ORIGINAL ARTICLE

Chemically reactive swirling fow of viscoelastic nanofuid due to rotating disk with thermal radiations

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Abstract

Researchers and engineers working in the feld of thermal analysis are in the pursuit of innovative methods to improve the performance of energy devices by enhancing their thermal characteristics. Aimed at this purpose, the fuid fow investigation comprising of nanoparticles is supposed to be one of the best signifcant procedures for augmenting heat transfer systems. The current study describes the investigation of Buongiorno model for the evaluation of transient fow and heat transfer of Maxwell nanofuids over a rotating and vertically moving disk. The signifcant impact of Lorentz forces due to the interaction of magnetic feld applied vertically on Maxwell fuid is also investigated. Additionally, the chemical reaction and thermal radiation efects have been discussed on heat and mass transfer mechanisms. Furthermore, Brownian motion and thermophoresis characteristics are studied due to nanofuids. With the help of similar transformations, the equations of motion are simplifed into a set of a nonlinear system of ordinary diferential equations. The solution of the problem is presented via numerical technique, namely bvp4c in Matlab. The numerical outcomes are illustrated through graphical and tabular forms. It is observed that the upward and downward motion of the disk exert similar efects to that of the injection/ suction through the wall. The boundary layer thickness of temperature and concentration felds are enhanced due to the presence of thermophoresis force. The impact of Lorentz force is to reduce the radial and azimuthal velocities and increase the temperature of nanofuid. Furthermore, it is noticed that the concentration profle reduces with the thermophoresis efect and Schmidt number.

Keywords Rotating disk · Maxwell nanofluid · Buongiorno model · Radiative flow · Numerical solutions

Abbreviations

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Introduction

The heat transfer mechanisms are important due to the efficiency of many technological and industrial applications. Over the decade, the scientists and engineers are taking advantages of nanofuid technology, to achieve the required goal. The term "nanofuid" was frst proposed by Choi and Eastman [\(1995](#page-12-0)). Recently, the practical applications of nanofuid in heat transfer equipment include radiators, heat exchanger, solar collectors, electronic cooling system, detergency, automobile, and medical applications. Temperature plays an important role in increasing the efect of thermal conductivity of nanofuid. However, the performance of the thermal conductivity depends on size, shape, and material of nanofuid. For example, metallic nanofuid have higher thermal conductivity than non-metallic nanofuid and the small-sized nanoparticle has higher thermal conductivity as compared to the large-sized nanoparticles. The temperature effects on the thermal conductivity have been studied in Refs. Das et al. [\(2003\)](#page-12-1), Chon and Kihm [\(2005](#page-12-2)), and Li and Peterson ([2006](#page-12-3)). The features of two slip mechanisms called Brownian difusion and thermophoresis were studied by Buongiorno [\(2006](#page-12-4)). These two features of nanofuid create enhanced heat transfer efects which were presented by Sheikholeslami et al. ([2014\)](#page-12-5). Heat transfer in nanofluid flow over a fat plate with the help of self-similar transformations was given by Avramenko et al. [\(2014\)](#page-12-6). The three-dimensional flow of nanofluid due to stationary or moving surface was presented by Khan et al. ([2014](#page-12-7)). Hayat et al. ([2015\)](#page-12-8) proposed the model for magnetohydrodynamic (MHD) three-dimensional flow over a couple of stress nanofluid in the presence of nonlinear thermal radiation over a stretchable surface. The stagnation point of the rotating nanofuid in boundary layer flow on the external surface was given by Anwar et al. (2015) . The nanofluid flow between two parallel plates in the presence of a magnetic feld was studied by Sheikholeslami et al. [\(2016](#page-12-10)). Mustafa [\(2017](#page-12-11)) studied the Buongiorno model of nanofluid flow due to a rough rotating disk. Khan et al. (2018) discussed the nanofluid flow over a rotating disk

under the infuence of magnetic feld and dissipation efects. The effects of chemically reaction, magnetic field and heat source on Sutterby nanofluid flow due to rotating stretchable disk were examined by Hayat et al. [\(2018\)](#page-12-13). The motion of nanofuid thin flm on a rotating disk under the infuence of non-linear thermal radiation was studied by Ahmed et al. [\(2019](#page-12-14)). Some recent articles on nanofuids are given in Refs. Turkyilmazoglu [\(2016](#page-13-0)), Turkyilmazoglu ([2019a](#page-13-1), [b\)](#page-13-2), Ahmed et al. [\(2019a,](#page-12-15) [b](#page-12-16), [c\)](#page-12-17), and Turkyilmazoglu [\(2020](#page-13-3)).

The heat transfer flow problem over a rotating disk has numerous practical applications in various engineering applications such as rotating machinery, gas turbine rotator, air cleaning machines, thermal power generating systems, computer storage devices, and electronic devices. The current problem also discusses the heat transfer fow over rotating disk in the presence of nanofuid, which is a quite interesting topic in recent literature. At very frst in 1920, Karman ([1921](#page-12-18)) presented the problem for rotating disk to the case of fow impulsively starting from rest. Following the pioneering work of Karman, many new problems have been introduced to the rotating disk fow problem, e.g., the surface of rotating disk having suction/injection properties was studied in Stuart [\(1954](#page-13-4)) and Kuiken ([1971\)](#page-12-19). The transfer of heat from an air-cooled rotating disk was proposed by Owen et al. ([1974](#page-12-20)). Hall [\(1986\)](#page-12-21) and Jarre et al. [\(1996\)](#page-12-22) have studied the aspects of rotating disk problem theoretically, numerically and experimentally. The characteristics of fow and heat transfer due to rotating disk was presented by Turkyilmazoglu [\(2014](#page-13-5)). Khan et al. [\(2020a](#page-12-23), [b](#page-12-24)) presented the Maxwell fuid model for rotating and vertically moving disk by analyzing fow features, MHD and non-linear thermal radiation over a rotating disk.

Fluids such as water, oil, and air are classifed as Newtonian fuids, while the non-Newtonian fuids are honey, blood, paint polymer solution, corn starch in water, ketchup, motor oil, lubricant spray, cofee in water and hydraulics fuids. However, in many industrial process of fuid motion, we have to deal with non-Newtonian fuids, due to the fact that various assumptions of Newtonian behavior are not valid. In general terms "non-Newtonian" is related as viscoelastic. Non-Newtonian can be defned as the dependence of its viscosity to the stress applied but this does not mean that all non-Newtonian fuids need to have elastic properties. There are some examples of inelastic behavior, i.e. shear stress dependence on viscosity in Bird et al. ([1977\)](#page-12-25). Ezzat ([2010\)](#page-12-26) investigated the conducting thermoelectric materials for a new class of thermoelectric non-Newtonian fuids. The applications and perspective of non-Newtonian fuids in industries were given by Peng et al. ([2014](#page-12-27)). Nadeem et al. [\(2014\)](#page-12-28) investigated a model of non-Newtonian nanofuid over a stretchable sheet. The characteristic connection of non-Newtonian nanofuid between two vertical plates is investigated analytically and numerically by Hatami and Ganji [\(2014](#page-12-29)).

Radiative efects are important during the heat transfer process because they have many applications in engineering, industries, and material science, for instance, gas for a cooled reactor, glass production, furnace design, polymer preparing, in space technology, etc. Furthermore, electromagnetic waves are responsible for transfer heat and energy via radiations. However, there is no attempt in the literature to consider the radiation efects on fow and heat transfer of Maxwell nanofluid over a vertically moving rotating disk. Radiation effects on free convection viscous incompressible flow past a vertical porous plate with uniform temperature and suction were analyzed by Hossain et al. ([1999](#page-12-30)). Some investigations regarding the effects of thermal radiation using linearized Rosseland approximation are given in Refs. Ellahi et al. ([2016\)](#page-12-31), Akbar et al. ([2016\)](#page-12-32), Alebraheem and Ramzan [\(2019\)](#page-12-33), Ellahi et al. ([2019](#page-12-34)), Alamri et al. ([2019](#page-12-35)), Sarafraz et al. ([2020](#page-12-36)), and Ellahi et al. [\(2020](#page-12-37)). Efects of thermal radiation in the peristaltic fow of Jefrey nanofuid and MHD nanofluid flow are discussed by Hayat et al. [\(2016](#page-12-38), [2015](#page-12-39)).

The aim of the present work is to investigate the effects of non-linear thermal radiation on the fow and temperature felds across an unsteady MHD nanofuid over a vertically moving disk. Buongiorno's model is implemented for the current analysis to show the impact of Brownian motion and thermophoresis due to nanoparticles. Using Karman transformation variables, the motion equations are integrated numerically for solution through the built-in scheme, namely *bvp*4*c* in MATLAB. Graphical behavior is presented to describe the role of physical parameters. Such as wall motion, magnetic parameter, Deborah number, and Schmidt number.

Mathematical modeling

The graphical view of rotating and vertically moving disk geometry is shown in Fig. [1.](#page-2-0) We consider an incompressible Maxwell nanofuid over a rotating and vertically moving disk. The physical problem is associated with the cylindrical coordinates (r, φ, z) with the directions of radial, azimuthal and axial as (*u*, *v*, *w*), respectively. A uniform beam of magnetic feld is thrown along the z-axis. A well-known Buongiorno's model is implemented to trace the features of thermophoresis and Brownian difusion. Furthermore, the disk is rotating as well as vertically moving so we have an ambient temperature T_{∞} and concentration C_{∞} of fluid, whereas the disk is subjected to the time-dependent wall temperature $T_w(t)$ and time-dependent wall concentration $C_w(t)$. So this will make the diference in temperature and concentration. Temperature and concentration diference are given as

$$
\Delta T = T_w(t) - T_{\infty}, \ \Delta C = C_w(t) - C_{\infty}.
$$
 (1)

Fig. 1 Flow confguration

The expressions for wall temperature (Turkyilmazoglu [2018\)](#page-13-6) and concentration are given as

$$
T_w(t) = \text{ca}(t)^{-2\alpha_1} + T_{\infty}, \ C_w(t) = \text{ca}(t)^{-2\alpha_2} + C_{\infty}, \tag{2}
$$

where *c* is the arbitrary constant and α_1 and α_2 are the wall temperature and wall concentration parameters, respectively. When $\alpha_1 = \alpha_2 = 0$, then the wall is sustained a constant wall temperature and constant wall concentration.

These assumptions lead to the following flow problem (Ahmed et al. [2019b\)](#page-12-16):

$$
u_r + \frac{u}{r} + w_z = 0,\t\t(3)
$$

$$
u_{t} + uu_{r} + wu_{z} - \frac{v^{2}}{r} + \lambda_{1}
$$
\n
$$
\begin{pmatrix}\nu^{2}u_{rr} + u_{tt} + 2uu_{rt} + 2wu_{zt} - 2\frac{v}{r}v_{t} - \frac{2vu}{r}v_{r} + \frac{v^{2}u}{r^{2}} - \frac{2wv}{r}v_{z} \\
+2wu_{rz} + w^{2}u_{zz} + \frac{v^{2}}{r}u_{r}\n\end{pmatrix}
$$
\n
$$
= v\{u_{zz}\} - \frac{\sigma B_{o}^{2}}{\rho f}(u + \lambda_{1}(u_{t} + wu_{z})),
$$
\n(4)

$$
v_{t} + wv_{z} + uv_{r} + \frac{vu}{r} + \lambda_{1}
$$
\n
$$
\begin{pmatrix}\nu^{2}v_{rr} + w^{2}v_{zz} + v_{tt} + 2uv_{rt} + 2\frac{v}{r}u_{t} + 2wv_{zt} - \frac{2vu^{2}}{r^{2}} + \frac{2vu}{r}u_{r} - \frac{v^{3}}{r^{2}}\\+2u w v_{rz} + \frac{2wv}{r}u_{z} + \frac{v^{2}}{r}v_{r}\end{pmatrix}
$$
\n
$$
= v\{v_{zz}\} - \frac{\sigma B_{o}^{2}}{\rho f}(v + \lambda_{1}(v_{t} + wv_{z})), \tag{5}
$$

$$
T_t + uT_r + wT_z + \frac{1}{\rho c_p} (q_{rad})_z
$$

= $\alpha \{T_{zz}\} + \tau \left(D_B T_z C_z + \frac{D_T}{T_{\infty}} (T_z)^2 \right),$ (6)

$$
C_t + uC_r + wC_z = \frac{D_T}{T_{\infty}}(T_{zz}) + D_B(C_{zz}),
$$
\n(7)

where the subscripts involving either of the variables *r*, *z*, and *t* represent the partial derivatives. Further (u, v, w) show the velocity components, (C, T) concentration and temperature, respectively, τ shows the heat capacities of ratio. (D_B, D_T) denote the Brownian diffusion and thermophoresis diffusion coefficients. With the help of Rosseland approximation, the radiative heat flux q_{rad} in Eq. ([6\)](#page-2-1) can be written as Ahmed et al. [\(2019b\)](#page-12-16)

$$
q_{\text{rad}} = -\frac{4\sigma^*}{3k^*} (T_z^4) = -\frac{16\sigma^* T^3}{3k^*} T_z.
$$
 (8)

In the above expressions, k^* and σ^* are denoted as mean absorption coefficient and Stefan–Boltzmann constant. Using Eq. (8) (8) in Eq. (6) (6) , we get

$$
T_t + uT_r + wT_z - \frac{16\sigma^*}{3\rho c_p k^*} (T^3 T_z)_{z}
$$

= $\alpha (T_{zz}) + \tau \left(D_B T_z C_z + \frac{D_T}{T_{\infty}} (T_z)^2 \right).$ (9)

Boundary conditions

The physical problem is modeled under the following conditions (Turkyilmazoglu [2018\)](#page-13-6):

$$
u = 0, v = \Omega(t)r, w = \beta a(t), C = C_w(t),
$$

\n
$$
T = T_w(t) \text{ at } z = a(t),
$$

\n
$$
u = v = 0, C = C_{\infty}, T = T_{\infty} \text{ as } z \to \infty,
$$
\n(10)

where β is the strength of wall porosity. The constant value of $\beta = 1$ implies $w = a(t)$ which means the moving surface is impermeable having no heat and mass transfer workout. As we are discussing the action of wall motion, the strength of wall porosity is either wall suction or wall injection. Here we classified the wall injection for the value $\beta > 1$ and for the wall suction β < 1. In the current study, the wall strength is set to be fixed with $\beta = 2$.

Similarity hypothesis

We define the following transformations (Hayat et al. [2015](#page-12-39)):

$$
(u, v, w, T, C)
$$

= $\left(F\frac{rv}{a^2(t)}, G\frac{rv}{a^2(t)}, H\frac{v}{a(t)}, T_{\infty} + \Delta T\theta, C_{\infty} + \Delta C\phi\right),$

$$
(\eta, \eta_t, \eta_z) = \left(\frac{z}{a(t)} - 1, -\frac{a(t)}{a(t)}(\eta + 1), \frac{1}{a(t)}\right),
$$
 (11)

where η is the non-dimensional distance measured along the axis of rotation, *F*, *G* and *H* are the radial velocity, tangential velocity and axial velocity, respectively, and these are the functions of η . Using Eq. ([11\)](#page-3-1) in Eqs. ([3–](#page-2-2)[5\)](#page-2-3), [\(7](#page-3-2)), [\(9](#page-3-3)) and (10) (10) , we obtain

$$
2F + H' = 0,\t(12)
$$

$$
F'' - F^2 + G^2 - HF' + S(1 - S\beta_1) \left(F + \frac{\eta + 1}{2} F' \right)
$$

\n
$$
- \frac{3}{2} S^2 \beta_1 \left(F + (\eta + 1) F' + \frac{(\eta + 1)^2}{6} F'' \right)
$$

\n
$$
+ 2\beta_1 (2HGG' - 2HFF' + H^2F'')
$$

\n
$$
- M \left(F - S\beta_1 (F + \frac{\eta + 1}{2} F') + \beta_1 HF' \right) + 2S\beta 1
$$

\n
$$
\left(HF + F^2 - G^2 + \frac{(\eta + 1)}{2} (FF' + GG' + HF'') \right)
$$

\n= 0, (13)

$$
G'' - 2FG - HG' + S(1 - S\beta_1) \left(\frac{\eta + 1}{2}G' + G\right)
$$

\n
$$
- \frac{3}{2}S^2 \beta_1 \left(G + (\eta + 1)G' + \frac{(\eta + 1)^2}{6}G''\right)
$$

\n
$$
- 2\beta_1 (2FHG' + 2HGF' + H^2G'')
$$

\n
$$
- M\left(G - S\beta_1 \left(G + \frac{\eta + 1}{2}G'\right) + \beta_1 HG'\right)
$$

\n
$$
+ 2S\beta_1 \left(2FG' + HG' + \frac{(\eta + 1)}{2} (GF' + FG' + HG'')\right)
$$

\n= 0, (14)

$$
\left(1+\frac{4}{3}Rd\right)\theta''
$$
\n
$$
+\frac{4}{3}Rd\left[\frac{(\theta_w-1)^3(3\theta^2\theta'^2+\theta^3\theta'')+3(\theta_w-1)^2(2\theta\theta'^2+\theta^2\theta'')}{+3(\theta_w-1)(\theta'^2+\theta\theta'')} \right]
$$
\n
$$
+Pr\left(\alpha_1\theta+\frac{\eta+1}{2}\theta'\right)
$$
\n
$$
+Pr\left(Nb\theta\phi'+Nt\theta'^2-H\theta'\right)=0,
$$
\n(15)

$$
\phi'' - \text{Sc}H\phi' + \frac{\text{Nt}}{\text{Nb}}\theta'' + \text{Sc}S\left[\alpha_2\phi + \frac{\eta + 1}{2}\phi\right] = 0,\qquad(16)
$$

$$
F(0) = 0, G(0) = \omega, H(0) = \beta \frac{S}{2}, \ \theta(0) = 1 = \phi(0),
$$

$$
F(\infty) = G(\infty) = \theta(\infty) = \phi(\infty) = 0.
$$
 (17)

In the above equations, F , G , H , θ , and ϕ are the dimensionless radial, azimuthal and axial velocities, temperature and concentration parameter, respectively. From Eqs. ([12](#page-3-5)[–17](#page-4-0)), there are some parameters that infuence the fow motion, temperature and concentration felds of Maxwell nanofuid. These are *S*, β_1 , Nt, Nb, β , Rd, θ_w , *M*, ω , Pr, α_1 , α_2 , and Sc, respectively, called wall motion up and down, Deborah number, thermophoresis, Brownian motion, wall permeability, radiation parameter, temperature ratio parameter, magnetics feld, rotation parameter, Prandtl number, wall temperature parameter, wall concentration parameter, and Schmidt numbers. The mathematical forms of these parameters are

$$
S = \frac{2a(t)a(t)}{v}, a(t) = h\sqrt{\frac{Sv}{h^2}t + 1}, \ \beta_1 = \frac{\lambda_1 v}{a^2(t)},
$$

\n
$$
Nt = \frac{\tau D_B ca(t)^{-2\alpha_1}}{\tau_0 v}, \ Nb = \frac{\tau D_B ca(t)^{-2\alpha_2}}{v},
$$

\n
$$
R_d = \frac{4\sigma^* T_{\infty}^3}{3kk^*}, \ M = \frac{\sigma B_0^2 a^2(t)}{v \rho_f}, \ \omega = \frac{\Omega(t) a^2(t)}{v},
$$

\n
$$
Pr = \frac{v}{\alpha}, \ S_c = \frac{v}{D_B}.
$$
\n(18)

Here $\Omega(t) = \frac{\omega v}{h^2 + vSt}$ implies the rotation of disk. The value *S >* 0 reduces the rotation of disk and thus causing disk decelerating rotation. Contrarily, *S <* 0 enhances the rotation of disk which accelerates the rotation of disk.

Nusselt number

From the engineering perspective, the quantity local Nusselt number Nu_r is very important. Physically, Nu_r is the wall heat transfer. This is expressed by the following expression:

$$
\text{Nu}_r = -\left[1 + \frac{16\sigma^* T_{\infty}^3}{3\rho c_p k^*}\right] \frac{r}{(T_w - T_{\infty})} \left(\frac{\partial T}{\partial z}\right) \big|_{z=0} \,. \tag{19}
$$

In dimensionless notation, one can write

$$
\text{Re}^{-1/2} Nu_r
$$

= $-\theta'(0) \Big(1 + \frac{4}{3} \text{Rd} \{ 1 + \theta(0)(\theta_w - 1) \}^3 \Big),$ (20)

where $Re^{1/2} = \frac{r}{a(t)}$ is the local Reynolds number.

Sherwood number

Mass transfer rate at the disk surface can be defned through Sherwood number as follows:

$$
Sh_r = -\frac{r}{(C_w - C_\infty)} \left(\frac{\partial C}{\partial z}\right) \big|_{z=0,}
$$
\n(21)

and dimensionless form is

$$
Sh_r Re^{-\frac{1}{2}} = -\phi'(0). \tag{22}
$$

Numerical solution procedure

The numerical solution of the dimensionless nonlinear momentum, temperature, and concentration Eqs. [\(12](#page-3-5)–[16\)](#page-4-1) with the boundary conditions [\(17\)](#page-4-0) are computed numerically with the bvp4c technique, one of the collection methods which uses the Lobatto formula. This technique requires initial guesses which satisfy the boundary conditions. Once initial guesses are provided by user then another built-in method, namely fnite diference method is used to modify the guesses for further iterations. The order of accuracy in the numerical calculation is controlled with error tolerance less 10[−]6. By default, this collocation method uses 61 grid points with CPU time of 12 s. In this process, we convert higher order system of ordinary diferential equations into a system of frst-order ordinary diferential equations by introducing some new variables defned as

$$
H = X_1, H' = X'_1, F = X_2, F' = X_3, F'' = X'_3,
$$

\n
$$
G = X_4, G' = X_5,
$$

\n
$$
G'' = X'_5, \theta = X_6, \theta' = X_7, \theta'' = X'_7, \phi = X_8,
$$

\n
$$
\phi' = X_9, \phi'' = X'_9.
$$
\n(23)

$$
X_1' = -2X_2,\tag{24}
$$

$$
X_2^2 - X_4^2 + X_1 X_3 + S(S\beta_1 - 1) \left(X_2 + \frac{\eta + 1}{2} X_3\right) + \frac{3}{2} S^2 \beta_1 \left(X_2 + (\eta + 1) X_3\right)
$$

\n
$$
-2S\beta_1 \left(X_2^2 - X_4^2 + X_1 X_2 + \frac{\eta + 1}{2} \left(X_2 X_3 + X_4 X_5\right)\right) - 4\beta_1 \left(X_1 X_4 X_5 - X_1 X_2 X_3\right)
$$

\n
$$
+ M\left(X_2 - S\beta_1 \left(X_2 + \frac{\eta + 1}{2} X_3\right) + \beta_1 X_1 X_3\right)
$$

\n
$$
1 - \frac{S^2 \beta_1}{4} (\eta + 1)^2 + S\beta_1 X_1 (\eta + 1) + 2\beta_1 X_1^2
$$
 (25)

$$
2X_2X_4 + X_1X_5 + S(S\beta_1 - 1)\left(X_4 + \frac{\eta + 1}{2}X_5\right) + \frac{3}{2}S^2\beta_1\left(X_4 + (\eta + 1)X_5\right)
$$

\n
$$
-2S\beta_1\left(2X_2X_5 + X_1X_5 + \frac{\eta + 1}{2}\left(X_2X_5 + X_4X_3\right)\right) + 4\beta_1\left(X_1X_2X_5 - X_1X_3X_4\right)
$$

\n
$$
+M\left(X_4 - S\beta_1\left(X_4 + \frac{\eta + 1}{2}X_5\right) + \beta_1X_1X_5\right)
$$

\n
$$
1 - \frac{S^2\beta_1}{4}(\eta + 1)^2 + S\beta_1X_1(\eta + 1) + 2\beta_1X_1^2
$$
 (26)

$$
X'_{7} = \frac{\Pr\left(X_{1}X_{7} - S\left(\frac{\eta+1}{2}X_{7} + \alpha_{1}X_{6}\right)\right) - 4\text{Rd}(\theta_{w} - 1)^{3}X_{6}^{2}X_{7}^{2} - 8\text{Rd}(\theta_{w} - 1)^{2}X_{6}X_{7}^{2}}{-4(\theta_{w} - 1)X_{7}^{2} - \Pr\left(NtX_{7}^{2} + NbX_{7}X_{9}\right)}
$$
\n
$$
1 + \frac{4}{3}\text{Rd} + \frac{4}{3}\text{Rd}(\theta_{w} - 1)^{3}X_{6}^{3} + 4\text{Rd}(\theta_{w} - 1)^{2}X_{6}^{2} + 4\text{Rd}(\theta_{w} - 1)X_{6}
$$
\n
$$
(27)
$$

$$
X_9' = Sc\left(X_1X_9 - S\left(\frac{\eta + 1}{2}X_9 + \alpha_2X_8\right)\right) - \frac{Nt}{Nb}X_7'\tag{28}
$$

with conditions

$$
X_1(0) = \beta \frac{S}{2}, X_2(0) = 0, X_4(0) = \omega,
$$

\n
$$
X_6(0) = 1 = X_8(0),
$$

\n
$$
X_2(\infty) = X_4(\infty) = X_6(\infty) = X_8(\infty) = 0.
$$
\n(29)

Code validation

The validation of numerical outcomes for local skin fric-tion and Nusselt number is shown in Tables [1](#page-11-0) and [2.](#page-11-1) Table [1](#page-11-0) shows the comparison with Turkyilmazoglu [\(2018\)](#page-13-6) for the efects of wall motion parameter *S* on local skin friction and Nusselt number by keeping other parameters $\omega = 1.0$, Pr = 1.0, $\beta = 2$ and $\alpha_1 = 0.5$ fixed and rest of parameters zero. In Table [2,](#page-11-1) we have fxed the values ω = 2.0, Pr = 1.0, β = 2 and α ¹ = 0.5 and other parameters are zero. These tables show an excellent comparison and correlation with Turkyilmazoglu ([2018\)](#page-13-6).

Graphical discussion

In this section, we present the physical description and numerical simulation for the velocity, temperature and concentration felds, local Nusselt and Sherwood numbers for an unsteady Maxwell nanofuid fow. Heat transfer analysis is done with the consideration of Buongiorno's model. The graphical and numerical results are discussed with the parameters in the following ranges:

S ∈ [−0.6, 0.4], *M* ∈ [0, 3.0], Nb ∈ [0.3, 2.0], $Nt \in [0.0, 1.2]$, $Pr \in [0.5, 2.5]$, β_1 ∈ [0.0, 2.8], Rd ∈ [0, 0.8], θ_w ∈ [1, 2.2], α_1 ∈ [−3, 1], α_2 ∈ [1, 1.8]

and fxing the values

 $\beta = \omega = 2.0, S = M = \text{Rd} = \beta_1 = 0.2, \theta_w = 1.2,$ $Sc = \alpha_1 = \alpha_2 = 1.0$, Nt = 0.4, Nb = 0.6.

Figure [2a](#page-6-0) shows the variation of radial velocity with the variation of wall motion *S*. It clearly shows that an upward wall motion reduces the rotational features of radial velocity. These efects on the rotating disk are blowing like for an upward action of wall motion. It is noted an enhancement in radial velocity with the action of wall motion. Similarly, Fig. [2](#page-6-0)b demonstrates the tangential velocity of nanofuid with varying values of wall motion parameter *S*. The infuence of wall motion is to enhance the tangential velocity of nanofuid. The efects of wall motion parameter on the axial velocity show the blowing which increases the axial velocity of nanofuid as shown in Fig. [2c](#page-6-0). In Fig. [2d](#page-6-0), e, the efects of wall motion parameter on the temperature θ and concentration ϕ fields of the nanofluids are shown. It is obvious from these fgures that both temperature and concentration profles are increasing function of *S*.

Figure [3](#page-7-0)a–d illustrates the graphical behavior of fuid velocity and temperature feld with the efects of Deborah number β_1 . Deborah number is defined as the ratio of time relaxation to observation time. So progressing value of β_1 increases the relaxation time which indicates the more solid-like characteristics. $\beta_1 = 0$ implies the Maxwell fluid reduces into case of viscous fuid. Figure [3a](#page-7-0), c shows the increase in quantity β_1 , for which the reduction in radial and axial velocities of nanofuids is observed. In Fig. [3b](#page-7-0)–d, it is noted the efects of Deborah number is to increase **Fig. 2** Variation of *S* on **a** radial velocity, **b** azimuthal velocity, **c** axial velocity, **d** temperature profile and e concentration profle

the azimuthal velocity and temperature feld of Maxwell nanofuid over vertically moving disk.

Figure [4](#page-8-0)a–d shows the efects of magnetic feld parameter *M*. The features of magnetic feld are tested on velocity feld of nanofuid over vertically moving disk. It is observed that the higher magnetic feld has the tendency to slow down the motion of nanofuid. Physically, the magnetic parameter *M* is ratio of the electromagnetic force to viscous force, so an increasing value of *M* implies the viscous force is dominant and as a result it decreases the radial and tangential velocity components. On the contrary it is noted that the axial velocity and temperature distribution enhance with the increase of magnetic feld efects.

Figure [5](#page-9-0)a, b shows the variation of temperature feld of nanofuids with the increasing efects of Brownian motion and thermophoresis parameter over vertically moving disk. Here both parameters Nt and Nb are showing a signifcant increase in temperature profle. This trend is expected because the properties of Brownian motion create the random motion in fuid that causes an increase in temperature

feld of nanofuid. Figure [5c](#page-9-0), d demonstrates the behavior of concentration feld of Maxwell nanofuid with the variation of Brownian motion and thermophoresis. It is obvious that the Brownian motion creates random motion in fuid that creates resistance and consequently the concentration of fuids decreases with the Brownian motion efects. On the contrary, variation of concentration profle against the thermophoresis efect is shown in Fig. [5d](#page-9-0). Physically, thermophoresis efects simply repel the particles away from a hot surface to cold surface due to which the concentration profle increases. The features of *Nt* are to enhance the concentration feld.

Figure [6](#page-10-0)a, b shows the effects of radiation parameter Rd and Prandtl number Pr on temperature feld of nanofuids.

An increase in temperature as well as thermal boundary layer thickness of nanofuid with the gradual enhancement in Rd is observed. However, the trends of temperature feld for Pr are quite opposite. Figure [6c](#page-10-0), d displays the variation of temperature field θ with the effects of temperature ratio parameter θ_w and wall temperature parameter α_1 . The temperature feld of nanofuid enhances with both temperature ratio parameter θ_w and wall temperature parameter α_1 . Figure [7a](#page-10-1) displays the variation of Schmidt number in the concentration profle. Concentration of fuid decreases due to decrease in mass difusivity. Figure [7](#page-10-1)b shows the variation of wall concentration parameter in a concentration profle. It is seen that ϕ is an increasing function of α_2 .

Figure [8a](#page-11-2), b shows the heat transfer rate with variation of parameters (Nt, S) and (ω , Rd). Figure [8a](#page-11-2) shows the decreasing behavior with increasing (Nt, *S*). Figure [8b](#page-11-2) illustrates an increase in heat transfer with increasing (ω, Rd) . Figure [8c](#page-11-2) displays an increase in mass transfer with increasing wall motion parameter *S*. Figure [8](#page-11-2)d presents an increase in mass transfer rate with increasing the fuid thermophoresis Nt and Brownian motion Nb.

Concluding remarks

In this study, we have investigated the flow behavior during an unsteady motion of Maxwell nanofuid over vertically moving as well as rotating disk in the presence of magnetic feld efects. The Buongiorno model is implemented to reveal the effects of Brownian motion and thermophoresis due to nanofuids. The impacts of some leading parameters on the fow behavior, temperature and concentration felds of nanofuids via graphical and tabular forms are discussed. The following signifcant features of this study can be summarized a

- The behavior of wall upward and downward motion parameter is observed similarly to that of injection and suction parameters.
- Overall the impact of wall motion parameter on radial, azimuthal, axial velocities, temperature and concentration profles is to enhanced, these.
- Temperature profle of nanofuid is enhanced, while concentration field reduces with higher values of Brownian motion.
- Boundary layer of both thermal and concentration profles is enhanced due to increasing thermophoresis effects.
- Magnetic field effects are observed to reduce the radial and azimuthal velocity of nanofuid.
- Nusselt number is increased by decreasing the values of wall motion parameter.

Fig. 7 Variation of concentration profile ϕ with **a** Sc, **b** α ₂

Fig. 8 Nusselt number for $\mathbf{\hat{a}}$ Nt, Nb **b**Rd, ω , and Sherwood number for **c** *S*, Nb **d** Nt, Nb

Table 1 A comparison of $F'(0)$, $G'(0)$ and $-\theta'(0)$ for various values of *S* when $\omega = 1.0$

		$S = -0.3$	$S = -0.2$	$S = 0.0$	$S = 0.5$	$S = 1.0$	$S = 2.0$
F'(0)	Ref. Turkyilmazoglu (2018)	0.4441589	0.4655632	0.5102326	0.6282715	0.7523955	1.0081383
F'(0)	Present	0.4441004	0.4545134	0.5101162	0.6282694	0.7480302	.0072935
G'(0)	Ref. Turkyilmazoglu (2018)	-0.7909736	$= 0.7320534$	-0.6159220	$= 0.3351635$	-0.0691935	0.4168670
G'(0)	Present	-0.7908021	-0.7319906	-0.6158492	0.3351622	-0.0675794	0.4169216
$-\theta'(0)$	Ref. Turkyilmazoglu (2018)	0.4968173	0.4585096	0.3962475	0.2543630	0.1221723	-0.1172784
$-\theta'(0)$	Present	0.4969023	0.4588884	0.3962613	0.2549728	0.1223241	$= 0.1174905$

Table 2 A comparison of $F'(0)$, $G'(0)$ and $-\theta'(0)$ for various values of *S* when $\omega = 2.0$

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