



# Processing and oxidation behavior of Pt-diffused coatings

Liang-Liang Wei, Hui Peng, Lei Zheng, Jing-Yong Sun, Hong-Bo Guo\*

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**Abstract** Pt-diffused coatings were synthesized on Ni10Al alloy by electroplating a thin layer of Pt (1–5  $\mu\text{m}$ ) followed by a diffusion treatment in vacuum at 1000–1100  $^{\circ}\text{C}$ . Effects of processing parameters (Pt thickness and vacuum diffusion temperature) on the microstructures and chemical composition of Pt-diffused coatings were investigated. Also, the oxidation behavior of the coatings was studied at 1100  $^{\circ}\text{C}$ . Pt film reveals nano-sized grain size of 93–113 nm. Vacuum diffusion treatment leads to the grain growth. 1- $\mu\text{m}$  Pt film with 1000  $^{\circ}\text{C}/1$  h vacuum diffusion fabricates nano-sized Pt-diffused coating which exhibits the best oxidation resistance. And a single continuous  $\text{Al}_2\text{O}_3$  scale forms on the coating with low Al ( $\sim 9$  at%) and Pt ( $\sim 6$  at%) contents. Increasing initial Pt thickness would introduce more defects and cracks, leading to a duplex scale and decreasing the oxidation resistance of Pt-diffused coatings.

**Keywords** Platinum-modified  $\gamma + \gamma'$  coatings; Pt-diffused coatings; Electroplating; Oxidation; Nano-structure

## 1 Introduction

Platinum-modified aluminide (Pt–Al) coatings have been used to provide oxidation resistance for Ni-based superalloy components of gas turbine engines for decades [1–6]. The content of Al in Pt–Al coatings should be higher than 40 at% to form a protective  $\text{Al}_2\text{O}_3$  scale during high-temperature service. Unfortunately, high concentration of Al in coatings is not compatible with advanced Ni-base single-crystal (SC) superalloy which contains larger amount of refractory elements such as W, Ta, Re and Ru. Inward diffusion of Al from Pt–Al coatings to the underlying superalloy would lead to the formation of secondary reaction zone (SRZ) and needle-like topologically closed-pack phases (TCP), which are detrimental to the mechanical properties of the coated components [7–12].

Recently, a new type Pt–Al coating with low Al content, which is called Pt-diffused coatings (sometimes called Pt-modified  $\gamma + \gamma'$  coatings or low-cost bond coats), has attracted increasing attention [13–18]. Pt-diffused coatings are usually produced by electroplating 5–10- $\mu\text{m}$  Pt film on the superalloy, followed by a vacuum diffusion treatment. Without an aluminizing process, Al diffuses from the superalloy to the coatings by the uphill diffusion. It is believed that Pt-diffused coatings have several advantages over traditional Pt–Al coatings, including better compatibility with the Ni-based SC substrate (no TCP and SRZ precipitation during service), higher creep resistance (more resistant to mechanical damage), superior durability in thermal barrier coatings (TBC) system and low process cost (without aluminizing process).

Jiang and Gleeson [17] have suggested that the good oxidation resistance of Pt-diffused coatings results from high Pt contents, which can cause the Al uphill diffusion

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L.-L. Wei, H. Peng, L. Zheng, H.-B. Guo\*  
School of Materials Science and Engineering, Beihang University, Beijing 100191, China  
e-mail: guo.hongbo@buaa.edu.cn

H. Peng, H.-B. Guo  
Key Laboratory of Aerospace Materials and Performance (Ministry of Education), Beihang University, Beijing 100191, China

J.-Y. Sun  
School of Energy and Power Engineering, Beihang University, Beijing 100191, China

from substrate. So most of the researchers have chosen high Pt thickness (more than 5  $\mu\text{m}$ ) and high vacuum diffusion temperature (1100–1190  $^{\circ}\text{C}$ ) to maintain high Al and Pt concentration in coatings [19–21]. Similar to Pt–Al coatings, the oxidation performance of Pt-diffused coatings is also greatly affected by the substrate elements. For example, Hf is a beneficial element [22, 23], whereas S, Co and Ti are harmful elements for the oxidation resistance of the coating [24–28]. Outward diffusion of these harmful elements to the coating surface will cause degradation of oxidation resistance. However, high-temperature vacuum diffusion will accelerate the outward diffusion of these harmful elements; it is necessary to develop a low-temperature diffusion technique to produce Pt-diffused coatings which could minimize or diminish this negative effect.

Niu et al. [29] produced a 1.5- $\mu\text{m}$  Pt film on a sputtered  $\text{Ni}_3\text{Al}$  coating, and an external  $\text{Al}_2\text{O}_3$  scale was formed on the coating at 1050  $^{\circ}\text{C}$  in air. Here, 1.5- $\mu\text{m}$  Pt is working to form an external  $\text{Al}_2\text{O}_3$  scale without heat treatment. In the present work, Pt-diffused coatings were produced by thin Pt film (1–5  $\mu\text{m}$ ) and relatively low vacuum diffusion temperature (1000–1100  $^{\circ}\text{C}$ ). The effects of processing parameters on high-temperature oxidation resistance of the coatings were investigated. In order to avoid the influence of substrate elements, Ni10Al alloy with 10 at% Al was used as the substrate materials.

## 2 Experimental

High-purity nickel and aluminum (purity higher than 99.99 at%) were used. The Ni10Al button was produced by arc melting, casted in argon atmosphere and then annealed in vacuum at 1150  $^{\circ}\text{C}$  for 24 h to ensure homogenization of the microstructure of the alloy. The chemical composition of annealed Ni10Al alloy is listed in Table 1. The concentration of sulfur impurity was also determined by inductively coupled plasma (ICP-AES, PHI700, Ulvacphi). Specimens were cut from the center of the button-shaped alloy into 10 mm  $\times$  8 mm  $\times$  3 mm, ground to 800-grit SiC finish and ultrasonically cleaned in alcohol and acetone prior to Pt plating.

Pt-diffused coatings were produced onto Ni10Al samples by electroplating Pt films with different thicknesses of 1, 3 and 5  $\mu\text{m}$ , followed by 1-h vacuum heat treatment

**Table 1** Chemical composition of as-annealed Ni10Al alloy by ICP-AES

Elements	$x_{\text{Al}}/\text{at}\%$	$x_{\text{Ni}}/\text{at}\%$	$S/10^{-6}$
Concentration	10.02	Bal.	< 20

( $\sim 1.1 \times 10^{-4}$  Pa) at 1000 or 1100  $^{\circ}\text{C}$ . Cyclic oxidation tests of the coated samples were carried out in an air furnace equipped with an automation system which allows the specimens moving in and out of the furnace automatically. Each specimen was hung in a pre-annealed alumina crucible by Pt wire to collect all oxide spalls. A cycle includes 25-h heating in air furnace at 1100  $^{\circ}\text{C}$  and subsequent 10-min cooling out of the furnace to ambient temperature by compressed air. Mass changes were measured using an electronic balance (Sartorius CPA 225D, Germany) with a precision of  $1 \times 10^{-4}$  g. The mass changes for each coating were determined based on average weight changes of two specimens.

The surface and cross-sectional morphologies of the specimens were characterized by field emission scanning electron microscope (FE-SEM, Quanta 200F). The phases of Pt films and oxides were identified by X-ray diffractometer (XRD, Rigaku D/max2200 PC) using Cu  $K\alpha$  radiation. The chemical compositions of the coatings and oxides were determined by electron probe micro-analyzer (EPMA, JXA-8100). For cross-sectional observation, the specimens after 300-h oxidation were embedded in epoxy, ground and finely polished.

## 3 Results and discussion

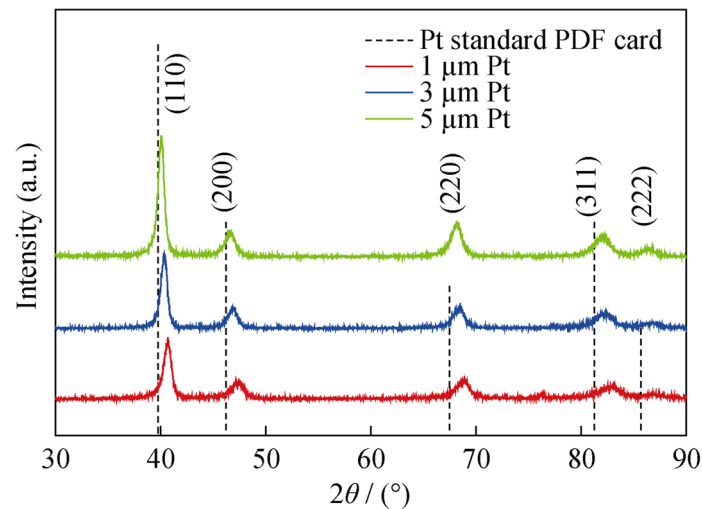
### 3.1 Pt films by electroplating

After platinum electroplating, Pt films were characterized by XRD. The lattice constant of Ni crystal is 0.3524 nm (PDF 65-2865), while that of Pt is about 0.3923 nm (PDF 65-2868). At the beginning of plating, Pt atoms deposited as Ni lattice constant like epitaxial growth. When Pt thickness is up to 5  $\mu\text{m}$ , the coating lattice changes to Pt lattice constant, as shown in Fig. 1. Curve 3 has almost the same peak position as standard Pt PDF card, while Curves 1 and 2 shift to right position, due to the influence of the substrate Ni10Al alloy. It can be inferred that the driving force of the mismatch between Ni10Al and 5- $\mu\text{m}$  Pt film would introduce more defects than 1- and 3- $\mu\text{m}$  Pt film specimens.

The grain size of Pt films was calculated from XRD data by Jade 5.0 software, as listed in Table 2. In order to calibrate the peak FWHM of XRD equipment, a standard Si powder XRD pattern was selected as reference. Pt films are composed of nano-sized grains.

### 3.2 Effect of Pt thickness

Vacuum diffusion treatment of three specimens with different Pt thicknesses was conducted at 1000  $^{\circ}\text{C}$ . For comparison, the specimen with 5- $\mu\text{m}$  Pt film was also heat-



**Fig. 1** XRD patterns of standard platinum card and 1-, 3- and 5- $\mu\text{m}$  Pt films

**Table 2** Average grain sizes of Pt films before and after 1000 °C diffusion calculated from XRD

Pt thickness/ $\mu\text{m}$	Average grain size/nm	
	Before 1000 °C diffusion	After 1000 °C diffusion
1	93	267
3	110	341
5	113	405

treated in vacuum at 1100 °C. Hereinafter, the specimens with 1-, 3- and 5- $\mu\text{m}$  Pt film diffused at 1000 °C are named as No. 1, No. 2 and No. 3, respectively, while the specimen with 5- $\mu\text{m}$  Pt film diffused at 1100 °C is named as No. 4.

The coating surface elements concentrations were analyzed by EDS, as shown in Table 3. Al does not uphill diffuse from the substrate (10 at% Al) at 1000 °C. However, a little higher Al content is obtained when the diffusion temperature increases to 1100 °C. It has been shown by Gleeson et al. [30] that the concentration of Pt and Al affects the selective oxidation of Al in Ni–Pt–Al alloy at 1150 °C. In such low Al content (10 at%), a duplex-scale

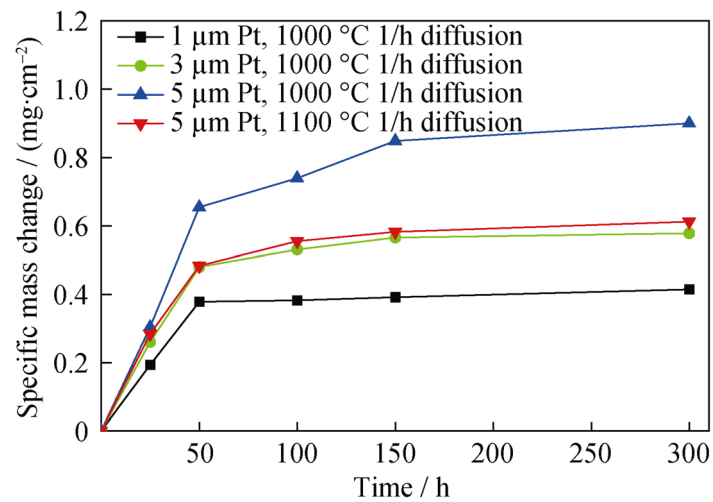
structure is formed on the alloy even the concentration of Pt is up to 25 at%. In this study, Al content is low (no more than 11 at%), Pt content is from 6 at% to 25 at%.

The oxidation of all specimens was performed in air at 1100 °C. The mass changes of Pt-diffused coatings on Ni10Al alloys are compared in Fig. 2. It should be noted that the coating with 1- $\mu\text{m}$  Pt film diffused at 1000 °C reveals the lowest mass change among all four coatings. Surface and cross-sectional morphologies of the specimens after 300-h oxidation at 1100 °C are shown in Figs. 3 and 4. The corresponding surface chemical composition is given in Table 4. According to XRD result in Fig. 5, external  $\text{Al}_2\text{O}_3$  scales are formed on No. 1, 2 and 4 specimens. Surface morphologies (Fig. 3a, b, d) are very similar with the oxide scale grown on  $\beta$ -NiAl coating, showing typical worm-like ridge structure.

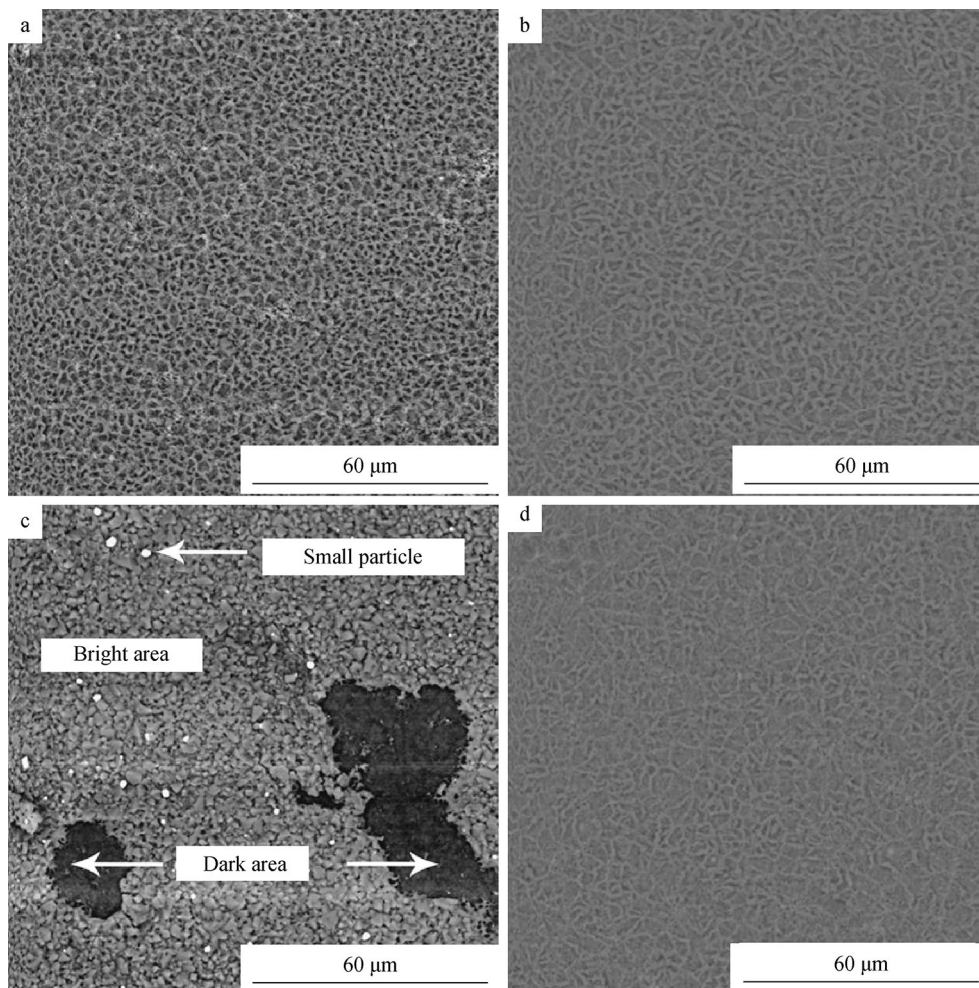
The spallation of the oxide scale can be seen in No. 3 specimen (Fig. 3c). Combining XRD (Fig. 5) and surface chemical composition results, it can be determined that the bright area is  $\text{NiAl}_2\text{O}_4$  with residual small Pt particles, while the dark area is  $\text{Al}_2\text{O}_3$ . As seen in Fig. 4c, the scale of No. 3 specimen consists of outer  $\text{NiAl}_2\text{O}_4$  spinel layer and inner  $\text{Al}_2\text{O}_3$  layer.

**Table 3** Processing parameters and surface element concentrations of Pt-diffused coatings

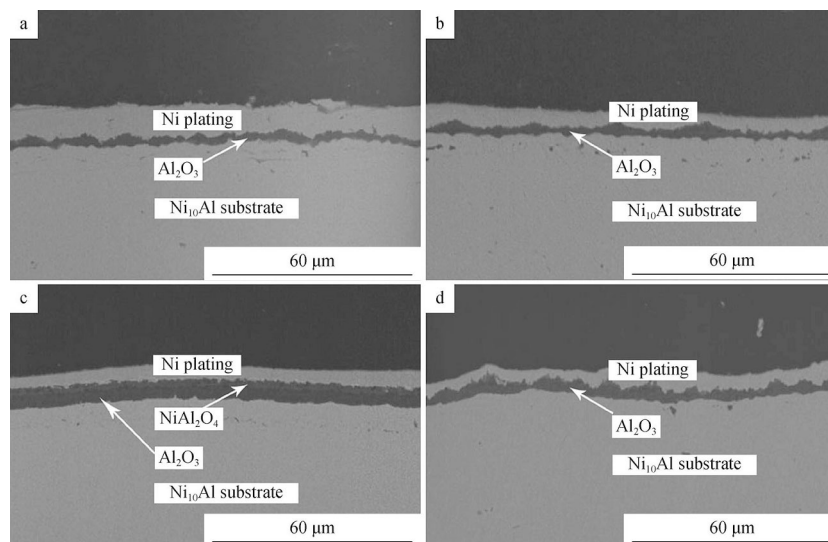
No.	Pt thickness/ $\mu\text{m}$	Temperature/°C	Time/h	Surface elements/at%		
				Pt	Al	Ni
1	1	1000	1	6.36	9.25	Bal.
2	3	1000	1	15.65	9.07	Bal.
3	5	1000	1	25.81	8.71	Bal.
4	5	1100	1	18.41	10.89	Bal.



**Fig. 2** Weight changes of Pt-diffused coatings on Ni10Al alloy at 1100 °C/300-h oxidation test in still air



**Fig. 3** Surface backscatter images of specimens after 1100 °C/300-h oxidation test **a** 1- $\mu$ m Pt with 1000 °C/1-h diffusion, **b** 3- $\mu$ m Pt with 1000 °C/1-h diffusion, **c** 5- $\mu$ m Pt with 1000 °C/1-h diffusion, **d** 5- $\mu$ m Pt with 1100 °C/1-h diffusion



**Fig. 4** Cross-sectional backscatter images of specimens after 1100 °C/300-h oxidation test **a** 1- $\mu\text{m}$  Pt with 1000 °C/1-h diffusion, **b** 3- $\mu\text{m}$  Pt with 1000 °C/1-h diffusion, **c** 5- $\mu\text{m}$  Pt with 1000 °C/1-h diffusion, **d** 5- $\mu\text{m}$  Pt with 1100 °C/1-h diffusion

**Table 4** Surface elements concentration of Pt-diffused coatings after 1100 °C/300-h oxidation (at%)

No.	Area	Al	Ni	Pt	O
1	Surface	71.98	10.73	–	Bal.
2	Surface	74.27	7.01	–	Bal.
3	Small particles	–	22.67	77.33	–
	Bright area	58.55	26.24	–	Bal.
	Dark area	71.47	5.39	–	Bal.
4	Surface	72.75	8.49	–	Bal.

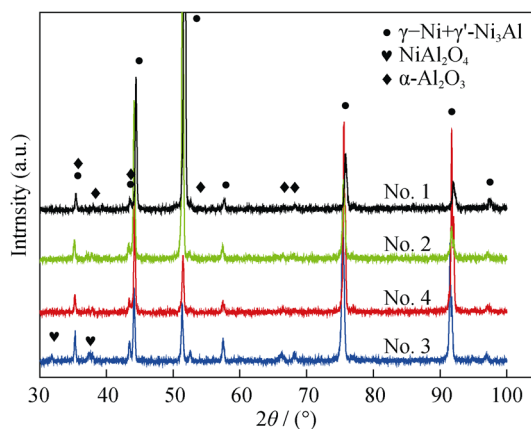
the defects introduced by electroplating. During low-temperature vacuum diffusion process (1000 °C), inward diffusion flux of Pt is higher than outward diffusion of Ni and Al from substrate, so these defects and cracks are generated near the surface, which could be the short path for oxygen and accelerate the oxidation. As shown in Fig. 6b–d, the surface morphologies of Pt-diffused coatings become coarser with Pt thickness increasing. The cross-sectional back-scattered morphologies of Pt-diffused coatings are shown in Fig. 7, which are typical dark  $\gamma$ -Ni and bright  $\gamma'$ -Ni<sub>3</sub>Al phase.

In summary, 1- $\mu\text{m}$  Pt film is sufficient to act as the third element for Al selective oxidation, and increasing Pt thickness does not show any advantage in oxidation resistance with low-temperature diffusion process.

### 3.3 Effect of diffusion temperature

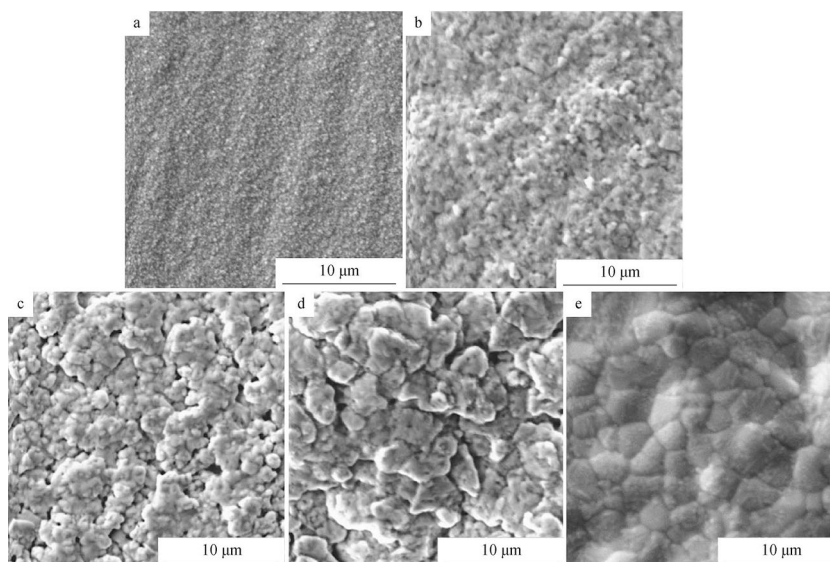
In order to examine the effect of diffusion temperature, No. 3 and 4 specimens with the same initial Pt thickness (5  $\mu\text{m}$ ) were comparatively studied at different diffusion temperatures. As shown in Fig. 2, No. 4 specimen diffused at 1100 °C shows better oxidation resistance than No. 3. In Fig. 6d and e, the surface of No. 4 specimen is smoother than that of No. 3, which has less cracks and defects due to the high diffusion temperature. In summary, thick Pt film needs high-temperature diffusion process, which could diminish the defects in Pt electroplating and make a smoother coating surface.

In the present work, 1- $\mu\text{m}$  Pt-diffused coating has the lowest Al and Pt content in all four coatings and it also has

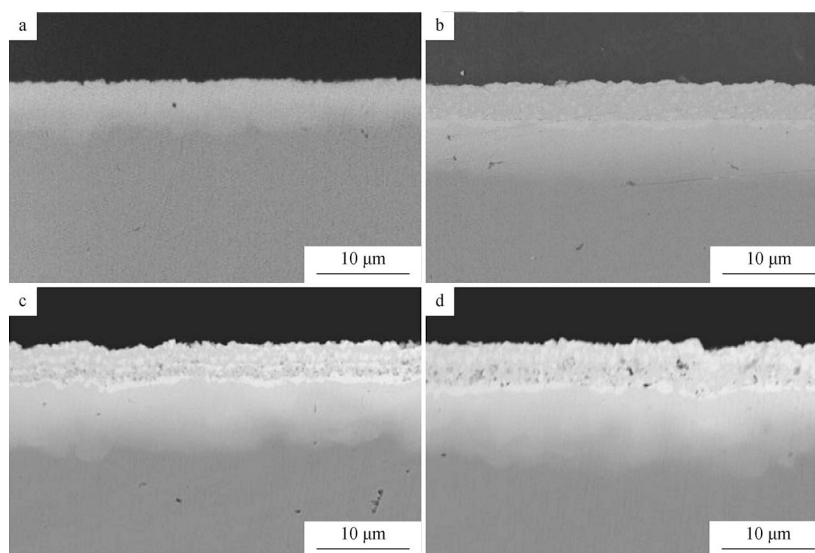


**Fig. 5** XRD patterns of specimens after 1100 °C/300-h oxidation test

In the present study, with the same vacuum diffusion process, increasing Pt thickness has a negative effect in high-temperature oxidation, which could be attributed to



**Fig. 6** Surface secondary electron images of specimens **a** 1- $\mu\text{m}$  Pt film, **b** 1- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **c** 3- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **d** 5- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **e** 5- $\mu\text{m}$  Pt with 1100  $^{\circ}\text{C}/1\text{-h}$  diffusion



**Fig. 7** Cross-sectional back scatter images **a** 1- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **b** 3- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **c** 5- $\mu\text{m}$  Pt with 1000  $^{\circ}\text{C}/1\text{-h}$  diffusion, **d** 5- $\mu\text{m}$  Pt with 1100  $^{\circ}\text{C}/1\text{-h}$  diffusion

the finest grain size. As shown in Fig. 6, high-temperature diffusion treatment leads to the growth of grain. The grain size of 1- $\mu\text{m}$  Pt-diffused coating on Ni10Al grows to  $\sim 267$  nm after 1-h diffusion treatment at 1000  $^{\circ}\text{C}$ , whereas 5- $\mu\text{m}$  Pt-diffused coating grows to 1–5  $\mu\text{m}$  after 1-h diffusion treatment at 1100  $^{\circ}\text{C}$ . Grain boundary is a short path for Al and oxygen diffusion. If the grain size is nano-sized, external  $\text{Al}_2\text{O}_3$  scale could form on NiCrAl alloy even at low Al content [31]. Consequently, 1- $\mu\text{m}$  Pt-diffused coating with nano-sized grain reveals the best oxidation resistance.

#### 4 Conclusion

Pt-diffused coatings were produced by electroplating 1–5- $\mu\text{m}$  Pt films on Ni10Al alloy and then followed by vacuum diffusion treatment at 1000–1100  $^{\circ}\text{C}$ . Pt film reveals nano-sized grain of 93–113 nm, which diffused at 1000  $^{\circ}\text{C}$  keeps nano-sized structure. 1- $\mu\text{m}$  Pt-diffused coating shows the best oxidation resistance even at such low Al (10 at%) and Pt (6 at%) content. Increasing initial Pt thickness would introduce more defects and cracks during vacuum diffusion

process, leading to a duplex scale and decreasing the coating oxidation resistance.

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