#### **ORIGINAL PAPER**



# **Characterization of polyethylene terephthalate (PET) materials under high‑energy electron exposure**

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#### **Abstract**

External spacecraft materials play an important role in satellite protection from the harsh space environment.Research has shown that the physical, chemical, and optical properties of matter change continuously as a result of exposure to solar radiation and aggressive chemical species produced in Earth's upper atmosphere. Thorough knowledge of the material properties evolution throughout a planned mission lifetime helps to improve the reliability of spacecraft. Moreover, the establishment of correlation factors between true space exposure and accelerated space weather experiments at ground facilities enables accurate prediction of on-orbit material performance based on laboratory-based testing. The presented work evaluates the radiation efects of diferent doses of high-energy electron exposure on surface morphology, optical, and charge transport properties of two materials from the PET family, Melinex<sup>®</sup>454 and Mylar<sup>®</sup>M021.

**Keywords** High-energy electron exposure · Geosynchronous Earth orbit (GEO) · Low Earth orbit (LEO) · Refectance spectroscopy · Surface morphology · Charge transport

# **1 Introduction**

Polyethylene terephthalate (PET) materials are proposed for many applications in a spacecraft industry, including construction of infatable structures for satellite deorbiting, [[1\]](#page-6-0) deployable membrane antenna structures [\[2](#page-6-1)], fabrication of fexible and stretchable electronics for harsh

work.

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radiation environment [[3,](#page-6-2) [4](#page-6-3)], and foldable organic solar cell arrays manufacturing  $[5, 6]$  $[5, 6]$  $[5, 6]$ . Most importantly, PET films are utilized in multilayer insulation (MLI) blankets that are employed on the exterior surfaces of spacecraft for passive thermal control purposes. Spacecraft operate in a harsh and demanding environment, which requires materials that can withstand extreme conditions such as temperature fuctuations, high levels of radiation, and vacuum. The ability to Jainisha R. Shah and Elena A. Plis have contributed equally to this maintain an acceptable temperature range during all phases

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of operation is an important task to ensure the success of the mission [\[7](#page-6-6), [8](#page-6-7)].

MLI composite materials work by limiting the amount of radiative heat transfer through multiple layers of thin refectors (shields) and spacer materials. The shields are generally PET or polyimide (PI) metal-coated flms with high mechanical strength and low thermal conductivity. An ideal thermal blanket completely refects the incident radiation. Although these perfect refectance characteristics have not been obtainable in practice yet [[9\]](#page-6-8) and research is being conducted on alternatives to traditional MLI blankets, such as those based on silica aerogels  $[10-13]$  $[10-13]$ , which offer improved refectivity and durability, PET-based shields are still an essential part of spacecraft thermal control system.

By nature of their usage, MLI blankets are exposed to harsh space weather environments comprising high vacuum, solar ultraviolet (UV) radiation, thermal cycling, and impacts from micrometeoroids and artifcial orbital debris. At low Earth orbit (LEO), single-oxygen atoms (atomic oxygen, AO) are the prevailing source of material degradation whereas at geosynchronous Earth orbit (GEO), highly energetic electrons are the dominant species interacting with the spacecraft surface [\[14](#page-6-11), [15\]](#page-6-12).

Space-weather events can cause damage to the MLI layers on spacecraft. This damage can weaken the adhesive that holds the layers of MLI together, leading to their delamination [\[16,](#page-6-13) [17\]](#page-6-14) thus contributing to the population of high-area-to mass (HAMR) space debris objects in orbit [\[18\]](#page-6-15). By comparing the reflectance spectra of the HAMR objects with the laboratory spectra of known spacecraft materials, researchers were able to identify the specifc refective material present in the MLI layers. This fnding supports the hypothesis that the HAMR debris was formed as a result of delamination of the MLI layers [[19–](#page-6-16)[22](#page-7-0)].

The effects of dominant GEO environment species, high energy electrons, on mechanical and charge accumulation properties of PI [\[23\]](#page-7-1) and PET [[24](#page-7-2)[–28\]](#page-7-3) flms causing the degradation and fragmentation of MLI have been studied. However, the number of studies devoted to the optical changes of PET under the infuence of space weather are limited [\[29\]](#page-7-4) even though understanding these optical changes is invaluable for identifying and tracking debris clouds and determining the origin of space debris [[30–](#page-7-5)[32](#page-7-6)]. This task is accomplished by comparing the refectance spectra of observed orbital bodies (such as HAMR objects) with a library of known (laboratory) refectance spectra of diferent materials. However, if PET layers are changing under the infuence of space weather, this must be taken into account when analyzing and interpreting refectance spectra. Any changes in the optical properties of PET could potentially lead to incorrect identifcation of debris materials. Moreover, the radiation-induced alteration of optical properties may serve as a proxy measurement for other, less tractable measurements such as electrical conductivity, embrittlement, surface morphology, and chemical reactivity.

In the presented work we studied changes of surface morphology, optical, and charge transport properties of two materials from the PET family, Melinex®454 and Mylar®M021, under high-energy (100 keV) electron irradiation. Evaluation of space weather effects on the change in material properties of MLI components is helpful for understanding of on-orbit characteristics of external spacecraft materials. Various techniques were employed to access the radiation-induced materials dynamics, such as atomic force microscopy (AFM), directional hemisperical reflectance (DHR), and surface potential decay (SPD) measurements. Additionally, we present the astronomical color index of chosen materials as a function of electron fluence.

The astronomical color index of a given material is a convenient metric that is experimentally tractable to remote observers in situations where measurement of a full reflection spectrum is not feasible [[33\]](#page-7-7). A body of literature is available on the utilization of the filter photometry approach for optical observation data analysis and interpretation. For example, Payne et al [\[34](#page-7-8)] emphasized the importance of color indices to distinguish the satellites with different configurations. Further, Cowardin et al [[35\]](#page-7-9) used the same approach to determine the man-made space body fragment brightness distribution. Beamer et al [[36](#page-7-10)] used the color-color technique for analyzing the wavelength band intensity of refected light from objects in space. Pearce et al [[37\]](#page-7-11) used the clustering of the color indices of Russian SL-12 rocket bodies for the identifcation of one unique object (SL-12 RB 2012-012D). Finally, attempts to classify spacecraft materials into families according to color index derived from their refectivity spectral curves were reported by Reyes et al [[31\]](#page-7-12). In our recent work [\[30](#page-7-5)] we compared all possible color indexes combinations of g' (406–544 nm), r' (558–682 nm), i' (705–835 nm), and the z' (838–1094 nm) passbands of Sloan Digital Sky Survey (SDSS) [[38\]](#page-7-13) astronomical flter set to illustrate the importance of the proper choice of flter combinations since the use of some flter combinations result in more dramatic radiation-induced changes to the color index of the material. Knowledge of the evolution of a material' color index may be harnessed to provide information about a material' chemical state and physical properties using remote observations [[35–](#page-7-9)[37,](#page-7-11) [39](#page-7-14)].

#### **2 Experimental Details**

#### **2.1 Materials**

This study was conducted using two PET materials, 5 mil (127  $\mu$ m) thick Melinex<sup>®</sup>454 film and 9 mil (229  $\mu$ m) thick Mylar®M021 flm from DuPont de Nemours, Inc. Visually, the pristine Melinex®454 sample appears as a high clarity flm with both sides pre-treated to promote adhesion to most Industrial coatings. Pristine Mylar®M021 is a low shrinkage, low moisture absorption, and high thermal durability flm with a white opaque appearance. The studied materials had no coatings applied.

#### **2.2 Irradiation Procedure**

Samples were irradiated with high energy (100keV) mono-energetic electron radiation from a Kimball Physics EG8105-UD food electron gun in the Spacecraft Charging and Instrument Calibration Laboratory (SCICL) at Kirtland Air Force Base in New Mexico, USA [\[40](#page-7-15)]. The energy of the electron beam was selected based on the continuous slowing down approximation (CSDA) ranges of highenergy electrons [\[41](#page-7-16)]. The details regarding the anticipated estimate of penetration depth of 100 keV electrons into each material is not investigated and surpass the scope of this manuscript. It is important to recognize that the space environment is characterized by a broad distribution of electron energies, which can cause energy deposition and charging of spacecraft surfaces.

Samples were mounted over a carousel that rotated through the hot spot of the electron beam to ensure uniform irradiation. Sample size was  $2.5 \text{ cm}^2$  and reflective metal surface of the same area was utilized as a backing substrate.Copper tape and aluminum foil were employed as backing materials for both irradiation experiments, respectively. Prior to electron bombardment, a dehydration bake-out of the loaded carousel was performed for 12 h at 60<sup>0</sup> C using a vacuum oven. More details of the electron irradiation procedure have been reported elsewhere [[42](#page-7-17)]. Irradiation was performed with two diferent electron beam fluences, 8.5 x  $10^{13}$  electrons/cm<sup>2</sup> and 9.2 x  $10^{14}$  electrons/  $\text{cm}^2$ , corresponding to 6 h and 24 h of irradiation time, respectively, which could be representative of a range of diferent space environments. During materials irradiation, background pressure was  $3 \times 10^{-7}$  Torr. The temperature of the sample holder was not measured.

#### **2.3 Characterization Methods**

#### **2.3.1 Optical properties**

The directional hemispherical refectance (DHR) of PET samples was measured *in situ* before and during the electron irradiation process in accordance with the optical data acquisition procedure reported elsewhere [[43\]](#page-7-18). In particular, the data collection procedure began by measuring white and black standards (Spectralon and Acktar Black, respectively) using a Spectralon integrating sphere mounted on a robotic arm. The Spectralon sphere was then moved to measure each of the samples mounted on the rotating platform. During the 10-minute measurement process, the electron beam was extinguished to avoid doing damage to the Spectralon standard.

In addition, the optical properties of pristine and radiation-damaged samples were assessed in the UV/ Vis (200–800 nm) spectral region using a Cary 2000 spectrophotometer with spectral resolution of 2 nm. Finally, color ratio plots were generated using astronomical Sloan Digital Sky Survey (SDSS) [\[38](#page-7-13)] flters to show changes in spectral brightness as a function of electron fluence [[31](#page-7-12)]. Color ratio plots were generated from the measured refectance curves calculating the ratio of brightness between two flter passbands (color index) using the equation [1](#page-2-0)

<span id="page-2-0"></span>
$$
A - B = -2.5 \left(\frac{I_A}{I_B}\right) \tag{1}
$$

where A and B represent the two filter passbands of interest, and  $I<sub>x</sub>$  is the brightness of the band  $x$  obtained by integrating the refectance curve over the wavelength range of a given band. Diferences between the brightness in the g' band (408–545 nm) and the z' band (865–960 nm) were determined.

#### **2.3.2 Surface characterization**

Surface morphology and roughness of studied materials were examined using Bruker Dimension ICON atomic force microscopy (AFM) allowing measurement of surface roughness up to 5  $\mu$ m on areas as large as 200  $\mu$ m x 200  $\mu$ m.

#### **2.3.3 Charge transport properties**

The volume resistivity of pristine and irradiated PET samples was evaluated using the surface potential discharge (SPD) measurements [[44\]](#page-7-19) performed in a vacuum environment with a low-energy (5 keV) Kimball Physics EGPS-2017B electron gun and a TREK probe model 370 high-speed electrostatic voltmeter. The back surface of the sample was attached to the grounded backplane via copper tape with conductive adhesive. To conduct the SPD experiment, the front surface of the irradiated material was bombarded by a beam of electrons during a short period of time, 1-2 s, immediately after which the non-contact voltmeter was positioned 1-2 mm from the surface and began to record the surface potential. After the front of the charge body had reached the grounded backplane, the dissipation of charge was primarily determined by the loss of electrons from the material. SPD measurements were performed in darkness to eliminate the possibility of optically excited states obscuring our analysis. Using the SPD method, the dark resistivity of the material may be derived from a plot of surface potential versus time, or decay curve, using equation [2:](#page-3-0)

$$
\rho = \frac{\tau}{\epsilon_0 \epsilon_r} \tag{2}
$$

where  $\tau$  is charge decay time in seconds determined from the linear ft of the post-transit region of the decay curve. It represents the time it takes electrons deposited from the beam to traverse the material and be lost to the grounded backing plate. The  $\epsilon_0$  and  $\epsilon_r$  are the permittivity of free space and relative permittivity of the material, respectively. The conductivity of the material is then calculated as inversely proportional to the resistivity of the material. Whereas the constant voltage method conforming to ASTM D-257 standard is commonly utilized by the material manufacturers to attest the charge transport properties, the SPD method is more applicable to test materials with irradiation-induced heterogeneity under space-simulated conditions [\[45](#page-7-20)].

#### **2.4 Sample handling**

Unlike radiation-induced material degradation measured by the *in situ* DHR measurements which were performed under high vacuum conditions ( $< 10^{-6}$  Torr), the post-irradiation measurements such as AFM or UV/Vis optical tests were performed at diferent facilities, necessitating considerable air exposure to the materials between their irradiation and characterization. Since air has been shown to obfuscate results for electron irradiated organic polymers (e.g., [[46\]](#page-7-21)), handling and characterization protocols of the irradiated air-sensitive materials must be scrutinized and carefully controlled. To reduce the healing rate of PET materials irradiated with high energy electrons upon exposure to atmosphere, the two-stage sample packaging procedure

comprising vacuum sealing performed with a Henkelman® industrial vacuum sealer was employed [\[47](#page-7-22)].

## <span id="page-3-0"></span>**3 Results**

Figure [1](#page-3-1) shows representative AFM scans for each studied sample under diferent electron irradiation dose. Table [1](#page-3-2) summarizes the measured surface roughness values of pristine and electron-irradiated samples. Average surface roughness  $(R_a)$  values were the average of several  $5\mu$ m x  $5\mu$ m scans taken at diferent parts of the respective samples.

Surface roughness of both PET materials decreased after LEO irradiation with  $8.5 \times 10^{13}$  electrons/cm<sup>2</sup> fluence which is attributed to the coalescence of some of the original defects. Higher irradiation fluence,  $9.2 \times 10^{14}$  electrons/cm<sup>2</sup>, caused the formation of multiple point defects, probably arcing sites, which contribute to the increased average roughness of the materials. The surface between the arcing sites is smoother compared to the pristine material and this is easier to observe for the Mylar®M021.

Absolute hemispherical refectance of Mylar®M021 and Melinex<sup>®</sup>454 samples measured at zero electron fluence of impinging 100 keV electrons (pristine material), and two

<span id="page-3-2"></span>**Table 1** Surface roughness of pristine and electron-irradiated polymer samples

Fluence $(e/cm^2)$	Mylar <sup>®</sup> M021, $R_a$ (nm)	Melinex <sup>®</sup> 454, $R_a$ (nm)
Pristine	7.8	8.2
$8.5 \times 10^{13}$	3.6	5.0
$9.2 \times 10^{14}$	4.2.	7.6



<span id="page-3-1"></span>**Fig. 1** Representative  $5 \mu m x$ 5μm AFM scans of (a) pristine and electron-irradiated with (b) 8.5 x  $10^{13}$  electrons/cm<sup>2</sup> and (c)  $9.2 \times 10^{14}$  electrons/cm<sup>2</sup> PET materials

<span id="page-4-0"></span>





<span id="page-4-1"></span>**Fig. 3** UV–Vis transmittance spectra of Mylar®M021 and Melinex®454 samples irradiated with diferent fuences of 100 keV electrons

diferent electron fuences is shown in Fig. [2](#page-4-0). The aluminum backing of the materials served as an optical mirror during the DHR measurements, making the "refection spectra" superpositions of refected and transmitted light.

The UV–Vis transmittance spectra of Mylar®M021 and Melinex®454 samples that were exposed to diferent fluences of 100 keV electrons are shown in Fig. [3](#page-4-1). Transmittance of both irradiated samples is decreased with an increase of irradiation dose, more for Melinex®454 than for the Mylar®M021.

The volume resistivity values of Mylar®M021 and Melinex®454 samples irradiated with diferent fuences of 100 keV electrons measured by SPD method are summarized in Table [2](#page-4-2).

The astronomical color index of a given material is a convenient metric that is experimentally tractable to remote observers in situations where measurement of a full

<span id="page-4-2"></span>**Table 2** Volume resistivity of Mylar®M021 and Melinex®454 samples

		$\rho$ ( $\Omega$ · cm)
Mylar <sup>®</sup> M021	Pristine	4.3 x $10^{18}$
	$8.5 \times 10^{13}$	$4.8 \times 10^{21}$
	$9.2 \times 10^{14}$	$3.8 \times 10^{19}$
Melinex <sup>®</sup> 454	Pristine	$9.6 \times 10^{18}$
	$8.5 \times 10^{13}$	$7.5 \times 10^{18}$
	$9.2 \times 10^{14}$	$1.6 \times 10^{19}$

reflection spectrum is not feasible [\[33](#page-7-7)]. Among twelve possible combinations of the g', r',i', and z' flters from the SDSS astronomical flter set, the g'-z' color index showed the greatest variation as a function of electron fuence and this flter combination was applied to the investigated flms [\[30](#page-7-5)].

## **4 Discussion**

Whereas the shape of the absolute hemispherical refectance spectrum of Mylar®M021 flm is more complicated than that of the Melinex®454, several common features are identifed, such as the absorption band at 830 nm which is attributed to the partial light absorption in the aluminum of the backing plate. Intensity of the 1650 nm feature is not signifcantly afected by electron irradiation, indicating that whatever chemical moiety is responsible for it is not infuenced by the impinging high energy electrons.

A notable decrease of absolute reflectance of both materials in a short wavelength range, 400–675 nm for Mylar®M021 and 400–830 nm for Melinex®454, was observed with increased exposure duration to the high energy electrons. Further increase in electron irradiation dose caused the 20% decrease in refectance values in 830–1800 nm range of Melinex®454 flm. Oppositely, the Mylar®M021 flm showed a nearly constant value of

absolute hemispherical refectance in 1000–1800 nm region, with a maximum of 10% refectance increase in 830–1000 nm range. The latter may be due to the radiation-promoted smoothness due to the radiation-induced crosslinking of the Mylar®M021 compared to the pristine material, since the reduced roughness causes a decrease of the spreading of refected light and, consequently, promotes more specular light. Although there is a lack of available data on the relationship between the refected light and the radiationchanged topography of PET materials, researchers have investigated the impact of surface roughness on refected light intensity in other materials such as pigmented plastics and paper [\[48](#page-7-23), [49](#page-7-24)].

The decreased transmittance of the electron-irradiated PETs suggests that exposure to high-energy electrons leads to a decrease in the optical transparency of these flms. This decrease in transmittance can be attributed to the formation of defects and color centers in the flms due to the ionization and excitation of the polymer chains by the high-energy electrons.

The radiation stability of PET has been observed by other researchers [[50\]](#page-7-25) and was attributed to the modifcation of aromatic rings from di-substituted to mono-substituted benzene groups [\[22](#page-7-0)]. The condensation of aromatic rings into compact carbonaceous clusters may also result in increased absorption of PET materials in a short wavelength range. Indeed, the increased absorption of the irradiated PET flms, beyond 500 nm for Mylar®M021 and in 300–600 nm range for Melinex<sup>®</sup>454, is shown in Fig. [2](#page-4-0).

Interestingly, the volume resistivity of the electronirradiated PET samples either increased (Mylar®M021) or did not change significantly (Melinex®454). The similar phenomenon has been observed by Chaudhary et al [[51](#page-7-26)] and Oproiu et al [[52\]](#page-7-27) (decreased conductivity of PET after electron irradiation) and is attributed to the increased crosslinking of the PET chains due to the electron irradiation, which may obstruct the charge carrier hopping from one chain to another chain resulting in decrease of electrical conductivity. This result is surprising, considering that one successful method for increasing the conductivity of other organic polymers based on a polyimide backbone (such as Kapton®) is to introduce conductive carbon clusters into the polymer. Studies of the role of crosslinking in surface roughening of electron-irradiated PET flms are limited; however, the smoother surface of electron-irradiated PET samples may also be a manifestation of radiation-induced increased cross-linking and demonstrates an example of another aromatic thermoplastic, polystyrene [\[53](#page-8-0)]. One very promising technique to study the fundamental causes of these changes is in-situ vibrational spectroscopy, a technique that is currently in development in the SCICL lab in collaboration with the University of New Mexico.

The g'-z' color index plot was utilized for the characterization of spectral brightness with increased electron fuence of both studied PET materials. As shown in Fig. [4](#page-5-0), both materials demonstrated a monotonic increase of g'-z' versus electron fuence characteristics, resulted in a change of the g'-z' index by factor of 6.3 from the initial (pristine) to the irradiated with maximum electron fuence values for both samples, in particular, from of 0.08 to 0.50 for Mylar®M021 and from 0.15 to 0.95 for Melinex®454. By understanding these optical changes i.e. the spectral regions over which the materials are stable and those where it varies with electron exposure, remote observers can get information about the material's state. This knowledge about the history of the material would be invaluable for identifying and tracking debris clouds and determining the origin of the space debris

# **5 Conclusion**

By understanding the behavior of satellite components throughout their mission lifetime, Earth-based observers may glean more detailed information from unresolved imagery to help prevent space-based catastrophes and to better understand the on-orbit life cycle of commonly used spacecraft materials. This knowledge of on-orbit material degradation will inform spacecraft designers and enable the construction of more robust spacecraft designs as well as improve the abilities of spacecraft operators to conduct accurate and timely anomaly resolution.

In this paper, we investigate a dependence between changes in optical behavior and other material properties of two PET polymers irradiated with high-energy electrons.



<span id="page-5-0"></span>**Fig. 4** g'-z' color index of pristine and irradiated with diferent fuences of 100 keV electrons Mylar®M021 and Melinex®454 samples

The alteration of volume conductivity observed in both types of PET materials following electron irradiation, which could be indicative of diverse space environments, implies that diferential spacecraft charging models, such as NASA/Air Force Spacecraft Charging Analyzer Program (NASCAP), should be revised to incorporate time- and environment-dependent material properties to accurately account for material aging. Further, as these polymers are among commonly used spacecraft surface materials, the accompanying optical changes may be of a magnitude that is discernible via resolved or unresolved remote imaging

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**Author Contributions** JRS and EAP conceptualized the idea of the study. JRS, SC, and MTB performed all the experiments reported in this manuscript excluding the surface morphology and FTIR measurements which were performed by EAP. Optical, charge transport, and surface morphology data were analysed by JRS, DPE, and EAP. Manuscript was written by JRS and EAP. RCH, DPE, and DCF reviewed, provided feedback, and approved the manuscript.

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**Data availability** Not applicable

**Code Availability** Not applicable

#### **Declarations**

**Disclaimer** The views expressed are those of the author and do not necessarily reflect the official policy or position of the Department of the Air Force, the Department of Defense, or the U.S. government.

**Conflict of interest** Authors declare no confict of interest/competing interests.

**Ethical approval** Not applicable

**Consent to participate** All authors consented to the participation in research described in this manuscript.

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