#### **ORIGINAL ARTICLE**



# Omnidirectional high reflector at 650, 850, 1300 and 1550 nm for optical fiber communication by fused silica/YBCO-superconductor Octonacci photonic crystal

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#### Abstract

The transfer matrix method (TMM) is deployed to determine the reflectance spectra of Octonacci photonic structures. First, the structures are designed using the TiO<sub>2</sub> and SiO<sub>2</sub> slabs materials. This design allows the obtainment of limited high reflectors for some optical communication wavelengths and for both TE and TM polarizations. After that, the superconductor YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> (YBCO) and the silica slabs replace the previous materials in Octonacci structures. This modification permits to extend the omni-directional reflectance bands for both polarizations. The iteration number of the Octonacci sequence has an important effect on these bands. Later the geometric thickness of the photonic structure is optimized by changing the reference wavelength  $\lambda_0$  and omnidirectional high reflectors that cover all optical communication wavelengths (650, 850, 1300 and 1550 nm) are obtained. In addition, for these wavelengths, a tiny effect of the ambient temperature is noticed. These omnidirectional high reflectors can find application in glass (GFO) and plastic (PFO) fiber optics and may be used in sensing applications.

Keywords Photonic crystal · Octonacci · Superconductor · High reflector · Fiber optic

## Introduction

The discovery of electricity permits to humans the use of electronic signals to transmit information inside copper wires and as an example; we find the old-wired phone and the Internet distributed through the wired network. However, this technology was accompanied by many problems, such as the raise of temperature inside the devices due to the Joule effect, its energy consumption, and its limited transfer of

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data. However, the substitution of the light pulses instead of electronic pulses offers solution to all these problems. In fact light made of photons travels much faster than electrons and consumes less energy and is not accompanied by the Joule effect. In addition, light can transmit more information flow. The optical communication also known as optical telecommunication uses light (optical signal) to carry information from a start location (sender) to its destination (receiver). A transmitter (can be laser or LED sources) is used to encode the information into an optical signal and a channel (a physical transmission medium such as the fiber-optic cable) is requested to convey the optical signals along it over long distances. The capacity of channel for transmitting information is measured by its data rate in bits per second or by its bandwidth in Hz. At the destination point of the system (the end point), the optical signal is received by photodiodes and converted back into electronic signals (Ohring 2002).

The visible spectrum that our eyes can detect goes from 400 to 700 nm (from violet to red).Under the red begin the infrared spectrum. The glass fiber optics (GFO) operate along the wavelengths 850, 1300 and 1550 nm. The attenuation (due to absorption and scattering) of this fiber is much less around these wavelengths values. The absorption



happens due to the tiny amounts of water vapor in glass; it exists in several wavelength bands called water bands. Scattering occurs when light is diffused by atoms or molecule in the glass. The lower scattering is found with longer wavelengths. There exist two families for the GFO: the multimode graded index fiber operates along the wavelengths 850 and 1300 nm; however, the single-mode fiber operates along 1310 and 1550 nm. Also for the shorter wavelengths like 650 nm of the red light and 850 nm the scientists develop plastic fiber optics (PFO) because the plastic material has lower absorption at these wavelengths (Rajiv 2002).

The photonic crystals (Brandao et al. 2015; Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015; Ali et al. 2010) are made by alternating two or more different materials lavers. This alternation can be periodic or aperiodic which makes it possible to build periodic or quasi-periodic photonic crystals such as Fibonacci, Octonacci, Thue-Morse, Cantor etc. (Brandao et al. 2015; Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015; Ali et al. 2010). These crystals are being studied by several researchers with the aim of building omnidirectional mirrors (Pandey et al. 2017; Nayak et al. 2019; Hsueh et al. 2010; Sayed et al. 2020), sensors (Qutb et al. 2021; Zaky 2021; Amiri et al. 2019; Shaban et al. 2020; Nouman et al. 2020), filters (Aly et al. 2020; Aly and Mohamed 2019), etc.... The omnidirectional mirrors have many applications, both for reflecting surfaces, for improving the performance of LEDs, or for their properties of very high reflectivity in the optical cavities of certain lasers (e.g.: VCSEL) (Ariza-Flores et al. 2012). In addition, these mirrors find applications in high-frequency band as an antenna substrate (Zandi et al. 2007), in optoelectronics devices (Ali and Kanzari 2010; Pandey 2012; Srivastava et al. 2008) and in optical communication devices (Gahef et al. 2017). Moreover, these photonic omnidirectional mirrors are useful to construct the multi-quantum wells (MQW) for the optical regeneration by saturable absorbers (SA) applications (Takahashi 1790; Mangeney et al. 2000).

In this paper, we search to construct omnidirectional mirrors using Octonacci photonic structure filled with silica and superconductor materials. In addition, the geometric and optical properties of these mirrors are optimized. We aim that these mirrors cover the operational wavelengths of the PFO and GFO devices.

## **Theoretical model**

#### Octonacci sequence

The photonic crystal layers are arranged according to the Octonacci (Brandao et al. 2015) sequence



 $S_n = S_{n-1} \times S_{n-2} \times S_{n-1}$ , where *n* is the iteration number,  $S_1 = H$  and  $S_2 = L$ . Here H and L represent the layer of high and low refractive index value respectively. Figure 1 illustrates an example of the geometric structure of the 4th Octonacci iteration. The used materials during this theoretical investigation are SiO<sub>2</sub>, TiO<sub>2</sub> and yttrium barium copper oxide (YBCO). The Gorter-Casimir two-fluid model is used to describe the optical response of the YBCO superconductor. The external magnetic field is supposed to be null (Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015). The refractive index of the YBCO superconductor depends on the ambient temperature T and the wave-frequency  $\omega$  (Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015):  $n_s = \sqrt{\varepsilon_s} = \sqrt{1 - \frac{1}{\omega^2 \mu_0 \varepsilon_0 \lambda_L^2(T)}}$ . Here  $\lambda_L(T) = \frac{\lambda_p}{\sqrt{1 - G(T)}}$ represents the temperature-dependent penetration depth,  $\mu_0$  and  $\epsilon_0$  symbolize, respectively, the permeability and the permittivity of free space (Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015). In the last formula and at T=0 K, the London penetration depth is  $\lambda_p = 140 \text{ nm}$ .  $G(T) = \left(\frac{T}{T_c}\right)^4$  is the Groter-Casimir expression. In addition, T represents the ambient temperature and  $T_c = 92$ K is the superconducting critical temperature (Trabelsi 2019; Baraket et al. 2017; Chung-An et al. 2013; Srivastava 2014; Wu and Gao 2015).

#### Transfer matrix method (TMM)

To extract the reflectance spectra, the transfer-matrix method (TMM) is employed. This method is introduced by Yeh and Yariv (1984) and Ali et al. (2020) and allows to determine the optical properties (reflectance, transmittance, absorption, electromagnetic field, etc.) of the multilayered structures. When juxtaposing successive layers, the amplitudes of the electric fields of incident wave



Fig. 1 Schematic representation showing the geometric structure of 4th Octonacci iteration

 $E_0^+$ , reflected wave  $E_0^-$  and transmitted wave  $E_{m+1}^+$  after m layers can be correlated via the following formula (Yeh and Yariv 1984; Ali et al. 2020):

$$\begin{pmatrix} E_0^+\\ E_0^- \end{pmatrix} = \frac{C_1 C_2 C_3 \dots C_{m+1}}{t_1 t_2 t_3 \dots t_{m+1}} \begin{pmatrix} E_{m+1}^+\\ E_{m+1}^- \end{pmatrix},\tag{1}$$

where the  $C_i$  (propagation matrix) for the *j*th layer is:

$$C_{j} = \begin{pmatrix} \exp\left(i\varphi_{j-1}\right) & r_{j}\exp\left(-i\varphi_{j-1}\right) \\ r_{j}\exp\left(i\varphi_{j-1}\right) & \exp\left(-i\varphi_{j-1}\right) \end{pmatrix},$$
(2)

 $\varphi_{j-1}$  indicates the phase shift of the wave between (j-1)th and *j*th boundaries and can be determined as:

$$\varphi_0 = 0, \tag{3}$$

$$\varphi_{j-1} = \frac{2\pi}{\lambda} \hat{n}_{j-1} d_{j-1} \cos \theta_{j-1}, \tag{4}$$

where  $\hat{n}_j$  and  $\theta_j$  are the complex refractive index and the complex refractive-wave angle, respectively.

For parallel *P*-polarization (TM mode), the Fresnel coefficients  $t_j$  and  $r_j$  are (Yeh and Yariv 1984; Ali et al. 2020):

$$r_{jp} = \frac{\hat{n}_{j-1}\cos\theta_j - \hat{n}_j\cos\theta_{j-1}}{\hat{n}_{j-1}\cos\theta_j + \hat{n}_j\cos\theta_{j-1}},\tag{5}$$

$$t_{jp} = \frac{2\hat{n}_{j-1}\cos\theta_{j-1}}{\hat{n}_{j-1}\cos\theta_j + \hat{n}_j\cos\theta_{j-1}}.$$
(6)

Moreover, for perpendicular *S*-polarization (TE mode) (Yeh and Yariv 1984; Ali et al. 2020):

$$r_{js} = \frac{\hat{n}_{j-1}\cos\theta_{j-1} - \hat{n}_j\cos\theta_j}{\hat{n}_{j-1}\cos\theta_{j-1} + \hat{n}_j\cos\theta_j},\tag{7}$$

$$t_{js} = 2 \frac{\hat{n}_{j-1} \cos \theta_{j-1}}{\hat{n}_{j-1} \cos \theta_{j-1} + \hat{n}_j \cos \theta_j}.$$
 (8)

For both polarization modes *S* and *P* the transmittance energy are:

$$T_{S} = \operatorname{Re}\left(\frac{\hat{n}_{m+1}\cos\theta_{m+1}}{\hat{n}_{0}\cos\theta_{0}}\right)\left|t_{S}\right|^{2},\tag{9}$$

$$T_P = \operatorname{Re}\left(\frac{\hat{n}_{m+1}\cos\theta_{m+1}}{\hat{n}_0\cos\theta_0}\right) \left|t_P\right|^2,\tag{10}$$

Re indicates the real part (Yeh and Yariv 1984; Ali et al. 2020).

#### **Results and discussions**

#### **Materials effect**

We begin this work by studying the material effect on the width of the photonic band gap (PBG). First, we choose SiO<sub>2</sub> and TiO<sub>2</sub> as two materials of the Octonacci layers with refractive indices 1.45 and 2.3, respectively. We choose these two materials because of their availability, its costs are cheaper compared with other types of semiconductor materials and it is easy to fabricate photonic crystals with them. The optical thickness  $n \times d$  of layers is chosen to satisfy the Bragg's condition:  $n \times d = \frac{\lambda_0}{4}$ , where  $\lambda_0$  is the reference wavelength (Ali et al. 2020). The iteration of the Octonacci multilayered structure is fixed at 5, so the structure's number of layers P is equal to 17. The  $\lambda_0$  is chosen to be equal to 1.5 µm; therefore, the structure thickness ds is equal to 3.92 µm. Figure 2 displays the 3D reflectance spectra as function of wavelength (µm) and incident angle (rad) for TE and TM wave-polarization. In Fig. 2 the PBGs areas are showed with yellow color and they are separated by several Bragg peaks in blue color for different wavelengths and incident angle.

Table 1 summarizes the intervals of wave-incidentangle for which the optical communication wavelengths are totally reflected. From Fig. 2 and Table 1, we can conclude that the wavelengths of the single-mode fiber (1300 and 1550 nm) are often transmitted through the photonic structure for TM-mode, and reflected for some incident angle when the wave is TE-polarized. The wavelengths 650 and 850 nm of the PFO and the multimode graded index fiber are often propagated through the Octonacci structure.

To expand the PBGs to cover all optical communication wavelengths, we try now to change the layers of TiO<sub>2</sub> materials with the superconductor yttrium barium copper oxide YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> (YBCO). This superconductor is a hightemperature superconductors and let know that a superconductor with Tc more than 30 K, is generally considered to be the high-temperature superconductor (HTS) material otherwise the superconductor is considered to be the lowtemperature superconductor (LTS) material. In addition, this superconductor has stimulated interest in manufacturing economic because the efficient cost of refrigeration to superconducting temperatures (often requiring cryogens such liquid nitrogen or liquid helium) of the HTS are less than that needed by the LTS material. Furthermore, the YBCO superconductor has been most successfully used in the form of epitaxial thin films or as single crystals.

Figure 3 illustrates the reflectance spectra for TE and TM wave-polarization. The reference wavelength and the number of layers are kept fixed  $\lambda_0 = 1.5 \text{ }\mu\text{m}$ , P = 17. The





Fig. 2 3D Reflectance spectra of 1D Octonacci multilayered stack (with TiO<sub>2</sub> and SiO<sub>2</sub> materials) as a function of wavelength ( $\mu$ m) and incident angle (rad) for TE- and TM-polarization modes:  $\lambda_0 = 1.5 \ \mu$ m, P = 17 and  $ds = 3.92 \ \mu$ m

 
 Table 1
 Intervals of incident angle for which the optical communication wavelengths are totally reflected

Optical communication wavelengths (nm)	Totally reflectance area	
	TE-mode (rad)	TM-mode
650	$\theta_0 \ge 1.37$	$\theta_0 \ge 1.44$ rad
850	$\theta_0 \ge 0.98$	_
1300	$\theta_0 \le 0.34$ and $\theta_0 \ge 0.79$	$\theta_0 \leq 0.27 \mathrm{rad}$
1550	$\theta_0 \geq 0.76$	-

The structure is Octonacci with TiO<sub>2</sub> and SiO<sub>2</sub> materials ( $\lambda_0 = 1.5 \mu m$ , P = 17 and ds = 3.92  $\mu m$ )

ambient temperature is set at 25 °C. The geometric thickness of the new Octonacci structure becomes  $ds = 3.2 \mu m$ . In addition, Table 2 shows the intervals of wave-incidentangle for which the optical communication wavelengths are totally reflected. It is clear from Fig. 3 and Table 2 that the wavelengths of the single-mode fiber (1300 and



1550 nm) are totally reflected, but the wavelengths 650 and 850 nm of the PFO and the multimode graded index fiber are often propagated through the Octonacci structure. Therefore, we can conclude that the replacement of the  $TiO_2$  layers with the YBCO layers permits the expansion of the main PBG, this physical phenomenon is due to the increase of the refractive index contrast between the materials that compose the photonic structure.

In the next part, and by changing the iteration number of Octonacci sequence, we will try to enlarge the PBG to cover these two last wavelengths.

#### **Iteration effect**

In this part, the iteration number of the Octonacci sequence is changed in order to enlarge the omnidirectional PBGs. The increase of the iteration number permits to change the number of layers and the thickness of the whole structure which permits to change the PBGs width.



**Fig. 3** Reflectance spectra of 1D Octonacci multilayered stack (with YBCO and SiO2 materials) as a function of wavelength ( $\mu$ m) and incident angle (rad) for TE- and TM-polarization modes:  $\lambda_0 = 1.5 \ \mu$ m, P = 17 and  $ds = 3.2 \ \mu$ m

 
 Table 2
 Intervals of incident angle for which the optical communication wavelengths are totally reflected

Optical communica-	Totally reflectance area		
(nm)	TE-mode (rad)	TM-mode (rad)	
650	$\theta_0 \le 0.33,$ $0.92 \le \theta_0 \le 1.19$ and $\theta_0 \ge 1.37$	$\begin{array}{l} \theta_0 \leq 0.28, \\ 0.98 \leq \theta_0 \leq 1 \text{ and} \\ \theta_0 \geq 1.47 \end{array}$	
850	$\theta_0 \le 0.37$ and $\theta_0 \ge 0.43$	$\theta_0 \le 0.4$ and $\theta_0 \ge 0.46$	
1300	$0 \leq \theta_0 \leq 1.$	$0 \le \theta_0 \le 1.5$	
1550	$0 \le \theta_0 \le 1.5$	$0 \le \theta_0 \le 1.5$	

The structure is Octonacci with YBCO and SiO<sub>2</sub> materials  $(\lambda_0 = 1.5 \ \mu\text{m}, P = 17 \text{ and } ds = 3.2 \ \mu\text{m}$ 

Therefore, in this part, we will change the number of iteration and keep the minimum one that permits to cover alloptical fiber wavelengths. The reference wavelength  $\lambda_0$  is still fixed at 1.5 µm and the ambient temperature is 25 °C. Figure 4 shows the reflectance spectra for both polarization modes. In Fig. 4a the iteration number is changed to 6, so the number of layers P becomes 41 and the structure thickness is  $ds = 7.73 \mu m$ . In addition, Fig. 4b shows the reflectance spectra when the iteration number is equal to 7, therefore, the number of layers P becomes 99 and the structure thickness is  $ds = 18.67 \mu m$ . When changing the Octonacci iteration number and by comparing Fig. 4a and b with Fig. 3, we can conclude that the wavelengths 1300 and 1550 nm are still omnidirectional reflected. However, we note a slight improvement in the reflection range of the wavelengths 650 and 850 nm. Therefore, in the next parts, we will keep the iteration number fixed at 5 and we will study the effect of the layer thickness on the reflection of the optical communication wavelengths.

#### Layers thickness effect

The layers thickness is monitored by changing the reference wavelength  $\lambda_0$ . Figure 5 shows the reflectance spectra depends on  $\lambda_0$  for both polarization modes. The iteration number and the ambient temperature are set at 5 and 25 °C respectively. The geometric thickness of the structure is  $ds = 2.13 \mu m$ . Figure 3 and Fig. 5a show the reflection spectra for the same iteration number P = 5. In Fig. 5a and for TE and TM modes there are only two brown lines in which the reflectance ratio is more than 95%. Therefore, we notice here that when reducing  $\lambda_0$  from 1.5 to 1 µm all the optical communication wavelengths (650, 850, 1300 and 1550 nm) are reflected regardless of  $\theta_0$  value. In Fig. 5b the  $\lambda_0$  becomes equal to 0.5  $\mu$ m, so thickness of the structure is ds = 1.07  $\mu$ m. Here for TE mode, the wavelength 650 nm is reflected only when  $\theta_0 \leq 0.79$ rad and  $\theta_0 \geq 0.85$ rad and the rest of the optical communication wavelengths are fully omnidirectional reflected. In addition, in Fig. 5b and for TM mode the wavelength 650 nm is reflected only when  $\theta_0 \leq 0.73$ rad and  $\theta_0 \ge 0.82$ rad. The wavelength 1550 nm is reflected for  $\theta_0 \leq 1.34$ rad and the rest of the optical communication wavelengths are totally reflected. In Fig. 5c the reference wavelength  $\lambda_0$  is changed to 0.25 µm, therefore, the geometric thickness of the structure becomes  $ds = 0.53 \mu m$ . For TE mode, the wavelengths 850 and 1550 nm are transmitted for some intervals of the incident angle  $\theta_0$  and for TM mode all the optical communication wavelengths are not omnidirectional reflected. So at the end of this part we can conclude that, the best value of the reference wavelength  $\lambda_0$  for which all the optical communication wavelengths are omnidirectional reflected is 1 µm. Physically this phenomenon is due to the convergence between the optical layer thickness  $\left(\frac{\lambda_0}{4\times n}\right)$ and the central wavelength spectrum value. Indeed, our





**Fig. 4** Reflectance spectra of 1D Octonacci multilayered stack (with YBCO and SiO<sub>2</sub> materials  $\lambda_0 = 1.5 \ \mu$ m) as a function of wavelength ( $\mu$ m) and incident angle (rad) for TE- and TM-polarization modes: **a** iteration = 6, *P*=41 and **b** iteration = 7, *P*=99

spectrum is [0.6–1.6 µm], so the coincidence of the value of  $\lambda_0$  with the center of this interval (approximately 1 µm) allows us to have a large PBG centered at this value and cover the majority of optical fiber wavelengths. In addition, when changing the iteration number from 7 to 5 and the reference wavelength  $\lambda_0$  to 1 µm, the geometric thickness of the structure is optimized to be ds = 2.13 µm.

#### Ambient temperature effect

For this part, we keep the iteration number *P* and the reference wavelength  $\lambda_0$  fixed at 5 and 1 µm, respectively, and we try now to study the dependence between the temperature and the reflectance spectra of the optical communication wavelengths. Figure 6 displays the variation of the reflectance spectra with the temperature *T* and for both polarization modes. From Fig. 6, it turns out that



the weather temperature has little effect on the reflectance spectra of the optical communication wavelengths. When T = 0 °C and for the TM mode (see Fig. 6a) only the wavelength 650 nm has a reflectance of 65% when  $0.85 \le \theta_0 \le 0.95$  rad, and the other wavelengths have a reflectance of more than 85%. After that when increasing the temperature to be more than 20 °C all the optical communication wavelengths become high reflected regardless of  $\theta_0$  value. These structures open the way to be used as optical devices in the optical industry. Then we can conclude that the structure can keep their reflectance performance whatever the temperature degree of the environment. In fact, the refractive index of the YBCO materials depends on temperature and increases with it. Indeed, when the temperature is 0 °C only the wavelength 650 nm cannot be totally reflected. After that, and with the increase of temperature the refractive index of YBCO



**Fig. 5** Reflectance spectra of 1D Octonacci multilayered stack (with YBCO and SiO<sub>2</sub> materials  $\lambda_0 = 1.5 \ \mu\text{m}$ ) as a function of wavelength ( $\mu$ m) and incident angle (rad) for TE- and TM-polarization modes: **a**  $\lambda_0 = 1 \ \mu\text{m}$ , **b**  $\lambda_0 = 0.5 \ \mu\text{m}$  and **c**  $\lambda_0 = 0.25 \ \mu\text{m}$ 





**Fig. 6** Reflectance spectra of 1D Octonacci multilayered stack (with YBCO and SiO2 materials  $\lambda_0 = 1 \ \mu m$ ) as a function of wavelength ( $\mu m$ ) and incident angle (rad) for TE- and TM-polarization modes: **a**  $T = 0 \ ^{\circ}$ C, **b**  $T = 20 \ ^{\circ}$ C, **d**  $T = 60 \ ^{\circ}$ C



layers increases which permits the enlargement of the main PBG to cover all-optical fiber wavelengths.

### Comparison with some previous works

The published paper of Pandey et al. (2017), studied plasma photonic crystal (PPC) which consists of alternate layers of thin micro-plasma with dielectric material in one-dimensional periodic structure (containing SiO<sub>2</sub> and Air layers). By introducing the plasma defect inside the periodic structure the band gap is slightly widened and containing two transmission peaks in symmetry (Pandey et al. 2017). In addition, Nayak et al. (2019) studied the near- and mid-infrared PBGs using periodic photonic structure that was composed of superconductor and semiconductor-metamaterial. They found and optimized two PBGs by manipulating the thickness of the semiconductor layers, the fill factor of the semiconductor-metamaterial and the wave-incidence. The researcher here (Navak et al. 2019) found that for the TM polarization, the PBGs disappeared at the incident angles of approximately 1.05 rad. In addition The PBGs does not cover all the near- and mid-infrared spectrum. Furthermore, Hsueh et al. (2010), studied one-dimensional periodic structure in multiple frequency ranges and for both polarization. They found one maximum range of the omnidirectional gap in each region, which is divided by the half-wave lines. The paper of Ariza-Flores et al. (2012), shows a comparison between theoretical and experimental study of the omnidirectional photonic bandgap for dielectric mirrors based on porous silicon. Here (Ariza-Flores et al. 2012), the main PBG covers only the spectral range [1100–1195 nm]. The paper of Ali and Kanzari (2010), studied a modified hybrid Fibonacci/Cantor structure showed a mirror covering only the optical telecommunication wavelengths centered at 850 nm, 1300 nm and 1550 and for the incident angles situated outside of the range [0.91–1.43 rad]. In addition, Gahef et al. (2017) presents an omnidirectional mirror covering only the optical fibers wavelengths 1300 and 1550 nm using a deformed Bragg reflector. Finally, by comparing these previous published works with our own, we can notice the importance of using Octonacci structure instead of periodic structures as well the importance of using the YBCO superconductor instead of ordinary materials if we seek to enlarge the PBG to cover all the optical communication wavelengths (650, 850, 1300 and 1550 nm).

## Conclusion

At the end of this paper, we can conclude that using the semiconductor YBCO and silica slabs in Octonacci photonic crystal instead of the  $TiO_2$  and  $SiO_2$  slabs permits to construct omnidirectional high reflectors for the optical

communication wavelengths (650, 850, 1300 and 1550 nm). By changing the reference wavelength  $\lambda_0$  to be equal to 1  $\mu$ m, the geometric thickness of the photonic structure is optimized to be  $ds = 2.13 \mu m$ . In addition, the reflectance ratio of the optical communication wavelengths is significantly improved. In last part of this paper, the weather temperature effect on the reflectance spectra has been studied and a small effect on the reflectance ratio of these wavelengths is noticed. Whereas the most optical communication wavelengths were reflected with large rates that exceeded 85%. Only the 650 nm wavelength was 65% reflected when the wave is TM-polarized, the wave incident angle is  $0.85 \le \theta_0 \le 0.95$  rad and the weather temperature is 0 °C. As a perspective of this work, we can conclude that these structures can be realized experimentally and compared with the theoretical results found here.

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#### Declarations

**Conflict of interest** The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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