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Development of a TPU/CNT/Cu Composite Conductive Filament with a High CNT Concentration

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Abstract

In this study, a fexible conductive flament was fabricated by mixing thermoplastic polyurethane (TPU), carbon nanotubes (CNTs), and Cu powder. A polymer extruder was used to disperse conductive materials in the TPU matrix. Because the dispersion of CNTs in polymers is difcult, the dispersion process was repeated several times for the homogeneity of the fabricated conductive flament. Cu powder with high electrical conductivity was additionally added to improve the electrical characteristics of the conductive polymer. As TPU generally has excellent ductility and durability, the fabricated flament can secure fexibility. The resistance was measured and compared according to the mixing ratio of CNT/Cu powder. Based on the obtained results, the resistance of the conductive flament decreased as the CNT and Cu powder contents were increased. The addition of metal powders, such as CNTs and Cu powder, however, reduced the ductility of TPU. Finally, the developed conductive flament was used to fabricate a simple closed photodiode circuit.

Keywords Conductive flament · TPU/CNT composite · 3D printing · Flexible composite

1 Introduction

Conductive composite materials are used in various areas, such as fexible circuits, fexible displays, wearables, and sensors, as they are highly suitable for the mechanical and electrical characteristics of flexible devices [\[1\]](#page-4-0)–[[5](#page-4-1)]. In addition, liquid or solid conductive composite materials are actively used in areas where printing technology is required because pneumatic injection or additive manufacturing technology can be easily applied to them. However, because they are printed on fexible electronic devices with an irregular and curved plane, flexibility and durability, including bending, folding, and twisting are required in addition to electrical conductivity stability [[6\]](#page-4-2).

Among various conductive composites, conductive polymer composites facilitate direct 3D printing, as they do not require solvents, complex processes, and additional processes, such as thermal annealing, which are required for

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² Smart Manufacturing Engineering Group, Institute for Advanced Engineering, Youngin‑Si 17180, Korea manufacturing metal ions, ink, and paste. In addition, they have longer lifespan than the described conductive materials and can be produced in the form of a filament [[7](#page-4-3)]. Conductive polymer composites have high commercial potential owing to high moldability and low density, electrical characteristics by conductive materials, and excellent fexibility and durability of the polymer matrix $[8]$ $[8]$. Therefore, the production cost of the conductive polymers and their applicability to printing have been examined [\[6,](#page-4-2) [9\]](#page-4-5).

Carbon nanotubes (CNTs) are difficult to disperse in the polymer structure owing to their high cohesive proper‑ ties. Further, high energy is required, as their concentration increases owing to an increase in the viscosity of the molten composite [[10\]](#page-4-6). However, they have high electrical conductivity because of the low percolation threshold and high aspect ratio [[11](#page-5-0)]. CNTs are also commonly used as composite materials owing to their excellent mechanical and thermal properties. In particular, conductive composites can be produced by forming a conductive path in insulating polymers with low density and high moldability, such as thermoplastic polyurethane (TPU) and PETG, by adding CNTs. As conductive polymers are easy to manufacture and have high printability, various conductive materials, such as CNTs $[12]$, carbon black $[13]$ $[13]$ $[13]$, carbon nanofiber $[14]$ $[14]$ $[14]$,

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graphite $[12]$ $[12]$ $[12]$, and graphene $[15]$ $[15]$, have been mixed with the polymer structure in many studies.

With rapidly increasing interest in 3D additive manufacturing technology, Cu powder as a conductive material, was mixed with ABS, PLA, and PS, which are most commonly used as commercial flaments [[16,](#page-5-5) [17\]](#page-5-6). It was reported that highly conductive flaments could be manufactured, and high percolation threshold values were observed when Cu powder was added. The polymers of commercial flaments, however, have high hardness and insufficient durability for bending.

No case has been reported for TPU/CNT and TPU/CNT/ Cu composite conductive filaments with high CNT concentration (12% or higher). Therefore, in this study, a TPU/ CNT composite flament was fabricated by including highconcentration CNTs in the TPU matrix, and the resistance was measured and analyzed while fexibility was maintained. In addition, Cu powder was added and its effect on the resistance of the TPU/CNT composite was observed. The dispersion process was repeated to obtain homogeneous electrical characteristics of the conductive composite.

2 Experiment

2.1 Materials

Table [1](#page-1-0) shows the properties of the materials used in this study. Huada Electronic Design Co., Ltd HD-E290I9 TPU was used to secure fexibility and durability, and Kumho Petrochemical Co., Ltd. (KKPC) K-Nanos 210P MWCNT was added as a conductive material to be dispersed in the TPU matrix. AV-CU003045US 45 µm/spherical Cu powder from AVENTION Co., Ltd. was added to secure additional electrical performance.

2.2 Manufacturing and Mixing Process

Homogeneous dispersion of CNTs in polymer matrix structures is difficult owing to their strong agglomeration properties caused by high surface energy. Polymer extruders are commonly used, as they facilitate the dispersion of the fller in the polymer structure as a melting mixing method that uses thermal and shear force. Therefore, in this study, the melting mixing method was used during the manufacturing

Table 1 Material properties

of the conductive flament for the homogeneous dispersion of CNTs in TPU.

Figure [1](#page-1-1) shows the conductive filament manufacturing process. When the materials to be mixed are placed in the hopper in sequence, they are transported to the nozzle section by the shear force of the screw inside the cylinder. Meanwhile, TPU is melted by the heat source of the coil heater. The materials are then gradually stagnated in the nozzle section, thereby forming a pressure inside the noz– zle space. The formed pressure, which is generated by the molten TPU with relatively high viscosity, causes mixing with conductive materials. The nozzle is flled with the mixed materials, and the internal shear force generates a pressure in the nozzle section direction, thereby extruding the mixture through the nozzle with a diameter of 1.5 mm. The temperature of the coil heater was set to 250 ℃ and the screw speed was 15 RPM.

When the degree of CNT dispersion is low, the electrical characteristics of the extruded conductive flament are not uniform. Therefore, the dispersion process was repeated by shearing the fabricated conductive flament wire into small sizes as shown in Fig. [2](#page-1-2)

2.3 Resistance and homogeneity measurement

The entire length of the extruded flament sample was cut into three pieces (start, middle, and end pieces), as shown in Fig. [3](#page-2-0), and the standard deviation of the measured resistance was calculated to confirm homogeneity $(R_E \cong R_M \cong R_S)$ of fabricated conductive flament. The resistance was measured using a multimeter, and the measured values were averaged. The measured resistance was converted into the volume

Fig. 1 Melt mixing method for conductive filament manufacture process

Fig. 2 Repeating the dispersion process

Fig. 3 Resistance measurement section and the homogeneity of conductive flament

Fig. 4 Four times dispersion of TPU/CNT 15 wt%

resistivity, $\rho(\Omega \text{ cm})$, using Eq. ([1\)](#page-2-1) for analysis. In Eq. ([1](#page-2-1)), A $\rm (mm^2)$ is the cross-sectional area, and L $\rm (mm)$ is the filament length.

$$
\rho = R \cdot A / L \tag{1}
$$

3 Result and discussion

3.1 High weight fraction CNT wt% TPU/CNT composite

Figure [4](#page-2-2) shows the results of repeating the dispersion process of CNT 15% four times. After repeating the dispersion process four times, the stifness of the flament was main‑ tained, and excellent surface roughness could be observed. As the CNT content increases, higher energy is required for dispersion because of an increase in the viscosity of the molten composite. Therefore, the results described above are considered to originate from the increasing CNT percolation capability in the TPU matrix due to repeated heating–shear– ing processes. In all TPU/CNT flament cases, dispersion was performed four times. Excellent flexibility and durability were observed under the application of twisting and bending for up to CNT 23%, but the fabrication failed from 25% owing to the high viscosity caused by poor surface roughness (Fig. [5](#page-2-3)).

Figure [6](#page-2-4) shows the standard deviation of the resistance of the fabricated filament calculated to examine homogeneity due to dispersion. As the percentage of CNT increased, the standard deviation decreased, showing that the distribution of CNT phases in TPU became easier. In other words, at a high CNT concentration, sufficient homogeneity can be secured even under low dispersion. In addition, high CNT concentration is considered to be favorable in terms of quality.

Fig. 5 Four times dispersion of TPU/CNT flament with high CNT wt%: 23.3% (left), 25% (right)

Fig. 6 Measured volume resistivity standard deviation on CNT ratio [wt%] in a TPU/CNT composite

Table 2 Reported percolation threshold in the literature

	Percolation threshold CNT, $wt\%$	Resistivity Ω cm
Bertollini et al. [18]	2	1.0×10^{2}
Sui et al. $[10]$	3	1.0×10^{3}
Ramoa et al. [19]	3	4.3×10^{1}
Kim et al. $[20]$		1.43×10^{1}
$N.P.$ Kim $[8]$	8	7.0×10^{5}

CNT has a low percolation threshold because its high aspect ratio makes it possible to obtain high electrical conductivity with only a small amount of the fller. Table [2](#page-2-5) summarizes the reported percolation thresholds of TPU/ CNT composites. It can be seen that each percolation threshold is diferent. This appears to be due to the low degree of CNT dispersion in polymer and the diference in temperature, RPM, and measuring equipment during

dispersion. Compared to the relatively high volume resistivity of TPU ($1.0 \times 10^{12} \Omega$ cm), the percolation threshold was found to be CNT 5% $(1.38 \times 10^1 \Omega \text{ cm})$ in this study. The obtained result is similar to that by Kim et al. (CNT 4% , $1.43 \times 10^{1} \Omega \text{ cm}$).

Figure [7](#page-3-0) shows the volume resistivity according to the percentage of CNT. As the percentage of CNT is increased, the volume resistivity decreased. The lowest volume resistivity of 0.12 Ω cm is obtained at CNT 23%, which is the maximum content applicable. The results obtained under the conditions of 240 ˚C/6 RPM/3 times and CNT 12% $(1.44 \times 10^2 \Omega \text{ cm})$ by N.P. Kim were compared with those under the conditions of 250 ˚C/15 RPM/4 times and CNT 11.7% (2.27 Ω cm) in this study. From this comparison, the results of this study were found to be superior. Highconcentration CNTs easily agglomerate even with a slight temperature change owing to the increased viscosity. Thus, higher energy is required for dispersion. Under the same dispersion method, it was difficult to identify a clear correlation with temperature for high percentage of CNT, but RPM was considered to be dominant. To explore this, the infuence of the temperature and shear force (RPM) on dispersion and resistance according to the percentage of CNT should be examined in the future. In the results of Sui et al. and Ramoa et al., high dispersion was induced by applying thermal and shear forces over an extended period of time. This procedure has the same principle as repeated dispersion performed in this study.

3.2 TPU/CNT/Cu composite

Figure [8](#page-3-1) shows the reduction in CNT mass in the total ratio. TPU and Cu mass were kept constant, and as the percentage of CNT decreased, the ratio of the percentage of Cu in the

Fig. 7 Measured volume resistivity versus CNT ratio [wt%] in a TPU/ CNT composite

total ratio increased. When Cu ratio was increased under the same the percentage of CNT, the resistance reduction efect was observed (Table [3](#page-3-2)). This is because Cu powder can easily form a conductive path by facilitating the electron movement. As shown in Fig. 8 , however, the volume resistivity increases with the percentage of Cu. This appears to be due to the reduction in the percentage of CNT rather than the increase in the Cu powder concentration. Podsiadly et al. reported that the percolation threshold was observed at polymer/Cu 80% [\[17\]](#page-5-6). We can conclude that for TPU/CNT/Cu in this study, the electrical resistance depends on the percentage of CNT because the percentage of Cu is relatively low.

Figure [9](#page-4-7) shows the volume resistivity according to the Cu content at high percentage of CNT. It can be seen that the resistivity decreases by approximately 1.3 times at Cu 23%, as compared to Cu 9%. At a relatively higher percentage of CNT, the addition of Cu powder has no signifcant impact on the resistance. Moreover, the hardness increases, and the fexibility signifcantly decreases. When CNT 19.2%/ Cu 23% were exceeded, high hardness was observed due to brittleness, and fexibility could be not secured owing to easy fracture during bending.

Fig. 8 Measured volume resistivity versus Cu ratio [wt%] in a TPU/ CNT/Cu composite

Fig. 9 Measured volume resistivity versus Cu ratio [wt%] in TPU/ CNT/Cu with high concentration CNT

4 Conclusion

In this study, TPU/CNT composite was fabricated by including high CNT concentration in TPU. In addition, Cu powder was added to the TPU/CNT composite to analyze its efect on the resistance. As melt mixing method, the thermal and shear force was used to disperse conductive materials in the TPU matrix.

CNT dispersion in the polymer structure is difficult owing to the high surface energy. Thus, dispersion needs to be repeated several times to secure homogeneous electrical characteristics of the fabricated conductive composite filament. The standard deviation of the conductive composite resistance was low after repeating the dispersion procedure four times, and excellent fexibility and flament stifness were maintained simultaneously.

As the percentage of CNT was increased, the volume resistivity decreased. The percolation threshold was found to be 5%, and excellent fexibility and durability were observed for up to 23%. The volume resistivity was found to be 0.12 Ω cm for the TPU/CNT 23% composite and 0.11 Ω cm for the TPU/CNT 19.2%/Cu 23% composite. The addition of CNTs and Cu powder, which are conductive materials, could reduce the electrical resistance by facilitating the electron movement. At the same the percentage of CNT, the addition of Cu powder decreased the volume resistivity. At a high CNT concentration, however, the addition of Cu did not improve the volume resistance signifcantly. Moreover, the addition of CNTs and Cu powder in large quantities to TPU reduced ductility and led to easy fracture due to brittleness.

A simple closed photodiode circuit was manufactured using the fabricated conductive composite flament (Fig. [10](#page-4-8)). The conductive composite flament developed in this study

Fig. 10 Conductive composite flament (left) and closed circuit(right)

can be applied to circuits and sensors in various felds. In the future, printing characteristics will be investigated using 3D printing, and changes in resistance due to the tension and bending of the output will be researched.

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