

# Enhancing low-temperature  $NO<sub>r</sub>$  storage and reduction performance of a Pt-based lean  $NO<sub>x</sub>$  trap catalyst

Tong Wang, Li-Wei Jia, Xiu-Ting Wang, Gang Wang, Fu-Qiang Luo, Jia-Ming Wang\*<sup>6</sup>

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**Abstract** Two lean  $NO_x$  trap (LNT) catalysts, Pt/BaO/  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  and Pt/BaO/CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>, were prepared and compared for low-temperature ( $\lt 250$  °C) NO<sub>x</sub> storage and reduction performance. The influence of the form of ceria on low-temperature  $NO<sub>x</sub>$  storage and reduction performance of LNT catalysts was investigated with the focus on  $NO<sub>x</sub>$  storage capacity,  $NO<sub>x</sub>$  reduction efficiency during lean/rich cycling, product selectivity and thermal stability. Inductively coupled plasma-atomic emission spectrometry  $(ICP-AES)$ , Brunner–Emmet–Teller  $(BET)$ , H<sub>2</sub>-pulse chemisorption and X-ray diffraction (XRD) were conducted to characterize the physical properties of LNT catalysts.  $NO_x$  storage capacity and  $NO_x$  conversion efficiency were measured to evaluate  $NO<sub>x</sub>$  storage and reduction performance of LNT catalysts. Pt/BaO/  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  catalyst exhibits higher NO<sub>x</sub> storage capacity than Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> catalyst in the temperature range of 150–250 °C. Meanwhile, Pt/BaO/  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  catalyst shows better NO<sub>x</sub> conversion efficiency and  $N_2$  selectivity. XRD results indicate that the thermal stability of  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  complex oxide is superior to that of pure  $CeO<sub>2</sub>$ . H<sub>2</sub>-pulse chemisorption results show that  $Pt/BaO/CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  catalyst has higher Pt dispersion than Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> catalyst over fresh and aged samples. The improved physical properties of Pt/BaO/CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub> catalyst are attributed

T. Wang, F.-Q. Luo

Wuxi Weifu Environmental Catalysts Co. Ltd, Wuxi 214028, China e-mail: wxt5409@126.com

to enhance the  $NO<sub>x</sub>$  storage and reduction performance over Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> catalyst.

**Keywords**  $NO<sub>x</sub>$  storage and reduction; Low temperature; Ceria; Ceria-alumina; LNT

# 1 Introduction

To meet the stringent China Stage-VI light-duty diesel vehicles'  $NO<sub>x</sub>$  emission regulations, a promising approach has been explored by a combination of lean  $NO<sub>x</sub>$  trap (LNT) and selective catalytic reduction (SCR) catalysts  $[1-3]$ , which can enhance NO<sub>x</sub> reduction while avoiding the need for urea injection to the SCR catalyst [\[4](#page-5-0)]. However, additional improvements are required in LNT system, especially for low-temperature  $NO<sub>x</sub>$  conversion [[5,](#page-5-0) [6](#page-5-0)].

LNT catalysts operate under cyclic lean/rich conditions [\[7](#page-5-0), [8\]](#page-5-0). During lean conditions,  $NO<sub>x</sub>$  is stored on the catalyst; while during rich conditions, stored  $NO<sub>x</sub>$  is released and reduced into  $N_2$  along with possible byproducts, such as  $NH_3$  and  $N_2O$  [[9–11\]](#page-5-0). A typical LNT catalyst contains basic components (alkali metal or alkaline earth metal compounds) for  $NO<sub>x</sub>$  storage, noble metals (Pt, Pd, Rh), and support oxides [[7\]](#page-5-0). In addition, ceria-based materials have been shown to be beneficial for LNT catalysts at low temperatures  $[12-14]$ . CeO<sub>2</sub> is a common rare earth metal oxide with special structure and properties [\[15–17](#page-5-0)], and many current commercial LNT catalysts have already incorporated ceria [\[5](#page-5-0), [18](#page-5-0)].

In the present work, the goal was to study the effects of the form of ceria on low-temperature  $NO<sub>x</sub>$  storage and reduction performance through surface/bulk analysis and activity tests. The first catalyst of Pt/BaO/CeO<sub>2</sub> +  $Al_2O_3$ 

School of Automotive and Traffic Engineering, Jiangsu University, Zhenjiang 212013, China

L.-W. Jia, X.-T. Wang, G. Wang, J.-M. Wang\*

used ceria as a support material as well as alumina, and the second catalyst of Pt/BaO/CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub> used complex ceria–alumina as a new support material. The low-temperature  $NO<sub>x</sub>$  storage capacity (NSC),  $NO<sub>x</sub>$  reduction efficiency,  $NH_3$  production and  $N_2O$  emissions were measured. Thermal stability of LNT catalysts was also investigated after aging for 20 h at 800  $^{\circ}$ C.

# 2 Experimental

# 2.1 Catalyst preparation

Catalysts were prepared by incipient wetness impregnation technique, using aqueous solutions of  $BaCH_3COO_2$  and Pt(NO<sub>3</sub>)<sub>2</sub>. In the preparation of Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> (1) wt% Pt and 9 wt% BaO), CeO<sub>2</sub> (specific surface area 152 m<sup>2</sup>·g<sup>-1</sup>) and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> (150 m<sup>2</sup>·g<sup>-1</sup>) were mechanically mixed at the weight ratio of 3:7. The impregnation was carried out in a sequential manner: The well-mixed  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  support was firstly impregnated with the Ba acetate solution followed by Pt nitrate solution. On the other hand, Pt/BaO/CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub> (1 wt% Pt and 9 wt%) BaO) was prepared similarly, but using a  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$ complex oxide (30 wt%  $CeO<sub>2</sub>$  and 70 wt%  $Al<sub>2</sub>O<sub>3</sub>$ , 154 m<sup>2</sup>·g<sup>-1</sup>) as the support. After each impregnation step, the catalyst was dried at 100  $^{\circ}$ C in air for overnight and then calcined in air at 500  $\degree$ C for 5 h. The obtained fresh catalysts were denoted as F-1 and F-2, respectively. In order to compare their thermal stability, the catalysts were further calcined in air at 800  $^{\circ}$ C for 20 h. The aged catalysts were denoted as A-1 and A-2.

# 2.2 Catalyst characterization

The actual elemental compositions of catalysts were analyzed by inductively coupled plasma-atomic emission spectrometry (ICP-AES, Optima 2100 DV, PerkinElmer). The Brunner–Emmet–Teller (BET) specific surface areas were measured by  $N_2$  adsorption–desorption at  $-196$  °C on a Micromeritics ASAP 2000 analyzer. Prior to measurements, the samples were pre-treated at  $150^{\circ}$ C under vacuum for 3 h to eliminate the adsorbed species. The Pt dispersions were determined by  $H_2$ -pulse chemisorption at  $-$  80 °C by a Micromeritics AutoChem II Analyzer. The crystalline phases of the catalysts were characterized by X-ray diffractometer (XRD, XRD-600, Shimadzu) with a Cu K $\alpha$  radiation ( $\lambda = 0.154056$  nm) at 36 kV with a graphite monochromator.

#### 2.3 Activity measurements

In  $NO<sub>x</sub>$  storage capacity (NSC) and  $NO<sub>x</sub>$  conversion efficiency measurements,  $0.25$  g Pt/BaO/Al<sub>2</sub>O<sub>3</sub> catalyst was mixed with 0.75 g quartz sand. The total flow rate is 1 L·min<sup>-1</sup>, corresponding to a space velocity of 60,000 h<sup>-1</sup>. Before each experiment, the sample was oxidized in 10%  $O_2/N_2$  balance at 350 °C for 30 min, and then reduced in 5%  $H_2/N_2$  balance at 450 °C for 20 min. The reactor was then cooled in  $N_2$  to the target test temperatures at 150, 200 and 250  $\degree$ C. The outlet gas of the reactor was maintained at 140 °C to avoid condensation and  $NH_3$  hold-up. A MKS MultiGas 2030 FT-IR analyzer was used to monitor NO,  $NO<sub>2</sub>, N<sub>2</sub>O, NH<sub>3</sub>, CO, C<sub>3</sub>H<sub>6</sub>, CO<sub>2</sub>$  and  $H<sub>2</sub>O$  concentrations of the outlet gas.

 $NO<sub>x</sub>$  storage capacity (NSC) tests were conducted by exposing the catalyst to the flowing gas containing  $250 \times 10^{-6}$  NO, 8% O<sub>2</sub>, 5% H<sub>2</sub>O, 5% CO<sub>2</sub> at 150, 200 and 250 °C. The storage time was 10 min at each temperature during NSC measurement.  $NO<sub>x</sub>$  conversion efficiency tests were also measured at 150, 200 and 250  $^{\circ}$ C, and LNT performance was evaluated in a lean/rich (100 s/17 s) cycle under the gas composition detailed in Table [1](#page-2-0). The average value of the last 5 cycles was calculated after 15 lean/rich cycles.

# 3 Results and discussion

# 3.1 Catalyst characterization

The contents of Pt, Ba, Ce and Al in catalysts are summarized in Table [2](#page-2-0). F-1 and F-2 samples have similar Pt and Ba contents. Ce content in F-1 is slightly lower than that in F-2 (26.24 wt% vs. 27.54 wt%).

BET specific surface areas and Pt dispersions of catalysts are listed in Table [3](#page-2-0). The specific surface areas of F-1 and F-2 samples are 117 and 122  $m^2 \cdot g^{-1}$ , respectively. Pt dispersion of F-1 is 60%, slightly lower than 62% of F-2. After thermal aging at 800  $^{\circ}$ C for 20 h, their surface areas decrease to 99 and 103  $m^2 \cdot g^{-1}$ , respectively. The Pt dispersions reach significantly low values, only 12% for A-1 and 19% for A-2, indicating that the sintering of Pt particles occurs during aging due to the mobility of Pt crystallites and eventually merged to form larger particles [\[19](#page-5-0)].

Figure [1](#page-2-0) shows XRD patterns of fresh and aged catalysts. The results show that Pt-related phases in all four samples were not detected because of either the low loading ratio or its small size. The main crystallite phases detected are  $CeO<sub>2</sub>$ , BaCO<sub>3</sub> and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> in all samples. The  $BaAl<sub>2</sub>O<sub>4</sub>$  peak only appears after aging [[20,](#page-5-0) [21\]](#page-5-0). Applying Scherrer equation, the average  $CeO<sub>2</sub>$  crystal size was calculated based on CeO<sub>2</sub> diffraction peak at  $2\theta = 28.5^{\circ}$ . The

<span id="page-2-0"></span>**Table 1**  $NO<sub>x</sub>$  conversion efficiency measurement: gas composition

| Gas composition | NO                   | CO                    | $C_3H_6$             | $CO2/\%$ | $H2O/\%$ | $O_2/\%$ | $H_2/\%$                 | $\rm N_2$ |
|-----------------|----------------------|-----------------------|----------------------|----------|----------|----------|--------------------------|-----------|
| Lean            | $250 \times 10^{-6}$ | $1800 \times 10^{-6}$ | $370 \times 10^{-6}$ |          |          | 10.00    | $\overline{\phantom{0}}$ | Bal.      |
| Rich            | $250 \times 10^{-6}$ | $3.00\%$              | $960 \times 10^{-6}$ |          |          | 0.60     | 0.25                     | Bal.      |

Table 2 Elemental composition of fresh catalysts (wt%)



F-1—fresh Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> catalyst; F-2—fresh Pt/BaO/  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  catalyst

Table 3 BET specific surface areas and Pt dispersions of catalysts

| Catalyst | Surface area/ $(m^2 \tcdot g^{-1})$ | Pt dispersion/% |  |  |
|----------|-------------------------------------|-----------------|--|--|
| $F-1$    | 117                                 | 60              |  |  |
| $F-2$    | 122                                 | 62              |  |  |
| $A-1$    | 95                                  | 12              |  |  |
| $A-2$    | 103                                 | 19              |  |  |

 $CeO<sub>2</sub>$  crystal size in F-1 is estimated to be 10 nm, while 6 nm in F-2, 16 nm in A-1, and 7 nm in A-2, respectively. These XRD results suggest that the thermal stability of  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  complex oxide is superior to that of pure  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  with regard to  $CeO<sub>2</sub>$  crystal size.

3.2  $NO<sub>x</sub>$  storage capacity (NSC)

The results of  $NO<sub>x</sub>$  storage capacity tests are reported in Table 4. All samples' NSCs increase substantially as the test temperature increases from 150 to 250  $\degree$ C due to

**Table 4** NO<sub>x</sub> storage capacity (250  $\times$  10<sup>-6</sup> NO, 8% O<sub>2</sub>, 5% H<sub>2</sub>O, 5% CO<sub>2</sub>, N<sub>2</sub> bal., GHSV = 60,000 h<sup>-1</sup>) of catalysts ( $\mu$ mol·g<sup>-1</sup>)

|       |       |       | $A-2$ |  |
|-------|-------|-------|-------|--|
| 36.4  | 39.6  | 32.3  | 36.1  |  |
| 88.2  | 98.5  | 75.4  | 88.0  |  |
| 226.7 | 243.3 | 164.4 | 188.2 |  |
|       | $F-1$ | $F-2$ | $A-2$ |  |

enhancing NO oxidation activity to produce  $NO<sub>2</sub>$  which is known to be more effective than NO to be adsorbed on LNT catalysts [\[22](#page-5-0)]. F-2 sample displays higher NSC compared to F-1 sample at 150, 200 and 250  $^{\circ}$ C. NSCs of aged samples are lower than those of the fresh samples. A-2 sample still has higher NSC than A-1 sample. The NSC results indicate that  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  complex oxide as the support loaded with Ba and Pt can trap  $NO<sub>x</sub>$  amount to more extent in comparison with  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$ .

# 3.3  $NO<sub>x</sub>$  conversion efficiency

 $NO<sub>x</sub>$  concentration profiles during the last 5 lean/rich cycles are shown in Fig. [2.](#page-3-0) Average  $NO<sub>x</sub>$  conversions during the last 5 cycles are presented in Table [5.](#page-3-0) For F-1 sample,  $NO<sub>x</sub>$  breakthrough is immediately observed after the feed gas switched into lean condition at 150  $\degree$ C, and the outlet  $NO<sub>x</sub>$  concentration decreases with time and gradually approaches the inlet  $NO<sub>x</sub>$  concentration. When the feed gas is subsequently switched to the rich condition, a sharp and intense  $NO<sub>x</sub>$  release peak appears and then intensity



Fig. 1 XRD patterns of fresh and aged catalysts: a F-1 and F-2 catalysts and b A-1 and A-2 catalysts

<span id="page-3-0"></span>

Fig. 2 NO<sub>x</sub> concentration profiles during last 5 lean/rich cycles: a F-1 catalyst, b F-2 catalyst, c A-1 catalyst, and d A-2 catalyst

| Temperature/°C | Catalyst | $NO_r$<br>conversion/ $%$ | Selectivity/%    |        |       |
|----------------|----------|---------------------------|------------------|--------|-------|
|                |          |                           | NH <sub>3</sub>  | $N_2O$ | $N_2$ |
| 150            | F-1      | 13.8                      | 8.6              | 51.1   | 40.3  |
|                | $F-2$    | 14.6                      | 7.4              | 51.5   | 41.1  |
|                | $A-1$    | 6.6                       | $\boldsymbol{0}$ | 66.9   | 33.1  |
|                | $A-2$    | 9.0                       | 4.9              | 55.6   | 39.5  |
| 200            | F-1      | 72.0                      | 38.5             | 34.7   | 26.8  |
|                | $F-2$    | 73.4                      | 29.6             | 33.8   | 36.6  |
|                | $A-1$    | 49.0                      | 46.4             | 38.3   | 15.3  |
|                | $A-2$    | 58.9                      | 36.4             | 38.2   | 25.4  |
| 250            | F-1      | 75.2                      | 22.6             | 23.8   | 53.6  |
|                | $F-2$    | 76.1                      | 18.9             | 20.7   | 60.4  |
|                | A-1      | 68.4                      | 42.3             | 28.6   | 29.1  |
|                | $A-2$    | 71.7                      | 31.4             | 25.5   | 43.1  |

**Table 5**  $NO<sub>x</sub>$  conversion and selectivity of N-containing products during last 5 lean/rich cycles

quickly decreases. The similar profile was also observed in a previous study [[23\]](#page-5-0). The average  $NO<sub>x</sub>$  conversion at 150 °C is 13.8%. At 200 °C, the outlet NO<sub>x</sub> concentration reaches only about  $90 \times 10^{-6}$  at the end of the lean duration. The amount of  $NO<sub>x</sub>$  release during switching to

rich condition becomes significantly lower compared to that at 150 °C. Therefore, the average  $NO<sub>x</sub>$  conversion increases to 72.0%. At 250  $\degree$ C, NO<sub>x</sub> concentration profile during lean duration is almost coincided with that at 200 °C. However, there is no  $NO_x$  release detected during switching to rich condition. Average  $NO<sub>x</sub>$  conversion reaches 75.2%. Raising reaction temperature increases  $NO<sub>x</sub>$ storage capacity, and on the other hand, high temperature is beneficial to promoting  $NO<sub>x</sub>$  reduction ability. As a result, the average  $NO<sub>x</sub>$  conversion increases with reaction temperature increasing from 150 to 250 °C.

In the case of F-2 sample,  $NO<sub>x</sub>$  evolutions at three temperatures are similar to those of F-1 sample, but F-2 sample has slightly higher average  $NO<sub>x</sub>$  conversions, 14.6% at 150 °C, 73.4% at 200 °C, and 76.1% at 250 °C, in accordance with the results of NSC measurements.

After thermal aging, the amount of  $NO<sub>x</sub>$  trapped on the aged catalyst at lean phase at 150  $\degree$ C becomes smaller in comparison with fresh catalysts and the outlet  $NO<sub>x</sub>$  concentrations gradually reach a constant level (around  $240 \times 10^{-6}$ ) for both aged catalysts. Higher NO<sub>x</sub> slip is observed during rich phase, and average  $NO<sub>x</sub>$  conversions of A-1 and A-2 samples are only 6.6% and 9.0%, respectively. At 200 °C,  $NO<sub>x</sub>$ -spill-out over A-1 is relatively larger in comparison with that over A-2 during switching to Rich

800

700

600

a



Fig. 3 Evolution of NH<sub>3</sub> and N<sub>2</sub>O concentrations during lean/rich cycles at 200 °C: a fresh samples and **b** aged samples

the rich condition, leading to a lower  $NO<sub>x</sub>$  conversion for A-1 (49.0% vs. 58.9% for A-2). NO<sub>x</sub> release still appears over aged samples at 250 °C, resulting in that  $NO<sub>x</sub>$  conversion decreases to some extent. Average  $NO<sub>x</sub>$  conversion sharply declines at 150 and 200  $^{\circ}$ C. Pt is known to have impacts on NO oxidation under lean conditions,  $NO<sub>x</sub>$ storage under rich/lean conditions and  $NO<sub>x</sub>$  reduction under rich conditions [[7\]](#page-5-0). The difference in  $NO<sub>x</sub>$  conversion may be correlated with different Pt dispersions of catalysts. Clayton et al. [[24\]](#page-5-0) also found that the differences in storage and reduction activity were the largest among three catalysts which have different Pt dispersions at low temperatures  $(< 200$  °C).

From the perspective of study on the law and production of NH<sub>3</sub> and N<sub>2</sub>O, their concentrations evolution at 200  $^{\circ}$ C during lean/rich cycles is taken as an example and shown in Fig. 3. For fresh and aged samples,  $NH_3$  and  $N_2O$  are both formed in lean and rich phases. During lean phase, NH<sub>3</sub> and  $N_2O$  are subsequently formed,  $NH_3$  intensity sharply decreases to below  $10 \times 10^{-6}$  at the initial lean phase, while a small  $N_2O$  peak appears, and then the  $N_2O$  intensity gradually becomes stabilized. A sharp  $N_2O$  peak is immediately observed at the beginning of rich phase, and  $NH<sub>3</sub>$  peak delays about 2 s. In comparison with the results obtained over fresh samples, the amount of  $NH_3$  and  $N_2O$ formation decreases over aged samples. In the lean and rich phase, NH<sub>3</sub> is mainly formed via the reduction in NO<sub>x</sub> by surface hydrogen, although  $NH<sub>3</sub>$  is also a product of isocyanate hydrolysis reaction [[25,](#page-5-0) [26](#page-5-0)], Dasari et al. [[25\]](#page-5-0) summarized the following reaction mechanism:

$$
Pt - H + Pt - NO \rightarrow Pt - HNO + Pt* \tag{1}
$$

 $Pt - HNO + Pt^* \rightarrow Pt - NH + Pt - O$  (2)

 $Pt - HNO + Pt \rightarrow Pt - N + Pt - OH$  (3)

$$
Pt - NH + Pt - H \rightarrow Pt - NH_2 + Pt* \tag{4}
$$

$$
Pt - NH_2 + Pt - H \rightarrow Pt - NH_3 + Pt*
$$
 (5)

$$
Pt - NH_3 \to NH_3 + Pt*
$$
\n<sup>(6)</sup>

 $N<sub>2</sub>O$  formation in lean phase is related to the reactions between surface-deposited reductants/intermediates (CO, HC, NH<sub>3</sub>, isocyanate) and gaseous  $NO/O<sub>2</sub>$ , and  $N<sub>2</sub>O$ release peak during rich phase may be attributed to that  $NO<sub>x</sub>$  partially reduced over platinum group metal (PGM) sites [[26–28\]](#page-5-0).

Concerning the product selectivity,  $N_2O$  is the main product at 150 °C. At 200 °C, selectivity of NH<sub>3</sub>, N<sub>2</sub>O and  $N_2$  is similar for fresh samples, but  $NH_3$  and  $N_2O$  become the main products for aged samples. By increasing the temperature to 250 °C,  $N_2$  selectivity of all samples shows a substantial enhancement. Moreover,  $N_2O$  selectivity decreases as the temperature increases from 150 to 250 °C.  $N_2$  selectivity decreases in the following order:  $F-2 > F 1 > A-2 > A-1$ . Thermal aging results are in an increase in NH<sub>3</sub> and N<sub>2</sub>O selectivity, except NH<sub>3</sub> selectivity at 150 °C. Compared to fresh samples, the higher  $NH<sub>3</sub>$  selectivity over aged LNT catalysts above 200  $\degree$ C was also found by Chatterjee et al. [\[29\]](#page-5-0) and Easterling et al. [[30\]](#page-5-0). Chatterjee et al. [[29\]](#page-5-0) suggested that the lower noble metal and oxygen storage activities correspond to the shifted light-off of the ammonia oxidation reactions to higher temperatures, which supports the faster  $NH<sub>3</sub>$  breakthrough.

### 4 Conclusion

The influence of the form of ceria on low-temperature  $NO<sub>x</sub>$ storage and reduction performance of LNT catalysts was investigated, using  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>33</sub>$  complex oxide or  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  mixed oxide as the support for BaO and Pt.  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  support exhibits the improvements on NO<sub>x</sub> storage capacity,  $NO_x$  conversion efficiency (especially for aged samples at 200  $^{\circ}$ C) and N<sub>2</sub> selectivity in comparison

<span id="page-5-0"></span>with  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$  support in the temperature range of 150–250 °C. After aging for 20 h at 800 °C, Pt/BaO/  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$  catalyst exhibits better thermal stability and chemical distribution than Pt/BaO/CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub> catalyst. Overall,  $CeO<sub>2</sub> - Al<sub>2</sub>O<sub>3</sub>$ -based catalysts show superior NO<sub>x</sub> storage and regeneration performance over  $CeO<sub>2</sub> + Al<sub>2</sub>O<sub>3</sub>$ based catalyst at low temperatures.

Concerning  $NH_3$  and  $N_2O$  selectivity of  $NO_x$  reduction,  $N_2O$  is the main product at 150 °C, and its selectivity decreases as the temperature increases from 150 to 250  $^{\circ}$ C. Thermal aging results are in an increase in the  $NH<sub>3</sub>$  and N<sub>2</sub>O selectivity at 200 and 250  $^{\circ}$ C.

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# References

- [1] Wang J, Ji YY, He ZW, Crocker M, Dearth M, McCabe RW. A non-NH<sub>3</sub> pathway for  $NO<sub>x</sub>$  conversion in coupled LNT-SCR systems. Appl Catal B Environ. 2012;111–112:562.
- [2] Liu Y, Harold MP, Luss D. Coupled  $NO<sub>x</sub>$  storage and reduction and selective catalytic reduction using dual-layer monolithic catalysts. Appl Catal B Environ. 2012;121–122:239.
- [3] Wang J, Ji YY, Jacobs G, Jones S, Kim DJ, Crocker M. Effect of aging on  $NO<sub>x</sub>$  reduction in coupled LNT–SCR systems. Appl Catal B Environ. 2014;148–149:51.
- [4] Johnson T, Joshi A. Review of vehicle engine efficiency and emissions. SAE Technical Paper 2017-01-0907. 2017, [https://](https://doi.org/10.4271/2017-01-0907) [doi.org/10.4271/2017-01-0907.](https://doi.org/10.4271/2017-01-0907)
- [5] Zheng Y, Liu Y, Harold MP, Luss D. LNT–SCR dual-layer catalysts optimized for lean  $NO_x$  reduction by  $H_2$  and CO. Appl Catal B Environ. 2014;148–149:311.
- [6] Neely GD, Sarlashkar JV, Mehta D. Diesel cold-start emission control research for 2015-2025 LEV III emissions. SAE Int J Engines. 2013;6(2):1009–20.
- [7] Roy S, Baiker A.  $NO<sub>x</sub>$  storage–reduction catalysis: from mechanism and materials properties to storage–reduction performance. Chem Rev. 2009;109(9):4054.
- [8] Epling WS, Campbell LE, Yezerets A, Currier NW, Parks JE. Overview of the fundamental reactions and degradation mechanisms of  $NO<sub>x</sub>$  storage/reduction catalysts. Catal Rev. 2004; 46(2):163.
- [9] Lindholm A, Currier NW, Dawody J, Hidayat A, Li JH, Yezerets A, Olsson L. The influence of the preparation procedure on the storage and regeneration behavior of Pt and Ba based  $NO<sub>x</sub>$ storage and reduction catalysts. Appl Catal B Environ. 2009; 88(1):240.
- [10] Mráček D, Kočí P, Marek M, Choi J-S, Pihl JA, Partridge WP. Dynamics of  $N_2$  and  $N_2O$  peaks during and after the regeneration of lean  $NO<sub>x</sub>$  trap. Appl Catal B Environ. 2015;166–167:509.
- [11] Masdrag L, Courtois X, Can F, Duprez D. Effect of reducing agent (C<sub>3</sub>H<sub>6</sub>, CO, H<sub>2</sub>) on the NO<sub>x</sub> conversion and selectivity during representative lean/rich cycles over monometallic platinum-based NSR catalysts. Influence of the support formulation. Appl Catal B Environ. 2014;146:12.
- [12] Ocampo F, Ohtake N, Southward BW. Recent developments for CeBa hybrid materials with enhanced properties for BS-6  $NO<sub>x</sub>$ storage applications. SAE Technical Paper 2017-26-123. 2017, <https://doi.org/10.4271/2017-26-0123>.
- [13] Ji Y, Toops TJ, Crocker M. Effect of ceria on the storage and regeneration behavior of a model lean  $NO<sub>x</sub>$  trap catalyst. Catal Lett. 2007;119(3):257.
- [14] Ocampo F, Harle V, Ohtake N, Rohe R, Southward BW. Innovative hybrid rare earth and barium materials with enhanced properties for  $NO<sub>x</sub>$  storage applications. SAE Int J Engines. 2015;8(3):1136.
- [15] He L, Sun DF, Wang TY, Xu YH, Li RX. Synthesis of nano-- $CeO<sub>2</sub>$  hollow spheres with high adsorption activity via template-free solvothermal method. Chin J Rare Met. 2016;40(5): 429.
- [16] Jin H, Wang YY, Wang YT, Yang HB. Synthesis and properties of electrodeposited  $Ni–CeO<sub>2</sub>$  nano-composite coatings. Rare Met. 2018;37(2):148.
- [17] Yang Q, Hu H, Wang SS. Preparation and desulfurization activity of nano-CeO<sub>2</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalysts. Rare Met. 2018;37(7): 554.
- [18] DiGiulio CD, Pihl JA, Choi J-S, Parks JE, Lance MJ, Toops TJ, Amiridis MD. NH<sub>3</sub> formation over a lean NO<sub>x</sub> trap (LNT) system: effects of lean/rich cycle timing and temperature. Appl Catal B Environ. 2014;147:698.
- [19] Auvray X, Pingel T, Olsson E, Olsson L. The effect gas composition during thermal aging on the dispersion and NO oxidation activity over  $Pt/Al_2O_3$  catalysts. Appl Catal B Environ. 2013;129:517.
- [20] Yang M, Li YP, Wang J, Shen MQ. Effects of  $CO<sub>2</sub>$  and steam on Ba/Ce-based  $NO<sub>x</sub>$  storage reduction catalysts during lean aging. J Catal. 2010;271(2):228.
- [21] Le Phuc N, Courtois X, Can F, Royer S, Marecot P, Duprez D.  $NO<sub>x</sub>$  removal efficiency and ammonia selectivity during the  $NO<sub>x</sub>$ storage-reduction process over Pt/BaO(Fe, Mn, Ce)/Al<sub>2</sub>O<sub>3</sub> model catalysts. Part I: influence of Fe and Mn addition. Appl Catal B Environ. 2011;102(3):353.
- [22] AL-Harbi M, Epling WS. Investigating the effect of NO versus  $NO<sub>2</sub>$  on the performance of a model  $NO<sub>x</sub>$  storage/reduction catalyst. Catal Lett. 2009;130(1):121.
- [23] Wang XY, Yu YB, He H. Effects of temperature and reductant type on the process of  $NO_x$  storage reduction over  $Pt/Ba/CeO<sub>2</sub>$ catalysts. Appl Catal B Environ. 2011;104(1–2):151.
- [24] Clayton RD, Harold MP, Balakotaiah V, Wan CZ. Pt dispersion effects during  $NO_x$  storage and reduction on Pt/BaO/Al<sub>2</sub>O<sub>3</sub> catalysts. Appl Catal B Environ. 2009;90(3):662.
- [25] Dasari PR, Muncrief R, Harold M. Elucidating  $NH<sub>3</sub>$  formation during  $NO<sub>x</sub>$  reduction by CO on Pt–BaO/Al<sub>2</sub>O<sub>3</sub> in excess water. Catal Today. 2012;184(1):43.
- [26] Wang J, Wang XT, Zhu JX, Wang JQ, Shen MQ. Elucidating  $N_2O$  formation during the cyclic  $NO_x$  storage and reduction process using CO as a reductant. Environ Sci Technol. 2015; 49(13):7965.
- [27] Zhu JX, Wang J, Wang JQ, Lv LF, Wang XT, Shen MQ. New Insights into the N<sub>2</sub>O formation mechanism over Pt-BaO/Al<sub>2</sub>O<sub>3</sub> model catalysts using  $H_2$  as a reductant. Environ Sci Technol. 2015;49(1):504.
- [28] Bártová Š, Kočí P, Mráček D, Marek M, Pihl JA, Choi J-S, Toops TJ, Partridge WP. New insights on  $N_2O$  formation pathways during lean/rich cycling of a commercial lean  $NO<sub>x</sub>$ trap catalyst. Catal Today. 2014;231:145.
- [29] Chatterjee D, Kočí P, Schmeißer V, Marek M, Weibel M, Krutzsch B. Modelling of a combined  $NO<sub>x</sub>$  storage and NH3-SCR catalytic system for diesel exhaust gas aftertreatment. Catal Today. 2010;151(3):395.
- [30] Easterling V, Ji YY, Crocker M, Dearth M, McCabe RW. Application of spaciMS to the study of ammonia formation in lean  $NO_x$  trap catalysts. Appl Catal B Environ. 2012;123-124: 339.