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Tunable Terahertz Dielectric Resonator Antenna

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Abstract



An annular dielectric resonator (DR) antenna (DRA) is implemented for THz applications. A silicon made DR is loaded with graphene disk for obtaining the tunability in the frequency response. The physical parameters of silicon annular DR can be set to obtain the resonance at any frequency in the lower THz band and can be tuned by changing the chemical potential of graphene nano-disk placed at the top of the DR. The response of antenna is preserved after changing the chemical potential of graphene. The higher order hybrid electromagnetic mode is excited in the antenna structure. The proposed research work provides a way to implement the antenna for THz frequency with high gain around 3.8 dBi and radiation efficiency in the range 72 - 75%.

Keywords Silicon · Dielectric resonator · Antenna · Graphene · Disk · Chemical potential · Tuning

1 Introduction

In the recent years, wireless communication systems are being developed considering the THz band in the applications [1]. The advantage of THz spectrum is its capability in offering the wide bandwidth and hence the high data transfer rate. An antenna is always an integral part of any wireless communication system. Several antennas have been implemented for THz spectrum. In concise manner, THz antennas can be categorized into three ways; (1) the antenna with metal/dielectric radiator [2-11], (2) antenna with the radiator of 2D material [12-26], and (3) with the interface of metal/dielectric/ graphene [27–34]. The first type of THz antennas can be sub categorized into two parts, one with the metallic radiator and second with dielectric radiator. In the case of metallic radiators, the surface wave and conductor losses are high at the THz frequency hence they become less efficient and they provide the efficiency around 50% [6, 8]. However, some metallic antennas were implemented providing the radiation efficiency around 80% [4, 5]. Still, the use of metal at THz frequency may be complex in practical due to their reduced conductivity [35]. The antennas implemented using the dielectric material as radiator always remains in advantage of

Gaurav Varshney gauravnitd@outlook.com providing the high gain and radiation efficiency [2, 11]. However, the dielectric resonator antennas (DRAs) were implemented at the higher THz spectrum falling in the optical regime. No DRA was implanted for the lower THz spectrum. Apart from these antennas, the techniques were implemented for the enhancement of gain, radiation efficiency and other performance parameters of the metal-dielectric based antennas like use of photonic crystal and frequency selective surface [10], Yagi-Uda structure with defected ground structure [9] and metamaterial cavity with reflector structure [7]. However, these improvement techniques offer complexity in terms of fabrication and size, which remains the main issue at the THz spectrum. In view of the fact that the performance parameters of THz antennas implemented using the metal/ dielectric interface and radiators can be improved but still there is one limitation i.e. non-reconfigurability of their response. Industries are seeking the solution for the implementation of tunable and reconfigurable devices at micro/nanoscale. At the microwave frequency, it is possible to refabricate the devices, but it becomes a difficult task at the THz spectrum due to small scale implementations. Also, it is easy to utilize varactor or PIN diode for obtaining the tunability in the microwave devices [36]. This is a difficult task to fabricate the micro/nanoscale devices with such incorporations.

At the micro/nanoscale, the material based tunability is being explored and recently 2D material like graphene is investigated which provides the solution to the problem of nonreconfigurability [37]. Currently, researchers are on the way of numerical investigations on this novel material-based

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Fig. 1 The geometry of the proposed silicon DR based tunable DRA $(r_i = 8, r_o = 25, h = 13.4, w_f = 2.8, l_f = 23, w_s = l_s = 60)$

device which is expectedly going to become a future of the technology. In the current electronic and optoelectronics, problems are being investigated through the implementation of the devices by utilizing the graphene material [38-40]. Specially, graphene based functioning gives a thrust due to its electrical tunability with the applied external electrostatic or magnetostatics biasing [41]. The electrical tunability of material properties confers the reconfigurability in response of devices. Considering the advantages of the graphene material, the antennas have been implemented by utilizing it that comes under the second and third categories of the THz antennas. The second category of antenna utilizes the radiator made up of the graphene material [14, 19–21]. The antenna with graphene based radiator provides the reconfigurability in different performance parameters like frequency response and radiation pattern [42, 43]. The limitation of these antennas is their low radiation efficiency and gain [12, 13, 18, 25, 26]. A Y-shaped graphene antenna was reported with 24% efficiency and 0.13 dBi gain. A 26% of radiation efficiency was obtained by graphene nano-ribbon based antenna [26] which is then improved to 44% with the gain of 2 dBi [25]. A multi layered graphene patch antenna and array was also reported to provide the efficiency around 45% [12, 13]. Somehow, the efficiency of graphene antennas was improved up to 90% by using the multilayer stacked structure of graphene [21]. However,

obtaining the tunability in the frequency response with multilayered structure practically becomes a complex task [21, 44]. Also, the high gain and radiation efficiency was obtained by introducing a dielectric cavity in the graphene dipole antenna [24]. In this case, it is necessary to couple the resonance of graphene radiator with the dielectric cavity so that proper functioning can be obtained which becomes a complex task at the design level. Thus, the THz antenna of second category can provide the reconfigurability but their performance is poor.

The problems associated with the antennas of first and second category are rectified by third category. In the third category, the THz antennas were implemented with the utilization of main radiating element made up of metal and the graphene material is introduced so that the reconfigurability in response can be obtained [27, 45]. In these antennas, resonance of graphene is not a matter, it is only used for obtaining the reconfigurability in the frequency response of the metal-based radiator [29, 30]. A metallic ring antenna was implemented with graphene for obtaining the reconfigurability [29]. This antenna provides the gain around 1 dBi. The radiation efficiency of the graphene antenna was improved by utilizing the metamaterial cells up to 60% [30]. A Yagi antenna was implemented with graphene for providing the reconfigurability in the frequency response and the gain around 8.24 dBi. A microstrip patch was reported with superstrate and graphene load that drastically improves the gain up to 11 dBi and provides the 78% radiation efficiency but this acquires a large size. In the sequence, a metallic ultra-wideband antenna with graphene ribbons was implemented with the tunable dual-band notch and provides the gain and radiation efficiency 6.3 and 80%, respectively [27].

The analysis of THz antennas reveals that it is still required to implement antenna which can be fabricated in an easy way in the future. Also desired performance parameters can be obtained. The main concern of THz antennas is their low gain and radiation efficiency. This enforces the exploring of suitable way for the implementation of THz antennas. In the way to find the solution for low gain and radiation efficiency, one can think about the implementation of a dielectric resonator (DR) antenna (DRA) for THz spectrum. The DRAs are

Fig. 2 The frequency response of **a** S₁₁-parameter and **b** impedance of antenna ($\mu_c = 0 \ eV, T = 300K, \tau = 1 \ ps$)





Fig. 3 *E*-field distribution in the DR with graphene disk at its top in $\mathbf{a} z = 0$, $\mathbf{b} z = h$, \mathbf{c} in different cross-sections, $\mathbf{d} z = h$ and $\mathbf{e} x$, $y = \pm r_o$ plane and *H*-field distribution in $\mathbf{f} z = 0$, \mathbf{g} and $\mathbf{h} z = h$ plane at frequency 4.104 THz

prominent since last three decades in microwave frequency regime since last three decades due to their capability in providing high gain and radiation efficiency and wide bandwidth [46, 47]. Also, the optical DRAs have been implemented for the same purpose [2, 11, 48]. The use of high permittivity material not only reduces size of the antenna but provides the enhanced performance also [49]. In the similar manner, the DRA can also be implemented for operating in 0.1 - 10 THz band. Following the properties of graphene, the DRA can be coupled with the non-resonant graphene material so that tunability can be obtained. Earlier, the graphene antenna was coupled to dielectric cavity for improving the performance of the graphene antenna [24].

Following the motivation obtained from the above discussion, a DRA is implemented for THz spectrum by utilizing the silicon made DR. The utilization of silicon material provides the high permittivity which can enhance the radiation properties like gain and radiation efficiency [11]. Also, this is abundantly available which can ease the fabrication. The DRA is loaded with a graphene disk at its top surface for obtaining the reconfigurability in the frequency response by changing the chemical potential of graphene. The research issues dictating the problem of low gain and radiation efficiency with tunability of frequency response of THz antenna can be solved by utilizing the DR interfaced with graphene material. The implemented antenna provides the gain around 3.8 dBi and radiation efficiency more than 72%. Thus, the proposed antenna can replace many others implemented for THz applications. Furthermore, a tunable THz antenna array can also be implemented in the future for improving the performance parameters by utilizing the proposed single unit of tunable DRA. Moreover, this is the first research work reporting a tunable DRA for THz applications with the help of graphene material.

2 Antenna Design

Figure 1 shows the antenna structure containing a substrate made of silicon dioxide ($\epsilon_s = 3.8$) placed at the top of the conducting ground plane. A silicon DR ($\epsilon_s = 11.9$) is placed at the top of the substrate having thickness 1.6 μm . The dispersive profile of silicon material is considered as constant over the operating frequency band. Initially the dimensions of DR are selected to operate with the fundamental hybrid electromagnetic mode using the formulae given in Eq. (1) [2]. After that, the dimensions have been optimized for obtaining the desired response.







Fig. 5 Radiation pattern of tunable DRA at frequency 4.104 THz in a xz, b yz and c xy-plane (solid line-co- and dotted line- cross-polarized components of radiated field)

$$f_{vpm} = \frac{6.324c}{4r_o \pi \sqrt{\epsilon_r + 2}} \left[0.27 + 0.36 \left(\frac{r_o}{h}\right) + 0.002 \left(\frac{r_o}{h}\right)^2 \right] (1)$$

Here, v, p and m are integers which represent the variation of field in terms of half-wavelength along the azimuth, radius, and height of the DR [50]. Here, the DR with zero inner radius provides the resonance of fundamental hybrid mode with the selected dimensions. The excitation of any mode in the DR depends upon its aspect ratio as well as the applied feeding technique [46]. The DR of optimized dimensions provides the resonance at frequency 4.088 THz with the field distribution of the higher order hybrid mode. The selected antenna parameters with the applied feeding suppress the lower order modes. The excitation is applied to DR by using a nanostrip line made of silver material. The selection of material properties at THz frequency band becomes important in terms of transmission losses hence the dispersive properties of the material used in the nanostrip are selected accordingly. For lower THz frequency spectrum, the silver material can be selected with the conducting and dispersive properties as given in [51]. The antenna structure can be fabricated by utilizing the process



Fig. 6 3D radiation pattern of tunable DRA at frequency 4.104 THz

explained in the literature [52–56] The metallic elements working as the feed and ground can be grown on SiO₂ substrate [54]. After fabricating the silicon in the shape of the proposed annular dielectric resonator, the chemical vapor deposition process can be utilized either for growing the graphene monolayer on it [55, 56] or by transferring approach [53, 54, 57]. A detailed discussion of the fabrication steps can be explored as reported in [52–56]. For obtaining the tunability in the antenna response, a graphene disk of thickness 0.34 *nm* having the properties defined by the parameters like chemical potential (μ_c), relaxation time (τ) at the room temperature *T* = 300*K* is placed at the top of the silicon DR. The antenna structure is numerically analyzed and implemented using CST microwave studio. The optimized dimensions of antennas are mentioned in the caption of Fig. 1.

3 Results and Discussion

For understanding of antenna operation, two structures are implemented and analyzed; one without and another with graphene disk at the top of the silicon DR. Figure 2 shows the frequency response of S₁₁ parameter and impedance of these both the antennas. The DRA without graphene disk at its top has the resonance at 4.088 THz. This antenna has the null-reactive impedance and peak of its real part at the resonant frequency. Placing the graphene disk with properties $\mu_c = 0 \ eV$ and $\tau = 1 ps$ at T = 300K shifts the resonant frequency and frequency response in the forward direction. After placing the graphene disk at the top of the antenna, the new resonance frequency of the antenna becomes 4.104 THz. The shift in the resonant frequency after placing the graphene disk can be attributed to change in the material profile and medium properties at the interface of silicon DR and graphene boundaries. Also, this indicates that changing the electrical properties of the material placed at the top of the DR can tune the antenna response. Also, it is showing that graphene disk remains non-resonant over the operating frequency. Moreover, the shift in the resonant frequency reveals that addition of graphene ring only adds the value in the inductive and

Table 1 Performance	e 1 Performance of the antenna with and without graphene ring							
Antenna	Operating mode	Resonant frequency (THz)	10 dB impedance bandwidth (GHz)	Gain (dBi)	Radiation efficiency (%)			
DRA	$HEM_{41\delta}$	4.088	68	3.81	75			
DRA+ Graphene disk	$HEM_{41\delta}$	4.104	67	3.79	72			

capacitive part of impedance which can be realized as the parallel tank circuit using circuit theory approach [20]. It can be noticed that the impedance bandwidth of antenna remains approximately same in both the cases. The radiation mechanism of the proposed tunable DRA with graphene disk can be understood by observing the electric (E) and magnetic (H)field distribution. The field distribution is shown in Fig. 3 which shows the generation of hybrid modes. In Fig. 3a-e, there are eight vertical quadruple of E-field in the DR. Also, the H-field distribution shown in Fig. 3f-h shows that the vertical electrical quadruples are surrounded by the horizontal magnetic rings. Thus, it can be concluded that there is the generation of four vertical electric dipole in the annular DR. Thus, there are four half-wave variation along the azimuth angle. Also, there is single half-wave variation of field along the radius of the resonator. The partial variation of field can be considered along the height of the DR. Thus, the antenna operates with $HEM_{41\delta}$ mode. Here, the indices in suffix are showing the variation along azimuth, radial and height of the DR. The field variation is corresponding to the modal field analysis reported in the literature [50, 58]. Figure 4 shows the plot of gain and radiation efficiency. The antenna provides the gain and radiation efficiency more than 3 dBi and 72%, respectively over the operating passband.

Figure 5 shows the radiation pattern of tunable DRA at resonant frequency in all the principal planes. The separation between the co- and cross-polarized component of the radiated far-field is more than 60 dB which shows a good signal detection capability of antenna at receiver. Also, the front-to-back ratio of antenna is sufficiently large that enables to provide the high directivity around 5.07 dBi denoted by the 3D radiation pattern plot shown in Fig. 6.

The performance of both the antennas with and without graphene disk is reported in Table 1. The antenna operates with fourth order hybrid mode and provides high gain and radiation efficiency at the resonant frequency. The gain and radiation efficiency of the antenna is slightly reduced in the case of graphene disk is placed at the top of the DR. This may be due to losses occurred at the interface of the silicon dielectric and graphene disk.

4 Antenna Performance Analysis

A parametric study is carried out to know the effect of variation in physical parameters of proposed tunable DRA (DRA with graphene disk) on its response. The main parameters of antenna are inner and outer radius, r_i and r_o , respectively and height of the DR. These parameters are varied and effect is reported in Fig. 7. The outer radius of DR can be selected to operate at any frequency as shown in Fig. 7a. The inner radius plays an important role in the impedance matching. The appropriate selection of r_i provides good impedance matching as shown in Fig. 7b. The variation in r_i changes the power coupled to the DR from feedline which affects the impedance matching severely. Here, the proposed antenna operates with δ variation along the height of the DR. So, it can be concluded that the variation in height will affect the impedance matching and resonant frequency accordingly. The effect of varying the height on antenna response is mentioned in Fig. 7c. It can be observed in the plot that the impedance bandwidth is varied by lowering the reflection coefficient in the lower frequency region. Lowering the reflection coefficient confirms about the operation of antenna with the multiple operating modes. Thus, the antenna response can be set either with the multiple



Fig. 7 The frequency response of tunable DRA for variable $\mathbf{a} r_o$, $\mathbf{b} r_i$ and $\mathbf{c} h$

Fig. 8 Tuning of frequency response of **a** magnitude and **b** phase of S₁₁-parameter **c** impedance and **d** gain with μ_c (*eV*) (*T* = 300*K*, τ = 1*ps*)



operating modes for providing the wide operating impedance bandwidth or with the single mode for providing narrowband frequency response with high selectivity. Moreover, the

antenna response with and without graphene disk varies with the small change, hence the parametric variation of the antenna without graphene disk provides the variation in antenna

Table 2 Comparison with the other THz antennas

Category	Ref	Antenna	10 dB Impedance bandwidth (THz)	Gain (dBi)	RE (%)	Size (λ^3)	Tunability
1	[4]	Metallic patch	0.3-9.3	9.5	0-80	$5.92 \times 7.9 \times 0.6$	No
	[5]	Metallic patch	0.46 - 5.46	12	0 - 80	$9.6 \times 12.8 \times 1.3$	No
	[6]	Metallic patch	0.7 - 0.85	3.502	55.88	$2.6 \times 2.6 \times 0.5$	No
	[7]	Metamaterial cavity with reflector	0.47 - 0.65	10	_	$0.86 \times 0.56 \times 0.112$	No
	[8]	Metamaterial loaded patch	1.053 - 1.141	3.57	_	0.7 imes 0.77 imes 0.04	No
	[9]	Yagi-Uda with grating	1.84 - 2.42	3.9	100	0.7 imes 0.64 imes 0.007	No
[10]	[10]	Patch with photonic crystal and FSS	0.5 - 0.7	7.3	_	$1.2 \times 1.2 \times 0.55$	No
2 [12] [13] [18] [21] [23] [24] [25] [26]	[12]	Graphene patch	0.48-0.6	_	50	$1 \times 1 \times 0.05$	Yes
	[13]	Graphene Patch	0.55 - 0.58	_	40	$1 \times 1 \times 0.05$	Yes
	[18]	Y-shaped graphene patch	0.42 - 0.48	0.13	24	$0.6 \times 0.7 \times 0.1$	No
	[21]	Graphene stack	1.35 - 1.5	_	90	$1 \times 1 \times 0.05$	_
	[23]	Graphene dipole	0.9-1	_	21	$0.64 \times 0.38 \times 0.13$	Yes
	[24]	DR coupled to graphene radiator	2-3	7	70	$1.7 \times 1 \times 1.05$	_
	[25]	Graphene nano-ribbon radiator	0.924 - 1.2	2	44	$1 \times 1 \times 0.1$	Yes
	[26]	Graphene nano-ribbon radiator	0.64 - 0.82	_	26	$1 \times 1 \times 0.64$	Yes
3	[27]	Metallic patch with graphene ribbons	4.76 - 19	6.4	80	$0.95 \times 0.8 \times 0.075$	Yes
	[29]	Metallic ring with graphene	1.10	1	_	$0.6 \times 0.6 \times 0.003$	Yes
	[30]	Graphene with metamaterial	1.7	_	60	$0.28 \times 0.06 \times 0.15$	Yes
	[31]	Yagi antenna with graphene	0.97 - 1.12	8.24	_	$0.77 \times 0.55 \times 0.0035$	Yes
	[32]	Patch with graphene load	0.95 - 1.05	11	78	$1.26 \times 1.26 \times 0.65$	Yes
	This	Graphene disk loaded DR	4.0629-4.1299	3.8	72 - 75	$0.81 \times 0.81 \times 0.18$	Yes
	Antenna	-					

-not reported, RE-radiation efficiency

response in the similar manner as with graphene disk (as mentioned in Fig. 2). For brevity, the parametric variation of the antenna without graphene disk is not reported in the manuscript.

5 Tuning of Frequency Response

The top of the silicon DR is coated with the monolayer graphene material having thickness 0.34 nm. The purpose of coating of silicon DR by graphene material is to utilize its property that its surface conductivity can be tuned by applying an external electrostatic DC field [59–61]. Figure 8 shows the antenna response with variation in μ_c . Figure 8a, b shows the variation in magnitude and phase of the S₁₁ parameter response of antenna. It can be observed in the plots that the resonant frequency and covered 10 dB impedance bandwidth can be steered over the frequency with the variation in μ_c . The phase of S₁₁ parameter at resonant frequency varies linearly with each value of μ_c confirming that the radiation properties of antenna remain same after changing the value of chemical potential of graphene. Figure 8c shows the impedance plot of antenna for different values of μ_c . This confirms about the shift in resonant frequency of the operating mode with the variation in μ_c . Also, linear plot shows the antenna operation with single mode. The gain plot is reported in Fig. 8d showing that the peak of gain is also shifting in correlation with the operating passband, as expected.

Table 2 shows the comparison of the proposed antenna with other THz antennas existing in the literature. The comparison table shows that many antennas of first category can provide high gain [4, 5, 7, 10] and radiation efficiency [4, 5, 9], but their response cannot be tuned like the proposed tunable DRA. Also, they have the limitation of large size in comparison to the proposed antenna. Also, it is still a question in the case of metallic antennas that whether practically they are this much efficient at higher frequencies or not [4, 5]. In the second category, most of the antennas provide the low value of gain and radiation efficiency in comparison to the proposed antenna. Some antennas provide high gain [24] and radiation efficiency [21] but they have large size in comparison. In the similar manner, some antennas in the third category can provide the tunability with high gain [31] and radiation efficiency [31, 32], but they have the limitation of size and other performance parameters. Overall, it can be concluded that the proposed antenna can replace many others in terms of gain, radiatin efficiency, size and tunability. Also, the proposed antenna can avoid the fabrication complexities in comparison to other implemented by utilizing the FSS and metamaterial [10, 30, 32]. Furthermore, in most of antennas of second and third categories, the tunability is achieved but the performance characteristics and frequency response is not preserved with the variation in the chemical potential of graphene [16, 31-34]. The proposed antenna offers the capability over such antennas and preserves its frequency response for all values of μ_c .

6 Conclusion

A tunable DRA is numerically analyzed and implemented for THz applications. The frequency response of antenna has been tuned by changing the chemical potential of graphene disk placed at the top of the DR. The parametric variation in the physical dimensions of antenna reveals that the antenna response can be tuned either with the single or multiple operating modes. The aspect ratio of DR and other parameters have been selected to suppress the lower order modes and to operate with the single higher order hybrid electromagnetic mode. Placing the graphene disk at the top of the antenna does not affect the antenna operation. The antenna response can be preserved over a wide range of chemical potential of graphene. The THz DRA without graphene disk at its top provides the gain and radiation efficiency around 3.81 dBi and 75%, respectively. The performance indices are slightly deteriorated with insignificant amount in the case of proposed tunable THz DRA with graphene disk. The proposed antenna provides gain around 3.79 dBi and radiation efficiency 72-75% with the tunable frequency response at THz frequency.

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