Simultaneous estimation of earthquake source parameters and crustal Q value from broadband data of selected aftershocks of the 2001 M_w 7.7 Bhuj earthquake

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This paper presents the simultaneous estimation of source parameters and crustal Q values for small to moderate-size aftershocks ($M_w 2.1-5.1$) of the $M_w 7.7$ 2001 Bhuj earthquake. The horizontal-component S-waves of 144 well located earthquakes (2001–2010) recorded at 3–10 broadband seismograph sites in the Kachchh Seismic Zone, Gujarat, India are analyzed, and their seismic corner frequencies, long-period spectral levels and crustal Q values are simultaneously estimated by inverting the horizontal component of the S-wave displacement spectrum using the Levenberg–Marquardt nonlinear inversion technique, wherein the inversion scheme is formulated based on the ω -square source spectral model. The static stress drops ($\Delta\sigma$) are then calculated from the corner frequency and seismic moment.

The estimated source parameters suggest that the seismic moment (M_0) and source radius (r) of aftershocks are varying from 1.12×10^{12} to 4.00×10^{16} N-m and 132.57 to 513.20 m, respectively. Whereas, estimated stress drops $(\Delta \sigma)$ and multiplicative factor $(E_{\rm mo})$ values range from 0.01 to 20.0 MPa and 1.05 to 3.39, respectively. The corner frequencies are found to be ranging from 2.36 to 8.76 Hz. The crustal S-wave quality factor varies from 256 to 1882 with an average of 840 for the Kachchh region, which agrees well with the crustal Q value of the seismically active New Madrid region, USA. Our estimated stress drop values are quite large compared to the other similar size Indian intraplate earthquakes, which can be attributed to the presence of crustal mafic intrusives and aqueous fluids in the lower crust as revealed by the earlier tomographic study of the region.

1. Introduction

The 2001 Bhuj earthquake of M_w 7.7 is one of the largest intraplate earthquakes in recent time, which claimed a death toll of 20,000 people. This earthquake (lat. 23.412°N and long. 70.232°E) took place on 26th January 2001 along a south dipping reverse fault at 23 km depth in the Kachchh rift zone, which is situated in the northwestern corner of peninsular India (Mandal *et al.* 2004a, 2004b). The maximum intensity was reported to be X+ on MM scale (Rastogi *et al.* 2001). Within a span of 192 yrs (1819–2011), two large intraplate earthquakes, *viz.*, the 1819 Kachchh (M_w 7.8) and the 2001 Bhuj (M_w 7.7) have occurred in the Kachchh region. These earthquakes caused widespread destruction of properties and casualties (at least 22,000 people). In spite of such devastation, the earthquake hazard assessments for various seismogenic zones of India have grossly been undermined. Under these circumstances, it is proposed here to analyze the source parameters from the recorded aftershock

Keywords. Earthquake source parameters; crustal Q-value; simultaneous inversion; S-wave spectra; aftershocks.

data of Bhuj earthquake from Kachchh region of Gujarat province, India to properly assess the earthquake hazard of the region.

The 2001 Bhui earthquake is perhaps one of the most enigmatic earthquake of the modern era as it raises some fundamental question regarding the existing paradigms for the earthquake, such as no surface expression of the causative fault, its occurrence in the stable continental regions away from the active plate boundaries and the high stress drop value associated with a smaller rupture area. This kind of intraplate earthquakes are rare and contributed 0.5% of the total annual global energy release through earthquakes (Johnston 1994). Only two intraplate regions in the world (e.g., Kachchh, India and New Madrid, USA) have got the unique distinction of experiencing large earthquakes of $M_w \geq 7.7$. But, the stress drop of the 2001 Bhuj mainshock was estimated to be around 200 bars (Antolik and Dreger 2003), which was larger than 1811–1812 New Madrid earthquakes with only 100 to 140 bars (Johnston and Schweig 1996). However, the 2001 Bhuj earthquake did not produce any clear discernible surface rupture except for a small 8 km-long zone of strike-slip faulting observed in the hanging wall of the causative fault plane (Wesnousky et al. 2001). The moment tensor inversion and aftershock studies delineate the causative fault for Bhuj earthquake, which is situated at 23 km of north of Kachchh Mainland Fault (KMF) and extends up to 40 km in depth with strike 65° . dip 50° and slip 50° that has been named as North Wagad Fault (Rastogi et al. 2001; Mandal et al. 2004a, 2004b). The rupture propagation study of the 2001 Bhuj mainshock using the waveform inversion revealed that the mainshock did release $\sim 65\%$ of moment energy with a peak slip of 12.4 m at the deeper part of fault (10–35 km), whereas, the remaining moment energy was released at the sallower part (0-10 km) with a maximum slip of 6.5 m^4 . Singh *et al.* (2004) proposed that the rupture process was quite slow and radially symmetric for the 2001 Bhuj earthquake.

Numerous attempts have been made to estimate the static stress drop for the 2001 Bhuj mainshock using the locations of aftershocks (Negishi *et al.* 2001; Bodin and Horton 2004; Singh *et al.* 2004). Negishi *et al.* (2001) obtained a static stress drop ranging from 12.6 to 24.6 MPa, for an equivalent source radius varying from 20 to 25 km. But, Bodin and Horton (2004) calculated a static stress drop of 16.0 ± 2 MPa over a rupture area of 1300 km². Singh *et al.* (2004) suggest that a frictional sliding model with an average dynamic stress drop of about 12 MPa and the ratio of rupture to shear wave velocity of 0.7 could satisfactorily explain the source complexity observed for the 2001 Bhuj mainshock. Based on waveform modelling, Antolik and Dreger (2003) proposed a stress drop value of 20.7 MPa with a small fault length of 45 km for the 2001 Bhuj mainshock. Mandal and Johnston (2006) found that the stress drop values show scatter above $10^{14.5}$ N-m for Bhuj aftershocks. The continued aftershock activity for more than 10 years, further, demonstrates the source complexity involved in generating these deeper earthquakes. Thus, this large variation in estimated source parameters of Bhuj mainshock suggests that the study of source parameters of its aftershocks became an important issue because of their continued nature as well as deeper origin (focal depths ~10–40 km).

In this study, we use a two-stage methodology for estimating the source parameters, which is mentioned below:

- 1. Spectral analysis of S-wave using SEISAN software (Havskov and Ottemoller 2003).
- 2. Inversion modelling using Levenberg–Marquadt non-linear inversion technique.

We apply the above technique to the broadband data of 136 well located aftershocks of the 2001 Bhuj earthquake, to estimate their source parameters and crustal Q values. Finally, the estimated parameters are used to understand the seismogenesis of the 2001 Bhuj earthquake sequence.

2. Geology and tectonics of the Kachchh region

Geologically, Quaternary/Tertiary sediments, Deccan volcanic rocks and Jurassic sandstones resting on Archean basement mainly characterize the Kachchh region (Gupta *et al.* 2001). The sediment fill thickens from less than 500 m in the north to over 4000 m in the south and from 200 m in the east to over 2500 m in the west (Gupta *et al.* 2001). To the north, Precambrian basement rocks are exposed in Meruda Takkar and Nagar Parkar (in Pakistan) hills (Biswas 1987). The Mesozoic rift-related extensional structures of the Kachchh basin got reactivated as strike-slip or reverse faults as a result of regional compressive stresses due to collision of Indian and Eurasian plates since Neogene times (Biswas 1987). The focal mechanisms of some earthquakes indicate reverse faulting suggesting ongoing inversion tectonics in the Kachchh basin (Chung and Gao 1995).

Major structural features of the Kachchh region include several E–W trending faults/folds as shown in figure 1. The rift zone is bounded by a north dipping Nagar Parkar Fault in the north and a south dipping Kathiawar Fault in the south. Other major faults in the region are the E–W trending Allah Bund Fault, Island Belt Fault, Kachchh Mainland



Figure 1. Location of the 10 mobile broadband stations (marked by solid black triangles), which were deployed during 2006–2010, alongwith the 2001 Bhuj mainshock epicenter (grey star symbol) while three stations, which were deployed in 2001, are shown by open triangles. Stations: VJP: Vajepar, TAP: Tapar, MTP: Motapaya, GDD: Gadhada, BHA: Bhachau, BEL: Bela, NGR: Nagor, BHU: Bhuj, TPM: Tappar (Mundra), MND: Mandvi, KVD: Kavada, RPR: Rapar, SKL: Samkhiyali. KMU: Kachchh mainland uplift. Major faults (solid lines): ABF, Allah Bund Fault; IBF, Island belt fault; KMF, Kachchh mainland fault; KHF, Katrol hill fault; NPF, Nagar Parkar fault; NKF, North Kathiawar fault; BF, Banni fault. And, NWF (North Wagad fault), the causative fault for 2001 Bhuj earthquake and Gedi fault, are shown by dotted line. The inset is showing the key map for the area, where, the study area is shown by a grey square. The epicentral location of the 1993 Latur earthquake is also shown by a grey dot.

Fault and Katrol Hill Fault. In addition, several NE and NW trending small faults/lineaments are observed (Biswas 1987). Seismic, gravity and magneto-telluric surveys indicate undulated basement with 2–5 km deep sediments and Moho depth at 35–43 km in southern Kachchh region (Gupta et al. 2001; Reddy et al. 2001). Prior crustal velocity investigations in Kachchh region suggest a large variation in the estimated Moho depths that varies from 37 to 48 km (Kumar et al. 2001; Reddy et al. 2001; Mandal 2006). Recently, a P-receiver function study also delineates a 4–6 km crustal as well as 6-12 km as then osphere ic thinning beneath the Kachchh rift zone (Mandal 2011). The crustal and lithospheric thicknesses obtained by Mandal (2011) vary from 35–43 and 62–90 km, respectively. In general, this region is very complex as it contains faults of multiple orientations and different natures (Biswas 1987). Focal mechanism solutions of a few of the major aftershocks obtained from waveform inversion of broadband data indicate a dominant reverse movement on the NWF (Mandal and Horton 2007). The focal mechanism solutions of 444 aftershocks (using 8–12 first motions) suggest that the focal mechanisms ranged between pure reverse and pure strike slip except some pure dip slip solutions (Mandal and Horton 2007). These mechanisms also suggest that the reverse movements on a preferred south-dipping plane mainly characterize the NWF, whereas, the strike slip movement along an almost vertical plane dominates the Gedi Fault (GF) (Mandal et al. 2009).

3. Past seismicity

The Kachchh region lies in the highest seismicity zone V, which is potential for M8 magnitude (BIS 2002). Large earthquakes have been occurring in the Kachchh region since historical times. It has been inferred, based on the radiocarbon dating that an earthquake occurred between 885 and 1035 AD along the Allah Bund Fault (Rajendran and Rajendran 2001). From historical records of earthquakes, a large earthquake occurred in 1030 AD (Williams 1958). In 1668, a moderate earthquake occurred west of Kachchh, with an epicenter at 24°N, 68°E (Rajendran and Rajendran 2001). The largest earthquake in the region occurred on June 6, 1819. This M_w 7.8 earthquake resulted in a 90 km long, 6.3 km wide and 4.3 m high ridge and created what is known as the Allah Bund (Johnston and Schweig 1996; Rajendran and Rajendran 2001). Between 1821 and 1996, 16 moderate earthquakes of magnitude varying from 4.2 to 6.1 have occurred in the region (Rajendran and Rajendran 2001). The last damaging earthquake of M_w 6.0 (Intensity IX) prior to the most recent M_w 7.7 2001 Bhuj event occurred along the Katrol Hill Fault near Anjar, Gujarat in 1956, which claimed 115 lives (Chung and Gao 1995). This earthquake was apparently a shallow reverse rupture, but did not rupture the surface. Most recently there was an earthquake in 1992 (Dodge et al. 1996), which was 19 ± 4 km deep. On December 24, 2001, an M5 earthquake struck north of Bhuj, the teleseismically-determined epicenter close to the western end of the Island Belt fault (Bodin and Horton 2004). The devastating 2001 Bhuj earthquake occurred on the ENE–WSW trending and south dipping reverse fault at a depth of 23 km (figure 1).

4. Aftershock data

In this study, we use 384 good seismograms (high S/N ratio) of 144 Bhuj aftershocks recorded at 3-5 digital seismograph stations. These aftershocks of moment magnitude 2.1 to 5.1 were recorded by

Table 1. One-dimensional P-wave velocity, S-wave velocity and density model (Berteusen 1977; Mandal 2007).

Depth (km)	V_p	V_s	ρ
	$(\rm km/s)$	$(\rm km/s)$	$({\rm kg/m^3})$
0.0 - 2.0	2.92	1.69	1700
2.0 - 10.0	5.93	3.43	2670
10.0 - 16.0	6.18	3.57	2750
16.0 - 29.0	6.40	3.70	2820
29.0 - 40.0	6.97	4.03	3000
40.0 - 100.0	8.20	4.74	3390

the close digital Kachchh seismological network of National Geophysical Research Institute (NGRI), Hyderabad during February 2001 to March 2010. The network consists of 13 3-component broadband seismographs (figure 1). Each seismograph is equipped with a 24-bit Reftek recorder (with an external hard disk of 2 GB and GPS timing system) and 3-component broadband sensors (CMG3T and CMG40T). During this period, the broadband stations were situated between latitude $23.24^{\circ}-23.87^{\circ}$ N and longitude $69.72^{\circ}-70.37^{\circ}$ E. All broadband stations are installed on the hard sediment resulting in good signal-to-noise ratio. The P- and S-arrival times recorded from the network enabled us to obtain a better estimation of hypocentral parameters (error in epicentral location <2 km, focal depth estimation <6 km and rms of P-residual < 0.3 s). A strong Sp converted phase appearing 0.7–1.1 s prior to the S-arrival, which is generated from the sedimentary-basement transition, characterizes the seismograms for Bhuj aftershocks (Mandal 2007). To avoid the influence of Sp converted phase on the event location, we picked strong S-phase on the horizontal components of seismograms leaving the weak beginning of the S wave train.

5. Location, delineation and characterization of the causative fault

Aftershock locations are obtained using the program HYPO71Pc (Lee and Valdes 1985) and the modified average one-dimensional crustal velocity model (Mandal 2007; table 1). The velocity model consists of six layers, the tops of which are at 0.0, 2.0, 10.0, 16.0, 29.0, and 40.0 km, with Pwave velocities of 2.92, 5.93, 6.18, 6.40, 6.97, and 8.20 km/s, respectively (Mandal 2007). The distance between station and epicenters varies from 5 to 90 km. This network provides an azimuthal gap of less than 180°. The average location rms was 0.03 s. The mean horizontal and vertical single 68% confidence estimates are 2.0 and 6.0 km, respectively, for the aftershocks (table 2).

The estimated relatively accurate hypocentral parameters (error in epicentral location <1.5 km, focal depth estimates <3 km and rms of P-residual <0.3 s) of 144 selected aftershocks (2001–2010) of the 2001 Bhuj mainshock show that most of the events are mainly clustered within an E–W trending crustal volume below the main rupture zone of the 2001 Bhuj mainshock, which extends 55 km in N–S (latitude $23.25^{\circ}-23.75^{\circ}$ N), 45 km in E–W (longitude $70.0^{\circ}-70.55^{\circ}$ E) and 35 km in depth (from 1 to 36 km) (figure 2a–c). However, a few events are clustered along the GF while some scattered events are also located along the ABF and IBF

Table 2. Estimated hypocentral parameters for selected 144 Bhuj aftershocks.

		Ori. time		$\operatorname{Depth}_{(\operatorname{lrm})}$			
Ev. nos	YearMnDa	(HrMnSs)	Lat. ($^{\circ}$)	Long. ($^{\circ}$)	(km)	M_w	
No 1	2001 208	1029 54.0	23.341	70.399	21.9	4.1	
No 2	$2001 \ 208$	0324 56.0	23.260	70.320	17.0	4.1	
No 3	$2001 \ 208$	$0931 \ 52.0$	23.430	70.499	26.3	4.4	
No 4	$2001 \ 208$	1411 55.0	23.389	70.279	29.2	3.3	
No 5	$2001 \ 208$	$1653 \ 52.0$	23.710	70.444	28.0	4.4	
No 6	$2001 \ 208$	$1704\ 51.0$	23.320	70.330	20.9	3.5	
No 7	$2006 \ 406$	$1202 \ 52.9$	23.780	70.740	3.1	4.8	
No 8	$2006 \ 406$	$1759\ 18.2$	23.340	70.390	29.3	5.1	
No 9	2009 411	$1231 \ 46.1$	23.491	70.267	15.5	2.8	
No 10	$2009 \ 412$	$1842 \ 10.8$	23.420	70.148	17.8	3.3	
No 11	2009 414	$1219\ 16.7$	23.387	70.344	10.0	2.6	
No 12	2009 414	$1943 \ 20.0$	23.472	70.290	17.5	2.1	
No 13	2009 415	0913 49.5	23.401	70.188	33.4	3.1	
No 14	2009 415	$1420 \ 34.3$	23.294	70.258	14.6	2.7	
No 15	2009 415	$2115 \ 14.6$	23.578	70.505	14.9	3.1	
No 16	2009 416	0018 55.5	23.434	70.185	12.4	3.4	
No 17	2009 416	1806 41.8	23.554	70.343	9.8	2.4	
No 18	2009 419	$1941 \ 56.4$	23.544	70.307	15.9	2.7	
No 19	2009 419	$1950 \ 27.6$	23.564	70.443	22.5	2.5	
No 20	2009 422	$1543 \ 17.3$	23.470	70.397	24.0	2.6	
No 21	2009 422	2253 29.9	23.434	70.368	17.8	2.2	
No 22	2009 423	0540 44.9	23.392	70.329	22.5	2.1	
No 23	2009 423	2042 52.2	23.361	70.390	22.4	2.9	
No 24	2009 425	$0347 \ 23.3$	23.475	70.405	26.2	2.2	
No 25	2009 425	$0424\ 28.0$	23.382	70.352	24.7	2.5	
No 26	2009 425	$1046 \ 33.3$	23.476	70.153	15.9	2.7	
No 27	2009 425	$1526\ 28.9$	23.450	70.174	0.7	2.4	
No 28	2009 425	$1816\ 21.5$	23.449	70.445	15.5	2.4	
No 29	2009 425	$1900\ 50.4$	23.466	70.179	20.1	2.5	
No 30	2009 426	$1403\ 26.4$	23.458	70.415	20.3	2.2	
No 31	2009 427	$0752 \ 17.9$	23.373	70.383	20.2	2.3	
No 32	2009 428	$1914 \ 36.2$	23.324	70.259	13.9	2.3	
No 33	2009 429	$1525 \ 9.3$	23.381	70.236	35.5	2.5	
No 34	2009 429	$2254 \ 11.5$	23.534	70.433	19.6	2.3	
No 35	$2009\ 5\ 2$	$1602 \ 0.6$	23.546	70.430	24.3	2.4	
No 36	$2009\ 5\ 3$	$2103 \ 30.1$	23.461	70.109	28.8	2.7	
No 37	$2009\ 5\ 4$	0532 49.9	23.614	69.977	24.4	2.2	
No 38	2009 6 3	$2231 \ 16.3$	23.375	70.082	20.5	2.6	
No 39	$2009 \ 6 \ 5$	$0418\ 1.8$	23.578	70.428	22.6	2.6	
No 40	$2009 \ 6 \ 5$	$1135 \ 14.5$	23.428	70.245	24.9	2.4	
No 41	2009 6 6	$1027 \ 32.1$	23.543	70.233	10.0	2.4	
No 42	$2009 \ 6 \ 7$	$0833 \ 39.8$	23.423	70.357	28.9	3.1	
No 43	$2009 \ 6 \ 7$	$1125\ 51.2$	23.429	70.368	28.0	3.0	
No 44	2009 6 9	$0403 \ 31.9$	23.537	70.057	22.4	2.6	
No 45	2009 6 9	$1119\ 22.5$	23.452	70.335	24.0	2.3	
No 46	2009 6 9	2359 46.3	23.536	70.032	10.9	2.4	
No 47	2009 610	$1414 \ 24.2$	23.463	70.349	15.7	2.3	
No 48	$2009 \ 610$	$1541\ 26.2$	23.587	70.491	15.7	2.7	
No 49	2009 611	$2151 \ 21.8$	23.548	70.049	14.2	2.6	
No 50	$2009 \ 612$	0043 58.7	23.371	70.149	24.0	2.3	
No 51	$2009\ 614$	0534 38.1	23.419	70.133	18.0	2.4	
No 52	$2009 \ 621$	$0359 \ 47.9$	23.432	70.180	24.5	2.5	
No 53	$2009 \ 621$	$1856\ 14.5$	23.496	70.365	18.0	2.3	
No 54	2009 622	$0811 \ 34.3$	23.496	70.433	21.9	2.5	

Table 2. (Continued)

Ev. ass YearAhnDa (IIrMnSs) Lat. (°) Long. (°) (km) M_{er} No 55 2000 623 1043 8.3 23.482 70.286 17.0 2.7 No 57 2000 624 0119 29.1 23.505 70.021 18.3 2.3 No 58 2000 624 0236 45.4 23.758 70.432 18.6 3.2 No 60 2000 624 0354 82.1 23.888 70.397 21.5 3.2 No 61 2000 627 0301 12.8 23.489 70.394 9.5 3.3 No 63 2009 627 0311 12.8 23.489 70.394 9.5 3.3 No 64 2009 627 0311 12.8 23.492 70.384 9.5 3.3 No 65 2009 627 031 12.8 23.492 70.394 9.5 3.3 No 65 2009 627 031 12.8 23.492 70.394 9.5 3.3 No 65 2009 620 0532 45.2 23.600 70.494 12.6 2.1			Ori. time	Depth				
No 55 2006 623 1043 8.3 23.482 70.260 17.0 27.7 No 56 2009 624 019 281 22.505 70.201 18.3 23.3 No 58 2000 624 0236 45.4 23.755 70.462 16.6 2.7 No 59 2000 624 0236 45.4 23.758 70.308 8.6 2.9 No 60 2000 627 0051 1.9 23.489 70.394 9.5 3.3 No 63 2000 627 021 1.28 23.495 70.394 9.5 3.3 No 64 2000 627 17.37 55.2 23.497 70.188 15.3 2.7 No 65 2009 620 0030 40.5 23.409 70.205 21.1 3.3 No 67 2000 630 0054 8.9 23.510 70.409 15.8 2.5 No 70 2000 630 1266 4.45 23.400 70.309 14.4 2.5 No 74 2000 7.1 223.452 23.666 70.055 16.1 2.8 <t< th=""><th>Ev. nos</th><th>YearMnDa</th><th>(HrMnSs)</th><th>Lat. ($^{\circ}$)</th><th>Long. ($^{\circ}$)</th><th>(km)</th><th>M_w</th></t<>	Ev. nos	YearMnDa	(HrMnSs)	Lat. ($^{\circ}$)	Long. ($^{\circ}$)	(km)	M_w	
No 56 2009 623 2059 25.1 23.315 70.027 1.7.7 2.3.35 No 57 2009 624 019 29.1 23.305 70.261 18.3 23.35 No 58 2009 624 0236 45.4 23.758 70.462 18.6 2.7.3 No 60 2009 624 1538 42.1 23.388 70.308 8.6 2.9 No 61 2009 627 0166 37.7 23.495 70.304 9.5 3.3 No 63 2009 627 0211 12.8 23.495 70.304 9.5 3.3 No 64 2009 627 1737 55.2 23.381 70.202 29.1 3.2 No 66 2009 628 0630 0.5 23.402 70.350 21.1 3.3 No 68 2009 620 030 0.27 23.402 70.305 21.1 3.3 No 68 2009 620 030 0.24 23.407 70.169 16.0 2.7 No 68 2009 620 030 0.24 23.407 70.300 14.1 2.5 No 76 2009 71 223.2 23.600 70.300 14.1	No 55	2009 623	$1943 \ 8.3$	23.482	70.280	17.0	2.7	
No. 57 2009 624 0119 22.3.05 70.201 18.3 2.3.758 No. 58 2009 624 0044 56.6 23.405 70.132 18.6 3.2.758 No. 60 2009 624 0044 56.6 23.405 70.132 18.6 3.2.758 No. 61 2009 627 0.150 37.7 23.485 70.304 9.5 3.3.8 No. 62 2009 627 1345 36.0 23.497 70.188 15.3 2.7.7 No. 64 2009 627 1737 52.2 23.381 70.202 29.1 3.2 No. 66 2009 629 0030 27.4 23.407 70.169 16.0 2.7.8 No. 67 2009 630 0.051 8.9 23.417 70.169 16.0 2.8.7 No. 70 2009 7.5 1915 8.9 23.437 70.214 19.6 2.7.7 No. 76 2009	No 56	2009 623	2059 25.1	23.514	70.027	17.7	2.3	
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No 59 2009 624 1984 58.6 23.405 70.132 18.6 3.2 No 60 2009 625 0807 51.9 23.488 70.308 8.6 2.99 No 61 2009 627 0166 37.7 23.485 70.304 9.5 3.3 No 64 2009 627 1315 36.0 23.497 70.188 15.3 2.7 No 66 2009 627 1315 36.0 23.469 70.225 15.4 2.8 No 66 2009 628 0633 0.5 23.469 70.225 15.4 2.8 No 67 2009 630 027.4 23.417 70.169 16.0 2.7 No 69 2009 630 1252 2.2 23.60 70.085 16.1 2.8 No 71 2009 75 19.15 8.2 3.417 70.141 19.6 2.7 No 73 2009 71 123.9	No 58	2009 624	0236 45.4	23.758	70.462	16.6	2.7	
No 60 2009 624 1538 42.1 23.388 70.308 8.6 2.9 No 61 2009 627 0156 37.7 23.495 70.394 9.5 3.3 No 62 2009 627 0201 12.8 23.495 70.394 9.5 3.3 No 64 2009 627 1345 36.0 23.497 70.188 15.3 2.7 No 65 2009 628 6034 0.5 23.402 70.350 21.1 3.3 No 66 2009 628 0832 12.0 23.402 70.300 14.4 2.5 No 70 2009 630 0054 4.5 23.407 70.169 15.8 2.5 No 71 2009 630 1206 4.5 23.407 70.303 14.4 2.5 No 72 2009 7<1	No 59	2009 624	0944 58.6	23.405	70.132	18.6	3.2	
No 61 200 625 0807 51.9 23.489 70.397 21.5 3.2 No 62 2009 627 0156 37.7 23.495 70.394 14.7 3.0 No 64 2009 627 17345 36.0 23.497 70.188 15.3 2.7. No 66 2000 628 0603 40.5 23.469 70.225 15.4 2.8. No 67 2009 629 0630 23.410 70.409 16.0 2.7. No 68 2009 630 0034 4.9 23.510 70.409 16.0 2.7. No 70 2009 630 1266 44.5 23.490 70.330 14.4 2.5. No 71 2009 75 1915 8.9 23.473 70.411 19.6 2.7. No 74 2009 78 1128 3.4 2.5.640 70.221 16.1 2.3. No 75 2009 71 1224 85.2 23.433 70.158 16.6 3.1 No 75 2009 71 0224 85.2 23.443 70.314 12.3 2.5.	No 60	2009 624	$1538\ 42.1$	23.388	70.308	8.6	2.9	
No 62 2009 627 0166 37.7 23.495 70.394 9.5 3.3 No 63 2009 627 1345 56.0 23.497 70.188 15.3 2.7 No 65 2009 627 1347 55.2 23.381 70.202 29.1 3.2 No 66 2009 628 0603 40.5 23.402 70.350 21.1 3.3 No 67 2009 630 0051 8.9 23.510 70.409 15.8 2.5 No 71 2009 630 1206 4.5 23.490 70.330 14.4 2.5 No 71 2009 630 122.8 2.3.402 70.410 15.4 2.6 No 73 2009 7.8 1915 8.9 2.3.433 70.110 15.4 2.6 No 74 2009 7.8 1912 2.3.331 70.121 16.1 2.3 No 75 2009 71 1223	No 61	2009 625	0807 51.9	23.489	70.397	21.5	3.2	
No 63 2009 627 0201 12.8 23.489 70.394 14.7 30 No 64 2009 627 1345 36.0 23.497 70.188 15.3 2.7 No 66 2009 628 0632 12.0 23.402 70.350 21.1 3.3 No 68 2009 628 0632 12.0 23.402 70.350 21.1 3.3 No 68 2009 630 0054 8.9 23.510 70.409 16.0 2.7 No 70 2009 630 1252 23.2 23.506 70.085 16.1 2.8 No 71 2009 7 1915 8.9 23.473 70.211 16.1 2.3 No 74 2009 7.8 1128 3.4 23.640 70.221 16.1 2.3 No 75 2009 71 2345 2.3331 70.313 12.0 2.7 No 78 2009 713 052 <td>No 62</td> <td>2009 627</td> <td>$0156 \ 37.7$</td> <td>23.495</td> <td>70.394</td> <td>9.5</td> <td>3.3</td>	No 62	2009 627	$0156 \ 37.7$	23.495	70.394	9.5	3.3	
No 64 2009 627 1345 36.0 23.497 70.188 15.3 2.7 No 65 2009 628 0633 0.5 23.463 70.225 15.4 2.8 No 67 2009 628 0632 12.0 23.402 70.350 21.1 3.3 No 68 2000 630 0064 8.9 23.610 70.409 15.8 2.5 No 70 2009 630 1266 44.5 23.490 70.330 14.4 2.5 No 71 2009 75 1915 8.9 23.473 70.241 16.6 2.7 No 74 2009 78 0621 12.1 23.572 70.158 15.6 3.1 No 75 2009 71 1283 4.3 24.640 70.221 16.1 2.3 No 75 2009 713 0404 5.8 2.3.91 70.319 12.0 2.7 No 78 2009 711 <td>No 63</td> <td>2009 627</td> <td>0201 12.8</td> <td>23.489</td> <td>70.394</td> <td>14.7</td> <td>3.0</td>	No 63	2009 627	0201 12.8	23.489	70.394	14.7	3.0	
No 65 2009 627 1737 55.2 23.381 70.202 29.1 3.2 No 66 2009 628 0633 40.5 23.469 70.225 15.4 2.8 No 68 2009 629 0030 27.4 23.477 70.169 16.0 2.7 No 69 2009 630 0054 8.9 23.510 70.409 15.8 2.5 No 70 2009 630 1262 23.2 23.606 70.085 16.1 2.8 No 72 2009 7.5 1915 8.9 23.473 70.241 19.6 2.7 No 75 2009 7.8 1128 3.4 23.404 70.431 21.3 2.5 No 75 2009 7.8 1023 19.5 23.433 71.170 29.2 2.8 No 77 2009 71.3 0.404 5.8 23.391 70.314 1.3 2.6 No 78 2009 7	No 64	2009 627	$1345 \ 36.0$	23.497	70.188	15.3	2.7	
No 66 2009 628 0603 40.5 23.469 70.225 15.4 2.8 No 67 2009 629 0030 27.4 23.477 70.169 16.0 2.7 No 60 2009 630 0064 8.9 23.510 70.409 15.8 2.5 No 70 2009 630 1266 41.5 23.490 70.330 14.4 2.5 No 72 2009 71 2234 55.2 23.431 70.110 15.4 2.6 No 73 2009 78 0621 12.1 23.572 70.158 15.6 3.1 No 76 2009 710 1239 19.5 23.433 70.1170 29.2 2.8 No 77 2009 713 0.040 5.8 23.391 70.314 10.2 2.6 No 79 2009 713 0.040 5.8 23.391 <	No 65	2009 627	1737 55.2	23.381	70.202	29.1	3.2	
No672009628083212.023.40270.35021.13.3No682009630003027.423.47770.10916.02.7No69063000548.923.51070.40915.82.5No702009630120523.223.50670.08516.12.8No72200971223455.223.43170.11015.42.6No7320097519158.923.47370.24119.62.7No7420097811283.423.64070.22116.12.3No7620097811283.423.64070.21116.12.3No762009711123919.523.43371.17012.02.7No7720097130.0405.823.39170.31410.22.6No7820097130.0405.823.39170.31410.22.6No842009720194710.23.6670.42429.92.8No852009720194710.23.6670.42429.92.8No842009723172151.923.65770.04215.42.5No852009723172151.923.46570.34413.32.6 <t< td=""><td>No 66</td><td>2009 628</td><td>$0603 \ 40.5$</td><td>23.469</td><td>70.225</td><td>15.4</td><td>2.8</td></t<>	No 66	2009 628	$0603 \ 40.5$	23.469	70.225	15.4	2.8	
No 68 2009 629 0030 27.4 23.477 70.169 16.0 2.7 No 69 2009 630 1026 44.5 23.510 70.409 15.8 2.5 No 71 2009 630 1252 23.23 23.506 70.085 16.1 2.88 No 72 2009 75 1915 8.9 23.431 70.110 15.4 2.60 No 74 2009 78 0621 12.1 23.572 70.158 15.6 3.1 No 76 2009 710 1239 19.5 23.433 71.170 29.2 2.8 No 77 2009 711 2021 16.1 2.3 No 78 2009 713 0040 5.8 23.331 70.314 10.2 2.6 No 81 2009 713 0553 23.677 70.424 29.9 2.8	No 67	2009 628	0832 12.0	23.402	70.350	21.1	3.3	
No69200963000548.923.51070.40915.82.5No702009630120644.523.49070.33014.42.5No712009630125223.223.50670.08516.12.8No7320097519158.923.47370.24119.62.7No74200978012123.57270.15815.63.1No7520097811283.423.64070.22116.12.3No762009711222218.223.44470.43121.32.5No77200971300405.823.39170.31410.22.6No78200971300405.823.39170.31410.22.6No78200971300425.723.67770.42429.92.8No81200971910553.4.623.68070.52015.22.3No82200972119314.323.46570.49215.42.5No83200972307134.323.46570.49215.42.5No842009723071323.54770.03616.03.3No852009723172151.923.54770.03013.82.4No <td< td=""><td>No 68</td><td>2009 629</td><td>$0030 \ 27.4$</td><td>23.477</td><td>70.169</td><td>16.0</td><td>2.7</td></td<>	No 68	2009 629	$0030 \ 27.4$	23.477	70.169	16.0	2.7	
No702009630120644.523.49070.33014.42.5No712009630125223.2223.06070.08516.12.8No7220097519158.923.47370.24119.62.7No74200978062112.123.57270.15815.63.1No7520097811283.423.64070.22116.12.3No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No782009713053528.323.39170.31912.02.7No792009713053528.323.39170.31912.02.6No802009717092457.323.67770.42429.92.8No812009719105534.623.66070.52015.22.3No82200972119314.323.46570.49215.42.5No84200972307134.323.46570.49215.42.5No85200972512250.923.51370.30313.82.4No8820097261220.923.51370.6819.62.2 </td <td>No 69</td> <td>2009 630</td> <td>0054 8.9</td> <td>23.510</td> <td>70.409</td> <td>15.8</td> <td>2.5</td>	No 69	2009 630	0054 8.9	23.510	70.409	15.8	2.5	
No712009630125223.223.50670.08516.12.8No72200971223455.223.43170.11015.42.6No73200978062112.123.57270.15815.63.1No7520097811283.423.64070.22116.12.3No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No78200971300405.823.39170.31912.02.7No78200971300405.823.39170.31410.22.6No802009717092457.323.67770.42429.92.8No81200972019471.023.51770.34413.32.6No82200972019471.023.51770.34413.32.6No842009723172151.923.58770.09516.03.3No852009724123017.323.44670.34424.92.3No852009724123017.323.51370.33313.82.4No85200972823.1370.33423.22.5No <t< td=""><td>No 70</td><td>2009 630</td><td>$1206 \ 44.5$</td><td>23.490</td><td>70.330</td><td>14.4</td><td>2.5</td></t<>	No 70	2009 630	$1206 \ 44.5$	23.490	70.330	14.4	2.5	
No72200971223455.223.43170.11015.42.6No7320097519158.923.47370.24119.62.7No74200978062112.123.57270.15815.63.1No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No78200971300405.823.39170.31410.22.6No792009713005228.323.60770.42429.92.8No812009710192457.323.66770.43413.32.6No82200972019471.023.51770.34413.32.6No832009721193149.823.49070.22817.82.6No842009723071343.46570.49215.42.5No852009723172151.923.58770.09516.03.3No86200972412250.923.51370.33313.82.4No87200972612250.923.51370.3649.62.2No88200972717221.423.49070.05725.92.2<	No 71	2009 630	1252 23.2	23.506	70.085	16.1	2.8	
No7320097519158.923.47370.24119.62.7No74200978062112.123.57270.15815.63.1No7520097811283.423.64070.22116.12.3No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No782009713053528.323.39170.31910.22.6No802009719092457.323.67770.42429.92.8No812009719105534.623.68070.52015.22.3No82200972019471.023.51770.34413.32.6No832009721193149.823.49070.22817.82.6No84200972307134.323.46570.49215.42.5No852009724122017.323.51370.03313.82.4No86200972717221.423.49070.05725.92.2No892009728213816.423.81270.6779.82.3No84200972612250.33.1382.410.662.3	No 72	2009 7 1	2234 55.2	23.431	70.110	15.4	2.6	
No74200978062112.123.57270.15815.63.1No7520097811283.423.64070.22116.12.3No762009711222218.223.44371.17029.22.8No772009711222218.223.44470.43121.32.5No782009713063528.323.39170.31912.02.7No792009713053528.323.39170.31410.22.6No802009717092457.323.67770.42429.92.8No81200972019471.023.51770.43420.92.8No822009721193149.823.40070.22817.82.6No84200972307134.323.46570.49215.42.5No852009724123017.323.58770.09516.03.3No86200972817251.923.58770.03313.82.4No88200972717221.423.49070.05725.92.2No8020097280.2132.351370.30313.82.4No8820097280.2132.3570.19621.22.2 </td <td>No 73</td> <td>2009 7 5</td> <td>$1915 \ 8.9$</td> <td>23.473</td> <td>70.241</td> <td>19.6</td> <td>2.7</td>	No 73	2009 7 5	$1915 \ 8.9$	23.473	70.241	19.6	2.7	
No7520097.811283.423.64070.22116.12.3No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No78200971300405.823.39170.31410.22.6No792009717092457.323.67770.42429.92.8No812009719105534.623.68070.52015.22.3No82200972019471.023.51770.34413.32.6No84200972307134.323.46570.022817.82.6No85200972307134.323.46570.09216.03.3No862009724123017.323.46670.34424.92.3No87200972512250.923.51370.03313.82.4No882009728020711.323.45170.6779.82.3No892009728207117.323.48170.6779.82.3No9120098116527.123.48270.6779.82.3No9220098116527.123.48270.6779.82.3	No 74	2009 7 8	0621 12.1	23.572	70.158	15.6	3.1	
No762009710123919.523.43371.17029.22.8No772009711222218.223.44470.43121.32.5No78200971300405.823.39170.31411.20.22.7No792009713053528.323.39170.31411.20.22.6No802009717092457.323.67770.42429.92.8No81200972019471.023.51770.34413.32.6No832009721193149.823.49070.22817.82.6No84200972307134.323.46570.49215.42.5No852009724123017.323.44670.34424.92.3No86200972717221.423.49070.05725.92.2No88200972717221.423.49070.6779.82.3No812009728231816.423.81270.6779.82.3No902009728231816.423.81270.6779.82.3No9120098.1161527.123.45170.3832.45No9220098.3145224.1123.45170.66115.	No 75	2009 7 8	1128 3.4	23.640	70.221	16.1	2.3	
No772009711222218.223.44470.43121.32.5No782009713053528.323.39170.31912.02.7No792009713053528.323.39170.31410.22.6No802009717092457.323.67770.42429.92.8No812009719105534.623.68070.52015.22.3No82200972019471.023.51770.34413.32.6No84200972307134.323.46570.49215.42.5No852009723172151.923.58770.09516.03.3No86200972717221.423.49070.05725.92.2No88200972717221.423.49070.05725.92.2No89200972820711.323.45170.38819.72.5No90200981161527.123.45270.19621.22.2No92200981161527.123.45170.6819.62.2No9220098.1195317.323.81370.6819.62.2No9320098.2185235.823.49170.09223.32.5<	No 76	2009 710	1239 19.5	23.433	71.170	29.2	2.8	
No78200971300405.823.39170.31912.02.7No792009713053528.323.39170.31410.22.6No802009717092457.323.67770.42429.92.8No81200972019471.023.51770.34413.32.6No832009721193149.823.49070.22817.82.6No84200972307134.323.46570.49215.42.5No852009724123017.323.44670.34424.92.3No86200972512250.923.51370.30313.82.4No88200972717221.423.49070.57725.92.2No892009728231816.423.81270.6779.82.3No91200981161527.123.48270.19621.22.2No92200981161527.123.48270.19621.22.2No92200981161527.123.48270.19621.22.2No9220098.1161527.123.48270.19621.22.2No9320098.1161527.123.48270.19621.22.2<	No 77	2009 711	2222 18.2	23.444	70.431	21.3	2.5	
No792009713053528.323.39170.31410.22.6No802009717092457.323.67770.42429.92.8No812009719105534.623.68070.52015.22.3No82200972019471.023.51770.34413.32.6No83200972119314.323.46570.49215.42.5No85200972317134.323.46570.49215.42.5No862009724123017.323.58770.09516.03.3No862009724123017.323.44670.34424.92.3No87200972512250.923.51370.30313.82.4No88200972717221.423.49070.05725.92.2No89200972820711.323.45170.6779.82.3No91200981161527.123.48270.19621.22.2No92200981161527.123.48170.6819.62.2No9220098.3175128.624.31569.81114.43.2No9420098.3175128.624.31569.81114.43.2 </td <td>No 78</td> <td>2009 713</td> <td>0040 5.8</td> <td>23.391</td> <td>70.319</td> <td>12.0</td> <td>2.7</td>	No 78	2009 713	0040 5.8	23.391	70.319	12.0	2.7	
No802009717092457.323.67770.42429.92.8No812009719105534.623.68070.52015.22.3No82200972019471.023.51770.34413.32.6No832009721193149.823.49070.22817.82.6No84200972307134.323.46570.49215.42.5No852009723172151.923.58770.09516.03.3No862009724123017.323.44670.34424.92.3No87200972512250.923.51370.09516.03.3No88200972717221.423.49070.05725.92.2No892009728231816.423.81270.6779.82.3No91200981161527.123.48270.19621.22.2No92200983145224.123.47470.26115.62.3No9420098.3145224.123.47470.26115.62.3No9520098.3145224.31569.81114.43.2No9620098.5041829.523.49170.38323.02.4 <t< td=""><td>No 79</td><td>2009 713</td><td>0535 28.3</td><td>23.391</td><td>70.314</td><td>10.2</td><td>2.6</td></t<>	No 79	2009 713	0535 28.3	23.391	70.314	10.2	2.6	
No 812009 7191055 34.623.68070.52015.22.3No 822009 7201947 1.023.51770.34413.32.6No 832009 7211931 49.823.49070.22817.82.6No 842009 7231721 51.923.58770.09516.03.3No 852009 7241230 17.323.44670.34424.92.3No 862009 7251225 0.923.51370.30313.82.4No 872009 7251225 0.923.51370.30313.82.4No 882009 7271722 1.423.49070.05725.92.2No 892009 7282011 1.323.45170.6779.82.3No 902009 728218 16.423.81270.6779.82.3No 912009 8 11953 17.323.48270.19621.22.2No 922009 8 11953 17.323.47470.26115.62.3No 942009 8 31751 28.624.31569.81114.43.2No 952009 8 50418 29.523.49170.38323.02.4No 972009 8 60204 41.423.45370.15814.92.5No 982009 8 70415 53.123.46670.38225.32.3No 992009 8 70415 53.123.46670.38225.32.3No 992009 8 60204 41.423.45370.15814.92.5No	No 80	2009 717	0924 57.3	23.677	70.424	29.9	2.8	
No 82 2009 720 1947 1.0 23.517 70.344 13.3 2.6 No 83 2009 721 1931 49.8 23.490 70.228 17.8 2.6 No 84 2009 723 0713 4.3 23.465 70.492 15.4 2.5 No 85 2009 724 1230 17.3 23.587 70.095 16.0 3.3 No 86 2009 725 1225 0.9 23.513 70.303 13.8 2.4 No 88 2009 727 1722 1.4 23.490 70.057 25.9 2.2 No 89 2009 728 0207 11.3 23.4151 70.368 19.7 2.5 No 90 2009 728 0207 11.3 23.812 70.677 9.8 2.3 No 91 2009 81 1615 27.1 23.482 70.196 21.2 2.2 No 92 2009 81 1953 17.3 23.813 70.681 9.6 2.2 No 92 2009 83 1751 28.6 24.415 69.811 14.4 3.2 No 95 2009 8.5 0418 29.5 23.491 70.383 23.0 <	No 81	2009 719	1055 34.6	23.680	70.520	15.2	2.3	
No83209721193149.823.49070.22817.82.6No84200972307134.323.46570.49215.42.5No852009723172151.923.58770.09516.03.3No862009724123017.323.44670.34424.92.3No87200972512250.923.51370.30313.82.4No88200972717221.423.49070.05725.92.2No892009728231816.423.81270.6779.82.3No91200981161527.123.48270.19621.22.2No92200981161527.123.48270.19621.22.2No92200981161527.123.48270.19621.22.2No92200981161527.123.48270.19621.22.2No9320098.115523.49170.08820.62.32.3No9420098.3175128.624.31569.81114.43.2No9520098.5041829.523.49170.38323.02.4No9620098.5041829.523.49170.38323.02.5 <td>No 82</td> <td>2009 720</td> <td>$1947 \ 1.0$</td> <td>23.517</td> <td>70.344</td> <td>13.3</td> <td>2.6</td>	No 82	2009 720	$1947 \ 1.0$	23.517	70.344	13.3	2.6	
No84200972307134.323.46570.49215.42.5No852009723172151.923.58770.09516.03.3No862009724123017.323.44670.34424.92.3No87200972512250.923.51370.03313.82.4No88200972717221.423.49070.05725.92.2No892009728201711.323.45170.38819.72.5No902009728231816.423.81270.6779.82.3No9120098.1161527.123.48270.19621.22.2No9220098.1195317.323.81370.6819.62.2No9320098.2185235.823.49170.09223.32.5No9420098.3175128.624.31569.81114.43.2No9520098.3175128.624.31569.81114.43.2No9620098.5041829.523.49170.38323.02.4No9720098.6020441.423.45370.15814.92.5No9820098.7041553.123.540170.34723.6 <td< td=""><td>No 83</td><td>2009 721</td><td>1931 49.8</td><td>23.490</td><td>70.228</td><td>17.8</td><td>2.6</td></td<>	No 83	2009 721	1931 49.8	23.490	70.228	17.8	2.6	
No 85 2009 723 1721 51.9 23.587 70.095 16.0 3.3 No 86 2009 724 1230 17.3 23.446 70.344 24.9 2.3 No 87 2009 725 1225 0.9 23.513 70.303 13.8 2.4 No 88 2009 727 1722 1.4 23.490 70.057 25.9 2.2 No 89 2009 728 2318 16.4 23.812 70.677 9.8 2.3 No 91 2009 81 1615 27.1 23.482 70.196 21.2 2.2 No 92 2009 81 1953 17.3 23.481 70.681 9.6 2.2 No 93 2009 82 1852 35.8 23.491 70.092 23.3 2.5 No 94 2009 8.3 1452 24.1 23.474 70.261 15.6 2.3 No 95 2009 8.5 0418 29.5 23.491 70.383 23.0 2.4 No 97 2009 8.6 0204 41.4 23.453 70.158 14.9 2.5 No 99 2009 8.7 0415 53.1 23.466 70.382 25.3	No 84	2009 723	0713 4.3	23.465	70.492	15.4	2.5	
No 86 2009 724 1230 17.3 23.446 70.344 24.9 2.3 No 87 2009 725 1225 0.9 23.513 70.303 13.8 2.4 No 88 2009 727 1722 1.4 23.490 70.057 25.9 2.2 No 89 2009 728 0207 11.3 23.451 70.388 19.7 2.5 No 90 2009 728 2318 16.4 23.812 70.677 9.8 2.3 No 91 2009 81 1953 17.3 23.481 70.681 9.6 2.2 No 92 2009 81 1953 17.3 23.813 70.681 9.6 2.2 No 93 2009 82 1852 35.8 23.491 70.092 23.3 2.5 No 94 2009 83 1452 24.1 23.474 70.261 15.6 2.3 No 95 2009 85 0418 29.5 23.491 70.383 23.0 2.4 No 97 2009 86 0204 41.4 23.453 70.158 14.9 2.5 No 99 2009 87 0415 53.1 23.466 70.382 25.3 2	No 85	2009 723	$1721 \ 51.9$	23.587	70.095	16.0	3.3	
No 872009 200972512250.923.51370.30313.82.4No 882009 200972717221.423.49070.05725.92.2No 892009 2009728231816.423.81270.6779.82.3No 902009 2009728231816.423.81270.6779.82.3No 912009 200981161527.123.48270.19621.22.2No 922009 200981195317.323.81370.6819.62.2No 932009 200982185235.823.49170.09223.32.5No 942009 200983145224.123.47470.26115.62.3No 952009 200983175128.624.31569.81114.43.2No 962009 200985041829.523.49170.38323.02.4No 972009 200986020441.423.45370.15814.92.5No 982009 200987041553.123.46670.38225.32.3No 992009 200981055422.823.74170.47012.02.4No 1012009 200981717286.623.54370.24220.32.4No 1022009 200981717	No 86	2009 724	1230 17.3	23.446	70.344	24.9	2.3	
No 88 2009 727 1722 1.4 23.490 70.057 25.9 2.2 No 89 2009 728 0207 11.3 23.451 70.388 19.7 2.5 No 90 2009 728 2318 16.4 23.812 70.677 9.8 2.3 No 91 2009 81 1615 27.1 23.482 70.196 21.2 2.2 No 92 2009 81 1953 17.3 23.813 70.681 9.6 2.2 No 93 2009 8.2 1852 35.8 23.491 70.092 23.3 2.5 No 94 2009 8.3 1751 28.6 24.315 69.811 14.4 3.2 No 96 2009 8.5 0418 29.5 23.491 70.383 23.0 2.4 No 97 2009 8.6 0201 36.8 23.40	No 87	2009 725	$1225 \ 0.9$	23.513	70.303	13.8	2.4	
No892009728020711.323.45170.38819.72.5No902009728231816.423.81270.6779.82.3No91200981161527.123.48270.19621.22.2No92200981195317.323.81370.6819.62.2No9320098.2185235.823.49170.09223.32.5No9420098.3145224.123.47470.26115.62.3No9520098.3175128.624.31569.81114.43.2No9620098.5041829.523.49170.38323.02.4No9720098.6020441.423.45370.15814.92.5No9820098.7041553.123.46670.38225.32.3No9920098.8020136.823.40170.34723.63.1No10020098.11063144.523.52170.1958.92.3No10120098.11063144.523.52170.1958.92.3No10220098.16101352.723.55070.29518.02.5No10320098.1717286.623.54370.41220.3 <td>No 88</td> <td>2009 727</td> <td>$1722 \ 1.4$</td> <td>23.490</td> <td>70.057</td> <td>25.9</td> <td>2.2</td>	No 88	2009 727	$1722 \ 1.4$	23.490	70.057	25.9	2.2	
No902009728231816.423.81270.6779.82.3No91200981161527.123.48270.19621.22.2No92200981195317.323.81370.6819.62.2No9320098.2185235.823.49170.09223.32.5No9420098.3145224.123.47470.26115.62.3No9520098.3175128.624.31569.81114.43.2No9620098.5041829.523.49170.38323.02.4No9720098.6020441.423.45370.15814.92.5No9820098.7041553.123.46670.38225.32.3No9920098.8020136.823.40170.34723.63.1No1002009811063144.523.52170.1958.92.3No1012009816101352.723.55070.29518.02.5No103200981717286.623.54370.21123.82.6No1042010131124358.823.42370.21123.82.6No10520102151155.723.58170.37625.9 <td< td=""><td>No 89</td><td>2009 728</td><td>0207 11.3</td><td>23.451</td><td>70.388</td><td>19.7</td><td>2.5</td></td<>	No 89	2009 728	0207 11.3	23.451	70.388	19.7	2.5	
No 912009 8 11615 27.123.48270.19621.22.2No 922009 8 11953 17.323.81370.6819.62.2No 932009 8 21852 35.823.49170.09223.32.5No 942009 8 31452 24.123.47470.26115.62.3No 952009 8 31751 28.624.31569.81114.43.2No 962009 8 50418 29.523.49170.38323.02.4No 972009 8 60204 41.423.45370.15814.92.5No 982009 8 70415 53.123.46670.38225.32.3No 992009 8 80201 36.823.40170.34723.63.1No 1002009 8110554 22.823.74170.1958.92.3No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.41220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 21511 55.723.58170.37625.92.4No 1062010 240447 49.824.10169.88215.72.8No 1062010 240512 2.923.41370.25626.42.6	No 90	2009 728	2318 16.4	23.812	70.677	9.8	2.3	
No9220098 1195317.323.81370.6819.62.2No9320098 2185235.823.49170.09223.32.5No9420098 3145224.123.47470.26115.62.3No9520098 3175128.624.31569.81114.43.2No9620098 5041829.523.49170.38323.02.4No9720098 6020441.423.45370.15814.92.5No9820098 7041553.123.46670.38225.32.3No9920098 8020136.823.40170.34723.63.1No1002009811055422.823.74170.1958.92.3No1012009811063144.523.52170.1958.92.3No1022009816101352.723.55070.29518.02.5No103200981717286.623.54370.21123.82.6No1042010131124358.823.42370.21123.82.6No10520102151155.723.58170.37625.92.4No10620102151155.723.58170.23625.9<	No 91	2009 8 1	1615 27.1	23.482	70.196	21.2	2.2	
No 93 2009 8 2 1852 35.8 23.491 70.092 23.3 2.5 No 94 2009 8 3 1452 24.1 23.474 70.261 15.6 2.3 No 95 2009 8 3 1751 28.6 24.315 69.811 14.4 3.2 No 96 2009 8 5 0418 29.5 23.491 70.383 23.0 2.4 No 97 2009 8 6 0204 41.4 23.453 70.158 14.9 2.5 No 98 2009 8 7 0415 53.1 23.401 70.347 23.6 3.1 No 100 2009 8 11 0554 22.8 23.741 70.470 12.0 2.4 No 101 2009 811 0631 44.5 23.521 70.195 8.9 2.3 No 102 2009 816 1013 52.7 23.550 70.295 18.0 2.5 No 103 2009 817 1728 6.6 23.543 70.412 20.3 2.4 No 104 2010 131 1243 58.8 23.423 70.211 23.8 2.6 No 105 2010 2 2 1511 55.7 23.581 70.376 25.9	No 92	2009 8 1	$1953 \ 17.3$	23.813	70.681	9.6	2.2	
No 94 2009 & 3 1452 24.1 23.474 70.261 15.6 2.3 No 95 2009 & 3 1751 28.6 24.315 69.811 14.4 3.2 No 96 2009 & 8.5 0418 29.5 23.491 70.383 23.0 2.4 No 97 2009 & 8.6 0204 41.4 23.453 70.158 14.9 2.5 No 98 2009 & 8.7 0415 53.1 23.466 70.382 25.3 2.3 No 99 2009 & 8.8 0201 36.8 23.401 70.470 12.0 2.4 No 100 2009 811 0554 22.8 23.741 70.470 12.0 2.4 No 101 2009 811 0631 44.5 23.521 70.195 8.9 2.3 No 102 2009 816 1013 52.7 23.550 70.295 18.0 2.5 No 103 2009 817 1728 6.6 23.543 70.442 20.3 2.4 No 104 2010 131 1243 58.8 23.423 70.211 23.8 2.6 No 105 2010 2 1511 55.7 23.581 70.376 <td< td=""><td>No 93</td><td>2009 8 2</td><td>$1852 \ 35.8$</td><td>23.491</td><td>70.092</td><td>23.3</td><td>2.5</td></td<>	No 93	2009 8 2	$1852 \ 35.8$	23.491	70.092	23.3	2.5	
No9520098.3175128.624.31569.81114.43.2No9620098.5041829.523.49170.38323.02.4No9720098.6020441.423.45370.15814.92.5No9820098.7041553.123.46670.38225.32.3No9920098.8020136.823.40170.34723.63.1No1002009811055422.823.74170.47012.02.4No1012009811063144.523.52170.1958.92.3No1022009816101352.723.55070.29518.02.5No103200981717286.623.54370.44220.32.4No1042010131124358.823.42370.21123.82.6No10520102151155.723.58170.37625.92.4No10620102151155.723.58170.37625.92.4No106201024044749.824.10169.88215.72.8No10720102405122.923.41370.25626.42.6	No 94	2009 8 3	$1452 \ 24.1$	23.474	70.261	15.6	2.3	
No 962009 8 50418 29.523.49170.38323.02.4No 972009 8 60204 41.423.45370.15814.92.5No 982009 8 70415 53.123.46670.38225.32.3No 992009 8 80201 36.823.40170.34723.63.1No 1002009 8110554 22.823.74170.47012.02.4No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 95	2009 8 3	1751 28.6	24.315	69.811	14.4	3.2	
No 972009 8 60204 41.423.45370.15814.92.5No 982009 8 70415 53.123.46670.38225.32.3No 992009 8 80201 36.823.40170.34723.63.1No 1002009 8110554 22.823.74170.47012.02.4No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 96	2009 8 5	0418 29.5	23.491	70.383	23.0	2.4	
No 982009 8 70415 53.123.46670.38225.32.3No 992009 8 80201 36.823.40170.34723.63.1No 1002009 8110554 22.823.74170.47012.02.4No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 97	2009 8 6	0204 41.4	23.453	70.158	14.9	2.5	
No 992009 8 80201 36.823.40170.34723.63.1No 1002009 8110554 22.823.74170.47012.02.4No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 98	2009 8 7	0415 53.1	23.466	70.382	25.3	2.3	
No 1002009 8110554 22.823.74170.47012.02.4No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 99	2009 8 8	0201 36.8	23.401	70.347	23.6	3.1	
No 1012009 8110631 44.523.52170.1958.92.3No 1022009 8161013 52.723.55070.29518.02.5No 1032009 8171728 6.623.54370.44220.32.4No 1042010 1311243 58.823.42370.21123.82.6No 1052010 2 21511 55.723.58170.37625.92.4No 1062010 2 40447 49.824.10169.88215.72.8No 1072010 2 40512 2.923.41370.25626.42.6	No 100	2009 811	0554 22.8	23.741	70.470	12.0	2.4	
No 102 2009 816 1013 52.7 23.550 70.295 18.0 2.5 No 103 2009 817 1728 6.6 23.543 70.442 20.3 2.4 No 104 2010 131 1243 58.8 23.423 70.211 23.8 2.6 No 105 2010 2 2 1511 55.7 23.581 70.376 25.9 2.4 No 106 2010 2 4 0447 49.8 24.101 69.882 15.7 2.8 No 107 2010 2 4 0512 2.9 23.413 70.256 26.4 2.6	No 101	2009 811	0631 44.5	23.521	70.195	8.9	2.3	
No 103 2009 817 1728 6.6 23.543 70.442 20.3 2.4 No 104 2010 131 1243 58.8 23.423 70.211 23.8 2.6 No 105 2010 2 2 1511 55.7 23.581 70.376 25.9 2.4 No 106 2010 2 4 0447 49.8 24.101 69.882 15.7 2.8 No 107 2010 2 4 0512 2.9 23.413 70.256 26.4 2.6	No 102	2009 816	1013 52.7	23.550	70.295	18.0	2.5	
No 104 2010 131 1243 58.8 23.423 70.211 23.8 2.6 No 105 2010 2 1511 55.7 23.581 70.376 25.9 2.4 No 106 2010 2 0447 49.8 24.101 69.882 15.7 2.8 No 107 2010 2 0512 2.9 23.413 70.256 26.4 2.6	No 103	2009 817	1728 6.6	23.543	70.442	20.3	2.4	
No 105 2010 2 1511 55.7 23.581 70.376 25.9 2.4 No 106 2010 2 0447 49.8 24.101 69.882 15.7 2.8 No 107 2010 2 0512 2.9 23.413 70.256 26.4 2.6	No 104	2010 131	1243 58.8	23.423	70.211	23.8	2.6	
No 106 2010 2 4 0447 49.8 24.101 69.882 15.7 2.8 No 107 2010 2 4 0512 2.9 23.413 70.256 26.4 2.6	No 105	2010 2 2	1511 55.7	23.581	70.376	25.9	2.4	
No 107 2010 2 4 0512 2.9 23.413 70.256 26.4 2.6	No 106	2010 2 4	0447 49.8	24.101	69.882	15.7	2.8	
	No 107	2010 2 4	0512 2.9	23.413	70.256	26.4	2.6	
No 108 2010 2 5 1514 37.6 23.505 70.247 16.1 3.1	No 108	$2010\ 2\ 5$	1514 37.6	23.505	70.247	16.1	3.1	

Table 2. (Continued)

		Ori. time			Depth	
Ev. nos	YearMnDa	(HrMnSs)	Lat. ($^{\circ}$)	Long. ($^{\circ}$)	(km)	M_w
No 109	2010 2 7	1244 28.0	23.496	70.475	22.2	3.3
No 110	2010 2 7	$2240\ 16.0$	23.488	70.420	20.4	2.3
No 111	2010 2 8	0954 49.9	23.504	70.493	20.7	2.1
No 112	2010 211	0906 56.7	23.474	70.136	24.4	2.1
No 113	2010 211	$1713 \ 1.8$	23.352	70.399	21.5	2.2
No 114	2010 211	$1719 \ 29.5$	23.488	70.113	20.5	2.6
No 115	$2010\ 212$	$1422 \ 31.3$	23.544	70.265	13.3	2.8
No 116	$2010\ 212$	$1532\ 18.6$	23.427	70.188	31.3	2.4
No 117	$2010\ 212$	$2132 \ 13.7$	24.711	70.712	21.2	2.8
No 118	$2010\ 213$	$0005 \ 43.9$	23.538	70.205	16.0	2.1
No 119	$2010\ 215$	0054 44.5	23.548	70.373	16.6	3.3
No 120	$2010\ 215$	0329 42.8	23.539	70.077	0.9	2.2
No 121	$2010\ 215$	$1626 \ 20.6$	23.464	70.334	27.6	2.0
No 122	$2010\ 218$	$1255\ 54.8$	23.397	70.322	19.0	2.2
No 123	$2010\ 219$	$0900 \ 0.7$	23.397	70.330	33.6	2.2
No 124	$2010\ 219$	2101 39.7	23.471	70.161	23.6	2.2
No 125	2010 220	$0726 \ 6.7$	23.416	70.443	19.6	2.2
No 126	$2010\ 221$	0238 49.3	23.479	70.428	17.7	2.6
No 127	$2010\ 224$	$1405\ 52.1$	23.579	70.256	9.9	2.1
No 128	$2010\ 224$	$1838 \ 6.9$	23.348	70.540	16.7	2.3
No 129	2010 225	$0604 \ 25.3$	23.404	70.418	21.1	2.7
No 130	2010 225	$1011 \ 36.6$	23.388	70.231	9.9	2.6
No 131	2010 225	$1428\ 16.5$	23.400	70.365	21.0	3.2
No 132	$2010\ 3\ 1$	$0925\ 18.9$	23.248	70.228	14.0	3.4
No 133	$2010 \ 3 \ 6$	$1748 \ 29.8$	23.392	70.307	32.1	2.4
No 134	$2010 \ 310$	$0344 \ 3.7$	23.391	70.365	21.6	2.6
No 135	$2010 \ 310$	$1514\ 17.0$	23.432	70.254	26.0	2.4
No 136	$2010 \ 310$	$1638 \ 22.7$	23.602	70.062	15.0	2.6
No 137	$2010 \ 310$	$2001 \ 46.5$	23.471	70.193	18.9	2.4
No 138	$2010 \ 311$	0034 49.2	23.599	70.408	25.3	2.5
No 139	$2010\ 4\ 2$	$1831 \ \ 33.6$	23.519	70.315	18.6	2.2
No 140	2010 4 6	$1256\ 41.9$	23.398	70.340	23.8	2.6
No 141	2010 4 8	$1517\ 50.3$	23.322	70.198	30.8	2.4
No 142	$2010\ 4\ 8$	$1654\ 54.0$	23.589	70.526	9.1	2.2
No 143	2010 411	$1758 \ 39.9$	23.521	70.403	16.5	2.3
No 144	2010 411	2258 47.2	23.477	70.183	19.5	2.3

(figure 2a). The N-S hypocentral depth distribution of aftershocks suggests a marked concentration along the south dipping NWF (figure 2b). The upward projection of this south-dipping plane (i.e., NWF, North Wagad Fault) touches the ground surface at Burudia village ($\sim 23.6^{\circ}$ N) and extending along Wagad uplift (figure 2c). This result is in good agreement with the geological trenching data of McCaplin and Thakkar (2001). The strike of the aftershock zone agrees well with the south-dipping E–W striking nodal plane of the mainshock (Mandal and Horton 2007). However, the E–W cross section shows a marked change $(\sim 10-15 \text{ km})$ in seismogenic depth across the main rupture zone of the 2001 Bhuj mainshock (figure 2c). This change in seismogenic change could

be attributed to the lateral variation in maficness across the main rupture zone (Mandal and Pandey 2010).

6. Methodology for estimating earthquake source parameters

First, we compute the S-spectra using the inbuilt program of SEISAN software (Havskov and Ottemoller 2003), where no-correction for the Q is applied. Next, these spectra are used as input data for the Fletcher's simultaneous inversion technique for estimating earthquake source parameters and crustal Q values (Fletcher 1995). However, here we used the Lavenberg–Marquart



Figure 2. (a) Epicenteral locations of the 136 selected aftershocks ($M_w 2.1-3.4$), which have occurred in the Kachchh seismic zone during March 2009 to March 2010, are shown by grey open circles. Epicentral locations of six selected 2001 aftershocks ($M_w 3.3-4.4$) and two selected 2006 aftershocks ($M_w 4.8-5.1$) are also shown. And, small grey open circles mark aftershocks with $M_w 1.1-2.9$ while medium grey open circles mark the epicenters of aftershocks with $M_w 3-3.9$. And, medium black open circles are showing the epicenters of aftershocks with $M_w 4.0-4.8$. The inferred causative faults are shown by grey dotted lines and are marked as NWF (North Wagad Fault) and GF (Gedi fault), respectively. The solid large grey circle shows the epicenter of the 2001 Bhuj mainshock of $M_w 7.7$ while large open black circle shows the event having highest magnitude ($\sim M_w 5.1$) in this study. (b) Hypocentral depth plots of selected 144 earthquakes in E–W direction. And, the dotted grey line marks the causative NWF. (c) Hypocentral depth plots of the selected earthquakes in N–S direction. Grey dotted lines mark the change in seismogenic depth.

inversion method instead of singular value decomposition technique as used by Fletcher (1995). This two-stage technique is discussed below:

6.1 Two-stage technique to estimate earthquake source parameters and crustal Q values

In the first stage, we estimate the displacement Swave spectra from the horizontal components of the three-component digital recording, using spectral technique in-built in the SEISAN software (Havskov and Ottemoller 2003). After obtaining the required spectra with low noise level (S/N ratio is high enough), we use it as the input data for the Levenberg–Marquadt inversion modelling. The Levenberg–Marquadt algorithm combines beneficial aspects of gauss Newton and steepest descend methods, which facilitates the faster convergence of the solution. First, we select the initial guessed values for corner frequency and long period spectral level from the respective spectra. Next, we use these initial values to calculate the inverted spectra using the ω -square source spectral model. Then, a normalized difference between inverted and observed spectra is calculated. The iteration continues until this difference converges to a minimum value, which gives a better visual fit between observed and inverted displacement spectra that provides us the required model parameters, i.e., corner frequency, long-period spectral level and crustal Q values. Finally, using these model parameters, we calculate the other source parameters like source radius, static stress drop, seismic moment and moment magnitude, using empirical relations.

6.2 Inversion procedure

Taking the attenuation factor in to account the spectral amplitudes at a distance R from the source can be written as:

$$A(f, R) = \left(A_0/R^{-\lambda}\right)\exp\left(\pi R f/Q_0 V_s\right) \quad (1)$$

where A_0 is the amplitude at source, Q_0 is the dimensionless frequency independent S wave quality factor, f is the frequency, λ is the geometrical spreading and V_s is the S wave velocity. The frequency independent Q_0 is assumed in this analysis because it is the best fit for datasets (Boatwright *et al.* 1991; Atkinson and Mereu 1992; Fletcher 1995).

The exponential term can be written as:

$$\pi r f / Q_0 V_s = 1/2 * 2 \left(\pi R f / Q_0 V_s \right) = \omega t^* / 2$$

where $t^* = R / Q_0 V_s$ (2)

where V_s is constant.

The equation (1) can be linearised by taking natural logarithm of both sides.

$$\ln A(f, R) = \ln A_0 - \lambda \ln R - \omega t^*/2.$$
 (3)

At this point we assumed that λ equals to 1 to simplify the algebra (Fletcher 1995). Now following Boatwright (1980), A_0 , the source term for S-waves (high frequency fall-off (γ) = 2) can be written as:

$$A_{0} = \Pi_{0} / \left[1 + (f/f_{c})^{2\gamma} \right]^{1/2}$$

= $\Pi_{0} / \left[1 + (f/f_{c})^{4} \right]^{0.5}$
= $(\Pi_{0} / B_{4}^{0.5}).$ (4)

Substitution of equation (4) into equation (3) yields:

$$\ln A(f,R) = \ln \Pi_0 / \left[1 + (f/f_c)^4\right]^{0.5} - \ln R - \omega t^*/2.$$
(5)

The B_4 term is expanded in a Taylor series as a Newton–Raphson's method for finding roots of non-linear equations (Press *et al.* 1992) and yields the final equation:

$$A(f) = \ln \Pi_0 - 0.5 \ln B_4 + 2B_4^{-1} (f/f_c)^4 (\Delta f_c/f_c) - \omega t^*/2.$$
(6)

 $^{\prime}R^{\prime}$ term is dropped because of the fact that the formula for moment is corrected from the geometrical spreading effect. Using least-squares algorithm with several iterations solves the model parameters.

The error is minimized in least squares sense by solving

$$\mathbf{D} = \mathbf{G}\mathbf{M}.\tag{7}$$

The model parameter matrix M, sensitivity matrix G and data matrix D are

$$M = [\ln \Pi_0, t^*, \Delta f_c]^T,$$

$$G = [1, -\omega/2, 2 B_4^{-1} (f/f_c)^4 / f_c]$$

and

$$D = [A(f) + 0.5 \ln B_4]$$
(8)

Using Newton's method for quasi-linear equation

$$\Delta \mathbf{M} = \left(\mathbf{G}^{\mathrm{T}}\mathbf{G}\right)^{-1}\mathbf{G}^{\mathrm{T}}\Delta\mathbf{D}$$
(9)

where, ΔM is the change in model parameters and ΔD is the difference between predicted data and observed data. The solution is found iteratively $M_k = M_0 + \Delta M_{k-1}$ where M_0 is the initial model. Because the sensitivity matrix is near to singular here. We used Marquart–Lavenberg inversion technique to estimate the ln Π_0 , t^* and Δf_c with 10 iterations. In the Marquart–Lavenberg inversion technique, it can be written as:

$$\Delta \mathbf{M} = \left(\mathbf{G}^{\mathrm{T}}\mathbf{G} + \lambda \mathbf{I}\right)^{-1} \mathbf{G}^{\mathrm{T}} \Delta \mathbf{D}$$
(10)

where ΔD is the difference between the predicted and observed data, λ is Levenberg–Marquardt adjustable damping parameter and I is the identity matrix. The Levenberg–Marquardt method is selected because (i) it combines beneficial aspects of Gauss–Newton and gradient methods while avoiding some of their weaknesses, (ii) the solution converges quickly, and (iii) in many cases a standard guess works well. In this study, λ value varies from 1 to 500.

The inversion begins with the initial guessed value of the model parameter (M_0) ; that is, corner frequency f_c , t^* and seismic moment M_0 . The initial guessed value of $f_{\rm c}$ was set at 0.1 Hz for all events, while that of M_0 was selected visually from the respective low-frequency spectral level. And, the initial guessed value of t^* is calculated using the equation (2) (i.e., $t^* = R/Q_o V_s$, where R is the epicentral distance (in km). And for the Kachchh region, Q_o considers to be 102 while Vs assumes to be 3.5 km/s). At each iteration, the normalized difference between the computed spectra obtained from the theoretical formula and that yielded from equation (5) was computed. The maximum and minimum expected values of such difference were preset at the start of the iteration. The maximum difference was selected from the initial guessed values of M_0 , t^* and f_c , and the minimum value was set based on the accuracy of the M_0 , t^* and f_c values that one can expect to obtain from the inversion of noisy data. We also assign an initial value to λ , say 0.001. By substituting these initial guessed values into equation (10), the change in model parameter vector, ΔM , is derived. In the next iterations, a new model parameter is computed according to $M_{r+1} = M_r +$ ΔM_r , where M_r and ΔM_r are the model parameters and change in parameter values at the rth iteration.

7. Estimation of source parameters

After obtaining model parameters from the abovementioned inversion technique source parameters like moment, source radius and stress drop are estimated using some empirical equations. These equations are:

Seismic Moment
$$(M_0) = 4\pi\rho V_s^3 R\rho \Pi_0 / PFR_{\theta\phi}$$

(Brune 1970) (11)

Source Radius
$$(r) = (2.34 * V_s) / (2\pi f_c)$$

(Brune 1970) (12)

Stress Drop
$$(\Delta \sigma) = (7/16) * (M_0/r^{**3})$$

(Keilis-Borok 1959) (13)

where V_s and ρ' are the S wave velocity in m/s and rock density in gm/cm^3 at the source, respectively. Here, we calculate ' ρ ' in kg /m³ from Vp =[$(0.32V_p + 0.77)$], where V_p is P-wave velocity in km/s] (Berteusen 1977). R denotes the hypocentral distance of the station in meters. 'R' is appearing in equation (11) to account for geometrical spreading term (1/R) in predicting ground motion for dominance of body waves for $R \leq 100$ km $(\approx \text{roughly twice the crustal thickness})$ (Hermann 1985). A 'P' factor of $(1/\sqrt{2})$ accounting for the partitioning of energy in the two horizontal components and a free surface amplification factor (F) of 2 are used to estimate M_0 . And the radiation factor $(\mathbf{R}_{\theta\phi})$ is considered to be 0.55 for the Kachchh region (Mandal and Johnston 2006), where deformation mode is mainly dominated by reverse faulting. The estimated ' M_0 ', 'r' and ' $\Delta \sigma$ ' are in 'Nm', 'm', and 'MPa', respectively. And, the moment magnitude is estimated using the equation given below:

$$M_w = (2/3) \log_{10} (M_0) - 6.06$$

(Hanks and Kanamori 1979) (14)

where M_0 is in N-m.

Estimated hypocentral and source parameters for each event are listed in tables 2 and 3.

8. Error analysis

Here, we analyze the error in source parameters by estimating the standard deviation and mean of moment (M_0) , source radius (r) and stress drop $(\Delta \sigma)$. We also calculate the standard deviation for corner frequency (f_c) and frequency independent quality factor Q_0 . The average seismic moment and source radius are estimated by the equations given below (Archuleta *et al.* 1982):

$$\langle M_0 \rangle = \text{antilog} \left[(1/\text{NS}) \Sigma \log M_{01} \right]$$
 (15)

and

$$\langle r \rangle = (1/\text{NS}) \Sigma r_{\text{i}}.$$
 (16)

The standard deviation of the log moment are calculated using the equation mentioned below:

s.d.
$$\left(\log \langle M_0 \rangle\right)$$

= $\left\{ \left(1/\mathrm{NS} - 1\right) \Sigma \left[\log M_{0\mathrm{i}} - \log \langle M_{0\mathrm{i}} \rangle\right]^2 \right\}^{0.5}$. (17)

We also estimate multiplicative error factor using equation as given below:

$$E_{\rm mo} = \operatorname{antilog} \left\{ \text{s.d} \left(\log \left\langle M_0 \right\rangle \right) \right\}.$$
 (18)

Similarly, we calculate the average and the standard deviation for source radius, corner frequency and quality factor.

Finally, the standard deviations of stress drops are estimated using the equation as given below (Fletcher 1995):

$$\sigma_{\rm std} = \Delta \sigma \{ ((\sigma_{\rm m}/M_0)^2 + 9 (\sigma_{\rm r}/r)^2 \}^{0.5}.$$
(19)

From the above discussion, the standard deviation of moment, corner frequency, source radius, stress drop and quality factor and factor $E_{\rm mo}$ have been estimated for the selected 136 Bhuj aftershocks, which are recorded on three or more stations. The maximum standard deviation in corner frequency, stress drop and source radius are 0.73 Hz, 2.20 MPa, and 0.02 km, respectively (table 3). The mean values of standard deviation in corner frequency, stress drop, source radius and quality factor (Q) are 0.22 Hz, 0.19 MPa, 7 m and 4.26, respectively (table 3). For the standard deviation of 0.73 Hz in corner frequency leads to the standard deviation of 0.073 MPa in stress drop (table 3).

9. Results and discussions

We present the earthquake source parameters and crustal Q values, which have been estimated simultaneously using the Levenberg–Marquardt inversion of S-wave spectra of 144 selected aftershocks (2001–2010) of the 2001 M_w 7.7 Bhuj mainshock. The estimated static seismic moment (M_0), corner frequency (f_c), source radius (r) and static stress drop ($\Delta \sigma$) estimated from the inversion modelling of S-wave spectra of 144 aftershocks of magnitude 2.1 to 5.1 are ranging from 1.12 × 10¹² to 4.00 × 10¹⁶ N-m, 2.36 to 8.76 Hz, 132.6 to 513.2 m and 0.01 to 20.0 MPa, respectively (table 3). The

Table 3. Estimated source parameters and crustal Q values for selected 144 Bhuj aftershocks.

Ev. nos	$f_{\rm c}({\rm Hz})$	s.d. $\langle f_c \rangle$	<i>r</i> (m)	s.d. $\langle r \rangle$	$M_0(\text{N-m})$	s.d. $\langle M_0 \rangle$	$\Delta \sigma$ (MPa)	s.d. $\langle \Delta \sigma \rangle$	$E_{\rm mo}$	Q_0
1	2.68	0.32	492.00	62.0	2.33×10^{15}	0.26	1.05	0.4000	0.26	608.0
2	2.42	0.14	540.00	29.0	2.70×10^{15}	0.15	1.00	0.3500	0.18	435.0
3	2.80	0.09	467.00	14.0	5.10×10^{15}	0.20	2.20	0.5000	0.27	450.0
4	3.44	0.56	388.00	63.0	1.24×10^{14}	0.13	0.09	0.0300	0.10	923.0
5	2.36	0.15	388.00	63.0	8.30×10^{15}	0.17	2.20	0.3000	0.14	278.0
6	2.63	0.16	497.00	30.0	2.50×10^{14}	0.23	0.08	0.0300	0.19	510.0
7	2.54	0.00	513.00	0.0	1.80×10^{16}	0.27	5.70	0.0000	0.24	530.0
8	2.62	0.14	498.00	27.0	6.37×10^{16}	0.21	22.0	8.5000	0.40	893.0
9	7.49	0.04	185.98	0.91	2.16×10^{13}	0.04	0.15	0.0021	1.08	1108.6
10	5.38	0.40	252.00	0.22	8.00×10^{13}	0.22	0.22	0.0020	1.09	393.4
11	7.59	0.32	183.00	7.81	1.01×10^{13}	0.06	0.07	0.0094	1.16	1127.1
12	8.01	0.04	172.14	0.77	1.88×10^{12}	0.01	0.02	0.0002	1.02	429.9
13	7.09	0.14	227.40	4.32	5.85×10^{13}	0.26	0.24	0.0136	1.82	1138.1
14	7.48	0.30	178.00	7.19	1.27×10^{13}	0.15	0.10	0.0121	1.42	849.6
15	7.08	0.25	188.02	6.65	5.46×10^{13}	0.03	0.37	0.0394	1.07	1077.0
16	6.41	0.45	214.65	4.00	1.38×10^{14}	0.49	0.92	0.0515	3.10	418.2
17	7.70	0.09	165.85	1.97	5.41×10^{12}	0.24	0.06	0.0020	1.72	919.8
18	7.71	0.11	178.39	7.03	1.51×10^{13}	0.28	0.13	0.0158	1.90	825.5
19	7.81	0.27	176.44	6.11	6.77×10^{12}	0.18	0.06	0.0059	1.51	1263.5
20	7.73	0.19	178.43	4.37	9.46×10^{12}	0.24	0.08	0.0061	1.75	1092.1
21	7.71	0.39	179.00	7.89	2.31×10^{12}	0.09	0.02	0.0023	1.22	1000.5
22	8.04	0.37	171.56	7.89	2.03×10^{12}	0.00	0.02	0.0024	1.01	453.6
23	7.19	0.14	191.75	3.70	2.60×10^{13}	0.39	0.20	0.0116	2.43	1284.8
24	7.70	0.41	179.84	8.59	2.21×10^{12}	0.25	0.02	0.0025	1.78	1018.4
25	7.80	0.00	176.69	0.00	6.91×10^{12}	0.00	0.05	0.0000	0.00	988.2
26	7.48	0.44	184.55	11.26	1.23×10^{13}	0.14	0.09	0.0158	1.39	555.3
27	7.42	0.32	172.37	7.43	5.18×10^{12}	0.21	0.12	0.0160	1.62	493.0
28	7.31	0.23	188.68	5.84	4.44×10^{12}	0.04	0.03	0.0002	1.09	640.6
29	7.88	0.25	174.92	5.52	6.45×10^{12}	0.07	0.05	0.0051	1.18	947.2
30	7.76	0.27	177.74	6.11	2.53×10^{12}	0.30	0.02	0.0022	1.98	992.6
31	7.73	0.00	178.16	0.00	3.24×10^{12}	0.00	0.03	0.0000	0.00	701.9
32	7.64	0.14	174.02	3.23	3.51×10^{12}	0.23	0.03	0.0018	1.68	703.4
33	7.35	0.16	204.18	4.41	6.52×10^{12}	0.11	0.03	0.0022	1.27	1030.4
34	7.58	0.38	181.79	9.05	3.56×10^{12}	0.24	0.03	0.0047	1.73	491.4
35	7.65	0.22	180.35	5.08	5.39×10^{12}	0.13	0.04	0.0034	1.36	884.1
36	7.48	0.43	184.56	10.85	1.36×10^{13}	0.19	0.10	0.0173	1.54	869.0
37	8.19	0.23	168.25	4.75	2.81×10^{12}	0.03	0.03	0.0022	1.07	786.4
38	7.46	0.07	184.69	1.68	8.90×10^{12}	0.21	0.07	0.0018	1.63	874.1
39	7.37	0.32	187.27	8.32	8.43×10^{12}	0.09	0.06	0.0075	1.24	942.6
40	7.61	0.73	182.12	16.76	5.53×10^{12}	0.16	0.04	0.0120	1.45	1123.0
41	7.31	0.15	174.75	3.71	4.14×10^{12}	0.23	0.04	0.0023	1.71	668.9
42	7.15	0.52	193.47	13.56	5.05×10^{13}	0.29	0.33	0.0694	1.94	1068.3
43	7.18	0.51	192.71	14.34	4.10×10^{13}	0.37	0.29	0.0649	2.33	1215.8
44	7.65	0.21	180.25	4.79	1.16×10^{13}	0.09	0.09	0.0070	1.24	992.5
45	7.97	0.25	172.89	6.84	4.00×10^{12}	0.56	0.05	0.0060	3.40	1023.5
46	7.90	0.21	161.77	4.42	5.28×10^{12}	0.23	0.05	0.0044	1.69	826.2
47	7.73	0.00	171.97	0.00	1.46×10^{12}	0.00	0.03	0.0000	0.00	935.0
48	7.29	0.24	182.56	5.99	1.62×10^{13}	0.14	0.12	0.0058	1.39	1517.7
49	7.45	0.62	179.17	15.03	1.09×10^{13}	0.07	0.08	0.0211	1.17	751.4
50	7.73	0.37	178.48	8.35	4.05×10^{12}	0.12	0.03	0.0045	1.32	1038.2
51	7.61	0.04	181.18	0.85	5.36×10^{12}	0.34	0.05	0.0006	2.17	926.5
52	7.47	0.23	184.57	5.59	6.85×10^{12}	0.15	0.05	0.0047	1.42	842.5
53	8.13	0.39	169.69	8.31	2.96×10^{12}	0.19	0.03	0.0040	1.55	1019.3
54	7.22	0.30	191.20	8.01	8.21×10^{12}	0.17	0.05	0.0066	1.48	761.9
55	7.49	0.06	183.99	1.44	1.24×10^{13}	0.04	0.09	0.0021	1.09	876.9

Table 3. (Continued)

Ev. nos	$f_{\rm c}({\rm Hz})$	s.d. $\langle f_c \rangle$	r (m)	s.d. $\langle r \rangle$	$M_0(\text{N-m})$	s.d. $\langle M_0 \rangle$	$\Delta \sigma$ (MPa)	s.d. $\langle \Delta \sigma \rangle$	$E_{\rm mo}$	Q_0
56	7.77	0.48	177.60	10.99	3.94×10^{12}	0.02	0.03	0.0057	1.06	495.9
57	8.07	0.20	170.89	4.20	3.61×10^{12}	0.24	0.04	0.0028	1.75	712.4
58	7.55	0.09	182.62	2.16	1.39×10^{13}	0.27	0.11	0.0039	1.86	951.1
59	6.51	0.11	211.80	3.44	6.76×10^{13}	0.18	0.32	0.0157	1.52	779.1
60	7.38	0.36	173.44	8.28	2.61×10^{13}	0.09	0.22	0.0314	1.24	758.0
61	6.05	0.00	227.74	0.00	8.19×10^{13}	0.00	0.30	0.0000	0.00	255.7
62	6.63	0.36	192.94	10.47	1.02×10^{14}	0.17	0.64	0.1046	1.47	586.5
63	6.70	0.65	196.69	15.04	3.31×10^{13}	0.19	0.20	0.0453	1.56	464.8
64	7.30	0.25	181.54	7.14	1.56×10^{13}	0.03	0.11	0.0133	1.06	588.2
65	7.24	0.22	190.35	5.76	6.84×10^{13}	0.13	0.44	0.0400	1.35	893.2
66	7.57	0.08	182.06	1.84	2.08×10^{13}	0.22	0.16	0.0049	1.68	696.8
67	6.90	0.33	200.02	9.54	1.10×10^{14}	0.16	0.61	0.0878	1.43	1035.4
68	7.46	0.15	184.70	3.75	1.59×10^{13}	0.05	0.11	0.0067	1.13	524.2
69	7.37	0.00	186.92	0.00	6.67×10^{12}	0.00	0.04	0.0000	0.00	468.5
70	8.10	0.06	170.12	1.23	6.12×10^{12}	0.11	0.06	0.0012	1.28	799.0
71	7.55	0.04	182.54	1.04	2.02×10^{13}	0.03	0.15	0.0025	1.08	999.1
72	8.60	0.11	152.0	3.30	1.10×10^{13}	0.32	0.13	0.0166	1.08	604.3
73	7.55	0.10	182.47	2.38	1.30×10^{13}	0.27	0.11	0.0041	1.85	563.5
74	6.96	0.35	191.36	9.99	6.04×10^{13}	0.32	0.42	0.0661	2.08	771.9
75	7.74	0.22	178.22	4.92	3.84×10^{12}	0.26	0.03	0.0027	1.81	875.7
76	7.71	0.02	178.73	0.41	2.27×10^{13}	0.14	0.18	0.0012	1.37	789.1
77	7.58	0.09	181.70	2.23	6.43×10^{12}	0.09	0.05	0.0017	1.23	1137.7
78	7.53	0.17	176.73	3.94	1.42×10^{13}	0.20	0.12	0.0081	1.57	679.1
79	7.54	0.17	176.36	3.97	9.02×10^{12}	0.23	0.08	0.0054	1.68	855.2
80	7.19	0.39	209.16	11.42	1.90×10^{13}	0.33	0.10	0.0171	2.11	920.7
81	7.66	0.17	173.51	3.90	3.72×10^{12}	0.22	0.04	0.0024	1.64	914.3
82	7.22	0.45	184.75	11.93	8.45×10^{12}	0.20	0.06	0.0116	1.59	1031.3
83	7.33	0.26	188.20	6.73	8.37×10^{12}	0.45	0.07	0.0072	2.80	553.3
84	7.40	0.00	179.64	0.00	6.23×10^{12}	0.00	0.05	0.0000	0.00	509.2
85	6.83	0.31	201.91	9.38	1.03×10^{14}	0.16	0.58	0.0804	1.44	603.6
86	7.48	0.16	184.34	3.91	3.52×10^{12}	0.14	0.03	0.0016	1.39	694.5
87	7.76	0.53	171.68	11.81	5.50×10^{12}	0.03	0.05	0.0099	1.06	1087.2
88	8.13	0.00	169.60	0.00	2.22×10^{12}	0.00	0.02	0.0000	0.00	1160.2
89	7.55	0.00	182.47	0.00	6.44×10^{12}	0.00	0.05	0.0000	0.00	781.6
90	7.55	0.03	169.12	0.56	3.28×10^{12}	0.22	0.03	0.0003	1.64	970.3
91	7.89	0.34	174.91	7.60	2.48×10^{12}	0.18	0.02	0.0027	1.51	854.5
92	8.04	0.02	164.37	7.31	2.85×10^{12}	0.22	0.04	0.0046	1.65	754.0
93	7.32	0.36	188.38	9.22	7.84×10^{12}	0.20	0.05	0.0080	1.57	1253.3
94	8.04	0.00	165.38	0.00	3.15×10^{12}	0.00	0.03	0.0000	0.00	561.2
95	7.04	0.29	188.97	7.69	9.04×10^{13}	0.23	0.65	0.0793	1.69	1240.5
96	7.89	0.12	190.35	2.97	4.79×10^{12}	0.12	0.03	0.0014	1.33	747.7
97	7.33	0.41	181.79	10.17	6.61×10^{12}	0.18	0.05	0.0087	1.48	790.7
98	7.51	0.16	183.57	3.92	3.37×10^{12}	0.31	0.03	0.0018	2.03	863.7
99	6.81	0.22	202.54	6.44	6.31×10^{13}	0.51	0.56	0.0532	3.24	864.1
100	7.84	0.31	172.65	2.38	4.78×10^{12}	0.07	0.04	0.0016	1.16	1265.6
101	8.18	0.10	156.11	1.83	2.18×10^{12}	0.25	0.03	0.0009	1.79	1109.5
102	8.14	0.10	169.36	2.02	5.85×10^{12}	0.01	0.05	0.0018	1.03	791.2
103	7.73	0.33	178.39	7.44	5.51×10^{12}	0.41	0.05	0.0064	2.56	1029.4
104	7.52	0.10	183.30	2.43	1.11×10^{13}	0.18	0.08	0.0033	1.53	827.6
105	7.85	0.23	175.54	5.01	4.24×10^{12}	0.35	0.04	0.0036	2.23	978.6
106	6.57	0.28	205.99	12.99	1.69×10^{13}	0.33	0.11	0.0200	2.11	1250.8
107	8.01	0.07	172.51	9.91	8.28×10^{12}	0.14	0.08	0.0131	0.37	998.3
108	6.80	0.23	204.41	6.86	5.12×10^{13}	0.21	0.29	0.0296	1.64	766.1
109	6.33	0.32	228.63	11.36	9.99×10^{13}	0.22	0.40	0.0595	1.65	432.6

Table 3. (Continued)

Ev. nos	$f_{\rm c}({\rm Hz})$	s.d. $\langle f_c \rangle$	r (m)	s.d. $\langle r \rangle$	M_0 (N-m)	s.d. $\langle M_0 \rangle$	$\Delta \sigma$ (MPa)	s.d. $\langle \Delta \sigma \rangle$	$E_{\rm mo}$	Q_0
110	7.42	0.31	185.81	7.64	3.16×10^{12}	0.27	0.03	0.0031	1.87	549.8
111	7.78	0.30	177.25	7.05	1.92×10^{12}	0.18	0.02	0.0019	1.52	1113.4
112	7.87	0.12	175.10	2.65	1.12×10^{12}	0.09	0.01	0.0004	1.22	468.4
113	8.11	0.00	169.92	0.00	2.48×10^{12}	0.00	0.02	0.0000	0.00	273.3
114	7.99	0.56	172.84	12.02	8.25×10^{12}	0.04	0.07	0.0150	1.09	309.0
115	7.64	0.30	182.06	7.22	2.15×10^{13}	0.36	0.20	0.0237	2.28	583.0
116	8.16	0.63	184.57	14.30	5.29×10^{12}	0.02	0.04	0.0086	0.05	1479.7
117	7.05	0.52	209.53	17.53	2.22×10^{13}	0.14	0.11	0.0269	1.38	1389.3
118	8.25	0.44	167.22	8.83	1.48×10^{12}	0.16	0.02	0.0024	1.46	705.2
119	6.98	0.41	198.93	13.36	1.17×10^{14}	0.14	0.71	0.1428	1.37	1526.0
120	7.58	0.17	168.63	3.80	2.60×10^{12}	0.03	0.02	0.0016	1.08	1021.8
121	8.26	0.41	167.16	8.28	1.33×10^{12}	0.24	0.01	0.0021	1.74	766.0
122	8.11	0.01	169.94	0.21	2.34×10^{12}	0.32	0.03	0.0027	2.10	699.9
123	7.64	0.00	211.11	0.00	2.65×10^{12}	0.00	0.01	0.0000	0.00	946.8
124	8.07	0.35	170.90	7.52	2.45×10^{12}	0.01	0.02	0.0029	1.02	830.8
125	7.93	0.33	182.44	7.69	2.24×10^{12}	0.40	0.02	0.0025	2.51	1136.0
126	7.15	0.33	202.30	9.24	9.39×10^{12}	0.16	0.05	0.0074	1.46	1221.1
127	7.86	0.24	132.57	5.08	1.85×10^{12}	0.47	0.02	0.0023	2.94	608.3
128	7.96	0.36	175.69	9.82	3.98×10^{12}	0.00	0.03	0.0055	1.01	588.4
129	7.74	0.12	186.80	2.78	1.46×10^{13}	0.26	0.11	0.0039	1.81	896.6
130	6.97	0.17	196.85	0.92	1.05×10^{13}	0.37	0.08	0.0010	2.36	1107.4
131	7.33	0.18	197.18	4.73	8.96×10^{13}	0.31	0.60	0.0431	2.03	640.9
132	6.90	0.17	201.44	5.05	1.48×10^{14}	0.35	0.97	0.0725	2.22	710.0
133	8.76	0.00	183.95	0.00	4.23×10^{12}	0.00	0.03	0.0000	0.00	1881.9
134	7.58	0.18	180.01	4.10	9.47×10^{12}	0.42	0.11	0.0075	2.61	682.2
135	7.02	0.02	196.35	0.59	4.87×10^{12}	0.14	0.03	0.0002	1.39	885.6
136	7.74	0.20	180.37	4.69	9.95×10^{12}	0.09	0.07	0.0058	1.24	676.3
137	7.32	0.24	188.37	6.20	4.67×10^{12}	0.14	0.03	0.0031	1.38	1099.6
138	7.76	0.00	198.18	0.00	6.34×10^{12}	0.00	0.04	0.0000	0.00	504.9
139	7.58	0.00	181.86	0.00	2.61×10^{12}	0.00	0.02	0.0000	0.00	1152.3
140	8.60	0.17	152.00	4.87	1.00×10^{13}	0.13	0.13	0.0020	1.36	659.3
141	8.08	0.24	170.62	5.06	9.86×10^{12}	0.31	0.05	0.0046	2.02	816.6
142	7.99	0.00	159.87	0.00	2.77×10^{12}	0.00	0.03	0.0000	0.00	417.4
143	8.04	0.00	171.34	0.00	3.51×10^{12}	0.00	0.03	0.0000	0.00	356.7
144	8.22	0.00	167.59	0.00	3.27×10^{12}	0.00	0.03	0.0000	0.00	316.0

crustal S-wave 'Q' varies from 139 to 1880, with an average of 840 for the region (table 3).

Next, we present 23 S-wave spectra of 11 events with moment magnitude varying from 2.1 to 5.1, which are estimated at nine different stations, i.e., TAP, GDD, VJP, BHU, TPM, MTP, BHA, SKL and RPR. The date, time, magnitude and corner frequency of events, and adjustable damping parameter (λ) used for the Levenberg–Marquardt inversion of S-wave spectra are also shown in figures 3–5. For this study, the sampling rate of broadband data is 100/50 sps, thus the maximum frequency content of spectra is defined by the nyquist frequency (sps /2), i.e., 50/25 Hz. The TAP station (out of seven stations considered here) is situated on the hard Jurassic sediments, which is clearly reflected by the stable nature of S-wave spectra for earthquakes of $M_w > 2.5$ as seen from figures 3(a– h), 4(a–h), and 5(a–g). However, the spectra for smaller earthquakes of $M_w \leq 2.5$ at TAP station show some abrupt changes in spectral amplitude at 1–9 Hz (figures 4 and 5). From the S-wave spectra at all stations except TAP, an abrupt fluctuation in the spectra is noticeable at 0.2–3.0 Hz (figures 3–5), which could be associated with the site amplification caused by low velocity sediments at 0.2–3.0 Hz (Mandal *et al.* 2008). We also notice poor fitting of S-wave spectra between 20 and 25 Hz (figures 3–5), which could be due to large variation in attenuation factor (k) associated with the low velocity sediments in the Kachchh rift basin.

We plot the estimated corner frequencies with their error bars versus $\log_{10}(M_0)$ in figure 6(a). The calculated corner frequencies range from 2.36



Figure 3. Cross plot of $\log_{10}(\text{spectral amplitude of S-wave (in nm-sec)})$ and $\ln(\text{frequency (in Hz)})$. Estimated S-wave spectra (solid grey line) and modeled spectra from inversion (dotted grey line) for the Bhuj aftershocks at different broadband sites (a) for an M_w 3.2 event at MTP, (b) for an M_w 3.4 event at TAP, (c) for an M_w 3.4 event at GDD, (d) for an M_w 3.4 event at TPM, (e) for an M_w 3.4 event at TAP, (f) for an M_w 2.6 event at BHA, (g) for an M_w 2.5 event at GDD, and (h) for an M_w 2.8 event at GDD. The date of occurrence, origin time, moment magnitude, corner frequency and corresponding adjustable damping parameter (λ) used for Levenberg–Marquardt inversion of S-wave spectra for each event are shown. A black arrow showing the corresponding corner frequency (f_c) for each event is also shown.

to 8.76 Hz. The maximum standard deviation or error in corner frequency is estimated to be 0.73 Hz (figure 6a; table 3). What is also obvious from figure 6(a, b) is that the relation between corner frequency and seismic moment can be separated in two regions. For events seismic moment smaller than about $10^{14.2}$ N-m, the logarithmic regression of corner frequency and seismic moment has a slope of -0.043 while the slope is found to be -0.033 for larger seismic moment events (> $10^{14.2}$ N-m). Thus, this observation indicates that seismic moments of smaller earthquakes in the Kachchh region do exhibit a different source scaling than the larger events with seismic moment larger than $10^{14.2}$ N-m. The seismic moment of $10^{14.2}$ N-m corresponds to a moment magnitude 3.4. We also notice that the estimated corner frequencies are found to decrease with the increasing moment magnitude values as expected. The maximum standard deviation or error in corner frequency is estimated to be 0.73 Hz (table 3).

The estimated seismic moments are plotted against the source radius in log-log plot with the constant stress drop lines (figure 7a), which show that the source radii for smaller events ($M_0 \leq 10^{14.2}$ N-m) are weakly dependent on event size, compared with larger events ($M_0 > 10^{14.2}$ N-m) where source radii increase with increasing



Figure 4. Same as figure 3. (a) For an M_w 2.8 event at TPM, (b) for an M_w 3.1 event at MTP, (c) for an M_w 3.1 event at TAP, (d) for an M_w 2.1 event at TPM, (e) for an M_w 2.1 event at TAP, (f) for an M_w 3.3 event at TAP, (g) for an M_w 3.3 event at VJP, and (h) for an M_w 2.2 event at GDD.

moment. This seems to suggest that a critical source radius may exist for intraplate earthquakes that would characterize the lower part of the magnitude range. Its value is around 200 m in source radius for the earthquakes in the Kachchh region we analyzed. The estimated error or standard deviations in source radii are found to be ranging from 0.20 to 19.34 m. For events seismic moment smaller than about $10^{14.2}$ N-m, the logarithmic regression of seismic moment and source radii has a slope of 9.28, which is larger than the expected slope for a constant stress drop, while the same slope is estimated to be 5.33 for larger events with seismic moment larger than $10^{14.2}$ N-m (figure 7b). Thus, this observation indicates that seismic moments of smaller earthquakes in the Kachchh region do not exhibit a constant stress drop.

In figure 8(a), we plot logarithm of static stress drops (in MPa) and logarithm of seismic moment (in N-m). The calculated stress drops are found to be varying from 0.01 to 20.0 MPa. The standard deviations of stress drops are found to be 0.0002 to 2.21 MPa (table 3). We notice that the relation of stress drop and seismic moment can be separated into two regions above and below about $10^{14.2}$ N-m in moment, like the source radius and corner frequency relation with seismic moment. The stress drops for events with the seismic moment less than about $10^{14.2}$ N-m increase with increasing moment, then become less dependent on moment for the larger events. The seismic moment of $10^{14.2}$ N-m corresponds to a moment magnitude 3.4. Our estimated stress drops reveal a more systematic nature $(\log_{10}\Delta\sigma = 0.88 \ \log_{10}M_0 - 12.6)$



Figure 5. Same as figure 3. (a) For an M_w 2.2 event at TAP, (b) for an M_w 2.3 event at GDD, (c) for an M_w 2.3 event at TAP, (d) for an M_w 2.3 event at VJP, (e) for an M_w 3.4 event at TAP, (f) for an M_w 4.9 event at SKL, and (g) for an M_w 4.9 event at RPR.

for smaller moment values (log $M_0 \leq 10^{14.2}$ N-m, smaller aftershocks), while, in the region with seismic moment larger than $10^{14.2}$ N-m, estimated stress drop define a different relation (log₁₀ $\Delta\sigma =$ 0.19 log₁₀ M_0 -12.6) for moderate size aftershocks (figure 8a). However, Mandal and Johnston (2006), based on their source parameter study of 300 Bhuj aftershocks, suggest a systematic scaling ($M_0^3 \propto \Delta \sigma$) for smaller seismic moments, whereas they suggest more scatter value for large M_0 value, suggesting on an average a scaling ($M_0^n \propto \Delta \sigma$) where *n* varies from 0.5 to 1. Thus, we infer that our results are in good agreement with the findings of Mandal and Johnston (2006).

Figure 8(b) reveals that large stress drops are confined to the 15–30 km depth range, which perhaps indicates the existence of the base of seismogenic layer in the same depth range. The maximum stress drop value is estimated to be 20.0 MPa at 29.3 km depth for the largest studied event of M_w 5.1, which occurred in 2006 on the NWF fault in a reverse sense of motion. We also plot the stress drop of 21 MPa for the 2001 Bhuj mainshock, which is taken from Antolik and Dreger (2003). The observed large stress drops in the 15–30 km depth range could be attributed to crustal mafic intrusives and presence of aqueous fluids in the lower crust as revealed by the earlier tomographic study of the region. The spatial distribution of estimated stress drops is shown in figure 9, which suggests a concentration of larger stress drops (>2.2 MPa)on the south dipping reverse NWF, the causative fault of the 2001 Bhuj mainshock. The calculated stress drops for two events, which took place on the almost vertical strike-slip GF, suggest a low stress drop value of the order of 0.035 MPa (table 3).



Corner Frequency, fc (Hz)

(a)

log₁₀ (f_cin Hz)



Figure 6. (a) Logarithmic plot between seismic moment, M_0 (in N-m) and source radii, r (in m). The ' M_0 ' and 'r' for the 1993 Latur, 1997 Jabalpur and the 2001 Bhuj earthquakes are shown by bigger black solid circles. (b) Cross plot between $\log_{10}(f_c \text{ in Hz})$ with error bars and $\log_{10}(M_0 \text{ in N-m})$.

It is well known that uncertainty in Q estimates can lead to significant error in earthquake source parameter estimates. In the same connection, we discuss here all available frequency dependent Q-estimates for the Kachchh region. Singh et al. (2004) have estimated a relation Q(f) = $800 f^{0.42}$ for the Indian shield region using the dataset of four earthquakes recorded in the distance range of 240–2400 km. In 2004, Bodin et al. (2004) estimated a frequency dependent Q_0 $(Q_c \text{ at 1 Hz})$ value of 790 for the Kachchh region from their study on ground motion modelling. Further, Mandal et al. (2004a, 2004b) found a frequency dependent Q_0 (Q_c at 1 Hz) value of 102 for the Kachchh region, based on their study on the coda- $Q_{\rm c}$ study. Recently, Sharma *et al.*



Figure 7. (a) Logarithmic plot between the seismic moment $(M_0, \text{ in N-m})$ and stress drops $(\Delta\sigma, \text{ in MPa})$. (b) Depth distribution of estimated stress drops of selected 144 aftershocks (marked by open squares). The stress drop estimate of the 2001 Bhuj mainshock (marked by large solid black circle) is taken from Antolik and Dreger (2003).

(2008) have also obtained a frequency dependent Q_0 value of 148 based on coda- Q_c study. Now, we know that the coda-based method used in Mandal et al. (2004a, 2004b) and Sharma et al. (2008) gives the low Q of a very shallow portion of the crust, while large Q estimates obtained by Singh et al. (2004) and Bodin et al. (2004) sample deeper in the crust. Next, we discuss our estimates of frequency independent average crustral Q, which are ranging from 256 to 1882 with an average of 840 for the region. The large value of crustal Q thus obtained (Q = 840), indicates a low shear-wave attenuation for the near-surface rocks of the Kachchh region, which can also explain the observation of an intensity XI close to the epicenter and severe damage up to 350 km away from the

epicenter of the 2001 Bhuj mainshock. Further, our estimates for crustal average Q are agreeing well with the findings of Singh *et al.* (2004) and Bodin *et al.* (2004). We also observe that our average crustal Q-value of 840 is very similar to Q_0 (Q_c at 1 Hz) value (~900) of the New-Madrid region, USA (Bodin *et al.* 2004). Thus, we can infer that the ground motion attention characteristics for the Kachchh and New Madrid regions are expected to be similar as observed by Bendick *et al.* (2001) in terms of similar variation in intensity with distances in these regions.



Figure 8. Spatial distribution of stress drops. The north Wagad fault and Gedi fault are marked by NWF and GF, respectively. Solid large black circle marks the stress drop (~21 MPa) of the 2001 Bhuj mainshock while solid medium size grey circles mark the larger stress drop estimates (> 2.2 MPa) for three aftershocks of M_w 4.4–4.9, which have occurred during 2001–2006. Solid large grey circle marks the stress drop (~20 MPa) of the 2006 M_w 5.1 event. The stress drop estimates for other selected aftershocks (2009–2010) are shown by open black circles (medium size for 1.0 < $\Delta\sigma \leq$ 2.2 MPa and smaller size for $\Delta\sigma \leq$ 1.0 MPa).



Figure 9. Spatial distribution of stress drops. The north Wagad fault and Gedi fault are shown by black dotted lines and marked as NWF and GF, respectively. Solid large black circle marks the stress drop (~21 MPa) of the 2001 Bhuj mainshock while solid medium size grey circles mark the larger stress drop estimates (> 2.2 MPa) for three after-shocks of M_w 4.4–4.9, which have occurred during 2001–2006. Solid large grey circle marks the stress drop (~20 MPa) of the 2006 M_w 5.1 event. The stress drop estimates for other selected aftershocks (2009–10) are shown by open black circles (medium size for 1.0 < $\Delta \sigma \leq 2.2$ MPa and smaller size for ≤ 1.0 MPa).

Next we present a comparative study of stress drops between the 2001 Bhuj aftershocks and various other intraplate earthquakes in India. The estimated stress drops of the M_w 7.7 2001 Bhuj, 1993 M_w 6.3 Latur and 1997 M_w 5.8 Jabalpur earthquakes are reported to be 21, 7, and 20 MPa, respectively (Baumbach et al. 1994; Antolik and Dreger 2003; Singh *et al.* 2004), while the stress drops of the reservoir triggered Koyna earthquake sequence (1994-1997) range from 0.03 to 19 MPa for events with M_w varying from 1.5 to 4.7 (Mandal et al. 1998). Interestingly, we notice that our estimated stress drop of 20 MPa for an $M_w 5.1$ aftershock is larger than that of the 1993 M_w 6.3 Latur earthquake (~ 7 MPa, Baumbach *et al.* 1994). This could be attributed to the rift tectonics of the Kachchh region, whereas, the Latur region is characterized by tectonics of stable continental regions. We know that Kachchh rift zone is characterized by a high velocity lower crust (Mandal and Pandey) 2010), which can explain the estimated large stress drop of 20 MPa for an M_w 5.1 Bhuj aftershock at 29.3 km depth in the mafic lower crust. Similarly, Mandal and Dutta (2011) also notice larger stress drop of 6.17 MPa (for an M_w 4.7 Bhuj aftershock) at 7 km below the NWF. Thus, it is apparent that the stress drops are found to be relatively less in the intermediate crust (6–14 km), but they reach their maximum in the lower crust (14–34 km depth).

This kind of depth dependency of stress drop values can be attributed to the increase in maficness of crustal rocks with increasing crustal depth below the main rupture zone of the 2001 Bhuj earthquake (Mandal and Pandey 2010).

10. Conclusions

The Fletcher's (1995) simultaneous inversion method provides an improved constraint on the estimation of source parameters of aftershocks of the 2001 M_w 7.7 Bhuj earthquake and crustal S-wave Q for the region. The estimated source parameters are robust and appearing to be more realistic than those obtained from the routine S-wave spectral analysis of Bhuj aftershocks.

The simultaneous estimation of source parameters and crustal Q for 144 selected Bhuj aftershocks of moment magnitude 2.1 to 5.1 led to following significant findings:

- The estimated seismic moment, stress drop, corner frequency, source radius and crustal Q are ranging from 1.12×10^{12} to 4.00×10^{16} N-m, 0.01 to 20 MPa, 2.36 to 8.76 Hz, 132.6 to 513.2 km and 256 to 1882, respectively.
- The estimated source radii for smaller events $(M_0 \leq 10^{14.2} \text{ N-m})$ are weakly dependent on event size, compared with two larger events $(M_0 > 10^{14.2} \text{ N-m}).$
- For aftershocks of the 2001 Bhuj intraplate earthquake we analyzed, a critical source radius of around 200 m characterizes the lower part of the magnitude range.
- Interestingly, corner frequency, source radii and stress drop estimates show a distinctly different behaviour for smaller (seismic moment $\leq 10^{14.2}$ N-m) and larger (seismic moment $> 10^{14.2}$ N-m) aftershocks for the 2001 Bhuj earthquake.
- Most interestingly, the estimated stress drop values for Bhuj aftershocks show more scatter ($\log_{10}\Delta\sigma = 0.19 \log_{10}M_0-12.6$) towards the larger seismic moment values (>10^{14.2} N-m, larger aftershocks), whereas, they show a more systematic nature ($\log_{10}\Delta\sigma = 0.88 \log_{10}M_0-12.6$) for smaller seismic moment ($\leq 10^{14.2}$ N-m, smaller aftershocks) values.
- This inversion technique would be very efficient for estimating earthquake source parameters for any virgin area of unknown crustal Q values.
- Estimated S-wave Q values are found to be ranging from 139 to 1880 with an average of 840 for the Kachchh region, which is very similar to Q_0 value (~900) of New Madrid region, USA.
- The estimated large stress drops in the 15–30 km depth range are attributed to the presence of

crustal intrusive and aqueous fluids in the lower crust below the main rupture zone of the 2001 M_w 7.7 Bhuj earthquake.

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