow near SP. The case of unequal difusivities of homogeneous-heterogeneous reactions in viscoelastic fuid fow with magnetic feld and nonlinear thermal radiation was studied by Animasaun et al. [[25\]](#page-8-2) and reached to the result that the change due to δ in concentration profile is more noticeable for concentration of specie B relative to the specie A. Sheikh and Abbas [[26\]](#page-8-3) considered SP flow of non-Newtonian fluid with HH reactions along with slip efects. Alghamdi [[27\]](#page-8-4) explores the viscoelastic fuid fow with HH reactions exposed to the magnetic feld.

The majority of flow and thermal transport phenomena are fundamentally nonlinear, so they are expressed by nonlinear equations. Accurate closed-form solutions to nonlinear problems are far more challenging to achieve than numerical ones. Researchers use several closed-form schemes and numerical schemes to fgure out the solution to the problems of the fuid fow under consideration. See references [[28](#page-8-5)[–33](#page-8-6)] for information.

Furthermore, in hydrometallurgical industries and chemical technologies such as polymer manufacturing and food processing, the chemical reaction efects on heat and mass transfer with radiation through porous media are of signifcant importance. See references. [[34–](#page-8-7)[43\]](#page-8-8)

A porous medium means a material composed of a solid matrix with interconnected empty spaces. These interlinked spaces permit the flow of at least one fluid through the material. Composite materials, metallic foams with high porosity and ceramics are some common examples of porous media. Due to its natural occurrence and relevance in many engineering problems such as porous rollers, porous bearings, porous layer insulation consisting of solids and pores, and in biomathematics, especially in the study of blood fow in arteries and lungs, etc., considerable interest has been shown in the study of fow past a porous medium. Role of radiative heat transmission is superficial in many engineering processes which occur at high temperatures such as in photochemical reactors, turbid water bodies, fuidized bed heat exchangers, nuclear power plants and the various propulsion devices. It is worth noting in all the above literature that little attention has been paid to investigate the movement of a viscous fuid with unequal difusivities of chemical reactions. So, the purpose of the present study is to examine the behaviour of BL flow of VF containing two chemically reactive species through porous media. This study also includes the effects of nonlinear TR, and here diffusion coefficients of both auto-catalyst and reactant are assumed to be unequal.

2 Governing Equation

On a stretchable surface near a SP, a steady BL flow is considered in the presence of porous medium and TR. Additionally, the sheet's temperature along with the temperature at free stream are assumed as θ_w and θ_∞ , respectively, with $\theta_w > \theta_{\infty}$. A basic HH reactions model is also taken, which links the species C and D in a BL flow as described by $[23]$ $[23]$ and [\[24\]](#page-8-1):

$$
C + 2D \rightarrow 3D, \text{rate} = k_e c d^2,\tag{1}
$$

$$
C \to D, \text{rate} = k_s c,\tag{2}
$$

Furthermore, both reactive processes are supposed to be isothermal and a homogeneous concentration c_0 of reactant *C* is in the free stream and no auto-catalyst *D* is present.

The governing equations of the present fow situation, in the light of above presumptions and BL approximations, are given below [[11](#page-7-10), [25](#page-8-2)]

$$
\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0,\tag{3}
$$

$$
u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = -\frac{1}{\rho}\frac{\partial p}{\partial x} + v\frac{\partial^2 u}{\partial y^2} - \frac{v}{\varsigma}u,\tag{4}
$$

$$
u\frac{\partial \theta}{\partial x} + v\frac{\partial \theta}{\partial y} = \frac{k}{\rho C_p} \frac{\partial^2 \theta}{\partial y^2} - \frac{1}{\rho C_p} \frac{\partial q_r}{\partial y},\tag{5}
$$

$$
u\frac{\partial c}{\partial x} + v\frac{\partial c}{\partial y} = D_c^* \frac{\partial^2 c}{\partial y^2} - k_e c d^2,\tag{6}
$$

$$
u\frac{\partial d}{\partial x} + v\frac{\partial d}{\partial y} = D_D^* \frac{\partial^2 d}{\partial y^2} + k_e c d^2.
$$
 (7)

The constraints at the surface of the sheet and away from it in the free stream are specifed by (Fig. [1](#page-4-0))

$$
u = u_w(x) = U_w x, v = 0, \theta = \theta_w, D_C^* \frac{\partial c}{\partial y} = k_s c, D_D^* \frac{\partial d}{\partial y} = -k_s c \text{ at } y = 0,
$$
\n(8)

$$
u = u_{\tilde{e}}(x) = U_{\infty}x, \theta = \theta_{\infty}, c \to c_0, d \to 0 \text{ as } y \to \infty.
$$
 (9)

Using the condition $u = u_{\tilde{e}}(x) \rightarrow U_{\infty}x$ as $y \rightarrow \infty$ in Eq. (4) gives

$$
u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = U_{\infty}\frac{du_{\infty}}{dx} + v\frac{\partial^2 u}{\partial y^2} + \frac{v}{\varsigma}U_{\infty}x - \frac{v}{\varsigma}u.
$$
 (10)

or

$$
u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = U_{\infty}\frac{du_{\infty}}{dx} + v\frac{\partial^2 u}{\partial y^2} + \frac{v}{\varsigma}(U_{\infty}x - u). \tag{11}
$$

With the help of RA $[15]$, the heat flux due to radiation is given as

$$
q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial \theta^4}{\partial y},\tag{12}
$$

Utilizing Eq. (12) (12) , Eq. (5) (5) (5) transforms into the form:

$$
u\frac{\partial\theta}{\partial x} + v\frac{\partial\theta}{\partial y} = \left(\frac{k}{\rho C_p} + \frac{16\sigma^*\theta_\infty^3}{3\rho C_p k^*}\right)\frac{\partial^2\theta}{\partial y^2}.
$$
 (13)

For the above equation, the temperature diference is supposed to be low sufficiently within the flow which leads to the linearization of θ^4 as

$$
\theta^4 \cong 4\theta_\infty^3 \theta - 3\theta_\infty^4
$$

via Taylors series about θ_{∞} and neglecting higher terms. Equation (13) (13) represents the flow equation of temperature with linear TR. But the present problem aims to explore

the infuence of nonlinear TR on the fow, so neglecting the above supposition, i.e. replacement of θ_{∞}^3 with θ^3 in Eq. ([12\)](#page-2-1) and then putting it in Eq. (5) (5) (5) gives [[34,](#page-8-7) [44\]](#page-8-9).

$$
u\frac{\partial\theta}{\partial x} + v\frac{\partial\theta}{\partial y} = \frac{k}{\rho C_p} \frac{\partial}{\partial y} \left(\left(1 + \frac{16\sigma^*\theta^3}{3kk^*} \right) \frac{\partial\theta}{\partial y} \right).
$$
 (14)

Now, introducing the similarity transformations and non-dimensional temperature and concentrations.

$$
\psi = (U_{\infty}v)^{\frac{1}{2}}xf(\eta), \Theta(\eta) = \frac{\theta - \theta_{\infty}}{\theta_w - \theta_{\infty}}, \phi_1(\eta) = \frac{c}{c_o},
$$

$$
\phi_2(\eta) = \frac{d}{c_o}, \eta = \left(\frac{U_{\infty}}{v}\right)^{\frac{1}{2}}y
$$
 (15)

The following normalized form of Eqs. (11) , (14) , (6) (6) and (7) (7) (7) is achieved after using Eq. (15) :

$$
f''' - f'^2 + ff'' + 1 + \beta(1 - f') = 0,
$$
\n(16)

$$
\left(\left(1 + Rd \left(1 + (\Theta_w - 1)\Theta \right)^3 \right) \Theta' \right)' + \Pr f \Theta' = 0, \tag{17}
$$

$$
\frac{1}{Sc_C} \phi_1'' + f \phi_1' - K \phi_1 \phi_2^2 = 0,
$$
\n(18)

$$
\frac{\delta}{Sc_D}\phi_2'' + f\phi_2' + K\phi_1\phi_2^2 = 0.
$$
 (19)

 $\text{Here } \beta = \frac{v}{\varsigma U_{\infty}}, \Theta_w = \frac{\theta_w}{\theta_{\infty}}, R d = \frac{16\sigma^*}{3kk^*}, Sc_C = \frac{v}{D_C^*}, Sc_D = \frac{v}{D_D^*},$ $K = \frac{k_e c_0^2}{U_\infty}$ and $\text{Pr} = \frac{v}{\alpha}$.

The surface constraints (8) and (9) become

$$
f(0) = 0, f'(0) = \lambda, \Theta(0) = 1,
$$

\n
$$
\phi'_1(0) = K_s \phi_1(0), \delta \phi'_2(0) = -K_s \phi_1(0),
$$
\n(20)

$$
f'(\eta) = 1, \Theta(\eta) \to 0, \n\phi_1(\eta) \to 1, \phi_2(\eta) \to 0
$$
 as $\eta \to \infty$. (21)
\nHere $\lambda = \frac{U_w}{U_\infty}, K_s = \frac{k_s}{Re^{1/2}D_c^*}, \delta = \frac{D_p^*}{D_c^*}.$

3 Numerical Solution

Shooting technique with the aid of Runge–Kutta algorithm is adopted to solve the two-point boundary value problem generated by nonlinear ordinary DEs (16) – (19) (19) (19) along with surface constraints (20) (20) (20) – (21) . First, the problem is transformed into an initial value problem (IVP) as

$$
f' = \xi_1,
$$

\n
$$
f'' = \xi_2,
$$

\n
$$
\xi_2' = \xi_1^2 - f\xi_2 - 1 - \beta(1 - \xi_1).
$$
\n(22)

$$
\Theta = \zeta_1,\n\zeta_1' = \zeta_2,\n\zeta_2' = \frac{\Pr f \zeta_2 - 3R d (\Theta_w - 1) \zeta_2^2 (1 + (\Theta_w - 1) \zeta_1)^2}{1 + R d (1 + (\Theta_w - 1) \zeta_1)}.
$$
\n(23)

$$
\phi_1 = \Psi_1, \n\Psi'_1 = \Psi_2, \n\Psi'_2 = Sc_C(K\Psi_1\Phi_1^2 - f\Psi_1).
$$
\n(24)

and

$$
\phi_2 = \Phi_1,
$$
\n
$$
\phi'_1 = \Phi_2,
$$
\n
$$
\phi'_2 = \frac{Sc_D}{\delta} \left(-K \Psi_1 \Phi_1^2 - f \Phi_2 \right),
$$
\n(25)

with the constraints

$$
f(0) = 0, \quad \zeta_1(0) = \lambda, \quad \Psi_1(0) = (1/K_s)\Psi_2(0),
$$

$$
\Phi_2(0) = -\left(K_s/\delta\right)\Psi_1(0).
$$
 (26)

The appropriate value of the finite value of $\eta \to \infty$ say η_{∞} has a vital role in this method. To solve Eqs. [\(22](#page-3-6))–[\(25](#page-3-7)) sub-ject to conditions ([26\)](#page-3-8) as an IVP, values for $\xi_2(0)$ i.e. $f''(0)$, $\zeta_2(0)$ i.e. $\theta'(0)$, $\Psi_2(0)$ i.e. $\phi'_1(0)$ and $\Phi_1(0)$ i.e. $\phi_2(0)$ are required, but the problem does not have such values. After selecting the initial guesses for $\xi_2(0)$, $\zeta_2(0)$, $\Psi_2(0)$, $\Phi_1(0)$ and employing the Runge–Kutta method, the solution is obtained. The better approximation of the solution is achieved by adjusting the values for $\xi_2(0)$, $\zeta_2(0)$, $\Psi_2(0)$ and $\Phi_1(0)$. For this, Newton's approach has been used.

4 Results and Discussion

A numerical technique, namely shooting procedure, is opted to fnd the solution of the fow equations for the fow near SP in the presence of generalized TR and porous zone. The unequal difusivities of two reactive species are also considered for the concentration profle. Graphs are presented to examine the response of velocity $f'(\eta)$, temperature $\Theta(\eta)$, and concentrations $\phi_1(\eta)$, $\phi_2(\eta)$ to the change in the governing parameters, i.e. λ , β , Rd , \Pr , Θ_w , δ , K_s , K_s , Sc_c and Sc_D arising in the fow equations.

Fig. 1 Schematic of the problem

Fig. 2 Variation in $f'(\eta)$ with λ when $\beta = 0.06$, Pr = 0.72, $\Theta_w = 1.01, Rd = 1, Sc_C = Sc_D = 0.8, \delta = 1.2, K = 1$ and $K_s = 1$

Figure [2](#page-4-1) shows the deviation in $f'(\eta)$ for various values of the SS parameter λ . λ < 0 means the shrinking of the surface, $\lambda = 0$ symbolizes the static surface while $\lambda > 0$ stands for stretching of the surface. From fgure, it can be viewed that $f'(\eta)$ increases with an increase in λ . However, the BL thickness for the shrinking surface is more signifcant than static and stretched surfaces. Figure [3](#page-4-2) is graphed to show the behavioural change in $f'(\eta)$ with an increment in β when the flow is over a shrinking wall. A decrease in the BL region is observed with a rise in the permeability of the porous zone. This reduction is related to Darcy's resistance which enhances with the increase in β .

Figures [4](#page-4-3), [5](#page-4-4), [6](#page-5-0), and [7](#page-5-1) are plotted to present the infuence of evolving parameters on the temperature profile $\Theta(\eta)$. Figure [4](#page-4-3) illustrates the effects of β on $\Theta(\eta)$ over a shrinking wall. It can be seen that $\Theta(\eta)$ as well as thermal BL is a decreasing function of β . Fig. [5](#page-4-4) depicts the change in $\Theta(\eta)$ with an increase in Θ_w . It can be noticed that both thermal

Fig. 3 Variation in $f'(\eta)$ with β when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01$, $Rd = 1$, $Sc_C = Sc_D = 0.8$, $\delta = 1.2$, $K = 1$ and $K_s = 1$

Fig. 4 Variation in $\Theta(\eta)$ with β when $\lambda = -1$, Pr = 1.5, $\Theta_w = 1.01$, $Rd = 1$, $Sc_C = Sc_D = 0.8$, $\delta = 1.2$, $K = 1$ and $K_s = 1$

Fig. 5 Variation in $\Theta(\eta)$ with Θ_w when $\lambda = -1, \beta = 1$, $Pr = 0.72$, $Rd = 1$, $Sc_C = Sc_D = 0.8$, $\delta = 1.2$, $K = 1$ and $K_s = 1$

Fig. 6 Variation in $\Theta(\eta)$ with *Rd* when $\lambda = -1, \beta = 1$, $Pr = 0.72$, $\Theta_w = 1.01$, $Sc_C = Sc_D = 0.8$, $\delta = 1.2$, $K = 1$ and $K_s = 1$

Fig. 7 Variation in $\Theta(\eta)$ with Pr when $\lambda = -1$, $\beta = 1$, $Rd = 1, \ \Theta_w = 1.01, \ Sc_C = Sc_D = 0.8, \delta = 1.2, K = 1 \text{ and } K_s = 1$

BL and $\Theta(\eta)$ enhance with a raise in θ_w . The change in $\Theta(\eta)$ with the increasing values of *Rd* can be observed from Fig. [6](#page-5-0) which depicts a rise in both $\Theta(\eta)$ and its BL region with raise in *Rd*. The decreasing effect of Pr on $\Theta(\eta)$ can be noticed in Fig. [7.](#page-5-1) The decrease in thermal BL is also seen in this Figure.

The impacts of ruling parameters on the concentration profiles $\phi_1(\eta)$, $\phi_2(\eta)$ are shown in Figs. [8](#page-5-2), [9](#page-5-3), [10,](#page-5-4) [11,](#page-6-0) [12.](#page-6-1) Fig-ure [8](#page-5-2) presents the change in the behaviour of $\phi_1(\eta)$, $\phi_2(\eta)$ with an increment in β . A decrement in the regions of BL for both $\phi_1(\eta)$ and $\phi_2(\eta)$ is observed from this Figure with an increase in β due to porosity resistance. However, $\phi_1(\eta)$ is showing an increment and $\phi_2(\eta)$ is decreasing with a rise in β . The response of $\phi_1(\eta)$, $\phi_2(\eta)$ with a hike in the values of K_s is portrayed in Fig. [9](#page-5-3). The effect of K_s on concentration BL is reverse of β , i.e. for both $\phi_1(\eta)$ and $\phi_2(\eta)$ BL increases with a raise in K_s . Figure also shows

Fig. 8 Variation in $\phi_1(\eta), \phi_2(\eta)$ with β when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01$, $Rd = 1$, $\delta = 1.1$, $Sc_C = Sc_D = 0.6$, $K = 0.9$ and $K_s = 0.9$

Fig. 9 Variation in $\phi_1(\eta), \phi_2(\eta)$ with K_s when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01$, $Rd = 1$, $\delta = 1.2$, $Sc_C = Sc_D = 0.8$, $K = 1$ and $\beta = 1$

Fig. 10 Variation in $\phi_1(\eta), \phi_2(\eta)$ with δ when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01$, $Rd = 1$, $\beta = 1$, $Sc_C = Sc_D = 0.8$, $K = 1$ and $K_s = 1$

Fig. 11 Variation in $\phi_1(\eta), \phi_2(\eta)$ with Sc_C and Sc_D when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01$, $Rd = 1, \beta = 1, \delta = 1.2$, $K = 1$ and $K_s = 1$

Fig. 12 Variation in $\phi_1(\eta), \phi_2(\eta)$ with *K* when $\lambda = -1$, Pr = 0.72, $\Theta_w = 1.01, Rd = 1, \beta = 1, \mathcal{S}c_C = \mathcal{S}c_D = 0.8, \delta = 1.2$ and $K_s = 1$

a reduction and an increment in $\phi_1(\eta)$ and $\phi_2(\eta)$, respectively. The varying behaviour of $\phi_1(\eta)$, $\phi_2(\eta)$ with change in δ is graphed in Fig. [10](#page-5-4). The response of $\phi_1(\eta)$ and $\phi_2(\eta)$ to the increase in δ is similar to that of β . However, the variance in $\phi_2(\eta)$ is greater relative to $\phi_1(\eta)$. Due to the rate of diffusion coefficient δ , the shift in the concentration profle is more notable in the concentration of species D relative to species C. A contraction in the BL region of both $\phi_1(\eta)$ and $\phi_2(\eta)$ with the increasing values of *Sc_C* and Sc_D is observed and can be seen in Fig. [11](#page-6-0). The change Sc_C leads to an increase in $\phi_1(\eta)$ while the rise in Sc_p reduces $\phi_2(\eta)$. As a consequence of increasing Schmidt number, the mass difusivity of the species decreases, thereby reducing the concentration BL thickness for both Sc_C and Sc_D . Figure [12](#page-6-1) shows that the variation in both $\phi_1(\eta)$ and $\phi_2(\eta)$ for distinct values of K. The change in the BL region for *K* has similar behaviour to that K_s , i.e. the thickness region of

Table 1 Comparison of $f''(0)$ for a stretching sheet obtained for different values of λ , for fixed values of $\beta = 1$

λ	Shaw et al. $[45]$	Present
0	1.23258766	1.23258766
0.1	1.14656100	1.14656100
0.2	1.05112999	1.05112999
0.3	0.94681612	0.94681612
0.4	0.83407209	0.83407209
0.5	0.71329496	0.71329496
1	Ω	θ
\mathfrak{D}	-1.88730667	-1.88730667
3	-4.276541	-4.276541
4	-7.086378	-7.086378
5	-10.264749	-10.264749

Table 2 Comparison of $f''(0)$ for a shrinking sheet obtained for different values of λ , for fixed values of $\beta = 1$

concentration boundary layer increases when K and K_s are increased, and it is because of reactants of diferent reactions of species. However, $\phi_1(\eta)$ reduces for larger values of *K* and the curve takes a S shape as *K* increases. An opposite trend is noticed for $\phi_2(\eta)$.

The comparison of the numerical values of $f''(0)$ with the fndings stated by Shaw et al. [\[45\]](#page-8-10) for the diferent values of λ are shown in Table [1](#page-6-2) and [2](#page-6-3) and found in excellent accordance. For $\lambda > 0$ (stretching sheet), a solution for all values of λ can be accomplished whereas the solution for $\lambda < 0$ (shrinking sheet) occurs only in the region $\lambda \geq \lambda_c = -1.2465$, here λ_c denotes the critical value of λ so that for $\lambda < \lambda_c$ no solution exist. However, for $\lambda_c < \lambda < -1$, the solution is not unique, so there exist two solutions $f_1(\eta)$ and $f_2(\eta)$. One can see from the literature that the first solution is stable and technically feasible, although the second solution is not.

5 Concluding Remarks

The impact of HH reactions on steady BL flow due to the SS surface close to the SP through a porous medium in the presence of nonlinear TR is investigated. By using the shooting method, a numerical solution is obtained. The following remarks have been made:

- Porous media acts as a source of resistance in a flow; therefore, an increase in permeability parameter β causes a decrement in velocity, temperature and concentration BL thickness.
- Prandtl number decreases the temperature BL thickness because the increment in Prandtl number Pr causes decrement in the thermal difusivity while BL thickness increases with *Rd*.
- When the magnitude of Θ_w is small, the decrease in temperature distribution from the wall to the free stream is marginal compared to the maximum decreasing trend when the magnitude of Θ_w is high.
- As a result of rising values of Schmidt number, the mass difusivity of the species decreases consequently both Sc_C and Sc_D reduce the concentration BL thickness.
- The increase in the magnitude of the ratio of diffusion coefficient is just a growing function of the catalyst concentration within the realm of fuid
- Both homogeneous and heterogeneous intensities increase concentration BL thickness.
- The results will be used in studies related to food processing, fog production and diffusion, highly acidic water bodies, chemical management equipment design, photocatalytic reactors, moisture over agricultural areas and fruit tree meadows, highly acidic water bodies, heat exchangers for fuidized beds.

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