Finite-time Event-triggered Extended Dissipative Control for a Class of Switched Linear Systems

Hui Gao* (), Kaibo Shi, Hongbin Zhang, and Jianwei Xia

Abstract: This paper investigates the problem of event-triggered finite-time extended dissipative control for a class of switched linear systems. We propose a novel event-triggered method that allows frequent system switching over an event-triggered interval, which is different from the previous work that only one switching happened over the event-triggered interval. By average dwell time and a novel controller-mode-dependent Lyapunov function method, we give sufficient conditions for finite-time extended dissipative analysis of the closed-loop switched linear system. LMIs are used for the design of the controller. Finally, numerical examples are given to illustrate the effectiveness of the proposed method.

Keywords: Event-trigger, extended dissipative control, finite-time, frequent asynchronism.

1. INTRODUCTION

Switched system belongs to a special class of hybrid systems, which can be modeled by a class of discrete or continuous-time subsystems and a logical rule that orchestrates the switching among the subsystems. It has attracted remarkable attention for its practical applications in traffic control, electrical systems and so on [1-5]. For example, switched model predictive control of switched linear systems: Feasibility, stability and robustness is investigated in [3], improved results on stability of continuous-time switched positive linear systems is researched in [4], respectively.

In many real world situations, especially in missile systems, chemical reaction process and robot control systems. The system behavior over a short time interval is very important, which required that the system state should not exceed a bounded domain over finite time. Compared with Lyapunov asymptotic stability, finite-time stability is more realistic and theoretical. Thus we are interested analysing finite-time stability of the switched systems and many results have been proposed for the related issues [6–9]. Specially, reliable finite-time filtering for impulsive switched linear systems with sensor failures is researched in [8], asynchronously switched control of a class of slowly switched linear systems is investigated in [9] and so on.

The problem of sampled-data control has been exces-

sively studied over the past decades, the periodic sampling or time-triggered sampling mechanism is the traditional method. However, this method may lead to unnecessary data transmission, which is undesired in practical engineering, especially in some networked control systems with limited communication bandwidth. On the other hand, event-triggered control is a hot topic in recent years, which can reduce the transmission resource efficiently compared with the periodic sampling. The event-triggered control method has been developed rapidly, especially for switched systems, for example, adaptive event-triggered control, observer based event-triggered control and so on. There are so many results occured [10-12]. However, the switching feather mixed event-triggered sampling makes it difficult to the analysis and synthesis of the switched system. For the difficulty dealing with asynchronism between subsystem and event-triggered controller, many works assume that at most one switching happens during an inter-event interval, which is unrealistic and not practical. Inspired by the work [5], which firstly searched the system switch more than once during the event-triggered period. We extended the method of [5] for switched linear systems with frequent switching over an inter-event interval, which motivates our current study.

The concept of extended dissipative was proposed by Zhang in [13], which unifies H_{∞} performance, $L_2 - L_{\infty}$ performance, Passivity performance and (Q, S, R)dissipativity performance together. It provids an efficient

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method for system performance analysis and has attracted remarkable attention [13-15]. So we are interested analysing the extended dissipative performance for switched linear systems.

The contributions of this paper are listed as follows: 1) A novel event-triggered method with frequent switching over an inter-event interval is proposed; 2) Finite-time extended dissipative performance is analysed for switched linear systems; 3) The novel controller-mode dependent Lyapunov functional is used for system analysis; 4) Matrix transformation technique is used for the controller design.

This paper is organized as follows: In Section 2, system descriptions and preliminaries are formulated. In Section 3, sufficient conditions of event-triggered finite-time extended dissipative control for switched linear systems are established. The design method of the state feedback controllers is proposed. In Section 4, numerical examples are presented. In Section 5, conclusion is given.

Notation: M^T represents the transpose of the matrix M; X > 0 denotes a positive-definite matrix. $\lambda_{min}(P)$, $\lambda_{max}(P)$ denote the minimum and maximum eigenvalue of matrix P respectively.

2. SYSTEM DESCRIPTIONS AND PRELIMINARIES

Consider the following switched linear system:

$$\begin{aligned} \dot{x}(t) &= A_{\sigma(t)} x(t) + B_{\sigma(t)} u(t) + C_{\sigma(t)} w(t), \\ y(t) &= D_{\sigma(t)} x(t), \\ x(t_0 + \theta) &= \varphi(\theta), \forall \theta \in [-\tau, 0], \end{aligned}$$
(1)

where $x(t) \in \mathbb{R}^n$ is the state vector, u(t) is the control input, w(t) is the exogenous disturbance which belongs to $L_2[0,\infty), L_2[0,\infty)$ denote something is bounded, $y(t) \in \mathbb{R}^n$ is the output of the system, $\varphi(\theta)$ is the initial condition of the system on $[-\tau, 0]$. The switching signal $\sigma(t) : [0,\infty) \mapsto$ $M = \{1, 2...l\}$ is a piecewise continuous function and for each $\sigma(t) = i, A_i, B_i, C_i, D_i$ are known constant matrices. Let $t_q, q \in N$, be the switching instant, where $N \in N^+$ stands for the positive integer.

Given the event-triggered scheme:

 $t_{k+1} = \min\{t_k + T < t < t_k + G \mid [x(t) - x(t_k)]^T \Phi_{\sigma(t_k)}[x(t) - x(t_k)] \ge \varepsilon x(t_k)^T \Phi_{\sigma(t_k)} x(t_k)\}, t_k$ denotes the sampling instants for any integer $k \ge 0$. $\Phi_{\sigma(t_k)}$ is positive definite matrices to be determined, $\varepsilon > 0$ and $0 < T < \tau_a$ are given event-triggered parameters. Note that the parameter *T* in the event-triggered mechanism limits the lower bound of inter-event intervals and meanwhile avoids the Zeno behavior. The parameter *G* in the event-triggered mechanism limits the upper bound of inter-event intervals and meanwhile restricts the total asynchronous time, which not only facilitates the analysis and synthesis problems but also avoids the controller not updated for too long a time.

The state feedback control law is given as $u(t) = K_{\sigma(t_k)}x(t_k), t \in [t_k, t_{k+1})$. Denote $e(t) = x(t) - x(t_k)$, then $u(t) = K_{\sigma(t_k)}(x(t) - e(t)), t \in [t_k, t_{k+1})$.

Then the closed-loop system can be obtained.

$$\begin{aligned} \dot{x}(t) &= \overline{A}_{\sigma(t),\sigma(t_k)} x(t) - \overline{B}_{\sigma(t),\sigma(t_k)} e(t) + C_{\sigma(t)} w(t), \\ y(t) &= D_{\sigma(t)} x(t), \\ x(t_0 + \theta) &= \varphi(\theta), \forall \theta \in [-\tau, 0], t \in [t_q, t_{q+1}). \end{aligned}$$

$$(2)$$

where

$$egin{aligned} &A_{\sigma(t),\sigma(t_k)} = (A_{\sigma(t)} + B_{\sigma(t)} K_{\sigma(t_k)}), \ &\overline{B}_{\sigma(t),\sigma(t_k)} = B_{\sigma(t)} K_{\sigma(t_k)}. \end{aligned}$$

Assume $\sigma(t_k) = i, \sigma(t_q) = j$, with $t_k < t_q$ and $\sigma(t) = j$ for all $t \in [t_q, t_{q+1})$.

We discuss the following two cases:

Case 1: If no event trigger happened in $[t_q, t_{q+1})$, i.e., $t_k < t_q < t_{q+1} \le t_{k+1}$, then the system is the form:

$$\begin{split} \dot{x}(t) &= \overline{A}_{j,i} x(t) - \overline{B}_{j,i} e(t) + C_j w(t), \\ y(t) &= D_j x(t), \\ x(t_0 + \theta) &= \varphi(\theta), \forall \theta \in [-\tau, 0], t \in [t_q, t_{q+1}). \end{split}$$

where $e(t) = x(t) - x(t_k), t \in [t_q, t_{q+1}).$

Case 2: If there are $m (\in N+)$ triggered instants in $[t_q, t_{q+1})$, i.e., $t_k < t_q < t_{k+1} < \cdots < t_{k+m} \le t_{q+1} < t_{k+m+1}$, then the system is the form

$$\dot{x}(t) = \begin{cases} \overline{A}_{j,i}x(t) - \overline{B}_{j,i}e(t) + C_{j}w(t), \ t \in [t_{q}, t_{k+1}), \\ \overline{A}_{j,j}x(t) - \overline{B}_{j,j}e(t) + C_{j}w(t), \ t \in [t_{k+1}, t_{k+2}), \\ \vdots \\ \overline{A}_{j,j}x(t) - \overline{B}_{j,j}e(t) + C_{j}w(t), \ t \in [t_{k+m}, t_{q+1}), \end{cases}$$
$$y(t) = D_{j}x(t), \\ x(t_{0} + \theta) = \varphi(\theta), \ \forall \theta \in [-\tau, 0], \ t \in [t_{q}, t_{q+1}), \end{cases}$$

where

$$e(t) = \begin{cases} x(t) - x(t_k), t \in [t_q, t_{k+1}), \\ x(t) - x(t_{k+1}), t \in [t_{k+1}, t_{k+2}), \\ \vdots \\ x(t) - x(t_{k+m}), t \in [t_{k+m}, t_{q+1}). \end{cases}$$

We use $T_{\uparrow}[t_q, t_{q+1})$ and $T_{\downarrow}[t_q, t_{q+1})$ to denote the asynchronous and synchronous interval of $[t_q, t_{q+1})$, respectively, the system can be rewritten as

$$\begin{split} \dot{x}(t) &= \begin{cases} \overline{A}_{j,i}x(t) - \overline{B}_{j,i}e(t) + C_jw(t), & t \in T_{\uparrow}[t_q, t_{q+1}).\\ \overline{A}_{j,j}x(t) - \overline{B}_{j,j}e(t) + C_jw(t), & t \in T_{\downarrow}[t_q, t_{q+1}) \end{cases}\\ y(t) &= D_jx(t),\\ x(t_0 + \theta) &= \varphi(\theta), \ \forall \theta \in [-\tau, 0], \ t \in [t_q, t_{q+1}). \end{split}$$

Proposition 1 [1]: The external disturbance satisfies

$$\int_0^t w^T(s)w(s)ds \le d, \ d\ge 0.$$

Proposition 2 [13]: Matrices ψ_1 , ψ_2 , ψ_3 , ψ_4 satisfy the following conditions:

1)
$$\psi_1 = \psi_1^T \le 0$$
, $\psi_3 = \psi_3^T > 0$, $\psi_4 = \psi_4^T \ge 0$;
2) $(\|\psi_1\| + \|\psi_2\|)\psi_4 = 0$.

Definition 1 [13]: Given matrices ψ_1 , ψ_2 , ψ_3 and ψ_4 satisfying Proposition 2, and for any $T_f \ge 0$ and all $w(t) \in L_2[0,\infty)$, system (2) is said to be extended dissipative if:

$$\int_{0}^{T_{f}} J(t)dt - \sup_{0 \le t \le T_{f}} y^{T}(t)\psi_{4}y(t) \ge 0,$$
(3)

where

$$J(t) = y^{T}(t)\psi_{1}y(t) + 2y^{T}(t)\psi_{2}w(t) + w^{T}(t)\psi_{3}w(t).$$
(4)

Remark 1: By setting the weighting matrices, we have 1) $L_2 - L_{\infty}$ performance: $\psi_1 = 0$, $\psi_2 = 0$, $\psi_3 = \gamma^2 I$, $\psi_4 = I$;

2) H_{∞} performance: $\psi_1 = -I$, $\psi_2 = 0$, $\psi_3 = \gamma^2 I$, $\psi_4 = 0$; 3) Passivity performance: $\psi_1 = 0$, $\psi_2 = I$, $\psi_3 = \gamma I$, $\psi_4 = 0$;

4) (Q, S, R)-dissipativity performance: $\psi_1 = Q$, $\psi_2 = S$, $\psi_3 = R - \beta I$, $\psi_4 = 0$.

Definition 2 [1]: Given positive constants c_1, c_2, T_f with $c_1 < c_2$, a positive definite matrix R and a switching signal $\sigma(t)$, $\forall t \in [0, T_f]$, switched system (2) is said to be finite-time bounded with respect to $(c_1, c_2, R, T_f, \sigma)$, if $\forall t \in [0, T_f]$,

$$\sup_{\substack{-\tau \le \theta \le 0}} \{x^{T}(\theta) R x(\theta), \dot{x}^{T}(\theta) R \dot{x}(\theta)\} \le c_{1}$$

$$\Rightarrow x^{T}(t) R x(t) \le c_{2}.$$
(5)

Definition 3 [1]: For any $T_2 > T_1 \ge 0$, let $N_{\sigma}(T_1, T_2)$ denotes the switching number of $\sigma(t)$ over (T_1, T_2) . If

$$N_{\sigma}(T_1, T_2) \le N_0 + \frac{T_2 - T_1}{\tau_a}$$
 (6)

holds for $\tau_a > 0$ and an integer $N_0 \ge 0$, then τ_a is called an average dwell-time and N_0 is the chatter bound.

3. MAIN RESULTS

3.1. Finite-time boundedness and extended dissipative performance analysis

Theorem 1: If there exist positive scalars b, α, β and $\mu \ge 1$, positive definite matrices P_i, Q_i, Φ_i , such that the following matrix inequalities hold for all $i, j \in N$.

$$P_i \le \mu P_j, \ \forall i \ne j, \tag{7}$$

$$\frac{1}{b}P_{i} - D_{i}^{T}\psi_{4}D_{i} > 0,$$

$$\begin{bmatrix} -\beta P_{i} + P_{i}\overline{A}_{ji} + \overline{A}_{ji}^{T}P_{i} & -P_{i}\overline{B}_{ji} & P_{i}C_{j} & \Phi_{i} \end{bmatrix}$$
(8)

$$\begin{vmatrix} * & -\Phi_{i} & 0 & -\Phi_{i} \\ * & * & -Q_{i} & 0 \\ * & * & * & -\Phi_{i} \end{vmatrix} < 0,$$
(9)

$$\begin{bmatrix} \alpha P_j + P_j \overline{A}_{jj} + \overline{A}_{jj}^T P_j & -P_j \overline{B}_{jj} & P_j C_j & \Phi_j \\ * & -\Phi_j & 0 & -\Phi_j \\ * & * & -Q_j & 0 \\ * & * & * & -\Phi_j \end{bmatrix} < 0,$$
(10)

$$\begin{bmatrix} \Theta_{11} & -P_i \overline{B}_{ji} & P_i C_j - D_j^T \psi_2 & \Phi_i \\ * & -\Phi_i & 0 & -\Phi_i \\ * & * & -\psi_3 & 0 \\ * & * & * & -\Phi_i \end{bmatrix} < 0,$$
(11)
$$\Theta_{11} = -\beta P_i + P_i \overline{A}_{ii} + \overline{A}_{ii}^T P_i - D_i^T \psi_1 D_i.$$

$$\begin{bmatrix} \Xi_{11} & -P_{j}\overline{B}_{jj} & P_{j}C_{j} - D_{j}^{T}\psi_{2} & \Phi_{j} \\ * & -\Phi_{j} & 0 & -\Phi_{j} \\ * & * & -\psi_{3} & 0 \\ * & * & * & -\Phi_{j} \end{bmatrix} < 0, \quad (12)$$
$$\Xi_{11} = \alpha P_{j} + P_{j}\overline{A}_{jj} + \overline{A}_{jj}^{T}P_{j} - D_{j}^{T}\psi_{1}D_{j}$$

hold, the average dwell-time satisfies

$$\tau_a \ge \frac{ln\mu + (\alpha + \beta)T}{\alpha},\tag{13}$$

and

$$(\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} (\lambda_2 c_1 + \lambda_3 d) < \lambda_1 c_2, \quad (14)$$

$$(\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} < b, \quad (15)$$

we define

$$\lambda_{min}(R^{-\frac{1}{2}}P_iR^{-\frac{1}{2}}) = \lambda_1, \lambda_{max}(R^{-\frac{1}{2}}P_iR^{-\frac{1}{2}}) = \lambda_2,$$

$$\lambda_{max}(R^{-\frac{1}{2}}Q_iR^{-\frac{1}{2}}) = \lambda_3.$$
 (16)

Then the switched system (2) is finite-time boundedness with extended dissipative performance.

Proof: Choose the following Lyapunov functional as

$$V(t) = x^{T}(t)P_{\sigma(t_{k})}x(t).$$
(17)

Case 1: If no triggered instant happened in $[t_q, t_{q+1})$, the closed-loop system is the same as the above Case 1 with $V(t) = x^T(t)P_ix(t)$. Then we have

$$\begin{split} \dot{V}(t) &- \beta V(t) - w^T(t) Q_i w(t) \\ &= 2x^T(t) P_i \dot{x}(t) - \beta x^T(t) P_i x(t) - w^T(t) Q_i w(t) \\ &\leq 2x^T(t) P_i (\overline{A}_{ji} x(t) - \overline{B}_{ji} e(t) + C_j w(t)) \\ &- \beta x^T(t) P_i x(t) - w^T(t) Q_i w(t) \\ &+ [x(t) - e(t)]^T \Phi_i [x(t) - e(t)] - e(t)^T \Phi_i e(t) \end{split}$$

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$$\leq X^{T}(t)\Omega_{ji}X(t), \tag{18}$$

where

$$X(t) = \begin{bmatrix} x^T(t) & e^T(t) & w^T(t) \end{bmatrix}^T,$$

and

$$\Omega_{ji} = \begin{bmatrix} -\beta P_i + P_i \overline{A}_{ji} + \overline{A}_{ji}^T P_i & -P_i \overline{B}_{ji} & P_i C_j \\ * & -\Phi_i & 0 \\ * & * & -Q_i \end{bmatrix} + E^T \Phi_i E,$$
$$E = \begin{bmatrix} I & -I \end{bmatrix}.$$

From (9), we have

$$\dot{V}(t) \le \beta V(t) + w^T(t)Q_iw(t), t \in [t_q, t_{q+1}).$$
 (19)

It can be concluded that

$$V(t_{q+1}) = V(t_{q+1}^{-1}) \le e^{\beta(t_{q+1}-t_q)}V(t_q) + e^{\beta(t_{q+1}-t_q)} \int_{t_q}^{t_{q+1}} w^T(s)Q_iw(s)ds, t \in [t_q, t_{q+1}).$$
(20)

Case 2: When there are $m(\in N_+)$ triggered instants in $[t_q, t_{q+1})$, the closed-loop system is the same as the above Case 2 with

$$V(t) = \begin{cases} x^{T}(t)P_{i}x(t), & t \in [t_{q}, t_{k+1}); \\ x^{T}(t)P_{j}x(t), & t \in [t_{k+1}, t_{q+1}), \end{cases}$$

similar to Case 1 and considering (7), we have

$$V(t_{k+1}) \leq \mu V(t_{k+1}^{-1}) \leq \mu e^{\beta(t_{k+1}-t_q)} V(t_q) + \mu e^{\beta(t_{k+1}-t_q)} \int_{t_q}^{t_{k+1}} w^T(s) Q_i w(s) ds, t \in [t_q, t_{k+1}).$$
(21)

For $t \in [t_{k+1}, t_{q+1})$, it holds that

$$\begin{split} \dot{V}(t) &+ \alpha V(t) - w^{T}(t)Q_{j}w(t) \\ &= 2x^{T}(t)P_{j}\dot{x}(t) + \alpha x^{T}(t)P_{j}x(t) - w^{T}(t)Q_{j}w(t) \\ &\leq 2x^{T}(t)P_{j}(\overline{A}_{jj}x(t) - \overline{B}_{jj}e(t) + C_{j}w(t)) \\ &+ \alpha x^{T}(t)P_{j}x(t) - w^{T}(t)Q_{j}w(t) \\ &+ [x(t) - e(t)]^{T}\Phi_{j}[x(t) - e(t)] - e(t)^{T}\Phi_{j}e(t) \\ &\leq X^{T}(t)\Omega_{jj}X(t), \end{split}$$
(22)

which implies

$$\dot{V}(t) \leq -\alpha V(t) + w^T(t)Q_j w(t).$$

From (10), we have

 $V(t_{q+1}) = V(t_{q+1}^{-1})$

$$\leq e^{-\alpha(t_{q+1}-t_{k+1})}V(t_{k+1}) + e^{-\alpha(t_{q+1}-t_{k+1})}\int_{t_{k+1}}^{t_{q+1}}w^{T}(s)Q_{j}w(s)ds \leq \mu e^{-\alpha(t_{q+1}-t_{k+1})}(V(t_{k+1}^{-1}) + \int_{t_{k+1}}^{t_{q+1}}w^{T}(s)Q_{j}w(s)ds) \leq \mu e^{-\alpha(t_{q+1}-t_{k+1})+\beta(t_{k+1}-t_{q})}(V(t_{q}) + \int_{t_{q}}^{t_{q+1}}w^{T}(s)Q_{j}w(s)ds).$$
(23)

Therefore, it can be concluded from (20) and (23) that

$$V(t_{q+1}) \leq \mu e^{-\alpha T_{\downarrow}[t_q, t_{q+1})} e^{\beta T_{\uparrow}[t_q, t_{q+1})} (V(t_q) + \int_{t_q}^{t_{q+1}} w^T(s) Q_i w(s) ds).$$
(24)

The controller switching $\tilde{N}_{\sigma}(0,t)$ is smaller than system switching $N_{\sigma}(0,t)$. Then for any t > 0,

$$V(t) \leq \mu^{\bar{N}_{\sigma}(0,t)} e^{-\alpha T_{\downarrow}[0,t)+\beta T_{\uparrow}[0,t)} \\ \times \left(V(0) + \int_{0}^{t} w^{T}(s)Q_{i}w(s)ds\right) \\ \leq \mu^{N_{\sigma}(0,t)} e^{-\alpha t} e^{(\alpha+\beta)TN_{\sigma}(0,t)} \\ \times \left(V(0) + \int_{0}^{t} w^{T}(s)Q_{i}w(s)ds\right) \\ \leq (\mu e^{(\alpha+\beta)T})^{N_{0}} e^{(\frac{in\mu+(\alpha+\beta)T}{\tau_{a}}-\alpha)t} \\ \times \left(V(0) + \int_{0}^{t} w^{T}(s)Q_{i}w(s)ds\right).$$

$$(25)$$

On the other hand,

$$V(0) = x^{T}(0)P_{i}x(0) = x^{T}(0)R^{\frac{1}{2}}(R^{-\frac{1}{2}}P_{i}R^{-\frac{1}{2}})R^{\frac{1}{2}}x(0)$$

$$\leq \lambda_{2}c_{1}.$$
(26)

We have

$$V(t) = x^{T}(t)P_{i}x(t) = x^{T}(t)R^{\frac{1}{2}}(R^{-\frac{1}{2}}P_{i}R^{-\frac{1}{2}})R^{\frac{1}{2}}x(t)$$

$$\geq \lambda_{1}x^{T}(t)Rx(t).$$
(27)

From (25)-(27) we have that

$$x^{T}(t)Rx(t) < \frac{(\mu e^{(\alpha+\beta)T})^{N_{0}}e^{(\frac{\ln\mu+(\alpha+\beta)T}{\tau_{a}}-\alpha)t}(\lambda_{2}c_{1}+\lambda_{3}d)}{\lambda_{1}}$$

Using (14), one obtains

$$x^T(t)Rx(t) < c_2.$$

Similar to the above proof, we have

$$\dot{V}(t) + \lambda V(t) - J(t) \leq X^T(t) \Phi_{\sigma(t)\sigma(t_k)} X(t),$$

where

$$\begin{split} \lambda &= \begin{cases} \alpha, & t \in T_s[t_q, t_{q+1}); \\ -\beta, & t \in T_{as}[t_q, t_{q+1}), \end{cases} \\ X(t) &= \begin{bmatrix} x^T(t) & e^T(t) & w^T(t) \end{bmatrix}^T, \end{split}$$

by virtue of (11) and (12) we have that

$$\dot{V}(t) + \lambda V(t) - J(t) < 0.$$

Similar to above proof, we have

$$V(t) \leq (\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} \times \left(V(0) + \int_0^t J(s)ds\right),$$
(28)

under zero initial condition V(0) = 0, we have

$$V(t) \le (\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{in\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} \int_0^t J(s) ds, \quad (29)$$

and it is equivalent to

$$\frac{V(t)}{(\mu e^{(\alpha+\beta)T})^{N_0}e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t}} < \int_0^t J(s)ds,$$

by (15), we have

$$\frac{V(t)}{b} < \int_0^t J(s) ds,$$

so we have

$$\int_{0}^{t} J(s)ds > \frac{V(t)}{b} > \frac{1}{b}x^{T}(t)P_{i}x(t) > 0,$$

considering inequality

$$\int_0^{T_f} J(t)dt - \sup_{0 \leq t \leq T_f} y^T(t) \psi_4 y(t) \geq 0,$$

when $\psi_4 = 0$, one obtains

$$\int_0^{T_f} J(t) dt \ge 0,$$

when $\psi_4 > 0$, by Proposition 2 we have $\psi_1 = 0$, $\psi_2 = 0$, $\psi_3 > 0$, then we have

$$\int_0^t J(s)ds = \int_0^t w^T(s)\psi_3 w(s)ds,$$

thus, for $\forall t \in [0, T_f]$, we have

$$\int_0^{T_f} J(s) ds > \int_0^t J(s) ds \ge \frac{1}{b} x^T(t) P_i x(t) > 0,$$

it follows from (8) that

$$\int_0^{T_f} J(s)ds \ge \frac{1}{b} x^T(t) P_i x(t) \ge x^T(t) D_i^T \psi_4 D_i x(t)$$
$$= y^T(t) \psi_4 y(t),$$

so we get

$$\int_0^{T_f} J(t)dt - \sup_{0 \le t \le T_f} y^T(t) \psi_4 y(t) \ge 0.$$

The proof is completed.

Remark 2: This work focuses on achieving the finitetime boundedness and extended dissipative performance of switched linear systems and meanwhile save limited transmission resource. The event-triggered mechanism is adopted to determine the data sending, which effectively reduces the data transmission compared with periodic sampling. Frequent system switching is allowed over an event-triggered interval, which is different from the previous work [16] and [17] that only one switching happened over the event-triggered interval.

Theorem 2: If there exist positive scalars b, α , β and $\mu \ge 1$, positive definite matrices P_i , Q_i , Φ_i , such that the following matrix inequalities hold for all $i, j \in N$.

$$\begin{split} P_{i} &\leq \mu P_{j}, \forall i \neq j, \\ \frac{1}{b} P_{i} - D_{i}^{T} \psi_{4} D_{i} > 0, \\ \begin{bmatrix} \Lambda_{11} & -B_{j} Y_{i} & C_{j} & \hat{\Phi}_{i} \\ * & -\hat{\Phi}_{i} & 0 & -\hat{\Phi}_{i} \\ * & * & -Q_{i} & 0 \\ * & * & * & -\hat{\Phi}_{i} \end{bmatrix} < 0, \quad (30) \\ & \Lambda_{11} &= -\beta R_{i} + A_{j} R_{i} + B_{j} Y_{i} + R_{i} A_{j}^{T} + Y_{i}^{T} B_{j}^{T}, \\ \begin{bmatrix} \Gamma_{11} & -B_{j} Y_{j} & C_{j} & \hat{\Phi}_{j} \\ * & -\hat{\Phi}_{j} & 0 & -\hat{\Phi}_{j} \\ * & -\hat{\Phi}_{j} & 0 & -\hat{\Phi}_{j} \\ * & * & * & -Q_{j} & 0 \\ * & * & * & -\hat{\Phi}_{j} \end{bmatrix} < 0, \quad (31) \\ & \Gamma_{11} &= \alpha R_{j} + A_{j} R_{j} + B_{j} Y_{j} + R_{j} A_{j}^{T} + Y_{j}^{T} B_{j}^{T}, \\ \begin{bmatrix} \Delta_{11} & -B_{j} Y_{i} & C_{j} - R_{i} D_{j}^{T} \psi_{2} & \hat{\Phi}_{i} & R_{i} D_{j}^{T} \\ * & -\hat{\Phi}_{i} & 0 & -\hat{\Phi}_{i} & 0 \\ * & * & * & -\psi_{3} & 0 & 0 \\ * & * & * & * & \psi_{1}^{-1} \end{bmatrix} < 0, \quad (32) \\ & \Lambda_{11} &= -\beta R_{i} + A_{j} R_{i} + B_{j} Y_{i} + R_{i} A_{j}^{T} + Y_{i}^{T} B_{j}^{T}, \\ & \begin{bmatrix} \Pi_{11} & -B_{j} Y_{j} & C_{j} - R_{j} D_{j}^{T} \psi_{2} & \hat{\Phi}_{j} & R_{j} D_{j}^{T} \\ * & -\hat{\Phi}_{j} & 0 & -\hat{\Phi}_{j} & 0 \\ * & * & * & -\psi_{3} & 0 & 0 \\ * & * & * & -\hat{\Phi}_{j} & 0 \\ * & * & * & * & -\hat{\Phi}_{j} & 0 \\ * & * & * & * & -\hat{\Phi}_{j} & 0 \\ * & * & * & * & \psi_{1}^{-1} \end{bmatrix} < 0, \quad (33) \\ & \Pi_{11} &= \alpha R_{j} + A_{j} R_{j} + B_{j} Y_{j} + R_{j} A_{j}^{T} + Y_{j}^{T} B_{j}^{T} \end{split}$$

hold, the average dwell-time satisfies

$$au_a \geq rac{ln\mu + (lpha + eta)T}{lpha},$$

and

$$(\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} (\lambda_2 c_1 + \lambda_3 d) < \lambda_1 c_2,$$

$$(\mu e^{(\alpha+\beta)T})^{N_0} e^{(\frac{ln\mu+(\alpha+\beta)T}{\tau_a}-\alpha)t} < b,$$

we define

$$P_i^{-1} = R_i, \hat{\Phi}_i = R_i \Phi_i R_i, K_i R_i = Y_i,$$

and

$$\begin{split} \lambda_{min}(R^{-\frac{1}{2}}P_{i}R^{-\frac{1}{2}}) &= \lambda_{1}, \lambda_{max}(R^{-\frac{1}{2}}P_{i}R^{-\frac{1}{2}}) = \lambda_{2}, \\ \lambda_{max}(R^{-\frac{1}{2}}Q_{i}R^{-\frac{1}{2}}) &= \lambda_{3}. \end{split}$$

Then the switched system (2) is finite-time boundedness with extended dissipative performance. The controller gains can be given by $K_i = Y_i R_i^{-1}$.

Proof: Similar to the proof of Theorem 1, we have

$$\dot{V}(t) - \beta V(t) - w^T(t)Q_iw(t) \le X^T(t)\Omega_{ji}X(t).$$

Pre- and post-multiplying (30) by $diag\{P_i, P_i, I, P_i\}$, by Schur complement, we have $\Omega_{ji} < 0$, we can conclude that

$$\dot{V}(t) - \beta V(t) - w^T(t)Q_iw(t) < 0.$$

Similarly,

$$\dot{V}(t) - \beta V(t) - J(t) \le X^T(t) \Phi_{ji} X(t).$$

Pre- and post-multiplying (32) by $diag\{P_i, P_i, I, P_i\}$, by Schur complement, we have $\Phi_{ii} < 0$, we can conclude that

$$\dot{V}(t) - \beta V(t) - J(t) < 0.$$

The following proof is similar to that of Theorem 1, it is omitted here. $\hfill \Box$

4. NUMERICAL EXAMPLE

Consider the switched linear system (2) with two subsystems.

$$A_{1} = \begin{bmatrix} 2 & -4 \\ 1 & -3 \end{bmatrix}, B_{1} = \begin{bmatrix} 1 & -4 \\ -1 & 1 \end{bmatrix}, C_{1} = \begin{bmatrix} 3 & 2 \\ 0 & -1 \end{bmatrix},$$
$$D_{1} = \begin{bmatrix} 0.02 & 0 \\ 0.02 & 0.02 \end{bmatrix};$$
$$A_{2} = \begin{bmatrix} 1 & -6 \\ 3 & -2 \end{bmatrix}, B_{2} = \begin{bmatrix} 2 & -5 \\ -2 & 2 \end{bmatrix}, C_{2} = \begin{bmatrix} 1 & 2 \\ 0 & 2 \end{bmatrix},$$
$$D_{2} = \begin{bmatrix} 0.02 & 0 \\ 0.01 & 0.01 \end{bmatrix}.$$

The initial condition is $x(0) = \begin{bmatrix} -0.2 & 0.2 \end{bmatrix}^T$, and $w(t) = \begin{bmatrix} e^{-t} * \sin(t) & e^{-t} * \cos(t) \end{bmatrix}^T$.

We choose $c_1 = 0.08$, $c_2 = 1$, $T_f = 8$, $\gamma = 0.6$, u = 1, $R = I_{2\times 2}$, b = 0.5, T = 0.2, G = 2, $\varepsilon = 0.5$, $\alpha = 0.3$, $\beta = 0.3$, $\tau_a = 0.5$. For (Q, S, R)-dissipativity performance, we choose $Q = I_{2\times 2}$, $S = I_{2\times 2}$, $R = I_{2\times 2}$.

Performance variable for each case is given in Table 1. By solving the LMIs in Theorem 2, we can obtain the

Table 1. Performance variable for each case.

$L_2 - L_\infty$ performance, $\gamma^2 = 0.6$
H_{∞} performance, $\gamma^2 = 0.6$
Passivity, $\gamma = 0.6$
Dissipativity, $\beta = 0.4$

Table 2. Controller gain for each case.

Subsystem 1
$L_2 - L_{\infty} \text{ performance, } K_1 = \begin{bmatrix} -0.4408 & 1.5744\\ 0.8595 & -0.6980 \end{bmatrix}$
H_{∞} performance, $K_1 = \begin{bmatrix} 5.2523 & 4.1620 \\ 6.1586 & 1.4482 \end{bmatrix}$
Passivity, $K_1 = \begin{bmatrix} 5.9603 & 3.9647 \\ 6.7264 & 1.4412 \end{bmatrix}$
Dissipativity, $K_1 = \begin{bmatrix} 246.9201 & 258.1637 \\ 196.0458 & 116.9295 \end{bmatrix}$

Table 3. Controller gain for each case.

Subsystem 2
$L_2 - L_{\infty} \text{ performance, } K_2 = \begin{bmatrix} 0.1064 & 0.3398\\ 0.1673 & 0.0774 \end{bmatrix}$
$H_{\infty} \text{ performance, } K_2 = \begin{bmatrix} 0.6618 & 1.2532\\ 1.1050 & 0.1570 \end{bmatrix}$
Passivity, $K_2 = \begin{bmatrix} 2.2579 & 2.5304 \\ 2.5768 & 0.7323 \end{bmatrix}$
Dissipativity, $K_2 = \begin{bmatrix} 0.5085 & 1.0527 \\ 0.8948 & 0.1090 \end{bmatrix}$

controller gains and event-triggered parameters listed in Tables 2, 3 and 4, 5, respectively.

The switching signal of the system is given in Fig. 1. From Fig. 2, we can see that when $x^T(0)Rx(0) \le 0.08$, the trajectory satisfies $x^{T}(t)Rx(t) \leq 1$, which demonstrates the finite-time boundedness of the closed loop system. Fig. 3 shows the event-triggered release instants and the interevent intervals induced by the designed event-triggered mechanism. To focus on the inter-event intervals [0.6, 0.9]and [4.1, 4.4], it can be seen from Fig. 1 that frequent switching occurs in these intervals. This is different from the Fig.3 in the Reference [16] that at most one switching occurs in the inter-event intervals. Also, different from the Fig.4 in the Reference [5], we not only added the parameter G = 2 in the event-triggered mechanism which limits the upper bound of inter-event intervals but also added the parameter T = 0.2 in the event-triggered mechanism which limits the lower bound of inter-event intervals and meanwhile avoids the Zeno behavior.

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Subsystem 1
$L_2 - L_{\infty}$ performance, $\Phi_1 = \begin{bmatrix} 0.0010 & -0.0013 \\ -0.0013 & 0.0018 \end{bmatrix}$
H_{∞} performance, $\Phi_1 = \begin{bmatrix} 0.0034 & 0.0004 \\ 0.0004 & 0.0003 \end{bmatrix}$
Passivity, $\Phi_1 = \begin{bmatrix} 0.0053 & 0.0005 \\ 0.0005 & 0.0004 \end{bmatrix}$
Dissipativity, $\Phi_1 = \begin{bmatrix} 0.0068 & 0.0033 \\ 0.0033 & 0.0028 \end{bmatrix}$

Table 4. Event-triggered parameters for subsystem 1.

Table 5. Event-triggered parameters for subsystem 2.





Fig. 1. The switching signal of the system.

5. CONCLUSION

In this paper, the problem of event-triggered finite time extended dissipative control for a class of switched linear systems with frequent asynchronism has been investigated. A novel event triggered method has been introduced. We can solve the H_{∞} , $L_2 - L_{\infty}$, Passivity and (Q, S,



Fig. 2. The state trajectory under event triggered $L_2 - L_{\infty}$ control.



Fig. 3. Event triggered transmission interval.

R)-dissipativity performance in a unified framework based on extended dissipative. LMIs are used to obtain the results, we give numerical examples to show the effectiveness of the method.

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