ORIGINAL ARTICLE

Thermal analysis in unsteady radiative Maxwell nanofuid fow subject to heat source/sink

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Abstract

Currently, various researchers achieved theoretical and experimental works to scrutinize the infuence of nanofuid in diverse forms of heat exchangers. In any engineering applications heat exchangers are critical components. Nanofuids are colloidal assortment of non-metallic or metallic particles suspended in base liquid. This study communicates a critical analysis of heat transport application of nanofuid. We established a model for unsteady fow of Maxwell nanofuid with the aspect of thermal radiation due to stretched cylinder. Moreover, heat source/sink is considered. Appropriate conversions yield the ordinary differential equations (ODEs) and then solved via homotopic methodology. Graphical outcomes of the velocity, temperature and concentration felds for infuential parameters are plotted and discussed physically. The achieved outcomes specify that the temperature and concentration distribution increases for the higher unsteadiness parameter, curvature parameter and Maxwell parameter. Moreover, both thermophoresis and Brownian motion parameters enhances the thermal energy transport in fow.

Keywords Maxwell fluid model · Unsteady flow · Nanofluid · Thermal radiation · Heat source/sink

Introduction

The subject of the heat transfer analysis attract the researchers now a days due its importance in the many engineering areas specially the heat transport in the fuid fow. Such as production of plastic and polymers needs the higher rate of heat transport for the better quality of the product. To replace the working liquids with nanoparticles as a innovative approach to enhance the heat transport phenomena in liquid. Nanofuid is a colloidal fusion where the possession of both nanomaterials and base liquids provide the change in the transport and thermal aspects of base liquids. In recent, diverse sorts of nanoparticles, for the instance, metallic and ceramic nanoparticles, have been utilized for formation of nanofuids. The notion of nanofuids concerning heat transport enhancement through dense particles of nano-meter was reported by Choi ([1995](#page-8-0)). Hsiao [\(2016\)](#page-8-1) analyzed the mixed convective stagnation point fow of nanofuid with the slip

 \boxtimes Abdul Hafeez ahafeez@math.qau.edu.pk boundary condition on the stretching sheet. Magnetohydrodynamics fow of micropolar nanofuid over stretching sheet under the impact of viscous dissipation was reported by Hsiao [\(2017](#page-8-2)). This study revealed that both magnetic parameter and Eckert number enhance the temperature feld. By utilizing FEM scheme, Haq and Aman [\(2019\)](#page-8-3) investigated the performance of *CuO* nanoparticles with inner heated obstacle, in partially heated trapezoidal cavity. Xu et al. ([2019\)](#page-8-4) studied the phenomena of thermal radiation, heat convection/conduction and phase change heat transport to nanofuid. The properties of radiation and chemical reaction in Maxwell nanofuid were addressed by Hayat et al. ([2019\)](#page-8-5). Impacts of activation energy and chemical reaction in peristaltic blood fow with nanoparticles was explored by Ellahi et al. ([2019\)](#page-8-6). They noted that the gold particles condenses large particles to transport important drugs powerfully to the efected portion of the organ. Additionally, relevant works dealing with nanofuid were reported in see Refs. Irfan et al. [\(2019\)](#page-8-7), Mahanthesh and Joseph ([2019](#page-8-8)), Khan et al. [\(2019\)](#page-8-9), Turkyilmazoglu ([2019a\)](#page-8-10), Turkyilmazoglu ([2019b](#page-8-11)) and Turkyilmazoglu [\(2020\)](#page-8-12).

Recently, the study of non-linear fuids have noteworthy consideration due to their practical applications in engineering and trade. For instance, piping, extrusion methodology in metallurgy, in large scale cooling/heating structures, and

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oil recovery etc includes the fow of non-linear liquids. To increase the efficiency in thermal extrusion manufacturing Hsiao [\(2017a\)](#page-8-13), Hsiao ([2017b\)](#page-8-14) studied the fow of non-Newtonian nanofuid with impact of thermal radiation, magnetic feld and viscous dissipation. One important aspect of these fuids is their advanced apparent viscosity. Additionally, various researchers have reported their investigations for the fow of non-linear fuids with diverse aspects (see Refs Malik and Khan [2018](#page-8-15); Bai et al. [2019](#page-7-0); Moshkin et al. [2019](#page-8-16); Khan and Nadeem [2019](#page-8-17); Hamid et al. [2018\)](#page-8-18). The considered Maxwell fuid model is the special type of non-Newtonian fuid in which the characteristics of both elastic and viscous forces are described. This model is good for viscoelastic fuids because it can described the stress relaxation phenomenon accurately in these types of fuid. Ahmed et al. ([2019\)](#page-7-1) analyzed thin flm fow Maxwell fuid with heat transport in the presence of non-linear radiation. The convective phenomena on Maxwell fuid utilizing Brownian and thermophrotic forces for nanofuid was studied by Khan et al. [\(2019\)](#page-8-19).

In view of the above studies, we noted that no study has been made to report the unsteady flow of Maxwell nanofluid towards stretched cylinder. Thus, the present analysis is reported to investigate the fow and heat transport of Maxwell nanofuid with impact of heat source/sink and thermal radiation. Additionally, the Brownian and thermophoretic forces are taken in account to study the convective heat transport enhancement. The well known homotopic approach (Turkyilmazoglu [2011](#page-8-20), [2012](#page-8-21), [2018\)](#page-8-22) is employed for solutions of the governing problem. The results are presented graphically and validated through tabular data.

Mathematical formulation

Consider 2D unsteady fow of Maxwell nanofuid induced by stretching cylinder of radius R_1 . The cylinder is stretched with velocity $u(t, z) = \frac{az}{1-\gamma t}$ along *z*−direction, where $a = \frac{U_0}{L}$ is the stretching rate, γ the positive constant with property $\gamma t \leq 1$. Let the cylindrical polar coordinates (z, r) are taken to be in such approach that *z* − *axis* runs along the axis of the cylinder and $r - axis$ is restrained perpendicular to it as exposed in blow (Fig. [1\)](#page-1-0). Additionally, heat sink/source aspects are considered. Under above consideration the governing boundary layer equations (Moshkin et al. [2019;](#page-8-16) Khan et al. [2019\)](#page-8-19) for Maxwell nanofuid model are specifed as follows.

$$
\frac{\partial(ru)}{\partial z} + \frac{\partial(rw)}{\partial r} = 0,\tag{1}
$$

Fig. 1 Physical sketch of the problem

$$
\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial z} + w \frac{\partial u}{\partial r} = v \left[\frac{\partial^2 u}{\partial r^2} + \frac{1}{r} \frac{\partial u}{\partial r} \right] \n- \lambda_1 \left[\frac{\partial^2 u}{\partial t^2} + 2u \frac{\partial^2 u}{\partial t \partial z} + 2w \frac{\partial^2 u}{\partial r \partial t} + 2uw \frac{\partial^2 u}{\partial r \partial z} + w^2 \frac{\partial^2 u}{\partial r^2} + u^2 \frac{\partial^2 u}{\partial z^2} \right],
$$
\n(2)

$$
\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial z} + w \frac{\partial T}{\partial r} = \alpha_1 \left[\frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} \right] \n- \frac{1}{(\rho c)_f} \left[\frac{1}{r} \frac{\partial}{\partial r} (rq_r) \right] \n+ \tau \left[D_B \frac{\partial C}{\partial r} \frac{\partial T}{\partial r} + \frac{D_T}{T_{\infty}} \left(\frac{\partial T}{\partial r} \right)^2 \right] + Q_{\circ} \left(\frac{T - T_{\infty}}{(\rho c)_f} \right),
$$
\n(3)

$$
\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial z} + w \frac{\partial C}{\partial r} = D_B \frac{1}{r} \frac{\partial}{\partial r} \left[\left(r \frac{\partial C}{\partial r} \right) \right] \n+ \frac{D_T}{T_{\infty}} \frac{1}{r} \frac{\partial}{\partial r} \left[\left(r \frac{\partial T}{\partial r} \right) \right],
$$
\n(4)

with boundary conditions

$$
u(t, z, r) = u(t, z) = \frac{az}{1 - \gamma t}, \ w(t, z, r) = 0,
$$

\n
$$
T = T_w, \ C = C_w \text{ at } r = R_1,
$$
\n(5)

$$
u \to 0, T \to T_{\infty}, C \to C_{\infty} \text{ as } r \to \infty.
$$
 (6)

Here (*u*, *w*) are the velocity components in the *z*− and *r*− directions, respectively, ν the kinematic viscosity, λ_1 the relaxation time, α_1 the thermal diffusivity, (T, C) the temperature and concentration of fluid, τ the heat capacity ratio of nanoparticles to base fluid and Q_0 the source/sink, T_w and C_w the wall temperature and concentration, respectively, T_∞ and C_{∞} the ambient temperature and concentration of fluid,

 08

 0.6

 0.2

 $\pmb{0}$

 $\overline{0}$

 $\widehat{\mathbf{e}}_{_{0.4}}$

Fig. 2 Impact of curvature parameter α on $\theta(\eta)$ and $\phi(\eta)$

 $\overline{2}$

 α = 0.1, 0.5, 0.9, 1.3

respectively, (D_B, D_T) the Brownian and thermophoresis diffusion coefficients, respectively. q_r the radiative heat flux which defned as

 η

 10

 $q_r = \frac{-16\sigma^*}{3k_*}T_{\infty}^3$ *𝜕T* $\frac{\partial T}{\partial r}$ where (σ^* , k *) the Stefan -Boltzmann constant and mean absorption coefficient, respectively.

Introducing the following conversions

Above conversions yield the following ODEs of Maxwell nanofluid flow with energy transport:

Fig. 3 Impact of Maxwell parameter β_1 on $\theta(\eta)$ and $\phi(\eta)$

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Fig. 4 Impact of thermophoresis N_t and Brownian motion parameters N_b on $\theta(\eta)$

Fig. 5 Impact of thermophoresis N_t and Brownian motion parameter N_b on $\phi(\eta)$

$$
(1 + 2\alpha\eta)f''' + 2\alpha ff'' - \frac{S}{2}\eta f'' - Sf'
$$

\n
$$
-f'^2 + ff'' - \frac{7}{4}\beta_1 S^2 \eta f''
$$

\n
$$
- \frac{\beta_1}{4}\eta^2 S^2 f''' - 2\beta_1 S^2 f' - 2S\beta_1 f'^2
$$

\n
$$
- \beta_1 \eta Sf' f'' + 3S\beta_1 ff''
$$

\n
$$
+ S\beta_1 \eta f'''' + 2\beta_1 f f' f''
$$

\n
$$
- \frac{\alpha \beta_1}{1 + 2\alpha \eta} f^2 f'' - \beta_1 f^2 f''' = 0,
$$

\n(8)

$$
(1 + \frac{4}{3}R_d)(1 + 2\alpha\eta)\theta'' + 2\alpha\theta' + \Pr f\theta' - \Pr \frac{S}{2}\eta\theta'
$$

+ (1 + 2\alpha\eta) \Pr N_b\theta'\phi' + (1 + 2\alpha\eta) \Pr N_t\theta'^2 + \Pr \delta\theta = 0, (9)

$$
(1 + 2\alpha\eta)\phi'' + 2\alpha\phi' + Le \Pr f\phi' - Le \Pr \frac{S}{2}\eta\phi'
$$

$$
+ (1 + 2\alpha\eta)\left(\frac{N_t}{N_b}\right)\theta'' + 2\alpha\left(\frac{N_t}{N_b}\right)\theta' = 0,
$$
(10)

with boundary conditions

$$
f(0) = 0, f'(0) = 1, \ \theta(0) = 1, \ \phi(0) = 1,\tag{11}
$$

Fig. 6 Impact of unsteadiness parameter *S* on $\theta(\eta)$ and $\phi(\eta)$

 0.8

 06

 $0₄$

 0.2

 $\mathbf 0$

 $\phi(n)$

Fig. 7 Impact of Prandtl number Pr and Lewis number *Le* on $\theta(\eta)$ and $\phi(\eta)$, respectively

$$
f'(\infty) = 0, \ \theta(\infty) = 0, \ \phi(\infty) = 0. \tag{12}
$$

Where *S* $\left(=\frac{y}{q}\right)$ is the unsteadiness parameter, $\alpha\bigg(=\frac{1}{R_1}$ $\sqrt{\frac{v(1-\gamma t)}{v(1-\gamma t)}}$ *a* the curvature parameter, $\beta_1 = \frac{\lambda_1 a}{1 - \gamma t}$ the Maxwell parameter, $Pr\left(=\frac{v}{\alpha_1}\right)$) the Prandtl number, N_b $\left(= \frac{\tau D_B(C_w - C_\infty)}{v} \right)$ the Brownian motion parameter, N_t $\left(= \frac{\tau D_T (T_w - T_\infty)}{\nu T_\infty} \right)$ the thermophoresis parameter, $Le \left(= \frac{\alpha_1}{D_B} \right)$ $\big)$ the Lewis number, R_d $\left(= \frac{4\sigma^* T_{\infty}^3}{k k^*} \right)$ radiation parameter and δ $\left(= \frac{Q_0(1-\gamma t)}{a(\rho c)_f} \right)$) the heat source/sink parameter.

(∞) = 0, *^𝜃*(∞) = 0, *^𝜙*(∞) = 0. **Physical quantities**

Expressions for the local Nusselt (*Nuz*) and local Sherwood (*Sh_z*) numbers are

 $S = 0.1, 0.5, 0.7, 0.9$

 η

$$
Nu_z = \frac{zq_s}{k(T_w - T_\infty)}, Sh_z = \frac{zj_s}{D_B(C_w - C_\infty)},
$$
\n(13)

where q_s and j_s are the heat and mass fluxes, respectively,

Fig. 8 Impact of heat sink $\delta < 0$ and heat source $\delta > 0$ on $\theta(\eta)$

Fig. 9 Impact of radiation parameter R_d on $\theta(\eta)$

Table 1 A comparison of $-f''(0)$ for β_1 when $\alpha = S = 0$

$$
q_s = -k \left(\frac{\partial T}{\partial r}\right)_{r=R_1} - \frac{4\sigma^* T_{\infty}^3}{3k^*} \left(\frac{\partial T}{\partial r}\right)_{r=R_1},
$$

\n
$$
j_s = -D_B \left(\frac{\partial C}{\partial r}\right)_{r=R_1},
$$
\n(14)

in dimensionless forms these are given by

$$
Nu_{z}\text{Re}_{z}^{-\frac{1}{2}} = -\left(1 + \frac{4R_{d}}{3}\right)\theta'(0), Sh_{z}\text{Re}_{z}^{-\frac{1}{2}} = -\phi'(0), \quad (15)
$$

where $\text{Re}_z = \frac{u(t,z)z}{v}$ signifies the Reynolds number.

Solution scheme

To achieve the series solutions of Eqs. (8) (8) – (10) along the boundary conditions given in Eqs. ([11,](#page-3-2) [12](#page-4-0)) the well known homotopy analysis method for the highly non-linear ordinary diferential system has been utilized. The following

f ��(0)

Table 2 A comparison of $f''(0)$ for *S* when $\alpha = \beta_1 = 0$

| f''(0) | | | | |
|--------|-------------------------------------|------------------------------------|-----------------------------|-------------|
| S. | Ref. Shari- dan et al. (2006) | Ref. Cham- kha et al. (2010) | Ref. Irfan et al. (2017) | Present |
| 0.8 | -1.261042 | -1.261512 | -1.261044 | -1.261043 |
| 1.0 | | | | -1.320522 |
| | $1.2 -1.377722$ | -1.378052 | -1.377728 | -1.377722 |
| 1.3 | | | | -1.405538 |
| 2.0 | -1.587362 | | -1.587371 | -1.587372 |

Table 3 A comparison of $-\theta'(0)$ for Pr when $\alpha = S = \beta_1 = N_t$ $= R_d = \delta = 0$, and $N_b \rightarrow 0$

initial estimates (f_0, θ_0, ϕ_0) and linear operators (f_f, f_θ, f_ϕ) are selected for the governing problem as

$$
f_0(\eta) = 1 - e^{-\eta}, \ \theta_0(\eta) = e^{-\eta}, \ \phi_0(\eta) = e^{-\eta}, \tag{16}
$$

$$
\mathcal{L}_f[f(\eta)] = f''' - f', \mathcal{L}_\theta[\theta(\eta)] = \theta'' - \theta, \mathcal{L}_\phi[\phi(\eta)]
$$

= $\phi'' - \phi.$ (17)

Results and discussion

This section discusses the aspects of infuential parameters on the velocity, temperature and concentration felds via homotopic scheme. The outcomes for scheming parameters are graphed and discussed in detail with physical arguments. The value of physical parameters are taken to be fixed as $S = \beta_1 = \alpha = R_d = 0.5$, $\delta = 0.2$, $N_t = N_b = 0.4$ and $Le = Pr = 7$. Figure [2](#page-2-0) illustrate the effect of curvature parameter α on nanoliquid temperature and concentration felds. We observed that the temperature, and concentration felds of Maxwell nanoliquid are increasing function of α . Physically, rise in the curvature parameter α declines the radius of cylinder due to which the interaction region of the cylinder with the liquid is diminished. Hence, fuid

Nusselt number and Sherwood number for various values of N_t , N_b , R_d and with fixed $S = \alpha = \beta_1 = 0.5$ and $\delta = 0.2$

Table 4 Numerical values of

infuenced in stretching cylinder is less. Furthermore, we noted that the higher values of α enhance both the temperature and its allied thermal thickness of boundary layer. The impact of α on temperature field is more prominent than the concentration feld. The temperature and concentration felds for Maxwell parameter are portrayed in Fig. [3](#page-2-1). From these interpretation, it is observed that the intensifcation in β_1 enhances both the temperature and concentration distribution in Maxwell liquid. As β_1 is the ratio of relaxation time to observation time and rise in β_1 means there is higher the relaxation time in the fuid. Due to which the fuid becomes solid like and consequently, the conduction of thermal and solutal energy increases in the fluid motion. Figures [4](#page-3-3) and [5](#page-3-4) are represented to envision the impact of thermophoresis N_t and Brownian motion N_b parameters on nanoliquid temperature and concentration felds. Here, we reported that a rise in the value of N_t enhances both the temperature and concentration fields. Physically, higher value of N_t enhances the temperature diference between wall and free stream. Hence, the heat transfer rate is enhanced which enhances the temperature feld. Furthermore, rise in Brownian motion parameter N_b causes the enhance of temperature field. Because for higher value of N_b the collision of nanoparticles boost up which intensify the temperature feld. On the other hand, concentration feld declines with higher values of N_b . Physically, for higher values of N_b the particles collision provides the disturbance for mass transfer and thus, as a result the declines in concentration feld is noted. To picture the impact of unsteadiness parameter *S* on nanoliquid temperature and concentration of Maxwell fuid Fig. [6](#page-4-1) are delineated. We observed that enhancement in the value of *S* rises the temperature and concentration felds. The impact of Prandtl number Pr and Lewis number *Le* on temperature and concentration felds, respectively, are visualized in Fig. [7.](#page-4-2) We noted that the increase in Pr and *Le* result in decreases the thermal and mass difusivity of naoliquid which declines the temperature and concentration in the Maxwell fuid fow. The temperature field for the effects of heat source/sink δ is illustrated in Fig. [8.](#page-5-0) The temperature feld increases for higher values of heat source and it declines for increasing heat sink parameter. Physically, the heat source provides the additional heat to the liquid which enhances the temperature feld and converse behavior is true for heat sink parameter. Moreover, for δ < 0 much heat is absorbed which declines temperature field. The effect of radiation parameter R_d on temperature feld is illustrated in Fig. [9](#page-5-1). We noted that the increase in values of R_d results in an enhancement in the heat transfer rate. Physically, the increase in R_d rises the ambient temperature of nanofuid and declines the mean absorption coefficient. Hence, the heat transfer rate increases which enhances the temperature feld.

Tabular comparisons

Tables [1](#page-5-2) and [2](#page-6-0) are assessment tables of $-f''(0)$ for different values of β_1 and *S* for Newtonian case. Table [3](#page-6-1) is a comparison of $-\theta'(0)$ in limiting case for various values of Pr . From these tables, we noted that the current outcomes are appropriate which assured the validation of our scheme. Table [4](#page-6-2) is also established for the Numerical values of Nusselt and Sherwood numbers for various values of N_t , N_b , R_d and M . These numerical values of Nusselt and Sherwood number are obtained by utilizing the built in MATLAB scheme namely as bvp4c. From these results we conclude that the higher value of both thermophoretic and Brownian forces decline the thermal gradient at the surface of cylinder.

Concluding remarks

A mathematical analysis for unsteady 2D fow of radiative Maxwell nanofuid with heat and mass transport in presence of heat source/sink has been achieved. Homotopy approach (HAM) has been utilized for the solutions of ODEs. The fnal conclusions of our study are given below:

- The unsteadiness parameter *S* enhanced both the temperature and concentration distributions.
- Both temperature and concentration felds enhanced for higher values of curvature parameter α .
- An increase in the value of Maxwell parameter β_1 augmented both the temperature and concentration felds.
- Temperature of Maxwell fuid intensifed for increasing Brownian motion parameter N_b whereas, conflicted behavior was noted on concentration feld.
- The temperature fields declined for higher value of Prandtl number Pr.
- Increase in radiation parameter R_d boost up the temperature profle.

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