



Characterization of ultra-fine aluminium particles with potential applications as composite propellants

K TEJASVI^{1,*} , V VENKATESWARA RAO¹ and Y PYDI SETTY²

¹Defence Research and Development Organization, Hyderabad 500058, India

²National Institute of Technology, Warangal 506004, India

*Author for correspondence (tejasvichem@gmail.com)

MS received 19 November 2018; accepted 13 March 2019; published online 28 June 2019

Abstract. High performance and reactivity of ultra-fine aluminium is the present new area of interest in aerospace and defence applications. Ultra-fine aluminium is an important ingredient in propellant compositions and formulations, which significantly improves the performance parameters of rockets. This paper discusses the characterization of synthesized ultra-fine aluminium, such as active (metallic) aluminium content, bulk density, X-ray diffraction, surface area (Brunauer–Emmett–Teller), scanning electron microscopy, transmission electron microscopy, thermal analysis and X-ray photo-electron spectroscopy. It is observed that the maximum metallic aluminium content of 85.93% was obtained by a gas volumetric method. The synthesized ultra-fine aluminium particles will greatly promote the application of these particles in composite propellants.

Keywords. Ultra-fine aluminium; metallic aluminium content; scanning electron microscopy; gas volumetry.

1. Introduction

Aluminium powder is a vital ingredient due to its innate properties like high density, low oxygen consumption and high-combustion enthalpy, which are beneficial for propellant compositions. Ultra-fine aluminium powder is an essential constituent in propellant composition and as an energy additive for a burning reaction. Aluminium is essentially micron-sized, owing to its long ignition delay, slow combustion power and incomplete combustion because its extensive oxidation is viewed as a major obstacle. It has been reported that a decrease in the particle size of aluminium [1] results in an increase in the surface area of the powder and greatly influences its chemical activity and hence, a decrease in activation energy. The use of Al nanoparticles is preferred because of a significant increase in the surface area and surface energy which aids in obtaining the enhanced burn rate and shorter and reduced ignition delay time [2], which results in improved combustion efficiency [3–5]. It has been reported that there is a significant increase in the burn rate by replacing micron-sized aluminium powder with ultra-fine aluminium. Further, it has been found that using ultra-fine aluminium by replacing conventional micron-sized aluminium powder, in the form of aluminium exploded grade, with a particle size ranging from 10–100 nm in the composite propellant resulted in a decrease in an ignition delay time and an augmented burning rate. Ultra-fine aluminium decreases the onset of the high-temperature decomposition temperature of ammonium perchlorate from 392.2 to 372.9°C in comparison with micron-sized aluminium

powder. Thus, a decrease in the decomposition temperature of ultra-fine aluminium-based compositions augments the burning rate of the propellants [6]. A better combustion efficiency of the ultra-fine aluminized propellant is achievable than that of micron-sized aluminium and it has also been reported that the size and morphology of the combustion product were affected [7,8]. Numerous techniques were reported in references for producing ultra-fine aluminium (particle size <200 nm, such as vapourization/condensation [9,10], plasma recondensation [11], milling [12], chemical method [13], inert gas method [14,15], plasma evaporation method [16] and electro-explosion of wire [17]). These methods paved the way for a number of studies and several researchers on the combustion behaviours of various propellant compositions and formulations containing ultra-fine aluminium powders. Of late, a radio frequency induction plasma (RFIP) process is played a significant role in synthesizing various metal [18–24] powders. RFIP has a unique advantage compared with several methods is that it has no electrodes; hence, contamination of the synthesized powder can be minimized to a great extent. The probable areas of using ultra-fine aluminium in chemical propulsion systems are (i) solid propellant formulations to change the burning rate and variation in pressure and (ii) solid propellant formulations and combinations to reduce agglomeration. Ultra-fine aluminium demands characterization of its properties. One of the most important characteristics of ultra-fine aluminium is active (metal) aluminium content. The reduced metallic Al content minimizes the oxidation enthalpy, which affects the propellant

Table 1. Characteristics of the synthesized ultra-fine Al powder.

Preparation method	Shape	Mean diameter (nm)	Thickness of coating layer (nm)	Reference
Electro-exploded wire	Sphere	56.1	2–4	[27]
Plasma synthesized process	Sphere	57.0	2–5	
Laser heating evaporation	Sphere, rod-like	51.9	3–5	
Induction heating evaporation	Sphere, rod-like	44.1	3–5	
Radio frequency induction plasma (as procured)	Sphere	126.8	1.0–2.5	This study

performance, such as ideal specific impulse [25]. According to the D2 law, a decrease in the particle size of aluminium reduces the burn time and aluminium oxide content on the surface reduces to significant amounts; thus, the available active metallic Al content increases [26]. Table 1 shows the characteristics of ultra-fine aluminium powder prepared by other methods. The size of ultra-fine Al is 100 nm–1 mm and is preferred as a propellant additive since it facilitates complete combustion. In the present work, the determination of metal aluminium in ultra-fine aluminium particles by means of a gas volumetry technique is considered. The ultra-fine aluminium particles synthesized by RFIP characterized through various techniques viz., X-ray diffraction (XRD), energy dispersive analysis by X-rays (EDAX), bulk density (BD), BET surface area, scanning electron microscopy (SEM), transmission electron microscopy (TEM), X-ray photo-electron spectroscopy (XPS) and thermal analysis. The characterization of ultra-fine powders synthesized by RFIP used in propellant manufacturing is performed to understand the effect of the ballistic properties and performance of a solid rocket motor. Thus, this study allows the determination of properties. The advantage of ultra-fine aluminium replacement in solid rockets is double-fold to decrease two-phase losses and an increase in specific impulse (I_s). Thus, the characterization of ultra-fine aluminium is required to know the actual reactivity as well as to predict and forecast the propellant behaviour with ultra-fine aluminium.

2. Experimental characterization

The BD was measured by the conventional method using tap densitometer equipment. An accurately weighed ultra-fine aluminium sample (~8 g) was taken in a 50 ml glass measuring cylinder and the material was tapped to realize a constant value. It took ~40 strokes to realize the minimum volume. The BD is given by the formula, $BD = m/V$, where m = powder mass (g) and V = volume (cm^3).

SEM enables investigation of the particle morphology. Specimens were observed directly with no surface preparation. In SEM, an electron beam falls on the sample and the sample, in turn, ejects electrons and X-rays. The SEM image

is created by detecting the emitted X-rays. SEM was used to study the topography, morphology and the composition of a sample. The large depth of the field of SEM allows the study of the morphology of the sample because of its three-dimensional appearance. The SEM uses electron beam than lenses, so it can be operated over a wide range of magnifications. Preparing the sample for SEM needs a lot of special attention, as SEM utilizes vacuum condition for the electron beam to form an image. Therefore, any wet sample must be dried before performing SEM on it, because water (or most other liquids) evaporates in vacuum.

The microstructure of ultra-fine particles was examined using a TEM (Tecnai G² FEI) with an accelerating voltage of 200 kV. For the TEM observations, the samples were ultrasonicated in ethanol and then, a drop of each sample was left to dry on a commercial carbon-coated Cu TEM grid. Thermogravimetric analysis (TGA) was carried out on a SDT Q600 V20.9 Build 20 thermal gravimetric system. The samples were heated at a rate of $10^\circ\text{C min}^{-1}$ with a gas glow of about 100 ml min^{-1} . The changes in energy were surveyed with differential scanning calorimetry (DSC Q20 V24.11 Build 124 instrument). XRD is a non-destructive technique. XRD is used to find information regarding crystal size, strain, chemical composition and physical properties of a material. In XRD, the intensity and the position of the diffracted beam are measured to find the all relevant information. Each crystalline material gives a unique diffraction pattern. One can identify the material by comparing the position and intensity of an unknown material with the diffraction pattern database provided by the Joint Committee for Powder Diffraction Standards (JCPDS). An X-ray beam hits the sample at an angle to the sample surface and the detector is placed in such a way to detect the reflection angle of the X-ray beam. The angle which is formed by the crystallites with the primary beam (X-ray) is called the Bragg's angle. During an experiment, the X-ray beam rotates so as to vary the angle, and the detector also rotates at the same angular velocity, so as to maintain the reflection geometry. XRD measurements are performed using a Philips X-ray diffractometer. A scanning rate of 2° min^{-1} at 2000 cycles using $\text{CuK}\alpha$ radiation (1.54056 \AA) is applied. Diffraction angle vs. intensity is obtained at the location of the peaks. The sample is loaded in the X-ray diffractometer

for XRD analysis. XPS spectra of the Al 2s, Al 2p, O 1s and C 1s photoelectron lines were recorded using monochromated AlK α radiation. The surface area measurement is quite important in the application where the material surface plays the key role. In solid propellants, the desirable traits of ultra-fine aluminium are because of its higher surface area. The surface area measurement is performed by the BET method (after Brunauer, Emmett and Teller, 1938) and expressed in m² g⁻¹. BET is a well-known and quite simple technique to find the surface area. The working principle for the BET measurement method is the adsorption of gas molecules on the solid surface. Mostly nitrogen is used as the gas because it is inert and available in high purity at reasonable cost. In the present study, a surface area analyser model number Smart Sob 92/93 Instrument finds the surface area. The range of measurement of the instrument is 0.1–2500 m² g⁻¹. The particle size distribution of ultra-fine aluminium was determined by a MALVERN-2000 particle size analyser based on the static light scattering technique.

Metallic aluminium content is determined as per IS-438 based on the gas evolution method, where the aluminium powder is reacted with sodium hydroxide in a closed system and the liberated hydrogen gas is collected and measured. The volume of gas liberated is depending on the purity/free metallic aluminium content of aluminium powder.

The percentage of metallic aluminium was calculated using the above formula:

$$\frac{(P - p) \times V \times 273 \times 10000}{(273 + T) \times 760 \times 124580 \times M} \quad (1)$$

where

P = atmospheric pressure of mercury in mm, at the instant measurement of volume of H₂ gas,

p = vapour pressure of mercury in mm of 10% sodium hydroxide at $T^{\circ}\text{C}$,

V = volume of H₂ gas produced in ml,

T = temperature in $^{\circ}\text{C}$ at the instant of measurement of the volume of H₂ gas produced,

M = mass of the aluminium powder sample taken for test.

3. Results and discussion

The investigated ultra-fine particles were labelled as UFAL. The particles of UFAL were commercial particles produced by the RFIP method, obtained from the known source and were characterized for potential application in composite propellant formulation.

3.1 Particle size distribution

The particle size of ultra-fine aluminium was determined by a MALVERN-2000 particle size analyser. The distribution

Table 2. Characteristics of the synthesized ultra-fine Al powder.

Sl. no.	Particle size distribution	Particle size (nm)
1	D_{10}	141
2	D_{50}	374
3	D_{90}	1309

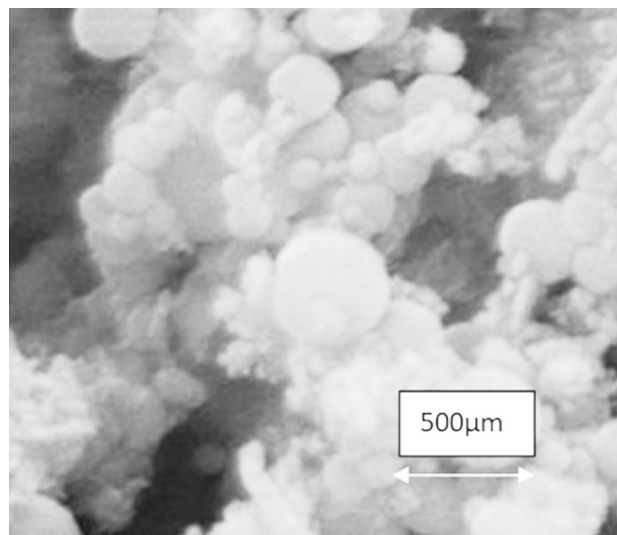


Figure 1. SEM micrograph of UFAP of magnification 80k \times .

of ultra-fine particles D_{10} to D_{90} is varied from 141 to 1309 nm and is shown in table 2. The data obtained from MALVERN are of a qualitative nature. They provided a reasonable evaluation of the size distribution for the tested powder.

3.2 Morphology of ultra-fine aluminium powder

The morphology of the ultra-fine powder was performed on a SEM, and the photographs are shown in figures 1–5 of different magnifications. The figure reveals the spherical nature of the ultra-fine particles.

3.3 Determination of active metallic content

The active metal content of ultra-fine aluminium powder was determined by the gas volumetric method using a 20 wt% NaOH solution and on reaction with aluminium powder produced hydrogen gas by the following equation:



The hydrogen gas produced was measured at a standard temperature and pressure, and based on the volume of hydrogen

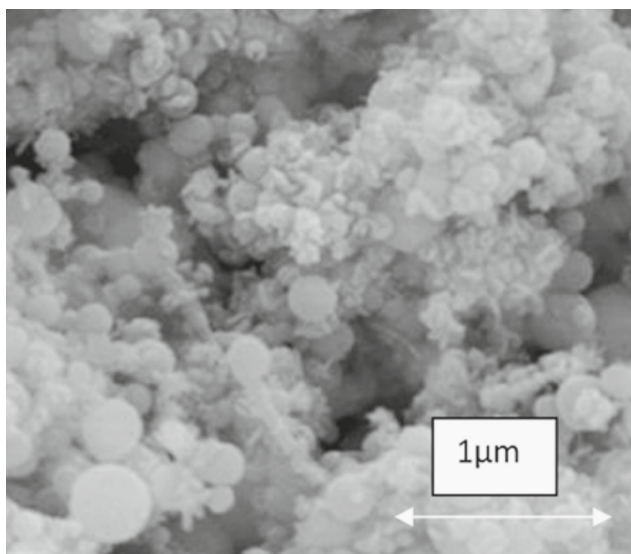


Figure 2. SEM micrograph of UFAP of magnification 50k×.

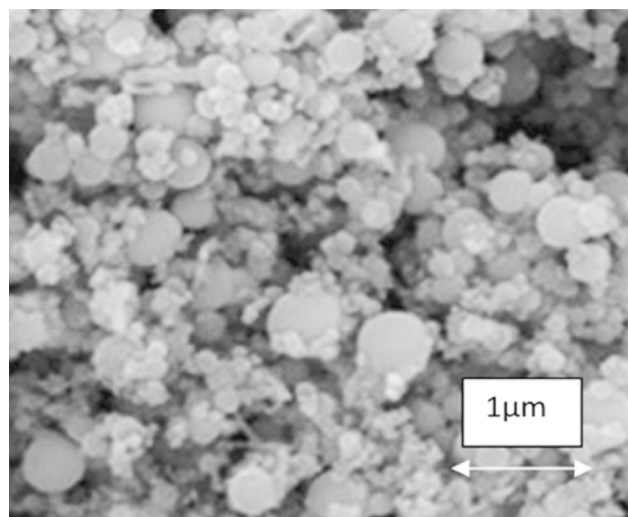


Figure 3. SEM micrograph of UFAP of magnification 30k×.

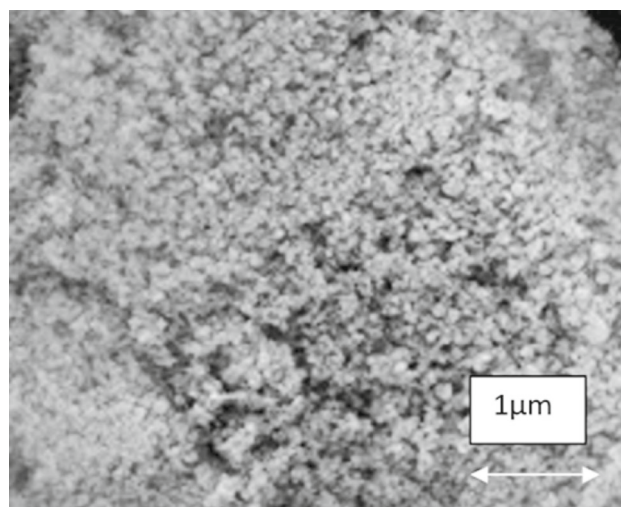


Figure 4. SEM micrograph of UFAP of magnification 5k×.

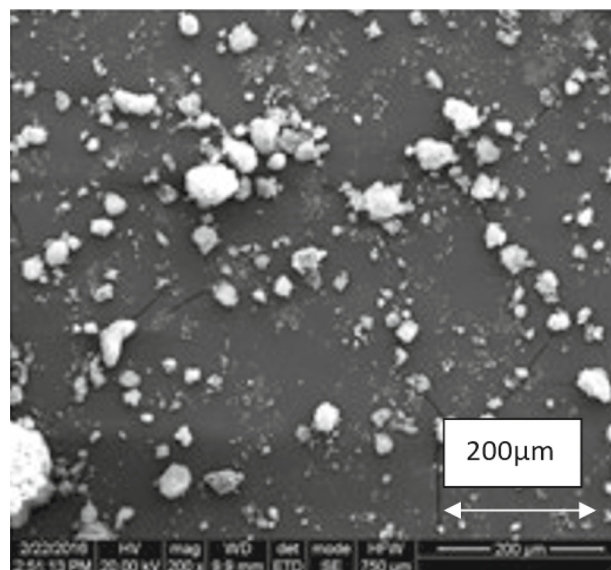


Figure 5. SEM micrograph of UFAP of magnification 200×.

gas; the active metal content was calculated. The active metal content for ultra-fine aluminium was found to be in the range of 82–86 wt% as shown in table 3. The error in the present analysis is < 0.5%.

3.4 XRD

Ultra-fine aluminium powder was characterized for its purity using the powder-XRD technique. A continuous scanning mode at a scanning rate of 2° min^{-1} was adopted. Figure 6 shows the XRD pattern of ultra-fine aluminium. Five characteristic peaks for aluminium ($2\theta = 38.6, 44.8, 65.2, 78.2$ and 82.4), corresponding to Miller indices (111), (200), (220),

Table 3. Result of metallic Al content.

Characteristics	Test method	Test values
Appearance of powder	Visual	Brackish grey fine powder in agglomerated form
Metallic aluminium content: by gas volumetry	IS: 438	85.93%

(311) and (222), were observed. This revealed that the resultant particles were pure face-centred cubic (ICDD: 04–0787) aluminium. In this pattern, there is no peak related to the aluminium oxide found under the sample, which suggests that the aluminium oxide layer is amorphous.

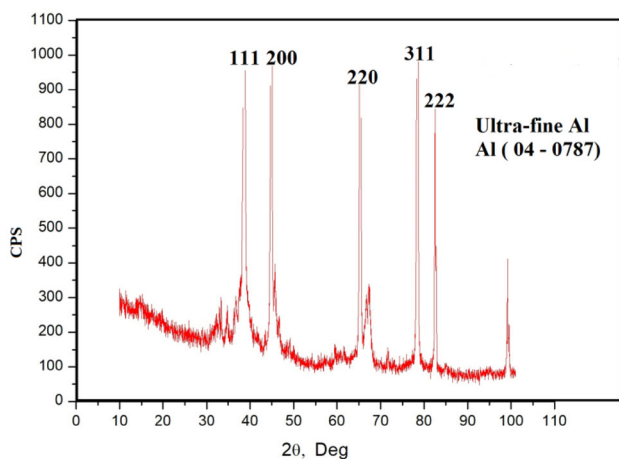


Figure 6. XRD of ultra-fine aluminium powder.

Table 4. Surface area measurement of UFAL.

Aluminium sample	Surface area (m ² g ⁻¹)	Particle size from BET tests	Reference
ALEX	11.3	197	[28]
UFAL	8.37	265	This study

3.5 Surface area measurement by BET method

The surface area of the samples obtained from the BET measurement is listed in table 4.

The surface area of the ALEX sample produced by an electrical explosion method is nearer to the value produced by RFIP. The particle size was calculated from the surface area measured by BET technique. This is a very simple technique for calculating particle size compared to TEM or SEM, which is not cost-effective and time consuming.

$$\text{Average particle size} = \frac{6 \times 1000}{\text{Surface area} \times \text{Density}}. \quad (3)$$

In the above equation, the average particle size is in nm, surface area is in m² g⁻¹ and the density is in g cc⁻¹. The above equation holds good for the particles of spherical shape. If the particles are not spherical, the above equation varies slightly, which is not included in the present study. In the present study, it is assumed that all the particles are spherical, which is not true for some of the samples tested in the present study. But the variations in the results are not much affected by this assumption.

3.6 EDAX analysis

Table 5 represents EDAX analysis carried out for the elemental composition of ultra-fine aluminium. It is observed that

Table 5. EDAX spectroscopic result of the sample.

Element	Wt%		At%	
	This study	[29]	This study	[29]
O	9.92	5.91	15.66	9.58
Al	90.08	94.09	84.34	90.42

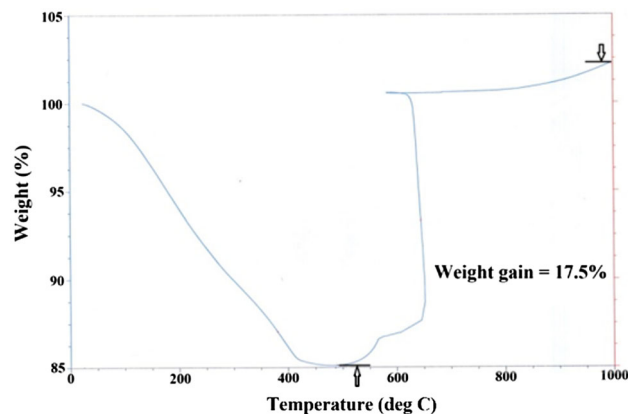


Figure 7. TGA of ultra-fine aluminium powder.

the compositions in the powder samples are aluminium and oxygen. Aluminium nanoparticles produced by other methods such as electrical explosion of wire and the elemental compositional analysis performed by an energy dispersive X-ray spectrometer show the atomic percentage of oxygen nearly 10%, which is having a size range of 20–200 nm [29].

3.7 Thermal analysis

Figure 7 shows the TGA plot of UFAL. Exotherm and mass gains of the sample between the TGA plots demonstrate a weight loss up to 450°C, which is due to the loss of adsorbed gases, water vapours and passivated from the surface of ultra-fine aluminium particles. Weight gain starts around 500°C, which continues upto 1000°C with an intermediate step around 640°C. Careful analysis of TGA plots reveals various processes involved in the oxidation of ultra-fine aluminium particles. Oxidation of ultra-fine aluminium particles is mainly governed by (i) chemical kinetics leading to the formation of a surface oxide shell and (ii) diffusion of oxygen leading to the oxidation of core aluminium which are very well discussed in the literature [27,30].

Figure 8 shows the DSC curve for UFAL. Here, we observe that an exotherm of the sample between 480 and 660°C is the result of the oxidation of solid aluminium, a phenomenon only observed with ultra-fine particles. The temperature of the oxidation peak (T_p) and the corresponding enthalpy change is 592.8°C (1.9 kJ g⁻¹). The UFAL gets highly oxidized even

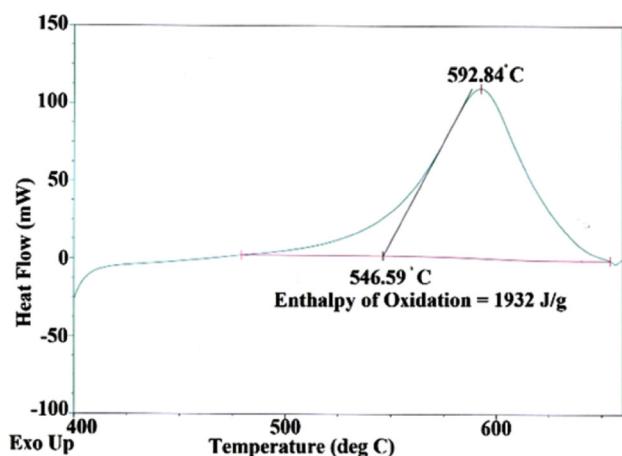


Figure 8. DSC of ultra-fine aluminium powder.

Table 6. XPS result of the sample.

Name	Binding energy (eV)	At%
O 1s	530.5	40.27
C 1s	283.5	44.29
Al 2p	73.0	15.44

before melting and leaving a small fraction of molten metal at 660°C, beyond the melting point, UFAL gets oxidized.

3.8 XPS

XPS profiles allow the investigation of atomic composition as shown in table 6 as a subsurface region and quantification of the concentrations of the main constitutive elements. By considering the whole aluminium peak, there is the possibility of decomposing it in metallic-Al and oxidized-Al components. Figure 9 shows the XPS survey spectrum (recorded with monochromatic AlK α radiation) and the inset shows the Al 2p region recorded at higher resolution showing the metallic (Al⁰) and oxide (Al³⁺) components as shown in table 7. Oxide films on ultra-fine aluminium particles are formed during their slow oxidation in air in the course of passivation. The thickness, composition and structure of the passive layer on the particles play an important role during their oxidation, because these parameters determine the diffusion rate of the gaseous oxidizer at low temperatures, and thereby, the ignition temperature. The oxide layer significantly lowers the particle energy density, slows the particle combustion rate and may prevent aluminium consumption.

3.9 TEM

Figure 10 shows TEM images of UFAL particles. Figure 10a and b show that the UFAL particles are all spherical with an average size of 126.8 nm and aggregate together. Figure 1b

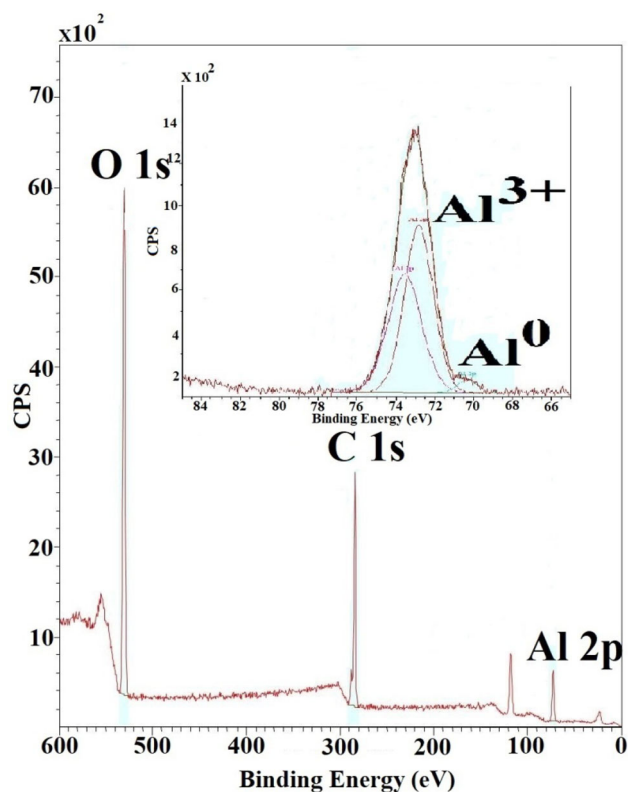


Figure 9. XPS survey spectrum of UFAL.

Table 7. Binding energy result of Al 2p.

Name	Binding energy (eV)
Al 2p	73.54
Al 2p	70.30
Al 2p	72.82

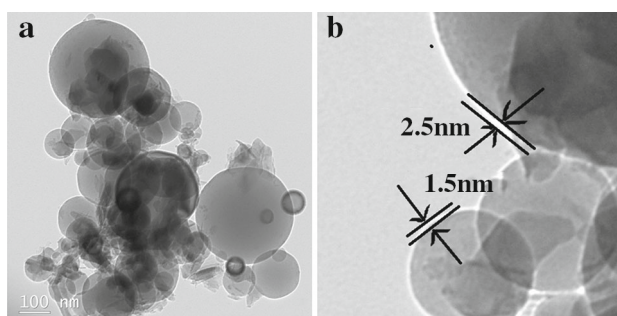


Figure 10. (a and b) TEM images of UFAL particles.

shows that the UFAL particles have a typical core-shell structure and the thickness of the oxide shell layer is 1.50 nm. There are no obvious lattices in the oxide layers, which show an amorphous structure.

3.10 Incorporation of ultra-fine aluminium in composite propellants

Mixing of the composite propellant was carried in batch mode in a vertical planetary mixer. A mixture of pre-polymer resin, plasticizer, antioxidant and bonding agent was mixed in the vertical planetary mixer. The mixture was agitated followed by mixing. Then, ultra-fine aluminium powder was added and mixed thoroughly. After the complete distribution of ultra-fine aluminium powder in the binder matrix, an oxidizer in the bimodal form was added in two proportions and mixed in such a way that homogenous mixing could take place. After the addition of all solid ingredients, further mixing of the composition was carried out. At this stage, curators were added and further mixed. The composition was cast into a mould by vacuum casting, and it was cured. The cured compositions were used for the determination of mechanical and ballistic properties. Ignition of aluminium closer to the surface of the propellant increases the heat feedback to the propellant, which accelerates the decomposition process of the propellant matrix and ultimately, the burning rate. The reduction in the particle size enhances the combustion reaction by several distinct mechanisms. Reduction in the particle mass decreases the transient heat conduction travel time through the particle, and an increase in the surface-to-volume ratio yields better dispersion of the particles in the propellant, thereby increasing the reactant sites. Finally, the ultra-scale particles can have completely different surface chemistry, often better than their micron-sized counterparts.

4. Conclusions

The synthesized ultra-fine aluminium powder obtained from a RF induction plasma technique was characterized by numerous investigation techniques viz., surface area, morphology and chemical species characteristics demonstrating highly crystalline spherical particles. A maximum metallic aluminium content of 85.93% was achieved by a gas volumetry technique. XRD patterns suggest that the aluminium oxide layers on these particles are amorphous. The TGA results reveal that there is a weight gain of 17.5% and exothermic characteristics are seen through DSC. The TEM results show that the UFAL particles have a core-shell structure on the surface of UFAL with an average thickness of 1.5 nm. This strongly demonstrates that this powder is best suitable for propellant compositions.

Acknowledgements

We gratefully thank Director ASL, for facilitating this research work.

References

- [1] Eisenreich N, Juez-Lorenzo M, Kolarik V, Koleczko A, Weiser V and Fietzek H 2004 *Propell. Explos. Pyrot.* **29** 137
- [2] Jayaraman K, Chakravarthy S R and Sarathi R 2010 *Combust. Explos. Shock Waves* **46** 21
- [3] DeLuca L T, Colombo G, Maggi F, Bandera A, Babuk V A, Galfetti L *et al* 2010 *J. Propul. Power* **26** 724
- [4] Ivanov Y F, Sedoi V S, Arkhipov V A, Bondarchuk S S, Vorozhtsov A B, Korotkikh A G *et al* 2003 *Propell. Explos. Pyrot.* **28** 319
- [5] Jayaraman K, Chakravarthy S R, Anand K V and Sarathi R 2009 *Combust. Flame* **156** 1662
- [6] Li F, Guo X, Liu L, Li M, Chen W, Jiang W *et al* 2011 *Int. J. Energ. Mater. Chem. Propul.* **10** 67
- [7] Babuk V, Dolotkazin I, Conti A, Galfetti L, DeLuca L T, Glebov A *et al* 2009 *Prog. Propuls. Phys.* **1** 3
- [8] Galfetti L, Severini F, Colombo G, Meda L, DeLuca L T and Marra G 2007 *Eur. Conf. Aerosp. Sci. EUCASS* **11** 26
- [9] Jigatch A N, Kuskov M L, Stoenko N I, Storozhev V, Leipunsky I O and Pribory B 2002 *Exp. Tech. Instrum.* **6** 122
- [10] Ya G M and Miller A V 1981 USSR inventor's certificate no. 814 432 Byull. Izobret no. **11**
- [11] Mazalov Y A, Bogdanova V V, Ivashkevich L S, Pavlovets G Y and Chinnov V V 1993 *Combust. Explos. Shock Waves* **29** 198
- [12] Khan A S, Farrokh B and Takacs L 2008 *Mater. Sci. Eng. A* **489** 77
- [13] Haber J A and Buhor W E 1998 *J. Am. Chem. Soc.* **120** 10847
- [14] Gutmanas E Y, Trusov L I and Gotman I 1994 *Nanostruct. Mater.* **4** 893
- [15] Sanchez-Lopez J C, Caballero A and Fernandez A 1998 *J. Eur. Ceram. Soc.* **18** 1195
- [16] Sun X K, Sun M, Cong H T and Yang M C 1999 *Nanostruct. Matter* **11** 917
- [17] Sedoi V S and Valveich V V 1999 *J. Tech. Phys.* **25** 81
- [18] Girshick S L, Muno R, Wu C Y, Yang L, Singh S K, Chiu C P *et al* 1993 *J. Aerosol. Sci.* **24** 367
- [19] Kobayashi N, Kawakami Y, Kamada K, Li J G, Watanabe R and Ishigaki T 2008 *Thin Solid Films* **516** 4402
- [20] Mamak M, Stadler U, Dolbec R, Boulos M, Choi S Y and Petrov S 2010 *J. Mater. Chem.* **20** 9855
- [21] Jung T, Kwon H, Park S, Ho J, Jung S, Baek J *et al* 2015 *J. Nanosci. Nanotechnol.* **15** 8424
- [22] Ananthapadmanabhan P V, Sreekumar K P, Thiyagarajan K and Venkatramani N 2004 *Scr. Mater.* **50** 143
- [23] Ye R, Li J G and Ishigaki T 2007 *Thin Solid Films* **515** 4251
- [24] Kim K I, Kim J H, Cho W S, Hwang K T, Choi S C and Han K S 2014 *Ceram. Int.* **40** 8117
- [25] Dreizin E L 2009 *Prog. Energy Combust. Sci.* **35** 141
- [26] Maggi F, Paravan C, DeLuca L T, Dossi S and Liljedahl M 2015 *Powder Technol.* **270** 46
- [27] Chen L, Song W, Lv J, Chen X and Xie C 2010 *Mater. Chem. Phys.* **120** 670
- [28] Gromov A A, Strokova Y I and Ditts A A 2010 *Russian J. Phys. Chem.* **4** 156
- [29] Wang F, Wu Z, Shanguan X, Sun Y, Feng J, Li Z *et al* 2017 *Sci. Rep.* **7** 5228
- [30] Wang S 2005 *Propell. Explos. Pyrot.* **30** 148