# ORIGINAL ARTICLE



# Effect of the Ni/Al ratio of hydrotalcite-type catalysts on their performance in the methane dry reforming process

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**Abstract** Hydrotalcite-type solids of the form NiAl-R, where R refers to the ratio of Ni to Al (R = 2, 3, 5, 8, and 10), were successfully synthesized following co-precipitation method at pH = 12. The obtained solids were calcined at 800 °C, except for NiAl-R<sub>2</sub> where calcination was performed at temperatures ranging between 300 and 800 °C. Following calcination, the resulting materials were evaluated for their catalytic activity and stability during the process of dry reforming of methane. Factors affecting the catalytic activity of the obtained materials such as the ratio R and calcination temperature were also studied. Prior to calcination, X-ray diffraction analyses clearly illustrated the typical hydrotalcite structure of the synthesized materials (when  $R \leq 5$ ). On the other hand, calcination at various temperatures prompted decomposition of all solids to form NiO, with exception to NiAl- $R_2$ , which upon calcinations at 800 °C was decomposed to form NiO and a second phase spinel containing NiAl<sub>2</sub>O<sub>4</sub>. The chemical composition of the obtained solids was determined by atomic absorption spectroscopy. Further characterization was performed using several techniques, including: surface area measurements  $(S_{\text{BET}})$ , scanning electron microscopy, Fourier transform infrared spectroscopy and thermogravimetric analysis. The reducibility of nickel species was studied via temperatureprogrammed reduction. The catalytic performance of the asprepared samples was studied for dry reforming of methane under atmospheric pressure at temperatures ranging between 400 and 700 °C. The catalytic activity of the designed substances highlighted the importance of molar ratios i.e. Ni<sup>2+</sup>/ Al<sup>3+</sup> on the success of the overall dry reforming of methane process. The catalytic activity of the synthesized materials was also found to be directly proportional to the ratio of Ni/ Al as well as the calcination temperature, with exception to NiAl- $R_2$  which was found to exhibit the highest activity of all. The latter observation was perhaps associated with the lower size of the crystalline particles in conjunction with the presence of a second phase containing NiAl<sub>2</sub>O<sub>4</sub>. In this study, it is shown that the calcination temperature has a significant effect on the catalytic property and the crystallite size of the metal.

**Keywords** Dry reforming of methane · Hydrotalcite-like compound · Nickel · Hydrogen

# Introduction

The development of novel metal-based complexes as catalysts for the production of synthesis gas via the process of dry reforming of methane (DRM) had attracted the attention of many environmental chemists in the past decades. DRM is considered as an eco-friendly process due to the consumption of two greenhouse gases, namely carbon dioxide and methane [1]. A feedstock gas mixture with low H<sub>2</sub>/CO ratio is preferentially used for the production of liquid hydrocarbons in the Fischer–Tropsch synthesis [2]. Previously, DRM reactions were catalyzed by group VIII transition metals such as Ni, Rh, Ru, Pd, Pt, Ir and Co [3].



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Despite current debates in relation to the order of activity of group VIII elements in DRM reactions, Rh was always elected as the catalyst of choice by most chemists. However, nickel was also reported as a very active metal for this reaction despite being deactivated by the formation of carbon [4, 5], since the reforming process is a relatively highly endothermic reaction (Eq. 1) [6, 7]. The formation of carbon is mainly produced by methane decomposition (Eq. 2) and carbon monoxide disproportionation (Boudouard reaction) (Eq. 3).

$$CH_4 + CO_2 \Leftrightarrow 2CO + 2H_2\Delta H^0 = +247.0 \text{ kJ mol}^{-1}$$
 (1)

$$CH_4 \Leftrightarrow 2H_2 + C\Delta H^0 = +75 \text{ kJ mol}^{-1}$$
 (2)

$$2CO \Leftrightarrow CO_2 + C\Delta H^0 = -173 \text{ kJ mol}^{-1} \tag{3}$$

The lower price and availability of nickel still provide an incentive for its continual utilization as a catalyst of choice, when compared to other noble metals. On the other hand, the generation of carbon can be reduced following the utilization of specific methods such as high dispersion of metal species over the surface area of the catalyst and incorporation of alkaline earth metal oxides within the catalyst in order to minimize coke formation [8, 9]. Following robust preparation procedures in conjunction with the addition of a suitable noble metal to the nickel-based catalyst, such as Pt, Ru and Rh, can also determine the success of a DRM reaction.

The incorporation of Ni<sup>2+</sup> ions within well-defined structures, such as perovskites [10, 11] and spinels [12], was also shown to increase the activity and catalytic stability via inhibiting the formation of carbon in DRM reactions. Other previously studied catalytic systems, such as those derived from layered double hydroxides (LDHs) that contain large surface areas, can result in the formation of homogeneous mixture of oxides with small crystal sizes. Reduction of LDHs prompts the formation of small, thermally stable, metal particles that can minimize the sintering of the nickel catalyst and enhance chemisorption of carbon dioxide [13], thus, avoiding the formation of coke [14, 15].

Layered double hydroxides (LDHs), or hydrotalcite-like compounds (HTLCs), are a family of compounds that have attracted considerable attention in recent years [16, 17]. Their structure can be derived from the brucite form of Mg(OH)<sub>2</sub>, where each Mg<sup>2+</sup> ion is octahedrally surrounded by six OH<sup>-</sup> ions. The hydrotalcite-type (HT) structure is obtained when some Mg<sup>2+</sup> ions, or other divalent cations, are replaced by trivalent cations, with similar atomic radius (r) to Mg<sup>2+</sup>(r = 0.65 Å) [18]. This substitution creates a positive charge in the hydroxide layer, which is compensated by interlayer anions and water molecules [19]. For this reason, they are also known as anionic clays. The

general formula of LDHs is  $[M_{1-x}^{2+}M_x^{3+}(OH)_2]A_{x/n}^{n-}$ , mH<sub>2</sub>O, where  $M^{2+}$  and  $M^{3+}$ , respectively, stand for divalent and trivalent cations.  $A^{n-}$  is an exchangeable interlayer anion [16] while x is the charge density of the layer which equals to the molar ratio of  $M^{2+}/(M^{2+}+M^{3+})$ .

It has been established [20, 21] that pure hydrotalcites can only be formed with stoichiometries in the range 0.2 < x < 0.33. Higher values of x (>0.33) may lead to the formation of Al(OH)<sub>3</sub>, usually undetected by PXRD; such occurrence is due to the increase of neighboring Al<sup>3+</sup> octahedral. Similarly, lower values of x (<0.2) may result in a high density of Mg<sup>2+</sup> octahedral, hence the formation of Mg(OH)<sub>2</sub>.

Following the co-precipitation method, Zhao et al. [17] successfully synthesized precursors of ZnNiFe-LDH with molar ratios  $M^{2+}/M^{3+}$  between 0.5 and 4 i.e. 0.2 < x < 0.66. XRD results showed that ZnNiFe-LDH, where x = 0.33, 0.25 and 0.2, has pure hydrotalcite-like phase. When x is large, e.g. x = 0.5 and 0.66, NiFe<sub>2</sub>O<sub>4</sub> was obtained. However, several papers stated that LDHs can be formed with x values outside the range (0.2 < x < 0.33). For example, syntheses of pure lamellar phases were achieved with 0.15 < x < 0.34 in Mg/Al LDHs [22]; other LDHs have been obtained with reported values of x lower than 0.07 (Mg/Ga-CO<sub>3</sub>) [23] or higher than 0.5 for Fe<sup>2+</sup>/ Fe<sup>3+</sup> LDHs [24]. Sometimes, the exact value of x can be challenging to estimate in hydrotalcite-like compounds: chemical analysis only provides limited information related to the metal content of all solids. The presence of metal oxides and/or metal hydroxides in LDHs, in addition to high or low molar ratios of M<sup>2+</sup>/M<sup>3+</sup>, may give rise to certain anomalies in the values of x [25].

LDHs can be synthesized by various methods depending on the specific requirement and properties of the desired compounds. However, co-precipitation is the most common synthetic process currently followed by chemists. LDHs have various widespread applications in a number of areas; they are used in catalysis [26], pharmaceuticals [27], chemical nanoreactors [28], photoactive materials, polymer additives [29, 30], environmental cleanup by ion exchange or adsorption processes [31], and in membrane technology [32].

Nickel-based LDHs have properties that make them suitable for preparing promising catalysts for dry reforming reactions. In this field, several research groups have investigated the utilization of Ni/Mg/Al LDH as potential catalysts with high activity. Nickel sites are highly dispersed inside the LDHs' structures. Hence, following reduction, high catalytic performance should be achieved [33]. Tsyganok et al. [34] also investigated dry reforming of methane with catalysts of nickel-containing Mg-Al LDHs; after 6 h, 95 % conversion of methane and 98 %



conversion of carbon dioxide were attained. On the other hand, Zhang et al. [35] carried out dry reforming of methane in the presence of Ni–Mg–Al LDHs/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst. Ni–Mg–Al catalysts, derived from LDHs and prepared in situ on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, showed excellent catalytic properties in dry reforming of methane, compared to a reference catalyst containing Ni/MgO/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> prepared by impregnation.

In the present work, a study was conducted to determine an adequate range of calcination temperature and molar ratios of Ni<sup>2+</sup>/Al<sup>3+</sup> in order to obtain a nickel-based catalyst with high catalytic performance and small particles upon reduction. The results show that calcination temperatures and molar ratios Ni<sup>2+</sup>/Al<sup>3+</sup> affect the reactivity and coke resistance of the metal particles, thus contributing to the overall catalytic process.

## **Experimental**

## Preparation of precursors and catalysts

Five samples of NiAl-R where R = 2, 3, 5, 8, and 10 were synthesized following the co-precipitation method at pH = 12. All catalysts were prepared following the same procedure. Two aqueous solutions were prepared: solution 1 containing  $Ni(NO_3)_2 \bullet 6H_2O$ (Biochem Chemopharma, ≥98 %) and Al(NO<sub>3</sub>)<sub>3</sub>. 9H<sub>2</sub>O (Biochem Chemopharma, >98 %) at different concentrations, to obtain various ratios R; solution 2 containing 2.0 M NaOH (Panreac, 98 % assay), and 0.4 M Na<sub>2</sub>CO<sub>3</sub> (Panreac, 98 % assay). Solution 1 was added dropwise to solution 2 under vigorous stirring at room temperature; the pH value was adjusted between 11 and 12. The precipitate formed was dried at 80 °C in an oil bath shaker for 15 h, then washed at ambient temperature using ultra-pure water to remove all residual salts. The resulting slurry was then dried overnight at 90 °C in dry oven.

The five samples obtained prior to calcination were assigned the following references: NiAl- $R_2$ , NiAl- $R_3$ , NiAl- $R_5$ , NiAl- $R_8$ , and NiAl- $R_{10}$ . Table 1 shows the different weights and concentrations utilized to synthesize hydrotalcites with different R values. To investigate the phase change of the catalyst during the thermal decomposition

process, NiAl- $R_2$  was calcined at different temperatures i.e. 300, 400, 500, 600, 700, and 800 °C, for 6 h. The samples were referred to as NiAl-T (NiAl-300, NiAl-400, NiAl-500, NiAl-600, NiAl-700, and NiAl-800). NiAl-R calcined at 800 °C were referred to as follows: NiAl- $R_2$ (800), NiAl- $R_3$ (800), NiAl- $R_5$ (800), NiAl- $R_8$ (800), and NiAl- $R_{10}$ (800). All samples were heated in increments of 5 °C per min and kept for 6 h at the ultimate calcination temperature.

#### Catalysts characterization

The chemical composition of each material was determined using atomic absorption spectroscopy (AAS) Varian spectra AA-110. The dissolution of solids was affected in the presence of nitric acid. Thermogravimetric analysis (TG) was carried out using Thermal Analyst (Setaram Set Sys 16/18) with temperatures ranging from 25 to 800 °C and heating increments of 5 °C per minute in the presence of air.

The crystal structure of the obtained solids was confirmed by XRD using two different apparatus, namely Siemens D5000 and Siemens D501 diffractometer equipped with a Cu-K $_{\alpha}$  radiation ( $\lambda=0.15418$  nm); the data were collected in  $2\theta$  scan mode.

The average crystallite sizes of Ni<sup>0</sup> following reduction were estimated using the Scherer equation:

$$D_{\rm hkl} = \frac{0.9\lambda}{\beta_{\rm hkl}\cos\theta} \tag{4}$$

where  $\lambda$  is the radiation's wavelength,  $\beta_{hkl}$  is the half width of the peak, and  $\theta$  is the Bragg's diffraction angle.

The specific surface area was determined following BET measurements under nitrogen adsorption—desorption isotherms in a Micrometrics Tristar 3000. This apparatus was also used to estimate porous volumes as well as the size of pores following Barret–Joyner–Halenda (BJH) method. FTIR spectra were obtained with a Perkin-Elmer spectrometer in the region of 4000–400 cm<sup>-1</sup> using KBr discs. The morphology of uncalcined samples was investigated using scanning electron microscopy (SEM) Jeol 320.

The calcined samples were analyzed by temperature-programmed reduction (TPR) TriStar 3000 V6.01, equipped with a TCD detector. 50 mg of the catalyst was loaded

Table 1 Weights and concentrations used to synthesize NiAl-R

Ni/Al ratio	2:1	3:1	5:1	8:1	10:1
Concentration of Ni(NO <sub>3</sub> ) <sub>2</sub> •6H <sub>2</sub> O (M)	1	1	1	1	1
Weight of Ni(NO <sub>3</sub> ) <sub>2</sub> •6H <sub>2</sub> O (g)	29.08	29.08	29.08	29.08	29.08
Concentration of Al(NO <sub>3</sub> ) <sub>3</sub> •9H <sub>2</sub> O (M)	0.50	0.33	0.20	0.12	0.10
Weight of $Al(NO_3)_3 \bullet 9H_2O(g)$	18.75	12.38	7.50	4.69	3.75



into the reactor and flushed with helium for 1 h at 200  $^{\circ}$ C. The temperature was lowered to room temperature and helium was replaced by 5 % hydrogen gas in argon. After 1 h of flushing, the temperature was raised to 900  $^{\circ}$ C with increments of 10  $^{\circ}$ C per minute.

## **Catalytic testing**

The catalytic tests were performed under atmospheric pressure, in a tubular fixed-bed quartz reactor (ID = 6 mm) and L = 16 cm), and placed in a furnace. The catalyst grains (100 mg) were kept in place using quartz wool plugs. A thermocouple was placed on top of the catalyst's bed to measure the temperature. The furnace's temperature was controlled by a Eurotherm temperature controller. For comparison, all catalysts were reduced with pure hydrogen at 750 °C over a period of 1 h. Following reduction, the temperature was lowered under argon to the initial reaction's temperature and a feed gas mixture containing CH<sub>4</sub>:CO<sub>2</sub>:Ar in a ratio of 20:20:60. The total flow rate was 20 mL min<sup>-1</sup>. The reaction products were analyzed using gas chromatograph (Delsi), equipped with a thermal conductivity detector (TCD) and Carbosieve B column, in the presence of carrier gas, argon.

Based on GC results, the conversion of methane, carbon dioxide, selectivity for hydrogen ( $S_{\rm H2}$ ) and carbon monoxide ( $S_{\rm CO}$ ) production were calculated using the following formulae:

$$(\%)CH_4 conversion = \frac{n_{CH_4,int} - n_{CH_4,out}}{n_{CH_4,int}} \times 100$$
 (5)

$$(\%) CO_2 conversion = \frac{n_{CO_2,int} - n_{CO_2,out}}{n_{CO_2,int}} \times 100$$
 (6)

$$S_{\rm H_2} = \frac{n_{\rm H_{2,out}}}{2 \times {\rm CH_{4,int} - CH_{4,out}}} \times 100 \tag{7}$$

$$S_{\text{CO}} = \frac{\text{CO}_{\text{out}}}{(\text{CO}_{2,\text{int}} - \text{CO}_{2,\text{out}}) + (\text{CH}_{4,\text{int}} - \text{CH}_{4,\text{out}})} \times 100$$

 $\frac{H_2}{CO} ratio = \frac{S_{H_{2,out}}}{S_{CO out}}$  (9)

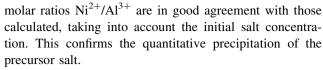
(8)

where  $n_{i, int}$  and  $n_{i, out}$  are the molar flow rates of *i*-species.

# Results and discussion

## Catalysts' characterization

To determine the metal content of NiAl-R catalysts, calcined at 800 °C, atomic absorption spectroscopy (AAS) was used. The obtained results are depicted in Table 2. The results of the elemental analysis by AAS show that the



Thermal decomposition of the hydrotalcites was evaluated by TG. Typical TG curve of the hydrotalcite with Ni/Al molar ratio of 2 (NiAl-*R*<sub>2</sub>) is illustrated in Fig. 1.

The curve illustrates three distinct steps of mass loss, corresponding to three endothermic peaks. The first peak with mass loss of 4 % occurring at about 87 °C is associated with the elimination of water, physically adsorbed on the external surface of the particle, [36] and Ni(NO<sub>3</sub>)<sub>2</sub> decomposition, while the second peak at about 227 °C with mass loss of 6 % may be attributed to the removal of –OH and water from the brucite-like layer as well as Al(NO<sub>3</sub>)<sub>3</sub> decomposition. In the third peak, 14 % of mass was lost up to 800 °C, this could be due to the simultaneous removal of carbon dioxide from the decomposition of interlayer carbonate anions [37]. During this step, the destruction of the layered structure of the hydrotalcite and the formation of NiAl mixed-oxide structure occurred.

X-ray diffraction patterns for NiAl-R (R = 2, 3, 5, 8and 10), prior to calcination, are illustrated in Fig. 2. A typical hydrotalcite-like type structure is present in all samples with  $R \le 5$  ( $x \ge 0.17$ ). This is not clearly highlighted for samples with R > 5 (x < 0.17). The peaks observed for NiAl-R<sub>2</sub>, NiAl-R<sub>3</sub> and NiAl-R<sub>5</sub> correspond to the layered double hydroxides structure Takovite [JCPDS file 15-0087]. XRD patterns for these catalysts showed several diffraction peaks at around  $2\theta = 11.61^{\circ}, 23.30^{\circ}, 35.20^{\circ}, 39.55^{\circ}, 47.07^{\circ}, 61.24^{\circ},$ 62.63°, and 66.40°, indexed at 003, 006, 012, 015, 018, 110, 113, and 116. Although XRD patterns for NiAl-R<sub>8</sub> and NiAl-R<sub>10</sub> displayed hydrotalcite-like phase as described above, an impurity phase around  $2\theta = 51.93^{\circ}$ was also observed. This impurity shows that Ni(OH)<sub>2</sub> [JCPDS file 14-0117] was obtained for lower values of x. A very low crystallinity was also observed for Ni/Al ratio higher than five compared to the other samples. In most circumstances, the sharpness and intensity of XRD peaks is proportional to the crystallinity of the LDHs i.e. LDHs with a highly ordered structure. Previous studies have described the relationship between crystallinity and peak intensity or sharpness [38, 39]. Moreover, Fig. 2 shows that the peak intensity of LDH decreases with increasing Ni/Al ratio, which suggests the presence of lower aluminum content; this can result in a disordered LDH layer which can cause disorder in the LDH structure.

After calcination, the lamellar structure disappears and only NiO phase is observed at around  $2\theta = 37^{\circ}$ ,  $44^{\circ}$ ,  $62^{\circ}$ ,  $76^{\circ}$ , and  $79^{\circ}$  [JCPDS file 47-1049], for NiAl-T (T = 300, 400, 500, 600, and 700 °C) as well as NiAl- $R_3$ , NiAl- $R_5$ ,



Table 2 Chemical compositions of catalysts NiAl-R, BET surface area ( $S_{\rm BET}$ ), surface area of the catalyst after reduction and Ni<sup>0</sup> crystallite size for all samples

Catalysts	Relative metal composition	M <sup>2+</sup> / M <sup>3+</sup>	Surface area <sup>a</sup> $(m^2g^{-1})$ $(S_{BET})$	Surface area <sup>b</sup> (m <sup>2</sup> g <sup>-1</sup> ) (S <sub>BET</sub> )	Surface area <sup>c</sup> (m <sup>2</sup> g <sup>-1</sup> ) (S <sub>BET</sub> )	Crystallite size <sup>d</sup> Ni° (nm)
NiAl- R <sub>2</sub> (800)	Ni <sub>0.67</sub> Al <sub>0.33</sub> -R <sub>2</sub>	2.03	90	120	119	6
NiAl- $R_3(800)$	$Ni_{0.73}Al_{0.27}-R_3$	2.70	111	124	70	18
NiAl- R <sub>5</sub> (800)	$Ni_{0.83}Al_{0.17}$ - $R_5$	4.88	93	119	95	15
NiAl- R <sub>8</sub> (800)	$Ni_{0.88}Al_{0.12}$ - $R_8$	7.33	110	123	101	12
NiAl- $R_{10}(800)$	Ni <sub>0.90</sub> Al $_{0.10}$ - $R_{10}$	9.00	109	121	114	8
NiAl-300	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	236	40	24
NiAl-400	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	184	42	24
NiAl-500	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	156	60	22
NiAl-600	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	156	90	20
NiAl-700	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	132	101	13
NiAl-800	$Ni_{0.67} Al_{0.33}$ - $R_2$	2.03	90	120	119	6

<sup>&</sup>lt;sup>a</sup> Before calcinations

<sup>&</sup>lt;sup>d</sup> From XRD measurements

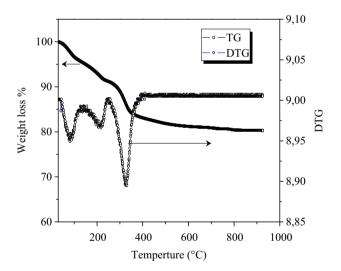
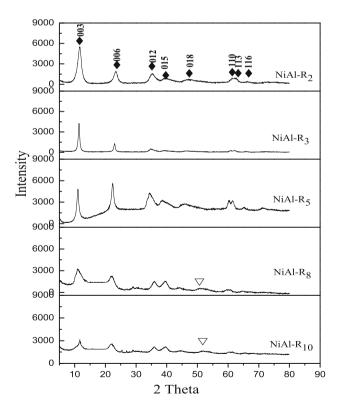


Fig. 1 TG analysis of NiAl-R<sub>2</sub>

NiAl- $R_8$  and NiAl- $R_{10}$  calcined at 800 °C (Fig. 3). Under such circumstances, the amorphous aluminum oxide phase would be formed but undetected by XRD; this is in agreement with other results previously reported in literature [33]. The spectrum of NiAl- $R_2$  sample calcined at 800 °C depicts two series of broad peaks corresponding to reflections close to those of NiO and NiAl<sub>2</sub>O<sub>4</sub> spinel phases [39], where  $2\theta = 19.14^{\circ}$ ,  $31.17^{\circ}$ , and  $37.56^{\circ}$  [JCPDS file 10-0339].

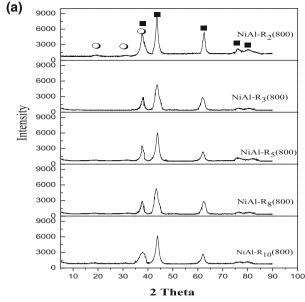


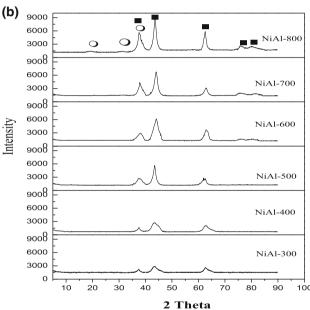
**Fig. 2** XRD of the sample NiAl-R ( $R=2,\ 3,\ 5,\ 8$  et 10), filled diamond hydrotalcite, inverted triangle Ni(OH)<sub>2</sub>



<sup>&</sup>lt;sup>b</sup> After calcinations

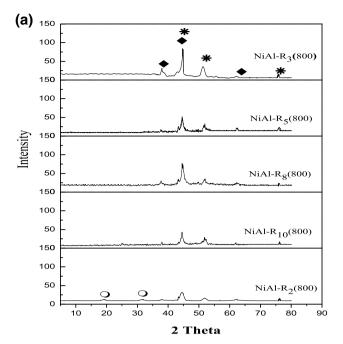
<sup>&</sup>lt;sup>c</sup> After reduction

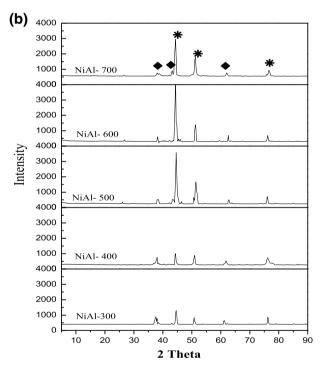




**Fig. 3** X-ray diffraction patterns of: (a) NiAl-R after calcinations at 800 °C, and (b) NiAl-T ( $T=300,\,400,\,500,\,600,\,700$  and 800 °C). *Filled square* NiO, *empty circle* NiAl<sub>2</sub>O<sub>4</sub>

XRD patterns of the reduced catalysts (prior to reaction) are provided in Fig. 4. After reduction at 750 °C, the diffraction lines resulting from the formation of nickel metal phase located at  $2\theta = 44.74^{\circ}$ ,  $51.41^{\circ}$  and  $76.13^{\circ}$  [JCPDS file 04-0850] were also observed with NiO, which decreased after reduction. The results indicate that a part of NiO was reduced to Ni metal. Very weak diffraction lines, due to a spinel phase of NiAl<sub>2</sub>O<sub>4</sub>, were also observed in NiAl- $R_2$ (800). Table 2 shows the size of nickel particles calculated from DRX results, for solids reduced by means of Scherer equation. In all cases, Ni<sup>0</sup> particle sizes obtained





**Fig. 4** XRD for the reduced catalyst (a) NiAl-*R* (800 °C) and (b) NiAl-*T. Empty square* (NiO), asterisk (Ni<sup>O</sup>), empty circle (NiAl<sub>2</sub>O<sub>4</sub>), at 750 °C with pure H<sub>2</sub>; 1.2 L/h

after reduction at 750 °C were between 6 and 24 nm. When R is greater than 2, the intensity of the peaks assigned to Ni<sup>o</sup> increases with decreasing the Aluminum content; thus, a reduction in the crystallite size is observed. Therefore, the crystallite size of nickel decreases in the following order: NiAl- $R_2$  < NiAl- $R_{10}$  < NiAl- $R_8$  < NiAl- $R_5$  < NiAl- $R_3$ .



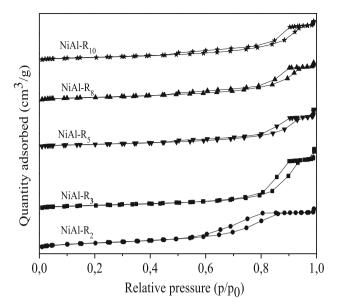
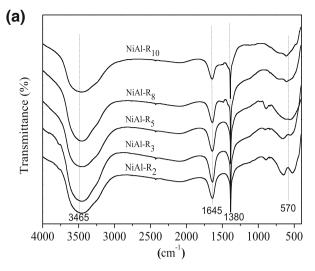


Fig. 5 N<sub>2</sub> adsorption/desorption isotherms of NiAl-R

textural properties of uncalcined  $R (R = Ni^{2+}/Al^{3+} = 2, 3, 5, 8, \text{ and } 10)$ . NiAl-R calcined at 800 °C, and NiAl-T (T = 300, 400, 500, 600, 700, and800 °C) are summarized in Table 2. The specific surface of the uncalcined NiAl-R is relatively unchanged. It can be noticed that the surface area  $(S_{BET})$  may be dependent of the nickel content. However, in a previous study, it was found that the surface area  $(S_{BET})$  may be independent of the nickel content [40]. For NiAl-T, the surface area is sharply increased from 90 m<sup>2</sup>g<sup>-1</sup> to a value greater than 100 m<sup>2</sup>g<sup>-1</sup> after calcination. It was assumed that a porous structure is developed in the calcined sample during removal of water and carbonate from the interlayer space by the transformation of  $CO_3^{2-}$  to  $CO_2$  [41–43]. The sample calcined at 300 °C (NiAl-300) presents the highest surface area (236 m $^2$ g $^{-1}$ ), while  $S_{\text{BET}}$  value decreased gradually with increasing calcination temperature. The nitrogen adsorption/desorption isotherms of NiAl-R for the five solids exhibit type IV isotherms (Fig. 5) according to the International Union of Pure and Applied Chemistry (IUPAC classification), which are typical of mesoporous and slitshaped materials [44]. The samples also exhibit the hysteresis type H<sub>2</sub> which is typical of clay minerals either of cationic or anionic types such as hydrotalcites [45].

FTIR spectra of NiAl-*R* (uncalcined sample) are illustrated in Fig. 6a. Usually, these spectra show peaks which are typical of LDHs structure containing mainly carbonate anions [33, 46]. IR spectra for all samples show similar absorption bands. The broadband at high frequency, i.e. around 3650 cm<sup>-1</sup>, is attributed to O–H stretching vibration of water molecules and the hydroxyl groups of the brucitic layers. The absorption at 1645 cm<sup>-1</sup> can be the result of O–H bending vibration of water molecules in the interlayer space, while



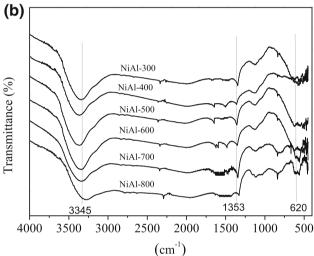


Fig. 6 The infrared spectrum of (a) NiAl-R and (b) NiAl-T

the active adsorption band at 1380 cm<sup>-1</sup> is a characteristic of O–C–O vibration of CO<sub>3</sub><sup>-2</sup> in the interlayer space. The peak below 1000 cm<sup>-1</sup> is attributed to metal–O–metal (Ni–O–Al) stretching mode [47, 48].

Compared to FTIR spectra of the uncalcined samples, phase transformations are observed after calcination, as shown in Fig. 6b. Trace amounts of the remaining carbonate were found around 1353 cm<sup>-1</sup> after calcination at 300, 400, 500, 600 and 700 °C, which then disappear after calcinations at 800 °C. At 620 cm<sup>-1</sup>, the metal–oxygen (Ni–O and/or Al–O) stretching mode was observed. The result suggests the transformation of the crystal phase to mixed oxides; this is in a good agreement with our XRD data.

The morphology of NiAl-R samples, prior to calcination, was investigated by SEM. From Fig. 7, the images of NiAl-R reveal that the studied solids consist of relatively uniform hexagonal platelet-like sheets; the hexagonal morphology is the characteristic of hydrotalcite materials.



Moreover, when  $\mathrm{Ni}^{2+}/\mathrm{Al}^{3+}=8$  and 10, the solids are composed of crystals with irregular shapes. This observation is in agreement with the result obtained with XRD analysis.

Figure 8a presents the temperature-programmed reduction (TPR) analysis of NiAl-*R* calcined at 800 °C. For NiAl-*R*<sub>3</sub> (800 °C), two reduction peaks were obtained.

According to previous work [33], the first reduction peak at 360 °C could be attributed to the reduction of NiO which is weakly interacting with Al<sub>2</sub>O<sub>3</sub> (undetected by XRD). The second peak at 776 °C is related to the reduction of Ni<sup>2+</sup> to Ni<sup>0</sup> in pure NiO [39, 48]. In another work by Perez-Lopez [40], it was suggested that in catalysts containing Ni/Mg/Al, when the ratio of Ni/Mg was

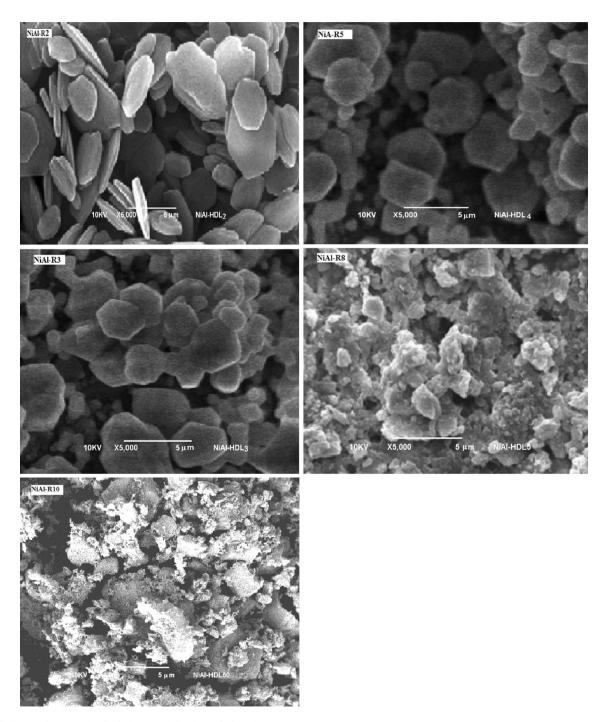
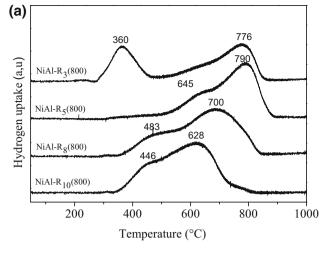
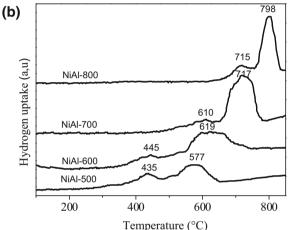


Fig. 7 SEM micro graph of NiAl-R uncalcined (scale bar 5 μm)





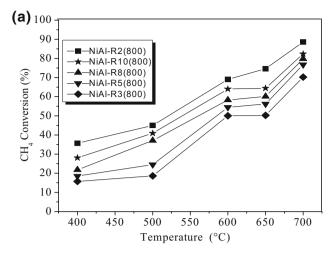


**Fig. 8** Temperature-programmed reduction (TPR) of (a) NiAl-R(800) and (b) NiAl-T

constant, the reducibility decreases with an increase in the amount of aluminum.

Figure 8b shows TPR profiles for NiAl- $R_2$ , calcined at 500, 600, 700 and 800 °C. In case of NiAl-800 sample, two reduction peaks were observed. The first peak observed at 715 °C is assigned to the reduction of Ni<sup>2+</sup> in NiO. The peak at 798 °C is assigned to the reduction temperature probably caused by the reduction of Ni<sup>2+</sup> to Ni<sup>0</sup> in NiAl<sub>2</sub>O<sub>4</sub>.

In summary, the dense structure of  $\rm NiAl_2O_4$  in  $\rm NiAl_{R_2}(800)$  can stabilize  $\rm Ni^{2+}$  ions, which leads to an increase in the reduction temperature. The maximum reduction temperature is shifted to lower values while there is a decrease in calcination temperature. The results indicate that higher calcination temperatures have an effect on increasing the interaction between the oxides present in the catalysts; this is probably owing to the formation of periclase  $\rm Al_2O_3$  and/or  $\rm NiAl_2O_4$  phase [49]. This reduction temperature is higher than required in pure NiO and is a typical feature of catalysts derived from hydrotalcites [39, 40].



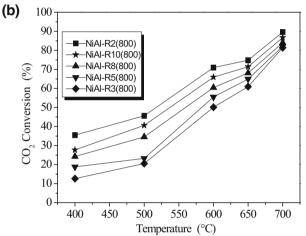


Fig. 9 Conversion of (a) methane and (b) carbon dioxide, for catalysts NiAl-R(800) versus temperature

#### Catalytic tests

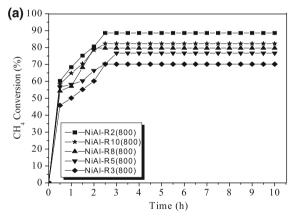
The performance of NiAl-*R* was tested in DRM reactions in the presence of equimolar amounts of methane and carbon dioxide. The reaction's temperature was gradually raised from 400 to 700 °C, followed by an in situ reduction of H<sub>2</sub> at 750 °C, over a period of 1 h. A graph showing the amount of methane and carbon dioxide conversion during the DRM process, in the presence of NiAl-*R* (800 °C), at various temperatures, is presented in Fig. 9a and b. Both graphs clearly demonstrate the direct proportionality between methane and carbon dioxide conversions, and the reaction's temperature.

A plot showing the amount of conversion of methane and carbon dioxide over time, at 700 °C, is also depicted in Fig. 10. The catalytic performance of our synthesized materials reaches its maxima during the first 2 h of the reaction, after which the amounts of methane and carbon dioxide conversion remain steady over the rest of time i.e. 8 h. The results also indicate that the activity of the



synthesized catalysts increases with the increase in Ni/Al ratio (when R > 2). From this relationship, it appears that the order of catalytic activity follows the sequence: NiAl- $R_2 > \text{NiAl-}R_{10} > \text{NiAl-}R_8 > \text{NiAl-}R_5 > \text{NiAl-}R_3$ . According to the results presented in Table 2, the activity of these catalysts can be attributed to the size of Ni<sup>0</sup>, and the specific surface obtained following the reduction step, with exception to NiAl- $R_2$  (800 °C), where the size of Ni<sup>0</sup> crystallites decreases with the increase in Ni/Al ratio. Hence, the catalytic activity of our catalysts is inversely proportional to the size of Ni<sup>0</sup> and directly proportional to the specific surface obtained after the reduction process. Previous studies also experienced similar results [40, 50]. It is worth noting that the amount of nickel used in our experiments remained unchanged throughout this project. In all cases, where R > 2, the molar ratio of the resulting hydrogen to carbon monoxide is always less than one (Table 3); it was also observed that the amount of carbon dioxide converted is greater than that of methane. Such results might be attributed to the reverse water-gas shift reaction (Eq. 10), which also explains the higher conversion of carbon dioxide [33].

$$CO_2 + H_2 \rightarrow CO + H_2O \tag{10}$$



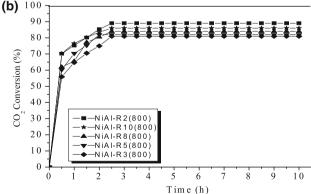


Fig. 10 Conversion of (a) methane and (b) carbon dioxide, for NiAl-R(800) versus time



In case of NiAl-R<sub>2</sub> (800 °C), the H<sub>2</sub>/CO molar ratio was close to one (Table 3), while the conversion rate of carbon dioxide is equal to that of methane, which indicates a very efficient DRM reaction. The ratio of hydrogen to carbon monoxide also tends to increase in the event of decreasing the amount of aluminum; such phenomenon can be explained by the acidic character of aluminum [40]. Furthermore, it was previously claimed that in the presence of lower aluminum content, the concentration of basic sites increases in Ni/Mg/Al catalysts, this observation was specific to those with identical Ni/Mg ratio (Ni/Mg = 5). Hence, catalysts containing low levels of aluminum tend to effect DRM reactions which produce higher hydrogen to carbon monoxide ratio. On the other hand, the presence of other Lewis acid sites in the catalyst tends to enhance the catalytic activity of the overall DRM process [28]. For example, HZSM-5 and USY zeolites, as well as Ni/γ-Al<sub>2</sub>O<sub>3</sub>, were found to exhibit a catalytic effect strongly dependent on the acidity and reducibility of the catalyst.

The high catalytic performance of NiAl- $R_2$  (800 °C) can be related to two parameters: (1) the low Ni<sup>0</sup> crystallite size and (2) the high stability of the support (NiAl<sub>2</sub>O<sub>4</sub>), which can maintain a very high specific surface area (119 m<sup>2</sup>g<sup>-1</sup>) following the reduction step when compared to other catalysts such as NiAl- $R_{10}$  (114 m<sup>2</sup>g<sup>-1</sup>), NiAl- $R_{8}$  (101 m<sup>2</sup>g<sup>-1</sup>), NiAl- $R_{5}$  (95 m<sup>2</sup>g<sup>-1</sup>), and NiAl- $R_{3}$  (70 m<sup>2</sup>g<sup>-1</sup>). The resulting effect might have been due to the spinel phase formation following the reduction step, as illustrated in Table 2.

Figure 11 shows the catalytic conversion of NiAl-T (T = 300, 400, 500, 600, 700, and 800 °C). Our results demonstrate that the calcination temperature has a minimal effect on the catalytic activity at temperatures less than 500 °C. Table 3 also shows that the size of Ni<sup>0</sup> and specific surface area after reduction remain unchanged for NiAl-300 and NiAl-400. At higher calcination temperatures, the size of Ni<sup>0</sup> shows a decreasing pattern; following reduction, the specific surface area tends to augment as calcination temperature rises.

However, for higher reaction temperatures i.e. 600, 650, and 700  $^{\circ}$ C, the conversion of CO<sub>2</sub> was higher than that of CH<sub>4</sub>, while the ratio of H<sub>2</sub>/CO was always less than one (0.58–0.71). This result can be attributed to the reverse water–gas shift reaction (Eq. 10) [33].

For NiAl-600 and NiAl-700, the ratio of H<sub>2</sub>/CO was about 0.95. This certainly indicates that such catalysts have the greatest stability, and the occurrence of reverse watergas shift is less significant. In this case, the optimum calcination temperature can be either 800, 700 or 600 °C. Feng et al. [32] investigated the effect of calcination temperature on the catalytic performance of NiO/MgO, prepared by impregnation and calcined at 600 and 800 °C.

 $NiAl-R_2(800)$ 

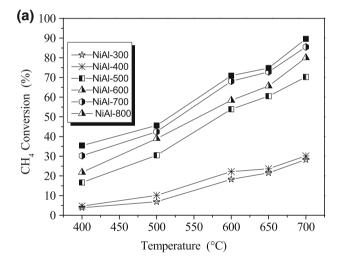
0.98

The samples	The reaction temperature							
	400 °C CO/H <sub>2</sub>	500 °C CO/H <sub>2</sub>	600 °C CO/H <sub>2</sub>	650 °C CO/H <sub>2</sub>	700 °C CO/H <sub>2</sub>			
NiAl-300	0.69	0.68	0.69	0.60	0.50			
NiAl-400	0.71	0.70	0.65	0.60	0.58			
NiAl-500	0.98	0.98	0.85	0.77	0.76			
NiAl-600	1.00	1.00	0.98	0.95	0.95			
NiAl-700	1.00	1.00	0.96	0.95	0.95			
NiAl-800	1.00	1.00	1.00	0.99	0.98			
NiAl- $R_3(800)$	0.94	0.90	0.89	0.89	0.84			
NiAl-R <sub>5</sub> (800)	0.96	0.91	0.90	0.90	0.89			
NiAl- $R_8(800)$	0.97	0.94	0.92	0.92	0.91			
$NiAl-R_{10}(800)$	0.98	0.95	0.93	0.93	0.93			

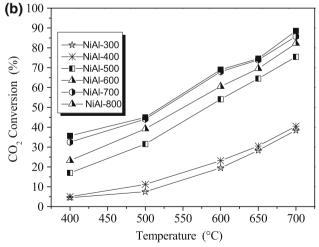
1.00

1.00

**Table 3** H<sub>2</sub>/CO as a function of reaction temperature for the NiAl-R(800) and NiAl-T, at reaction conditions: P = 1 atm,  $CH_4/CO_2 = 1$ 



1.00



**Fig. 11** Conversion of (a) methane and (b) carbon dioxide for NiAl-T versus temperature

Their results indicated that NiO/MgO catalysts calcined at 800 °C displayed stronger interactions between the metal and the support, as well as exhibited higher activities.

0.99

The effect of calcination temperature on the activity of alumina supported nickel ( $Ni/\gamma$ - $Al_2O_3$ ) catalyst in DRM reactions was also studied by Al-Fatesh and co-workers [51].

At calcination temperatures of 500, 600, 700 and 800 °C, it has been shown that increasing the temperature also enhances the catalysts' activity. The highest conversion was obtained at 800 °C in the presence of a catalyst calcined at 900 °C and activated at 700 °C.

In previous work, Perez-Lopez et al. [40] have studied the influence of the calcination temperature on Ni–Mg–Al catalysts in DRM reactions performed between 500 and 700 °C. The effect of calcination temperature on the catalysts' activity is smaller and practically does not affect the conversion of methane; however, its influence is only limited to the specific surface area.

#### Conclusions

Hydrotalcite-like precursors NiAl-R (R = 2, 3, 5, 8 and 10) were successfully synthesized using co-precipitation at pH = 12, and calcined at different temperatures. XRD of the synthesized materials clearly demonstrated the hydrotalcite-like structure of all samples where  $R \le 5$ . After calcination of NiAl-T (T = 300, 400, 500, 600, and 700 °C) as well as NiAl- $R_3$ , NiAl- $R_5$ , NiAl- $R_8$  and NiAl- $R_{10}$ , calcined at 800 °C, the lamellar structure disappears and only NiO phase is observed. The spectrum of NiAl- $R_2$ , calcined at 800 °C, shows two series of broad peaks



corresponding to reflections close to those of NiO and NiAl<sub>2</sub>O<sub>4</sub> spinel phases. The best catalytic results for DRM reactions were obtained with NiAl-R<sub>2</sub>, where values of conversion and selectivity were near thermodynamic equilibrium at 700 °C. The high performance of the catalytic process can be attributed to the lower size of nickel, and the high stability of the support (NiAl<sub>2</sub>O<sub>4</sub>). This shall equally maintain a very high specific surface area following the reduction step.

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