



A new approach for predicting oil recovery factor during immiscible CO₂ flooding in sandstones using dimensionless numbers

Davood Zivar¹ · Peyman Pourafshary²

Received: 21 December 2018 / Accepted: 16 February 2019 / Published online: 20 February 2019
© The Author(s) 2019

Abstract

CO₂ injection is one of the most promising techniques to enhance oil recovery. The most favorable properties of CO₂ made this method popular and it has been widely used since 1950. Experimentally, the effect of CO₂ injection on incremental oil recovery is widely measured by the core-flooding approach. An accurate estimation of the recovery factor is required to analyze the performance of the method to design the enhanced oil recovery method successfully. Hence, knowledge of the effects of different parameters on recovery is essential. Various reported experimental CO₂ core-flooding data for the immiscible condition in sandstones were analyzed to develop the parametric relationships affecting ultimate oil recovery using data analytics. Selected data support a wide range of porosity (10.8–37.2%), permeability (1–18000 mD), injection pressure (2.73–11.44 MPa), injection rate (0.1–1.0 cm³/min), and crude oil types, which enhance the methodology used to develop more comprehensive dimensionless numbers and correlations to predict the oil recovery. Series of new dimensionless numbers were defined and used for the study to develop a correlation for predicting oil recovery factor. Capillary number, relative radius, injection pressure ratio, and oil composition number are used as dimensionless numbers in our approach. The oil recovery prediction by the developed correlation was in agreement with the experimental data. The proposed correlation shows that capillary number is the most effective parameter when predicting oil recovery.

Keywords Gas flooding · Dimensionless numbers · Capillary number · Oil recovery · Immiscible gas injection

List of symbols

N_c	Capillary number (dimensionless)
R_r	Relative radius (dimensionless)
MMP	Minimum miscibility pressure (MPa)
MCM	Multi-contact miscibility
OCN	Oil composition number (dimensionless)
PRF	Predicted oil recovery factor (dimensionless)
P_i	Injection pressure (MPa)
P_r	Injection pressure ratio (dimensionless)
μ_g	CO ₂ viscosity (Pa s)
V	Darcy velocity (m/s)
σ_{go}	Interfacial tension between oil and CO ₂ (N/m)
w_{C_i}	Weight fraction of composition i (dimensionless)

k	Permeability (mD)
\emptyset	Porosity (fraction)

Introduction

CO₂ injection is one of the most utilized, in most cases cost-effective, and popular methods used for pressure maintenance and EOR in sandstone oil reservoirs (Alvarado and Manrique 2010). In the past 5 decades, there have been extensive laboratory studies, numerical simulations, and field applications of CO₂ EOR processes (Alipour Tabrizy 2012; Arshad et al. 2009; Ghasemi et al. 2017; Godec et al. 2011; Gozalpour et al. 2005; Holm and Josendal 1974; Jarrel et al. 2002; Jianbo et al. 2016; Koottungal 2014; Kuuskraa and Koperna 2006; Mohammed-Singh and Ashok 2005). The most important mechanisms affecting oil displacement using CO₂ injection include oil swelling, reduction in oil viscosity, and interfacial tension (IFT) reduction (Holm and Josendal 1974; Jarrel et al. 2002; Orr Jr et al. 1982). Displacement efficiency of CO₂ flooding in porous media at immiscible condition is affected by the oil and CO₂ density

✉ Peyman Pourafshary
peyman.pourafshary@nu.edu.kz

¹ Center of Research in Enhanced Oil Recovery, Universiti Teknologi PETRONAS (UTP), 32610 Seri Iskandar, Perak Darul Ridzuan, Malaysia

² Department of Petroleum Engineering, School of Mining and Geosciences, Nazarbayev University, 53 Kabanbay Batyr Ave., Astana 010000, Kazakhstan

difference, wetting properties of fluids, viscosity ratio of fluids, reservoir pressure and temperature, oil composition, and the rate of CO₂ injection (Holm and Josendal 1974). These parameters can be categorized into various dimensionless numbers, which provide appropriate tools to analyze different mechanisms such as capillarity, gravity, miscibility, and mobility in the porous media during the gas injection.

The effect of dimensionless groups on the oil recovery factor was investigated by Kulkarni and Rao (2006) using the results of miscible and immiscible CO₂ gravity drainage experiments. Wood et al. (2006) used dimensionless numbers to describe CO₂ flooding in a dipping, water-flooded reservoir. Dimensionless numbers were introduced for designing a series of experiments to develop screening criteria applicable to Gulf Coast reservoirs. Trivedi and Babadagli (2008) proposed a new group including the matrix-fracture diffusion transfer for scaling of the miscible displacement in fractured porous media. Rostami et al. (2010) conducted a series of forced gravity drainage experiments using a wide range of physical and operational conditions. Their results showed that use of each number alone is inadequate to obtain an acceptable correlation to predict recovery. They proposed a group of dimensionless numbers to provide an acceptable correlation with recovery.

Alipour Tabrizy (2014) investigated CO₂ EOR in sandstone and chalk rocks. The results show that a higher Bond number has a positive effect on oil recovery but there are limitations to capillary number performance. Eventually, Alipour Tabrizy introduced a dimensionless group to analyze the effect of parameters such as permeability, injection rate, capillarity, and CO₂ diffusion on the oil recovery factor. Rostami et al. (2018) conducted a complete series of PVT tests and core-flooding experiments in sandstones to investigate the effects of injectant type, reservoir pressure, and injection rate. The results show that oil swelling and oil viscosity reduction are the most effective parameters during gas injection in high permeable porous media saturated with semi-heavy oil. A new correlation, composed of empirical dimensionless numbers, was also proposed by results of core-flooding experiments, to predict oil recovery in heavy oil reservoir under gas flooding. Also, several studies have been carried out by researchers to predict the ultimate recovery of the oil fields which are under CO₂ injection. Data mining methods were used to develop dimensionless numbers that are able to predict oil recovery (Srivastava et al. 2016; Talluru and Wu 2017).

Some key parameters were neglected in some of papers mentioned above and this affects the accuracy of the oil recovery prediction, especially during immiscible-CO₂ flooding. On the other hand, taking into account all of the parameters makes the correlation complex and a lot of input data are required for oil recovery prediction. Hence, a comprehensive analysis of immiscible-CO₂ flooding in sandstone

lithology is required to select all of the main governing parameters and develop new dimensionless numbers to predict the oil recovery factor.

The objective of this paper is to study the governing parameters affecting the performance of immiscible CO₂ flooding in sandstone core samples. A dataset of CO₂ core-flooding experiments was provided with a wide range of permeability, porosity, IFT, CO₂ injection pressure, and injection rate. These parameters have been analyzed to develop parametric numbers such as capillary number (N_c), relative radius (R_r) as a ratio of pore throat radius-to-core sample radius, pressure ratio of injection pressure and minimum miscibility pressure (P_r), and oil composition number (OCN). A new correlation based on the developed dimensionless groups was proposed to predict the oil recovery by CO₂ flooding at the core scale by combining the effects of different parameters such as porosity, permeability, capillarity, injection rate, injection pressure, and type of crude oil.

Methodology

Dataset

In this work, the parameters affecting ultimate oil recovery during CO₂ core flooding are categorized into operational parameters and rock/fluid properties. Parameters such as injection pressure, minimum miscibility pressure (MMP), temperature, and CO₂ injection flow rate are categorized in the former group and porosity, permeability, rock lithology, viscosity and density of crude oil and CO₂, IFT, and composition of crude oil are considered in the properties group. The results of various immiscible CO₂ flooding experiments at the core scale were collected to cover wide ranges of the mentioned parameters. As the aim of this paper is to develop a correlation for immiscible CO₂ flooding in sandstones, the lithology of the porous media and the state of injection, attempts were made to keep the parameters the same in all experiments. The range of the collected data is shown in Table 1 (Cao and Gu 2013; Kazemi et al. 2015; Khosravi et al. 2014, 2015; Nobakht et al. 2007; Norouzi et al. 2018; Shyeh-Yung 1991; Wang and Gu 2011).

Key parameters

The application of dimensionless numbers provides a way to scale and reduce the dimensionality of the dataset to analyze a phenomena more easily. This approach is widely used in reservoir engineering to analyze the governing forces and mechanisms during fluid flow in porous media. Also, the performance of different operational conditions and recovery scenarios can be compared. The mechanisms behind different recovery methods are studied by analyzing the relative

Table 1 Range of used parameters

Parameters	Range
Porosity (%)	10.8–37.2
Permeability (mD)	1–18,000
Lithology	Sandstone
CO ₂ viscosity (Pa s)	1.36E–5–1.01E–4
Interfacial tension (N/m)	0.001–0.017
Injection rate (cm ³ /min)	0.1–1.0
Injection pressure (MPa)	2.73–13.79
Core inclination	Horizontal
Temperature (°C)	27–80

importance of driving forces, such as viscous and capillary forces, in the form of dimensionless numbers. There are different definitions of the dimensionless variables in the literature (Abrams 1975; Alipour Tabrizy 2014; Brownell and Katz 1947; Dombrowski and Brownell 1954; Foster 1973; Green and Willhite 1998; Kulkarni and Rao 2006; Moore and Slobod 1955; Pennell et al. 1996; Rostami et al. 2010, 2018; Srivastava et al. 2016; Talluru and Wu 2017; Trivedi and Babadagli 2008; Wood et al. 2006). Our analysis showed that four different dimensionless numbers describe the physics of CO₂ flooding in porous media and can be used to predict the oil recovery. These parameters are capillary number (N_c), relative radius (R_r), injection pressure ratio (P_r), and oil composition number (OCN).

The capillary number shows the competition between viscous force and capillary force in the porous media during the course of an immiscible displacement, which is defined by Eq. 1 in our study.

$$N_c = \frac{\mu_g V}{\sigma_{go}} \quad (1)$$

where N_c is the dimensionless capillary number, μ_g is dynamic viscosity (Pa.s), V is Darcy velocity (m/s), and σ_{go} is interfacial tension between oil and CO₂ (N/m). Capillary number is a representative of the main forces during immiscible CO₂ flooding into horizontal cores. The large viscous force, developed by high-rate gas flooding, is characterized by large capillary numbers which leads to an unstable front and oil bypassing/trapping. However, low-rate gas flooding or high IFT may lead to considerable residual oil, as the pressure drop across the core cannot overcome the capillary threshold in the pores. Hence, different conditions of fluid flow in porous media emphasize the importance of N_c on accurately predicting oil recovery during CO₂ flooding.

Hydrocarbon storage capacity and deliverability indicate the quality of a porous media. The hydrocarbon storage capacity is characterized by the effective porosity, whereas the deliverability of porous media is a function of the permeability. Routine

core analysis can provide these two parameters. Data obtained from core provided information on pore geometry, based on a modified Kozeny–Carmen equation and the concept of mean hydraulic radius (Amaefule et al. 1993). In this study, a dimensionless number is defined as a ratio of the pore throat radius-to-core sample radius. The value of relative radius (R_r) shown in Eq. 2, is a good indicator of a physical properties of rock that strongly affects oil recovery factor during CO₂ core flooding.

$$R_r = 3.14 \times 10^{-6} \frac{\left(\frac{k}{\phi}\right)^{0.5}}{\frac{d}{2}} \quad (2)$$

where R_r is relative radius (dimensionless), k is permeability (mD), ϕ is porosity (fraction), and d is core diameter (cm).

Interactions between the injected gas and oil directly depend on the state of injection (immiscible, near miscible, and miscible). For example, the effect of injection rate is significant in the near-miscible condition, while a lower injection rate results in more chance of multiple contact miscibility (MCM). Pressure difference between injection pressure and minimum miscibility pressure (MMP) shows the state of injection. In the immiscible condition (where injection pressure is lower than MMP), injection pressure plays an important role in altering the ultimate recovery of CO₂ core flooding (Li et al. 2017). Injection at pressure values closer to MMP affects the oil recovery and hence, in this study, the pressure ratio number (P_r) considers the effect of operational conditions. This pressure ratio is the ratio of injection pressure-to-minimum miscibility pressure as defined by Eq. 3.

$$P_r = \frac{P_i}{MMP} \quad (3)$$

where P_r is injection pressure ratio (dimensionless), P_i is injection pressure (MPa), and MMP is minimum miscibility pressure (MPa).

As already mentioned, the most important mechanism in the immiscible CO₂ flooding process is oil viscosity reduction due to the dissolution of CO₂ in the crude oil. The solubility of CO₂ is a function of crude oil composition, operational pressure and temperature values. Hence, crude oil composition plays an important role in changing the ultimate oil recovery by immiscible CO₂ flooding (Holm and Josendal 1974; Li et al. 2013). Also, composition of oil affects the extraction and vaporization mechanisms during MCM (Holm and Josendal 1974). Preliminary analysis showed that the effect of heavier components in the oil affects recovery more significantly. Hence, the effect of oil composition is considered in a developed dimensionless number called “oil composition number (OCN)” as shown in Eq. 4.

$$OCN = \sum_{i=10}^n w_{C_i} \quad (4)$$

where OCN is the dimensionless oil composition number and w_{C_i} is the weight fraction of composition i (dimensionless).

Results and discussion

For all of the tests in our dataset, we calculated proposed dimensionless numbers to find an appropriate correlation between oil recovery factor and each number. Figure 1 shows the relation of recovery factor and capillary number for different CO₂ core-flooding experiments on a semi-logarithm plot. Different flow regimes are expected for systems without gravity depending on the capillary number. For very slow displacements, the displacement is controlled by the heterogeneity of the capillary pressures along the interface. The capillary fingering regime is observed in such a system. For fast displacements, where viscous forces overcome capillary

effects, a viscous fingering regime is observed, with a rapid breakthrough of the non-wetting fluid into the wetting fluid. As can be seen in Fig. 1, a higher capillary number leads to a higher oil recovery factor. This means that reduction in capillary force mobilizes the remaining oil in porous media, which decreases the trapping phenomena.

As mentioned before, relative radius is a good indicator of a rock’s physical properties. Figures 2 and 3 show the results of relative radius versus oil recovery factor for two low and high relative radius ranges. Since the relative radius represents the ratio of the microscopic radius to the macroscopic radius, values with low relative radius indicate that porous media consist of pores with a small throat size, compared to an area open to flow. This means that the porous media has low quality and will be faced with fluid flow problems, such as hydrocarbon trapping. Otherwise, reported oil recovery factor is high for some cases

Fig. 1 Capillary number of CO₂ core-flooding tests

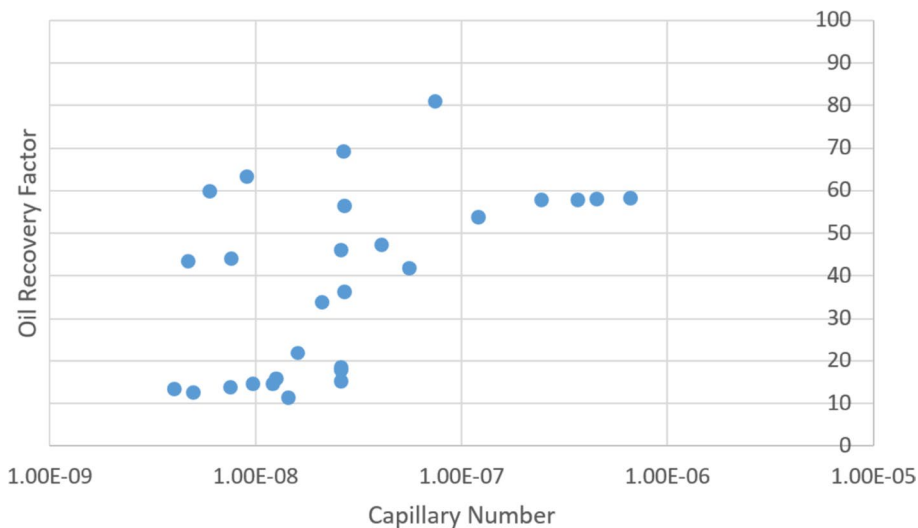


Fig. 2 Relative radius values for low-quality category of porous media

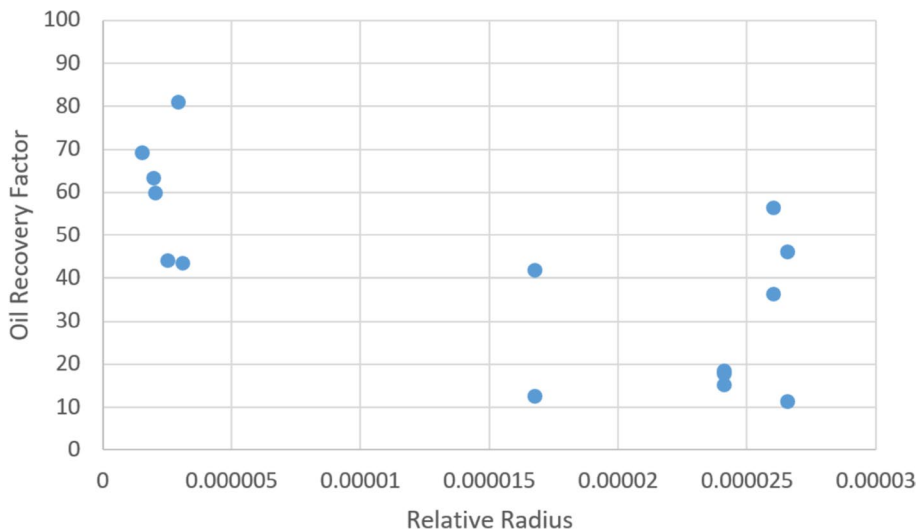
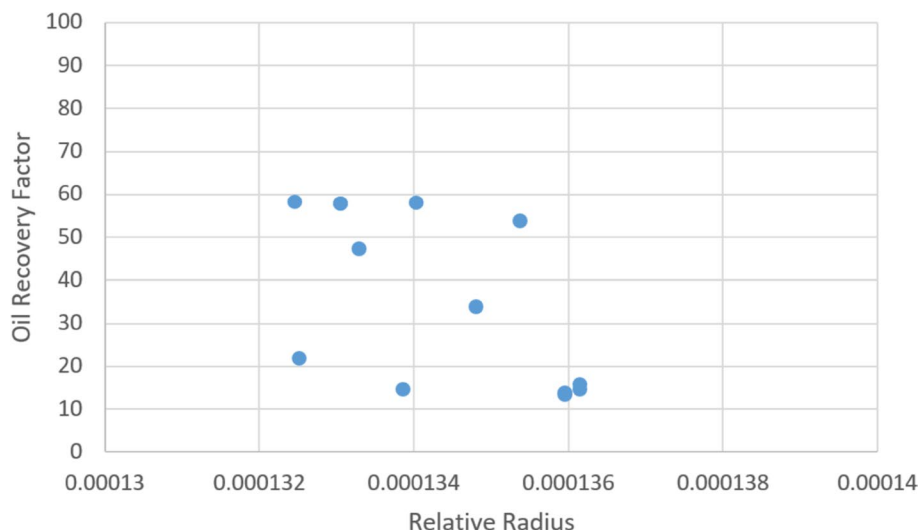


Fig. 3 Relative radius values for high-quality category of porous media



in this category. A high relative radius category leads to better physical quality of porous media, so it is expected that the fluid will flow more easily. It is obvious that there is no clear trend in the reported data, therefore effective parameters should be analyzed together.

Figure 4 depicts oil recovery factor versus injection pressure ratio values. As can be seen, higher pressure ratios result in higher oil recovery factor. This observation comes from the fact that miscible CO_2 flooding is subjected to a higher oil recovery factor compared to immiscible CO_2 flooding. In the higher pressure ratios (the values close to 1), partial miscibility occurs between the oil and CO_2 phase results in the CO_2 dissolution into oil phase. Dissolution of CO_2 contributes to oil production, as it reduces oil viscosity and capillary pressure. It also causes swelling of the oil, which increases oil saturation in the pore space and subsequently the relative permeability of the oil. All of the

mentioned mechanisms improve oil recovery factor during immiscible- CO_2 flooding.

OCN values are presented in Fig. 5. These values are arranged versus oil recovery factor. Three ranges of OCN values have been selected in this study. The first range of OCN values covers the crude oil samples where 0.65 of their compositions consists of components with a carbon number of 10 and higher. This range is a good representative of light oil. In the second range of OCN values, the fraction of C_{10} and heavier hydrocarbons is 0.80–0.85. This range represents moderate oil. The third range covers heavy oil with a carbon number of 10 and higher. The results demonstrate that there is no clear trend between OCN and oil recovery factor; however, crude oil with lower OCN is expected to have more potential to be recovered.

The results presented in the above figures showed that a single dimensionless number could not forecast the oil production

Fig. 4 Injection pressure ratio for CO_2 core-flooding tests

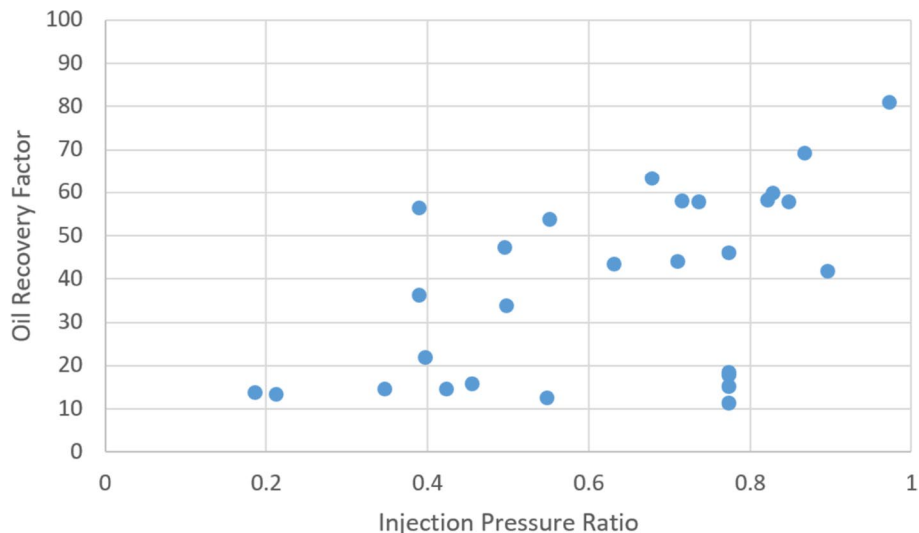
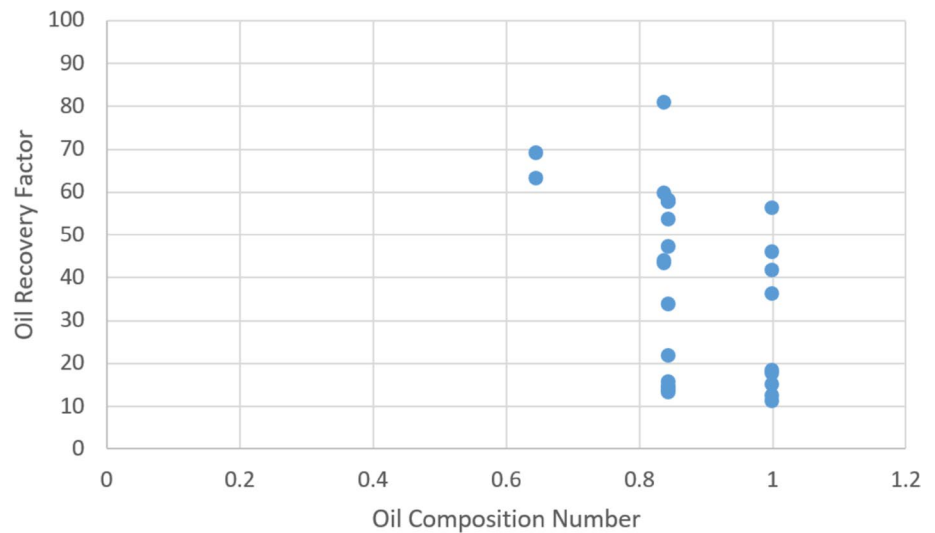


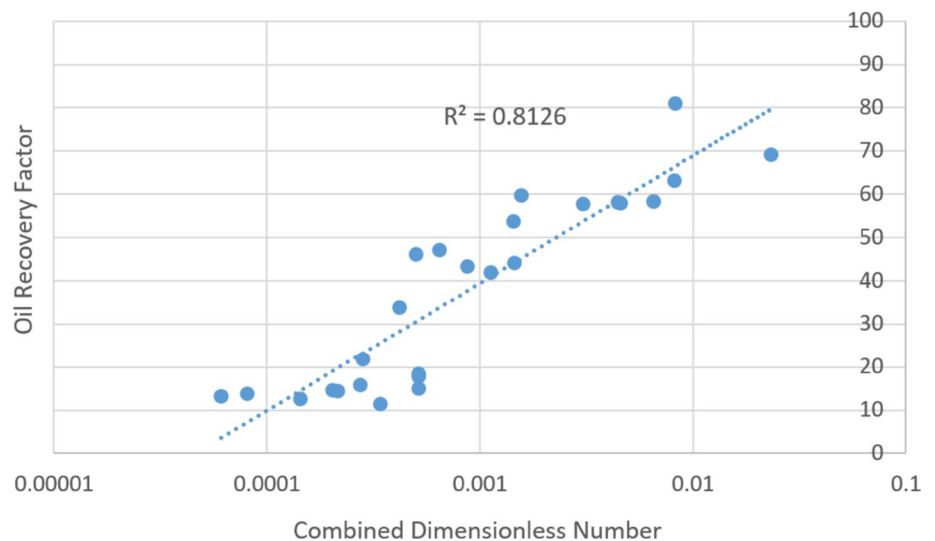
Fig. 5 Oil composition number for CO₂ core-flooding tests



characteristics during immiscible CO₂ core flooding due to the complexity of fluid flow in porous media. A combination of rock/fluid properties and operational conditions is needed to predict the oil recovery factor. Hence, a new approach is required to develop a relationship between oil recovery and operational and rock/fluid dimensionless numbers. Analysis using nonlinear regression was applied using programming code. The results of the analysis suggest a combined dimensionless number that consists of the capillary number and injection pressure ratio in the form of a fraction, with relative radius and oil composition number in the denominator. Equation 5 depicts the proposed combined dimensionless numbers.

$$N_{Co} = \frac{N_c^{0.65} \times P_r}{R_r^{0.38} \times OCN^6} \quad (5)$$

Fig. 6 Comparison of predicted oil recovery factor and experimental oil recovery factor



where the subscript Co stands for the term combined. A correlation has been developed based on N_{Co} and its corresponding experimental oil recovery factor for predicting oil recovery factor. Equation 6 shows the correlation that was developed and it follows the natural logarithm equations from the exponential models family.

$$ORF = 12.806 \ln N_{Co} + 127.87 \quad (6)$$

The results of the predicted oil recovery factor using combined dimensionless numbers and experimental immiscible-CO₂ flooding data are presented in Fig. 6 on a semi-logarithm plot. As can be seen, the proposed correlation can predict oil recovery factor with good agreement. The predicted oil recovery factor and experimental oil recovery factor are matched with 81% confidence. It shows that N_{Co} can be a good representation of the critical parameters that affect the results.

The significance of this study lies in the discovery that by incorporating rock/fluid properties and operational conditions, the accuracy of predicted oil recovery will be improved. Also, the capillary number connects all parameters and plays an important role in predicting oil recovery factor.

Conclusion

An accurate estimation of the oil recovery factor is required to analyze the performance of the method to design the EOR method successfully. In this study, a comprehensive analysis has been carried out to predict the oil recovery factor during the immiscible CO₂ flooding process. Hence, a new dimensionless number (relative radius) is suggested in this study to represent the ratio of pore throat radius-to-core sample radius, using permeability and porosity of the core samples. Additionally, the effects of oil quality and operational conditions were considered using the concept of injection pressure ratio and oil composition number. Also, a new correlation based on the developed dimensionless groups was proposed to predict the oil recovery by CO₂ flooding at the core scale. The results presented in this study suggested that capillary numbers, relative radius, injection pressure ratio, and oil composition number alone could not predict the oil production characteristics because there are a lot of forces and factors affecting oil recovery factor in porous media. To correlate the competition of forces in a porous media that eventually results in the oil recovery factor, a group of dimensionless numbers is needed that can handle a wide range of data. This allows a good correlation between oil recovery factor and the newly proposed group of dimensionless numbers used in this study. A logarithmic relationship was found between the proposed group and oil factor recovery. Predicted oil recovery factor shows good agreement with experimental data (with 81% confidence). This correlation is applicable for a wide range of porosity (10.8–37.2%), permeability (1–18,000 mD), injection pressure (2.73–11.44 MPa), injection rate (0.1–1.0 cm³/min), and crude oil types.

Open Access This article is distributed under the terms of the Creative Commons Attribution 4.0 International License (<http://creativecommons.org/licenses/by/4.0/>), which permits unrestricted use, distribution, and reproduction in any medium, provided you give appropriate credit to the original author(s) and the source, provide a link to the Creative Commons license, and indicate if changes were made.

References

- Abrams A (1975) The influence of fluid viscosity, interfacial tension, and flow velocity on residual oil saturation left by waterflood. *Soc Petrol Eng J* 15:437–447
- Alipour Tabrizy V (2012) Investigated miscible CO₂ flooding for enhancing oil recovery in wettability altered chalk and sandstone rocks. University of Stavanger, Stavanger
- Alipour Tabrizy V (2014) Investigation of enhanced oil recovery using dimensionless groups in wettability modified chalk and sandstone rocks. *J Petrol Eng* 2014:16
- Alvarado V, Manrique E (2010) Enhanced oil recovery. An update. *Rev Energies* 3:1529–1575. <https://doi.org/10.3390/en3091529>
- Amaefule JO, Altunbay M, Tiab D, Kersey DG, Keelan DK (1993) Enhanced reservoir description: using core and log data to identify hydraulic (flow) units and predict permeability in uncored intervals/wells. In: SPE annual technical conference and exhibition. Society of Petroleum Engineers
- Arshad A, Al-Majed AA, Menouar H, Muhammadain AM, Mtawaa B (2009) Carbon dioxide (CO₂) miscible flooding in tight oil reservoirs: a case study. In: Kuwait international petroleum conference and exhibition. Society of Petroleum Engineers
- Brownell LE, Katz DL (1947) Flow of fluids through porous media. 2. Simultaneous flow of 2 homogeneous phases. *Chem Eng Progress* 43:601–612
- Cao M, Gu YG (2013) Oil recovery mechanisms and asphaltene precipitation phenomenon in immiscible and miscible CO₂ flooding processes. *Fuel* 109:157–166. <https://doi.org/10.1016/j.fuel.2013.01.018>
- Dombrowski HS, Brownell LE (1954) Residual equilibrium saturation of porous media. *Ind Eng Chem* 46:1207–1219
- Foster WR (1973) A low-tension waterflooding process. *J Petrol Technol* 25:205–210
- Ghasemi M, Astutik W, Alavian S, Whitson CH, Sigalas L, Olsen D, Suicmez VS (2017) High pressure tertiary-CO₂ flooding in a fractured chalk reservoir. In: SPE annual technical conference and exhibition. Society of Petroleum Engineers
- Godec M, Kuuskraa V, Van Leeuwen T, Melzer LS, Wildgust N (2011) CO₂ storage in depleted oil fields: the worldwide potential for carbon dioxide enhanced oil. *Recov Energy Proc* 4:2162–2169. <https://doi.org/10.1016/j.egypro.2011.02.102>
- Gozalpour F, Ren SR, Tohidi B (2005) CO₂ EOR and storage in oil reservoirs. *Oil Gas Sci Technol* 60:537–546. <https://doi.org/10.2516/ogst.2005036>
- Green DW, Willhite GP (1998) Enhanced oil recovery, vol 6. In: Henry L. Doherty Memorial Fund of AIME, Society of Petroleum Engineers
- Holm LW, Josendal VA (1974) Mechanisms of oil displacement by carbon dioxide. *J Petrol Technol* 26:1427–421438
- Jarrel PM, Fox C, Stein M, Webb S (2002) Practical aspects of CO₂ flooding. Society of Petroleum Engineers, Kuala Lumpur
- Jianbo W, Yuncong G, Chang Z (2016) Response characteristics of CO₂-immiscible flooding WAG in the ultralow-permeability oil reservoirs. *Petrol Geol Oilfield Dev Daqing* 35:116–120
- Kazemi K, Rostami B, Khosravi M, Bejestani DZ (2015) Effect of initial water saturation on bypassed oil recovery during CO₂ injection at different miscibility. *Cond Energy Fuel* 29:4114–4121. <https://doi.org/10.1021/ef502799g>
- Khosravi M, Bahramian A, Emadi M, Rostami B, Roayaie E (2014) Mechanistic investigation of bypassed-oil recovery during CO₂ injection in matrix and fracture. *Fuel* 117:43–49. <https://doi.org/10.1016/j.fuel.2013.09.082>
- Khosravi M, Rostami B, Emadi M, Roayaei E (2015) Marangoni flow: an unknown mechanism for oil recovery during

- near-miscible CO₂ injection. *J Petrol Sci Eng* 125:263–268. <https://doi.org/10.1016/j.petrol.2014.11.030>
- Koottungal L (2014) Survey: Miscible CO₂ continues to eclipse steam in US EOR production. *Oil Gas J* 112:78–91
- Kulkarni MM, Rao DN (2006) Characterization of operative mechanisms in gravity drainage field projects through dimensional analysis. In: SPE annual technical conference and exhibition. Society of Petroleum Engineers
- Kuuskräa VA, Koperna GJ (2006) Evaluating the potential for “game changer” improvements in oil recovery efficiency using CO₂ EOR prepared for US Department of Energy, Office of Fossil Energy—Office of Oil and Natural Gas
- Li HZ, Zheng SX, Yang DY (2013) Enhanced swelling effect and viscosity. Reduction of solvent(s)/CO₂/heavy-oil systems. *Spe J* 18:695–707. <https://doi.org/10.2118/150168-Pa>
- Li L, Zhang Y, Sheng JJ (2017) Effect of the injection pressure on enhancing oil recovery in shale cores during the CO₂ huff-n-puff process when it is above and below the minimum miscibility pressure. *Energy Fuel* 31:3856–3867. <https://doi.org/10.1021/acs.energyfuels.7b00031>
- Mohammed-Singh LJ, Ashok K (2005) Lessons from Trinidad’s CO₂ immiscible pilot projects 1973–2003. In: IOR 2005-13th European symposium on improved oil recovery
- Moore TF, Slobod RL (1955) Displacement of oil by water-effect of wettability, rate, and viscosity on recovery. In: Fall meeting of the petroleum branch of AIME, 1955. Society of Petroleum Engineers
- Nobakht M, Moghadarn S, Go Y (2007) Effects of viscous and capillary forces on CO₂ enhanced oil recovery under reservoir conditions. *Energy Fuel* 21:3469–3476. <https://doi.org/10.1021/ef700388a>
- Norouzi H, Rostami B, Khosravi M, Shokri Afra MJ (2018) Analysis of secondary and tertiary high-pressure gas injection at different miscibility conditions: mechanistic study. In: SPE reservoir evaluation & engineering
- Orr FM Jr, Silva MK, Lien CL, Pelletier MT (1982) Laboratory experiments to evaluate field prospects for CO₂ flooding. *J Petrol Technol* 34:888–898
- Pennell KD, Pope GA, Abriola LM (1996) Influence of viscous and buoyancy forces on the mobilization of residual tetrachloroethylene during surfactant flushing. *Environ Sci Technol* 30:1328–1335
- Rostami B, Kharrat R, Pooladi-Darvish M, Ghotbi C (2010) Identification of fluid dynamics in forced gravity drainage using dimensionless groups. *Transp Porous Media* 83:725–740. <https://doi.org/10.1007/s11242-009-9478-y>
- Rostami B et al (2018) A new approach to characterize the performance of heavy oil recovery due to various gas injection. *Int J Multiph Flow* 99:273–283. <https://doi.org/10.1016/j.ijmultiphaseflow.2017.10.014>
- Shyeh-Yung JG (1991) Mechanisms of miscible oil recovery: effects of pressure on miscible and near-miscible displacements of oil by carbon dioxide. In: SPE annual technical conference and exhibition. Society of Petroleum Engineers
- Srivastava P, Wu X, Amirlatifi A, Devegowda D (2016) Recovery factor prediction for deepwater Gulf of Mexico oilfields by integration of dimensionless numbers with data mining techniques. In: SPE intelligent energy international conference and exhibition. Society of Petroleum Engineers
- Talluru G, Wu X (2017) Using data analytics on dimensionless numbers to predict the ultimate recovery factors for different drive mechanisms of Gulf of Mexico oil fields. In: SPE annual technical conference and exhibition. Society of Petroleum Engineers
- Trivedi JJ, Babadagli T (2008) Efficiency of diffusion controlled miscible displacement in fractured porous media. *Transp Porous Media* 71:379–394. <https://doi.org/10.1007/s11242-007-9131-6>
- Wang XQ, Gu YA (2011) Oil recovery and permeability reduction of a tight sandstone reservoir in immiscible and miscible CO₂ flooding. *Process Ind Eng Chem Res* 50:2388–2399. <https://doi.org/10.1021/ie1016046>
- Wood DJ, Lake LW, Johns RT, Nunez V (2006) A screening model for CO₂ flooding and storage in Gulf Coast reservoirs based on dimensionless groups. In: SPE/DOE symposium on improved oil recovery. Society of Petroleum Engineers

Publisher’s Note Springer Nature remains neutral with regard to jurisdictional claims in published maps and institutional affiliations.