#### **ENGINE AND EMISSIONS, FUELS AND LUBRICANTS**



# **Study on the Necessity of Real‑World Driving Tests for Passenger Electric Vehicles**

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## **Abstract**

Numerous studies are currently focused on improving the performance and efficiency of electric vehicles (EVs). This research aims to evaluate the necessity for a practical testing methodology to simulate real-world driving scenarios by comparing the driving range measured on a chassis dynamometer with the ranges observed under various actual driving conditions. Tests were conducted on the chassis dynamometer using the multi-cycle test (MCT) mode, employing the urban dynamometer driving schedule (UDDS) and the highway fuel economy driving test (HWFET). Subsequently, we assessed the energy efficiency of three routes compliant with the real-driving emissions-light duty vehicles (RDE-LDV) regulations under realworld driving conditions. Our findings revealed disparities in energy efficiency ranging from 10.8 to 22.9% when driving on the same route and up to 29.3% when driving on diferent routes. This study highlights the importance of tailoring information provision, such as certifcation tests, to each country's environmental context.

**Keywords** Electric vehicle  $\cdot$  Energy efficiency  $\cdot$  Driving range  $\cdot$  Real-world driving

## **Abbreviations**



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# **1 Introduction**

As the signifcance of environmental protection and energy efficiency continues to increase, the development and proliferation of electric vehicles (EVs) are advancing rapidly (Sanguesa et al., [2021](#page-7-0)). Electric vehicles strive to minimize carbon dioxide emissions and promote sustainable utilization of energy, with ongoing research focusing on enhanc-ing vehicle performance and efficiency (Park et al., [2023](#page-7-1)). Extensive research is underway on battery technology (Chen et al., [2022](#page-7-2)), lightweight materials (Cimprich et al., [2023](#page-7-3)), and regenerative braking (Hamada & Orhan, [2022\)](#page-7-4).

To evaluate the performance of EVs under development, Europe employs the WLTP (UNECE, [2021\)](#page-7-5), and the United States and Korea utilize the MCT (SAE, [2021\)](#page-7-6). China adopts the CLTC (Yu et al., [2020\)](#page-7-7) to assess the driving range and energy efficiency of each vehicle. This test mode involves the progression of the state of charge (SOC) of an EV from fully charged to fully discharged. With the advancement of the EV driving range owing to technological progress, there has been an associated increase in test time and costs, resulting in signifcant fatigue for certifcation test performers (Choi et al., [2021](#page-7-8)). Hence, Noh et al., ([2024\)](#page-7-9) conducted a study on methods for shortening tests and determined that the short process test (SPT) method can reduce testing times

by up to 85%. Rho et al*.*, [\(2021](#page-7-10)) found that applying an improved MCT methodology can reduce the time by up to 19 and 23 min. Furthermore, a study conducted by Rho and Noh ([2022\)](#page-7-11) concluded that implementing the SPT method could reduce the testing time by 3 h for Vehicle A and 4 h for Vehicle B in comparison with the current EV test, thereby enhancing the test efficiency and ensuring field safety.

However, persistent issues arise from internal combustion engine vehicles, highlighting that certification tests conducted on chassis dynamometers fail to accurately replicate the diverse driving conditions experienced in individual countries. Ma et al., ([2019](#page-7-12)) emphasized that the lack of representativeness of the driving cycle used during regulatory laboratory tests signifcantly contributes to the substantial gap between actual energy consumption and type-approval levels. Similarly, Pavlovic et al., ([2016\)](#page-7-13) found that measurements obtained from chassis dynamometers tend to overestimate vehicle fuel consumption, exacerbating the disparity between real-world fuel consumption and type-approval values. This disparity has continued to widen over time, with the average disparity in Europe increasing from 8 to 39% between 2001 and 2007, as reported by a study conducted by the International Council on Clean Transportation (ICCT) (Greene et al., [2017\)](#page-7-14). Furthermore, research has shown that the performance of EVs is signifcantly infuenced by various factors in real-world driving conditions, including ambient temperature (Hao et al., [2020](#page-7-15)), driving route (Lajunen, [2014](#page-7-16)), and driver behavior (Braun & Rid, [2018](#page-6-0)).

Therefore, our objective is to assess the disparity between certifcation tests conducted on chassis dynamometers and the energy efficiency observed during real-world driving across diverse Korean road conditions, confirming the necessity for a practical testing methodology aligned with real-world driving scenarios in the future.

# **2 Methodology**

## **2.1 Test Vehicle and Equipment**

In this study, approximately 90 data points, including vehicle speed, motor speed/torque, and battery current/voltage, were collected at 1 Hz intervals using CAN equipment connected to the vehicle's on-board diagnostics (OBD) system during both chassis dynamometer tests and real-world driving tests using a battery electric vehicle (BEV). A schematic illustrating the test setup with the CAN equipment is presented in Fig. [1.](#page-1-0) The detailed specifcations of the CAN equipment are listed in Table [1.](#page-1-1) The test vehicle employed was a rear-wheel drive (RWD) vehicle equipped with a 72.6 kWh



<Data Acquisition using CAN equipment>

<span id="page-1-0"></span>**Fig. 1** Data acquisition using CAN equipment

<span id="page-1-1"></span>**Table 1** Specifcations of the CAN equipment

<b>Item</b>	Parameters
<b>Size</b>	$64$ mm $\times$ 41 mm $\times$ 21 mm
Working voltage	5 V
Power consumption	240 mA, 10 W
Temperature range	$(-40 \text{ to } 85)$ °C
Timing specifications	64-bit timestamping to accuracy of 25 ns

battery capacity, with comprehensive specifcations listed in Table [2.](#page-2-0)

#### **2.1.1 Verifcation of CAN Equipment Utilization**

In our previous study Lee et al. [\(2023a\)](#page-7-17), Lee et al. [\(2023b](#page-7-18))), correlation validation was conducted by comparing data concurrently obtained from the CAN equipment of a test vehicle and a power analyzer using a chassis dynamometer. Data on vehicle speed, battery current, and battery voltage were collected over 2-min intervals at speeds ranging from 0 to 120 km/h in increments of 10 km/h. A comparison of the data acquired from both instruments revealed exceptionally high correlations, with R-squared  $(R^2)$  values of 0.9998, 0.9929, and 0.9845 for the vehicle speed, battery current, and battery voltage, respectively. Consequently, the discrepancy between the power analyzer and CAN equipment in evaluating battery consumption was only 0.2%, confrming the reliability of acquiring test data through CAN equipment for future experiments.

<span id="page-2-0"></span>



<span id="page-2-1"></span>



# **2.2 Test Mode**

To analyze the energy consumption characteristics with respect to ambient temperature, a comprehensive testing setup was established. Tests were conducted under controlled laboratory and real-driving conditions.

#### **2.2.1 Chassis Dynamometer Test**

The MCT mode, employed as a certifcation test mode for evaluating the EV energy efficiency and driving range, involves repeating the UDDS-HWFET-UDDS-CSC (constant-speed cycle) sequence twice, proceeding from full battery charge to discharge. The CSC segment was designed to ensure reliable battery discharge through constant-speed driving while concurrently reducing the overall test duration. To maintain efficiency, the CSCE section should not exceed 20% of the total driving distance during the test. In this study, data were collected with the CSC segment set at a speed of 88.5 km/h, in accordance with the SAE regulation ([2017](#page-7-19)). The real-time speed profle and battery SOC obtained during the MCT are shown in Fig. [2.](#page-2-1) Detailed

<span id="page-2-2"></span>**Table 3** Specifcations of the chassis dynamometer

<b>Item</b>	Parameters	
Model	<b>CDE 4200</b>	
Type	MIM type	
Inertia range	500-5400 kg	
Temperature range	$(-10 \text{ to } 40)$ °C	
Motor specifications	150 kW class	
Max. speed	$200 \text{ km/h}$	
Speed measurement	10,000 encoder	

specifcations of the chassis dynamometer used in the tests are listed in Table [3.](#page-2-2)

#### **2.2.2 Real‑World Driving Test**

In response to the challenge of indoor certifcation tests for internal combustion engine vehicles failing to replicate the diverse driving patterns encountered in real-world scenarios, research endeavors have been undertaken to formulate various driving routes that align with real-driving emissionslight duty vehicles (RDE-LDV) regulations (Kang et al., [2017\)](#page-7-20). The RDE-LDV route regulations require division into sections based on vehicle speed, categorizing them as urban (60 km/h or less), rural (exceeding 60 km/h but not exceeding 90 km/h), or motorway (exceeding 90 km/h). For each section, the RDE-LDV regulations stipulate a minimum driving distance of 16 km, which must be continuous and follow the sequence of urban, rural, and motorway. The distribution of driving distance by section can be adjusted within 10%, with the allocation set at 34% in urban, 33% in rural, and motorway areas; however, the urban portion must exceed 29%. However, regulations and systems for conducting real-world tests on EVs have not yet been established.

Therefore, this study assesses and compares the performance of EVs on diverse routes adhering to the route criteria outlined in the RDE-LDV, which has been implemented for internal combustion engine vehicles. Test data were collected on the Konkuk University (KU) Route (Lee et al., [2024](#page-7-21)) and the GangNam Route (Lee et al., [2023a,](#page-7-17) [2023b](#page-7-18)), as detailed in the author's previous research, along with the Korea National University of Transportation (KNUT) route examined by Yu et al., ([2019\)](#page-7-22). These routes represent distinct driving characteristics: the KU and GangNam routes typify metropolitan driving conditions, whereas the KNUT route mirrors the driving behaviors observed in smaller provincial cities. The data were obtained using the same vehicle across all test routes. The driving routes, speed profles, and battery consumption for each route are shown in Fig. [3](#page-3-0). In addition, altitude data for each route sourced from Google Earth were provided, with sections featuring rapid altitude changes indicating tunnel passages.

#### **2.3 Data Analysis**

In this study, battery consumption was computed using the battery current and voltage data obtained through the CAN, employing the equation shown in Eq. ([1](#page-3-1))

<span id="page-3-1"></span>
$$
BC [kWh] = Vol
$$
 (V) × Current [A] × Time [h], (1)

where BC is battery consumption.

Equation  $(2)$  $(2)$  $(2)$  was utilized to calculate the energy efficiency for each section by dividing the driving range of each section by the battery consumption

<span id="page-3-2"></span>
$$
EE_{section}[km/kWh] = \frac{R_{section}[km]}{BC_{section}[kWh]},
$$
\n(2)

where  $\text{EE}_{\text{section}}$  is energy efficiency of each section, and R<sub>section</sub> is the driving range of each section.

# **3 Results**

### <span id="page-3-4"></span>**3.1 Comparison of Chassis Dynamometer Test**

The UDDS mode evaluates urban driving characteristics over an 11.8 km distance, whereas the HWFET mode assesses high-speed driving characteristics over a 16.4 km



<span id="page-3-0"></span>**Fig. 3** Test route: speed profle, battery consumption, and altitude

<span id="page-3-3"></span>

distance. The MCT mode, depicted in Fig. [2,](#page-2-1) was conducted at 25 °C by repeating the UDDS-HWFET-UDDS-CSC sequence twice. The test results, which represent energy efficiency, were calculated based on data obtained during driving in the MCT mode on the chassis dynamometer and are presented in Table [4](#page-3-3).

Under cold-start conditions, UDDS1 exhibited the lowest energy efficiency among the UDDS tests, measured at 8.53 km/kWh. It was observed that the energy efficiency improved in the UDDS section following the CSCM section drive compared with the UDDS section before the CSCM section drive. UDDS3 demonstrated approximately 5.3% higher energy efficiency than UDDS2, whereas UDDS4 exhibited approximately  $4.1\%$  higher energy efficiency than UDDS2. After the cold-start condition concluded, the battery temperature gradually rose from 23 to 25 °C during the CSC section drive, indicating enhanced performance within the battery temperature range of 25 °C. HWFET1 and HWFET2 recorded energy efficiencies of 6.92 and 6.76 km/ kWh, respectively, with a marginal diference of about 2.3%. This discrepancy falls within the acceptable margin of error, as stipulated by the Korean government, which considers a 3% margin of error (K-Petro, [2014\)](#page-7-23).

## **3.2 Comparative Analysis of Real‑World Driving Tests**

#### **3.2.1 KU Route**

Figure [3](#page-3-0) displays the outcomes derived from driving along the identical route (KU Route) under ambient temperature ranging from 21 to 28  $\degree$ C, similar to the 25  $\degree$ C conditions maintained by the chassis dynamometer during the MCT mode as detailed in Sect.  $3.1$ . To emulate a consistent traffic environment on the same route, data were analyzed from



<span id="page-4-0"></span>**Fig. 4** Repetition of testing along the KU route

13 instances in which the same driver operated the vehicle between 9 and 11 pm with the air conditioning system turned off. The energy efficiency across the urban, rural, and motorway sections is shown in Fig. [4](#page-4-0).

Despite driving along the same route under similar environmental conditions, variations in factors such as traffic signals and volume led to disparities of up to 20.2% in urban areas, 10.8% in rural areas, and 22.9% in motorways. This represents a substantial deviation from our previous study (Lee et al., [2024](#page-7-21)), wherein the battery consumption difered by approximately 3% under comparable ambient temperatures and traffic conditions.

In urban sections, the primary factors contributing to the diferences in battery consumption were identifed as the number of stops, frequent acceleration and deceleration, and specific traffic patterns. Higher instances of stopping, and frequent acceleration, and deceleration are correlated with increased battery consumption. Conversely, in rural and motorway sections characterized by fewer traffic signals, disparities in speed owing to traffic volume were identified as the principal cause. Higher average speeds are associated with lower energy efficiency.

#### **3.2.2 Various Driving Route Meeting RDE‑LDV Criteria**

The data collected while driving the KU, GangNam, and KNUT routes under equal temperature conditions of 21 °C were analyzed. Considering the varying driving ranges for each section of the routes, the distance traveled for each section was divided by the amount of battery consumed and compared in km/kWh, as shown in Table [5](#page-4-1). In the urban section, the KNUT route exhibited the highest energy efficiency of 9.58 km/kWh. This observation suggests that the KU and GangNam routes, which represent driving characteristics in metropolitan areas, experienced frequent acceleration and deceleration due to traffic signals and traffic volume. Consequently, it is inferred that the primary cause of increased battery consumption in a low-efficiency zone, as indicated by the "Stop & Go" segments in Fig. [5.](#page-5-0) The KNUT route exhibited a low frequency of deceleration and acceleration, including stopping, resulting in a high energy efficiency. Notably, in the rural section, the GangNam route demonstrated the highest energy efficiency of 9.22 km/ kWh, whereas the KNUT route demonstrated the lowest

<span id="page-4-1"></span>**Table 5** Energy efficiency of various driving route

Energy efficiency [km/ kWh]	Real-world driving		
	KU	GangNam	<b>KNUT</b>
Urban	9.09	8.73	9.58
Rural	7.63	9.22	6.52
Motorway	6.08	5.94	5.98



<span id="page-5-0"></span>**Fig. 5** Comparison of motor operating area

efficiency of 6.52 km/kWh. The driving characteristics of the GangNam route are illustrated in Fig. [5,](#page-5-0) where the impact of acceleration and deceleration is minimal, indicating a narrow operational range and low battery consumption as the vehicle maintains a constant speed. The KNUT route is illustrated in Fig. [3.](#page-3-0) Observing the altitude data presented in Fig. [3](#page-3-0), it is apparent that the vehicle was driving along a route with an uphill slope in a mountainous area. The significant decrease in energy efficiency in the rural section is attributable to the infuence of these slopes. Notably, the motorway section exhibited the highest efficiency on the KU route at 6.08 km/kWh, owing to the lower average speed compared to the other routes and the substantial energy recovery achieved through regeneration. Conversely, the motorway section, which was minimally affected by traffic conditions, exhibited a similar performance across all routes, with a diference of only 2.3%.

# **3.3 Comparative Analysis of Overall Results**

The results derived from the MCT mode and the real-world driving tests conducted using the chassis dynamometer are depicted in Fig. [6](#page-6-1). Additionally, the certifcation values of the test vehicle, incorporating the correction coefficient (0.7) applied in the MCT mode, are denoted as the certifed UDDS and certifed HWFET.



<span id="page-6-1"></span>**Fig. 6** Comparison of test mode

In real-driving scenarios adhering to the RDE-LDV regulations, EV exhibited variances in energy efficiency ranging from 4 to 8.9% in urban sections, 14.5 to 29.3% in rural sections, and 0.7 to 2.3% in motorway sections, depending on the driving environment.

When comparing the certification tests with actual road driving routes, disparities of 2–11% were observed in the UDDS and urban sections. Conversely, the energy efficiency was notably higher on real-world roads, ranging from 32.4 to 38.4%, compared with the vehicle's certifed UDDS value of 5.9 km/kWh, which incorporated the correction coefficient  $(0.7)$ . In the HWFET and motorway sections, the certifcation test was higher with a diference of 12.1 to  $14.2\%$ . In addition, the energy efficiency in the real world surpasses the vehicle's certifed HWFET value of 4.5 km/kWh by 24.2–26.0%. This indicates superior energy efficiency during real-world driving within a similar ambient temperature range. This underscores the signifcant variations in efficiency within specific regulations influenced by factors, such as route slope and traffic conditions.

# **4 Conclusions**

The aim of this study was to compare chassis dynamometer tests of EVs with various real-world driving scenarios to ascertain the necessity of real-world driving assessments by examining the disparities between certifcation values declared in indoor certifcation and actual driving results. The principal findings of this study are summarized as follows:

1. Utilizing the MCT mode of the chassis dynamometer, we confirmed the energy efficiency of UDDS1 under cold-start conditions at 8.53 km/kWh, which is the lowest among the UDDS tests. It was observed that during the CSC section drive, the battery temperature increased to 25 °C, with UDDS3 and UDDS4 demonstrating improved performance. The HWFET was within an acceptable range across tests, with an approximate error of 2.3%.

2. Even when driving along the same route (KU Route) under similar conditions, disparities of 20.2% in the urban section, 10.8% in the rural section owing to factors such as traffic signals impacting acceleration and deceleration, and 22.9% in the motorway section owing to speed variances according to traffic volume were observed. Furthermore, across various routes driven under comparable conditions, discrepancies in energy efficiency ranged from  $4$  to  $8.9\%$  in the urban section, 14.5 to 29.3% in the rural section, and 0.7 to 2.3% in the motorway section, which is attributable to diferences in the traffic environment and route slope.

This study presents diverse test results for assessing the energy efficiency and driving range of BEV. Additionally, it underscores the importance of conducting tests that refect real-world driving conditions alongside future certifcation tests tailored to the unique environmental contexts of each country. The need for real-world driving evaluations is further emphasized by the limitations observed in chassis dynamometer testing. Although these tests are controlled and repeatable, they fail to account for dynamic factors such as different traffic conditions, road slopes, and environmental infuences that greatly afect the performance of EVs in real-world driving scenarios. The signifcant discrepancies observed between dynamometer results and real-world data highlight the need for real-world driving tests to gain a more accurate and comprehensive understanding of the energy efficiency and driving range of EVs. This approach has signifcant implications for informing future research and policy decisions in the feld.

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**Data availability** Data will be made available on request.

#### **Declarations**

**Conflict of interest** The authors declared no competing interests. Suhan Park is an Editor of the International Journal of Automotive Technology. Editor status has no bearing on editorial consideration.

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