

Corrosion-resistant composite coatings based on a graphene oxide-metal oxide/urushiol formaldehyde polymer system

Lei Zhang, Wupin Wang, Haitang Wu, Zeyu Zheng, Ming Wei, Xiaohua Huang

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Abstract Composite coatings were fabricated based on a graphene oxide-metal oxide/urushiol formaldehyde polymer (GO-TiO₂/UFP, GO-SiO₂/UFP and $GO-Y_2O_3/UFP$) system with modifications, and its effectiveness in corrosion protection of metal substrates was demonstrated. First, a GO-TiO₂ composite was synthesized using titanium dioxide loading on GO via 3-aminopropyltriethoxysilane (APTES). The GO-Y₂O₃ composite was synthesized using nano-yttrium oxide intercalating into GO through two different silane coupling agents. The GO-SiO₂ composite was synthesized via an in-situ two-step sol-gel process utilizing APTES and tetraethylorthosilicate (TEOS) in an aqueous ethanol solution. The morphology and structure of the GO-metal oxide composites (GO- TiO_2 , $GO-Y_2O_3$ and $GO-SiO_2$) were studied. Subsequently, GO-metal oxides were incorporated into UFP

L. Zhang, H. Wu (⊠), X. Huang (⊠) Key Laboratory of Exploitation and Utilization of Economic Plant Resources of Shaanxi Province, College of Forestry, Northwest A&F University, 3 Taicheng Road, Yangling 712100, China e-mail: haitangwu@hotmail.com

X. Huang e-mail: 1067716566@qq.com

L. Zhang

Research Institute of Chemical Defense, Academy of Military Sciences, Changping District, Beijing 102205, People's Republic of China

W. Wang

Xi'an Research Institute of Chinese Lacquer Under All China Federation of Supply and Marketing Cooperatives, Xixian New District, Xi'an 712000, China

Z. Zheng, M. Wei

Wuhan University of Technology, 122 Luo Shi Road, Wuhan 430070, China

to investigate the composite's effectiveness in corrosion protection of metal substrates. Compared with GO-TiO₂/UFP and GO-Y₂O₃/UFP, GO-SiO₂/UFP showed superior alkali-resistance enhancing performance. Additionally, GO crosslinked with APTES-TiO₂ via covalent bonds and the well-dispersed GO-TiO₂ in UFP improved the electrochemical corrosion properties of the UFP coatings, most likely due to the obstruction of the diffusion pathways inside the UFP coating matrix, thus preventing the diffusion of penetrating species. It was revealed that the corrosion resistance of GO-TiO₂/UFP composite coating was noticeably higher than GO-SiO₂/UFP and GO-Y₂O₃/ UFP composite coatings.

Keywords Urushiol-formaldehyde polymer, Graphene oxide, Silica, Titanium dioxide, Yttrium oxide, Alkali resistance

Introduction

Urushiol formaldehyde polymers (UFPs) are usually used in corrosion protection.¹ However, their low alkali resistance greatly limits their application scope, and it is thus necessary to enhance the alkali resistance of UFP.² Incorporation of dispersed graphene oxide (GO)–nano oxide can efficiently obstruct micropores by reducing internal stresses, thus enhancing the barrier properties of UFP-containing film as a nanofiller.^{3–5}

GO has been successfully used to improve the formulation and anticorrosive properties of polymer coatings.^{1,2,6} The development of composite coatings functionalized by GO-polymers could effectively enhance the anticorrosion and physico-mechanical properties of anticorrosive coatings used for industrial equipment.⁷ Currently, GO is mainly fabricated from natural graphite via the modified Hummers method,^{8,9}

which produces a nonuniform distribution of oxygen functional groups (carboxylic at the edges, hydroxyl on the surface and epoxide in the basal plane) on the graphene sheets. The preparation of GO-polymer composite coatings for various fields is strongly limited by the low dispersibility of GO. However, a variety of processing methods for improved dispersion of GO in polymer composites have been recently developed, including surface grafting and decorating with nanoparticles, in situ polymerization and organic modification. 8,10,11 In particular, some studies have reported that the properties of GO can be improved by decorating it with nanoparticles such as oxides of titanium, aluminum, yttrium and zinc, as well as silica.^{12–17} At the same time, organic coatings comprising blended GO decorated with nanoparticles were introduced to achieve better dispersion of GO by preventing it from aggregating within the polymer coating.¹

Nano-TiO₂ has been widely applied as a polymer filler in organic coatings because of its high resistance to weathering and corrosion. Nevertheless, the high polarity and large surface area of nano-TiO₂ particles make them prone to aggregation in polymer coatings.^{13,18,19} In addition, nano-silica (SiÔ₂) was introduced into polymeric composite coatings which showed high corrosion resistance and mechanical properties. These were characterized by nano-SiO₂ chain-like aggregates characterized by hydrogen bonds between the polymer and the surface hydroxyls of the nanoparticles.^{20–24} Similarly, nano-yttrium oxide has been exploited as a very promising additive to polymeric organic coatings on metal substrates, owing to its high thermal and chemical stability,^{25,26} as well as good mechanical and barrier properties.^{27,28} An as–fabricated GO-oxide dispersed composite was added into a polymeric organic coating, which not only greatly improved the corrosion resistance of the polymer coating but also improved the dispersion of nanoparticles within the matrix via a loose structure of GO.²⁹

With potentially important applications and theoretical implications, the GO-metal oxide composites were prepared via a novel route in this study, which not only combined their inherent advantages but also improved the dispersion of GO within UFP. The synthesis of $GO-TiO_2$ was conducted using 3aminopropyltriethoxysilane (APTES), GO-SiO₂ was fabricated via a sol-gel method using APTES and TEOS, while $GO-Y_2O_3$ was prepared via a chemical reaction between GPS-Y2O3 and APS-GO. Afterward, the GO-TiO₂, GO-SiO₂ and GO-Y₂O₃ particles were dispersed in UFP as nanofillers, and the corresponding UFP composite coatings were obtained via a solution-blending process. Finally, differences in the resistance of the resulting composite coatings against corrosion and alkali were investigated.

Materials and methods

Materials

Graphite powder with $< 20 \mu m$ particle size was sourced from the Chinese Academy of Sciences Chengdu Organic Chemical Co., Ltd. (China). Nano-TiO₂ (about 30 nm) was supplied by Guangzhou Metal Metallurgy Co., Ltd. (China). Nano-Y₂O₃ (about 20 nm) was purchased from Ji'nan Huasen Metal Products Co., Ltd. (China). Tetraethyl orthosilicate (TEOS) was sourced from Tianjin Kermel Chemical Reagent Co., Ltd. (China), and the silane coupling agents (SCA): (3-amino-propyl)-trimethoxysilane (APS), y-(2,3-epoxypropoxy)propyl-trimethoxy silane (GPTMS) and 3-aminopropyltriethoxysilane (APTES) were obtained from Nanjin Chuanshi Chem Co., Ltd. (China). Pure urushiol was obtained via xylene extraction of raw lacquer sap (Shaanxi Lacquer Culture Industry Co., Ltd. China), as described previously.³⁰ Analyticalgrade potassium permanganate, hydrogen peroxide, aqueous ammonia solution, hydrochloric acid, sulfuric acid, xylene, methanol, formaldehyde, ethanol and acetone were commercially available.

Fabrication process of the composite coatings

Synthesis of APTES-GO

The modified Hummers method was used to synthesize graphene oxide (GO) from natural graphite.³¹ Briefly, 1 g of APTES and 0.05 g of GO were first suspended in 50 g of anhydrous ethanol ultrasonication at 50°C for 60 min. Subsequently, the resulting solution was stirred in a water bath at 80°C for 4 h. Then, 5 g distilled water was dropped into the mixed solution, and the asprepared solution filtrated and washed several times with a 50% (v/v) aqueous ethanol solution to remove the unreacted coupling agents. The obtained solid was dried for 24 h at 60°C to obtain APTES-GO powder. The synthesis of APS–GO powder using the second silane coupling agent APS was done in analogy to that of APTES-GO.

Synthesis of GO-SiO₂

A one-step sol-gel process was used to prepare the nano-GO–SiO₂.^{32,33} A schematic of the GO–SiO₂ fabrication process is shown in Fig. 1. Specifically, 0.05 g of APTES-GO was added to 288 mL of an aqueous ethanol solution (240 mL ethanol and 40 mL DI water) and dispersed by ultrasonication at 50°C for 60 min to form a homogenous solution. Subsequently, 360 μ L of a 28% (*w*/*v*) aqueous ammonia solution and 0.6 mL of TEOS were dissolved in the APTES-GO suspension in a 500-mL three-necked condenser flask with a magnetic stirrer. The reaction was performed at



Fig. 1: A schematic illustration of the GO–SiO₂ synthesis procedure

60°C in a water bath for 4 h to ensure the complete hydrolysis of the mixture, followed by incubation of 75°C for another 1 h. The as-prepared solution was filtrated and washed several times with a 50% (ν/ν) aqueous ethanol solution to remove the unreacted coupling agents, and the solid was dried for 24 h at 60°C to obtain GO–SiO₂ powder.

Synthesis of GO–TiO₂

As illustrated in Fig. 2, the preparation of $\text{GO}-\text{TiO}_2$ followed a two-step method as follows:

(1) 6 g of APTES and 0.2 g of nano-TiO₂ were suspended in 150 g of anhydrous ethanol by ultrasonication at 50°C for 30 min. The resulting solution was stirred for 6 h in a water bath at 80°C, after which 44 g of a 15/7 (*w*/*w*) aqueous/ ethanol solution were dropped into the mixed solution. Finally, the as-prepared solution was filtrated and washed several times with the aqueous ethanol solution to remove the unreacted coupling agents. The remaining solid was dried for 24 h at 60° C to obtain APTES–TiO₂.

(2) 0.3 g of GO and 0.2 g of APTES–TiO₂ were added to 100 mL of xylene and uniformly dispersed through ultrasonication for 30 min. The reaction mixture was stirred for 3 h at 105°C, and the resulting GO–TiO₂ was obtained by filtrating, washing five times with anhydrous ethanol, and drying for 24 h at 60°C, followed by repeated grinding to obtain a powder.

Synthesis of $GPS-Y_2O_3$ and $GO-Y_2O_3$

The amino-functionalized Y_2O_3 was obtained using GPS to modify nano- Y_2O_3 . Briefly, 0.1 g of nano- Y_2O_3 and 2 g of GPS were homogeneously dispersed in 100 g of anhydrous ethanol by ultrasonication at 50°C for 30



Fig. 2: A schematic illustration of the GO-TiO₂ synthesis procedure



Fig. 3: A schematic illustration of the preparation of GO-Y₂O₃ and the corresponding UFP coatings

min. The resulting solution was stirred for 4 h in a water bath at 78°C with drop-wise addition of DI water (10 g). Finally, the as-prepared solution was filtered and washed several times with a 50% (ν/ν) aqueous ethanol solution to remove the unreacted chemicals. The remaining solid was dried for 24 h at 60°C to obtain GPS-Y₂O₃.

A schematic representation of the reaction between APS-GO and GPS- Y_2O_3 is shown in Fig. 3. An aliquot comprising 0.25 g of APS-GO was added to 100 mL of xylene and dispersed through ultrasonication for 30 min. Subsequently, 0.05 g of GPS- Y_2O_3 was added

into the suspension and dispersed via ultrasonication for 30 min. The resulting mixed solution was stirred for 5 h at 105°C, after which the GO–Y₂O₃ solid was filtered, washed several times with a 50% (ν/ν) aqueous ethanol to remove the unreacted coupling agents, and dried at 60°C for 24 h.

Preparation of the UFP composite coatings

A homogeneous distribution of nanofiller was ensured by using a low content of $GO-TiO_2$, $GO-SiO_2$ and

 $GO-Y_2O_3$ in the organic coating to prevent them from agglomerating within the UFP matrix. For this purpose, the modified GO dispersion in xylene (1:30, w/w)was sonicated for 30 min and then added to a stoichiometric amount of UFP resin at room temperature using an S312-250H high shear mechanical mixer (SENCO Technology Co., Ltd., China). The mixing ratio of UFP to modified GO was 100:1 by weight. The prepared coatings were applied to JDMK-50 tinplates (Tianjin Jingkelian Material Testing Machine Co., Ltd., China) using the roll coating technique.³³ The UFP composite coated tinplates were sequentially baked at 120°C for 1 h and 220°C for 2 h in an oven to achieve complete curing. In addition, the 30 µm thickness GO-metal oxide/UFP composite coatings were prepared on the tinplates and glass sheets as a reference sample.

Characterization of composite coatings

The FTIR test was performed in a wavelength range of $400-4000 \text{ cm}^{-1}$ using a NICOLET IS10 FTIR spectroscopy instrument (PerkinElmer, USA). A K-Alpha X-ray photoelectron spectrometer (XPS; Thermo Fisher Scientific, USA) was used as follows: Al Ka was used as the radiation source at 10^{-7} mbar and a voltage of 5 kV. An S-4800 field emission scanning electron microscope (FE-SEM, Hitachi Ltd., Japan) was used to examine the morphology of the prepared coatings. XRD (D8 ADVANCE A25, Bruker, Germany) was used to measure the phase crystallinity and composition of the prepared coatings, with Cu Ka as the radiation source at 40 kV and 30 mA.

A PGSTAT 30 electrochemical workstation was used for electrochemical impedance spectroscopy (EIS) and potentiodynamic polarization curve measurements, with a three-electrode cell configuration for both EIS tests and Tafel plots.²⁹ The measurement apparatus consisted of a 1 cm^2 tinplate sample coated with the modified GO-metal oxide/UFP as the working electrode, a platinum counter electrode and a saturated calomel electrode (SCE) as the reference electrode.^{12,37} An applied potential range from -0.25to +0.25 V and relative to open circuit potential (OCP) were used for the polarization curves test at a scan rate of 1 mV/s.³⁷ A frequency range from 0.01 Hz to 100 kHz, with a sinusoidal voltage of 10 mV, was used for the EIS test. All EIS measurements were implemented on three different replicates for checking the repeatability of data.

Analysis of chemical resistance properties

The anticorrosion properties of the UFP composite coatings were investigated using an induced corrosion experiment in chemical solutions. Individual coated glass sheets were separately immersed in 3% NaCl, 30% H₂SO₄ and 10% NaOH for 14 days at room

temperature. Loss of color, brightness or the formation of foam on the surface of the coating were visually followed. Every 24 h, the samples were checked and photographed.

Results and discussion

FTIR analysis

A goal of the structural analysis was to investigate the completion of the reaction between GO and APTES–TiO₂. The FTIR spectra of GO–TiO₂/UFP and GO–TiO₂ are shown in Fig. 4a. The absorption peaks at 2920, 2843, 1038 and 1109 cm⁻¹ could be attributed to the stretching vibrations of –CH₃ and –CH₂, as well as Si–O–C and Si–O–Si, respectively, most likely corresponding to the functional groups of APTES. The – NH₂ absorption band at 1640 cm⁻¹ and the Ti–O–Ti stretching band at 765–620 cm⁻¹ of GO–TiO₂ were observed. These results indicated that nano-TiO₂ had been successfully modified using silane molecules (APTES) through chemical reactions with functional groups.

When comparing typical spectra of $GO-TiO_2$ and GO, it can be seen that the stretching vibration of C– O–C (GO) at 1120 cm⁻¹ disappeared along with appearance of the stronger –CN and –NH absorptions at 1545, 801 and 1545 cm⁻¹, respectively, which demonstrated the successful chemical reaction between epoxide groups on GO surface and amino groups from the modified nano–TiO₂ in APTES.¹⁵

The FTIR peaks of APS-GO, GPS-Y₂O₃, GO- Y_2O_3 and $GO-Y_2O_3/UFP$ are shown in Fig. 4b. The distinctive absorption peaks of GO generally appear at $3447, 1220, 1120 \text{ and } 1741 \text{ cm}^{-1}$ corresponding to -OH, C-O, C-O-C and C=O, respectively, indicating the presence of hydroxyl, epoxide and carboxyl groups on the GO surface. Accordingly, the feature in the range of 2800–3000 cm^{-1} was the result of the –CH stretching modes in the FTIR spectra of APS-GO and GPS- Y_2O_3 . The strong peaks at 1040 cm⁻¹ were associated with Si-O-Si/Si-O-C bonding from APS and GPS, with the appearance of new peaks at 1385 and 1508 cm^{-1} corresponding to Si–O–Y,³⁵ indicating the Y_2O_3 and GO have been successfully modified by the silane coupling agents APS and GPS through chemical bonding, accordingly. In the FTIR spectra of the GO-Y₂O₃ example, the absorption peaks of C–O–C bonding became obscured by the appearance of a stronger absorption at 1525 and 1410 cm⁻¹ attributed to the bending of the secondary amide N-H and the C-N stretching vibration, while Si-O-Si/Si-O-C and Si-O-Y bonding was still observed (Fig. 4b). These results implied that reactions took place between the epoxide and amino groups to some extent.³⁶

Figure 4c shows the FTIR spectra of APTES–GO and GO–SiO₂. In the spectrum of APTES–GO, many new characteristic absorption peaks were clearly



Fig. 4: FTIR spectra of UFP films and pure urushiol (a), $GO-TiO_2/UFP$ films and $GO-TiO_2$ (b), $GO-Y_2O_3/UFP$ films, APS-GO, GPS-Y_2O_3 and $GO-Y_2O_3$ (c), APTES-GO and $GO-SiO_2$ (d)

observable, including strong bands at 465 and 1100 cm⁻¹ assigned to the Si–O–Si bending vibration and the Si–O–C/Si–O–Si asymmetric stretching vibration, respectively, which could be attributed to the chemical reaction between GO and APTES. After APTES-GO reacted with TEOS, three new characteristic peaks appeared at 465 (1090), 694 (1124) and 3260 cm⁻¹. These were attributed to the Si–O–Si bending vibration (asymmetric vibration), Si–O–C stretching and NH₂, respectively.^{12,37} This suggests that SiO₂ was formed on the GO surface through chemical reactions between epoxy and hydrogen groups of GO and the silane coupling agent APTES,^{38,39} which was in good accordance with the XPS analysis.

Microstructure and chemical composition of GO-metal oxide in UFP

To evaluate the distribution of $GO-Y_2O_3$, $GO-TiO_2$ and $GO-SiO_2$ composites in the UFP matrix, SEM images of the cured UFP composite coatings were also recorded. The SEM micrographs in Fig. 5 show the bulk structural information on the $GO-TiO_2/UFP$, $GO-Y_2O_3/UFP$ and $GO-SiO_2/UFP$ composite films. Figs. 5a and 5b show the fracture morphology of the GO-TiO₂/UFP composite coating. As can be seen in Fig. 5a, $GO-TiO_2$ had a better dispersion performance in UFP at 2 wt%, arising from the composite blending process of GO-TiO₂ in UFP, which has been observed to result in thin layers. By contrast, the GO-Y₂O₃/UFP showed an entirely different fracture morphology. As shown in Figs. 5c and 5d, GO-Y₂O₃ exhibited a good affinity and compatibility with UFP. There was no obvious aggregation into clusters, and a thin-layered structure was observed instead, which improved the poor dispersion of GO-Y2O3 nanoparticles or the laminar pattern within the UFP polymer. The fractured morphology of the GO-SiO₂/UFP composite (Figs. 5e and 5f) showed no visible agglomerations or clusters. In particular, GO-SiO₂ was well dispersed in the UFP matrix with a multilayered structure, implying that covalent bonds were formed between the APTES and the GO surface, which was consistent with the structure deduced from the FTIR results. The excellent dispersion could enhance the anticorrosion properties of the UFP coatings, which should be verified in further measurements.



Fig. 5: SEM images of (a) the GO–TiO₂/UFP composite coatings, (b) high magnification image of the GO–TiO₂/UFP coating, (c) the GO–Y₂O₃/UFP composite coating, (d) high magnification image of the GO–Y₂O₃/UFP coating and (e) the GO–SiO₂/UFP composite coating, (f) high magnification image of the GO–SiO₂/UFP coating on silicon chip substrates

XRD analysis

XRD spectra of GO–TiO₂ composite and the GO– TiO₂/UFP composite coating are shown in Fig. 6a. In the as-prepared GO–TiO₂ samples, a new diminished protuberance was visible at $2\theta = 12.5^{\circ}$ corresponding to the structure of GO (Fig. 6a), which suggested that the introduction of nano–TiO₂ did not destroy the closely packed layered and highly ordered structure of GO.^{7,33} The GO–TiO₂ wide-angle X-ray diffraction showed a very broad peak at 21.7°, which could indicate that the amorphous GO–TiO₂ structure was transformed through APTES.⁴⁰ When comparing the pattern of GO–TiO₂ with GO–TiO₂/UFP, no obvious characteristic diffraction peaks of GO–TiO₂ were observed in the XRD pattern of the GO–TiO₂/UFP because the TiO_2 -GO hybrid nanoparticles were completely dispersed in the UFP matrix.

Figure 6b shows the XRD patterns of APS–GO, GPS–Y₂O₃, GO–Y₂O₃ and GO–Y₂O₃/UFP. According to the Bragg equation $[2d\sin\theta=\lambda \ (\lambda=0.154 \text{ nm})]$,³³ the interlayer distance of GO (0.80 nm) was larger than that of pristine graphite (0.34 nm) owing to the presence of oxygenated functional groups on the carbon sheets. When comparing the XRD pattern of GO–Y₂O₃ with that of APS–GO, a small peak is visible around $2\theta = 7.8^{\circ} \ (d = 1.13 \text{ nm})$ in the curve of GO–Y₂O₃, which can be attributed to GO. The expansion of the interlayer distance of GO confirmed the successful blending process between APS–GO and GPS–Y₂O₃.¹⁴

The XRD spectra of APTES–GO, GO–SiO₂ and GO–SiO₂/UFP are shown in Fig. 6c. Wide-angle X-ray



Fig. 6: XRD spectra of GO–TiO₂ and GO–TiO₂/UFP films (a), APS–GO, GPS–Y₂O₃, GO–Y₂O₃ and GO–Y₂O₃/UFP films (b), APTES–GO, GO–SiO₂ and GO–SiO₂/UFP films (c)

diffraction displayed a very broad peak at 19.9° due to the presence of amorphous structure domains in the UFP, which was characteristic of UFP.⁴¹ Figure 6c also shows that the intrinsic diffraction peak of GO was apparently weakened in the GO–SiO₂ and disappeared in the XRD spectrum of the GO–SiO₂/UFP. This means that better dispersion of GO–SiO₂ nanohybrids was achieved in this case.¹²

XPS analysis

To investigate interactions between GO and the metal oxide nanoparticles (TiO₂, Y_2O_3 and SiO₂) as well as the chemical state of the GO-metal oxide composites, XPS was applied to identify the changes in the surface elemental composition of the GO-metal oxide.

The XPS survey results of $GO-TiO_2$ (a). C 1s (b). O 1s (c), and Ti 2p (d) are shown in Fig. 7. In the XPS survey spectrum of the composite comprising GO- TiO_2 (Fig. 7a), the C 1s spectrum exhibited four peaks located at 284.4, 284.9, 286.6 and 287.9 eV (Fig. 7b), which could be assigned to Ti-O-C, C-C, C-O and C=O, respectively. Observation of Ti-O-C bonding revealed that nano-TiO₂ has been modified by APTES to some extent. The O 1s signals at, respectively, 530.6 and 532.3 eV were associated with two Gauss-Lorentzian peaks related to Ti–O and C–O (Fig. 7c).⁴² The Ti 2p, which consisted of peaks at 458.9 and 456.8 eV (Fig. 7d), was related to the Ti 2p1/2 and Ti 2p3/2 core levels of TiO₂, respectively. Taken together, the XPS results indicated that GO was effectively reacted with APTES– TiO_2 to form the surface coating.

The main structural information, including GO- Y_2O_3 , N 1s and O 1s, is shown in the XPS survey spectrum (Fig. 8). As can be seen in Fig. 8a, C 1s, O 1s, N 1s, Si 2p and Y 3d were the main signals observed in the XPS spectrum of the $GO-Y_2O_3$. The O 1s spectrum (Fig. 8b) was separated into five peaks attributed to the binding energies of C-O-C/OH/Si-O-Si (532.8 eV), O=C-O (532.7 eV), C=O/C-O/C-O-Si (532.1 eV), Y–O–Si (531.7 eV) and Y-O (530.6 eV).^{14,43} These results indicated that GO and Y_2O_3 were modified by APS and GPS to some degree. The N 1s spectrum of $GO-Y_2O_3$ in Fig. 8c could be decomposed into two peaks, in which C-N was assigned to 399.1 eV and N-H to 400.4 eV. Based on the results obtained from the XPS analysis, it could be clearly seen that the GPS-Y₂O₃ were grafted onto the APS-GO surface via chemical bonding with two types of functional groups (hydroxyl and carboxylic).

Figure 9 shows wide-scan XPS spectra of GO-SiO₂, whereby peaks in the C 1s, O 1s and Si 2p spectra were detected at binding energies of 283.8, 526.8 and 101.2 eV, respectively. Figure 9b displays the C1s XPS spectrum of GO-SiO₂ with seven peaks appearing at 284.1, 284.7, 285.3, 285.5, 286.7, 288.0 and 289.1 eV. These peaks correspond to the C-Si, C-C/C=C, C-N, C-O/C-O-Si, C-O-C, C=O and O-C=O bonds, respectively, indicating that APTES and TEOS successfully reacted with GO forming chemical bonds with two types of functional groups.^{44,45} In addition, the O 1s signals at 530.9, 531.7, 532.3, 532.9 and 533.4 eV were, respectively, related to the five Gauss-Lorentzian peaks of O–C=O, C=O, C–O/C–O–Si, Si–O–Si and C–O–C/OH (Fig. 9c).^{46,47} It could be observed that two peaks at 102.5 and 103.4 eV in the Si 2s spectrum (Fig. 9c) were assigned to C-Si and Si-O-Si, respectively, indicating that the GO successfully reacted with



Fig. 7: (a) XPS survey spectrum and high-resolution spectra of GO-TiO₂, (b) C 1s, (c) O 1s, and (d) Ti 2p

silane groups, mainly in the form of SiO_2 nanoparticles.⁴⁴

As can be seen from Table 1, the Ti 2p, Y 3d and Si 2s signals included 37.12% O–Ti–C, 27.11% Y–O–Si, 23.66% Si–C and 76.34% Si–O–Si peaks, which indicated that most of the silane moieties could be successfully grafted onto the GO surface via chemical bonding in the formation of the UFP composite coatings. Importantly, the results were in good agreement with the FTIR analysis described above.^{33,48}

Electrochemical tests

For better understanding and to judge the corrosion stage, the Nyquist and Bode plots were fitted with proper equivalent electrical circuits as shown in Fig. 10. The EIS fitted results were indicative of the two different stages of the corrosion process (the initial and terminal stages). In the equivalent electrical circuits, the elements contain the electrolyte resistance (R_s) , coating capacitance (C_c) , and coating resistance (R_c) , respectively.

Potentiodynamic analysis

The anticorrosive properties of the three UFP composite coatings were estimated using the potentiody-namic polarization analysis.^{37,49} Figure 11 shows the Tafel plots of tinplates with and without coatings (GO-SiO₂/UFP, GO-TiO₂/UFP and GO-Y₂O₃/UFP) in 3.5% NaCl after soaking for 18 d. The electrochemical parameters from the polarization curves were obtained and listed in Table 2. According to the polarization curves, the samples coated with GO-TiO₂/UFP displayed more negative corrosion potentials $(E_c,$ -461.48 mV) and significantly lower corrosion current densities (i_c , 1.86×10⁻⁹ A/cm²). By contrast, the GO– Y_2O_3/UFP -coated tinplate substrate exhibited a more positive E_c (-374.82 mV vs SCE), with a significant increase of i_c (1.29×10⁻⁸ A/cm²). However, the corrosion rate (C.R., 2.18×10⁻⁵ mm/a) and corrosion protection efficiency (P.E., 99.59%) of the GO-TiO₂/UFP composite coatings were significantly changed by the reduction of i_c accompanied by a more positive E_c due to the addition of GO-TiO₂.⁴⁹ These results indicated that the GO-TiO₂/UFP coating provided better corrosion protection to the metal substrate than other UFP composite coatings and effectively decreased the corrosion rate of the tinplate. Thus, the anticorrosion



Fig. 8: (a) XPS survey spectrum and high-resolution spectra of $GO-Y_2O_3$, (b) O 1*s*, and (c) N 1*s*

properties of the GO–TiO₂/UFP composite coating were improved by adding GO–TiO₂, especially due to its good distribution within the UFP matrix,⁵⁰ which further reinforced the composite's anticorrosion performance. Well-dispersed GO–TiO₂ embedded in UFP matrix provided a superior barrier effect due to its twodimensional sheet structure and plugging inherent micropores properties, thereby exhibiting superior corrosion protection to the metals.

In this study, the protection efficiency (P.E.) and corrosion rate (C.R.) of composite coatings were used to better understand the corrosion process of metal substrates coated with the UFP composite coatings. The corresponding values were calculated based on equations $(1)^{53}$ and $(2)^{51,52}$ respectively.

$$C.R. = 3.27 \times 10^{-3} \times \frac{i_{corr}}{\rho} \times E_w \tag{1}$$

$$P.E.(\%) = (I_0 - I_c/I_0) \times 100$$
(2)

In equation (1), $E_{\rm W}$ is the equivalent weight of the tinplate (4.01 g) and ρ is the density of the tinplate (7.85 g/cm³). In equation (2), I_0 (μ A/cm²) is the corrosion current of the neat tinplate, while $I_{\rm c}$ (μ A/cm²) is the corrosion current of the tinplate coated with the UFP composite coating. The parameters extracted from the polarization curves were in good agreement with the electrochemical tests (Table 2).

EIS measurements of the composite coatings

The electrochemical impedance spectroscopy (EIS) measurements of the different GO-metal oxide/UFP composite coatings were displayed in the form of the Nyquist plots and Bode diagrams. In addition, the EIS fitted data with suitable electrically equivalent circuits were also shown in the figures for comparison (solid lines). The determination of the corrosion stage plays a key role in the study of corrosion processes. In the initial stage of the corrosion process, the electrolyte solution penetrated into the coating through inherent micropores. In the middle stage, the corrosion reaction occurred. The terminal stage comprises a diffusion process, but UFP polymer wearing is nonconspicuous.^{53–56}

Figures 12 and 14 show the Bode and Nyquist plots of GO–SiO₂/UFP, GO–TiO₂/UFP and GO–Y₂O₃/UFP composite coatings after immersion for 2 and 16 days, respectively.

Figures 12a and 12b, respectively, showed the Nyquist and Bode plots of the GO–SiO₂/UFP, GO– TiO₂/UFP and GO–Y₂O₃/UFP coatings after 2 days of immersion in 3.5% NaCl solution. The radius of the impedance arc of the GO–TiO₂/UFP composite coating was significantly higher than that of the other two composite coatings; the impedance modulus at the low frequency for GO–SiO₂/UFP, GO–TiO₂/UFP and GO–Y₂O₃/UFP coatings was 1.62×10^8 , 1.27×10^{10} and $4.14 \times 10^8 \Omega$ cm², respectively. Signals at the larger radius of the impedance arc correspond to greater anticorrosion resistance and more difficult electron transfer,^{37,57} whereby the GO–TiO₂/UFP composite coating exhibited a significantly higher value than both GO–SiO₂/UFP and GO–Y₂O₃/UFP.



Fig. 9: (a) XPS survey spectrum and high-resolution spectra of GO–SiO₂, (b) C 1s, (c) O 1s, and (d) Si 2s

Table 1:	The XPS results for the $GO-TiO_2$, $GO-Y_2O_3$ and
GO-SiO ₂	sample

Signal	Bond	Energy of bonds/eV	Components/%
0 1 <i>s</i>	Y–O–Si	531.7	27.11
C 1 <i>s</i>	O–Ti–C	284.4	37.12
Si 2 <i>s</i>	Si–O–Si	103.4	76.34
Si 2 <i>s</i>	Si–C	102.5	23.66



Fig. 10: The proposed equivalent circuit used to fit the EIS experimental data

According to Figs. 12a and 12b, one time constant appeared in initial state, which indicated that the corrosion process did not occur, and these three coatings displayed excellent barrier properties. In addition, in Bode plots of the three composite coatings, the



Fig. 11: Potentiodynamic polarization curves for the GO– TiO_2/UFP , GO– Y_2O_3/UFP and GO– SiO_2/UFP composite coatings on tinplate substrates after immersion in 3.5% NaCl solution for 18 days

phase angle of the GO–TiO₂/UFP composite coatings could reach more -90° of the highest value (Fig. 12b) even after immersing for 2 days, which indicated that the GO–TiO₂/UFP composite coatings had pronounced anticorrosive properties. This indicated that incorporation of GO–TiO₂ is a promising approach for

Table 2: Electrochemical parameters obtained from the polarization curves of the UFP coatings containing different contents of GO–TiO₂, GO–Y₂O₃, GO–SiO₂ and MGO

Sample	Composite	<i>E</i> _c /mV	<i>i</i> _c /A/cm ²	$R_{\rm c}/{\rm K}\Omega/{\rm cm}^2$	i _o /A/cm ²	CR/mm/a	PE/%
1	GO-TiO ₂	- 461.48	1.86E-09	1.40×10 ⁴	4.54E-07	2.18×10⁻⁵	99.59
2	$GO - Y_2O_3$	- 374.82	1.29E-08	2.02×10 ³	4.54E-07	1.52×10 ⁻⁴	97.15
3	GO-SiO2	- 400.34	1.08E-08	24.14	4.54E-07	1.27×10 ⁻²	97.62
4	MGO	- 414.91	2.49E-09	1.05×10 ⁴	4.54E-07	2.93×10⁻⁵	99.45
5	UFP	- 509.80	3.73E–08	7.00×10 ²	4.54E-07	4.39×10 ⁻⁴	91.79



Fig. 12: Nyquist (a) and Bode (b) plots of UFP coatings corresponding to $GO-TiO_2/UFP$, $GO-Y_2O_3/UFP$ and $GO-SiO_2/UFP$ after 2 days of immersion in 3.5% NaCl solution; the marker points and solid lines show the experimental and fitted data, respectively



Fig. 13: Nyquist (a) and Bode (b) plots of UFP coatings corresponding to $GO-TiO_2/UFP$, $GO-Y_2O_3/UFP$ and $GO-SiO_2/UFP$ after 16 days of immersion in a 3.5% NaCl solution; the marker points and solid lines show the experimental and fitted data, respectively

improving the barrier properties of the UFP coatings at initial immersion. The corresponding phase angle of the GO–TiO₂/UFP composite coating was the highest among the three UFP composite coatings, which was another clear sign of the improved corrosion resistance of GO–TiO₂/UFP composite coatings.

Figures 13a and 13b showed the Nyquist and Bode plots of the GO–SiO₂/UFP, GO–TiO₂/UFP and GO– Y_2O_3 /UFP composite coatings. GO–TiO₂/UFP maintained a relatively high modulus and phase angle, which may be attributed to the GO–TiO₂ hybrid nanoparticles, including their two-dimensional structure and uniform dispersion properties. Accordingly, it



Fig. 14: The variation of the $|Z|_{0.01}$ $_{Hz}$ value versus immersion time in a 3.5% NaCl solution for GO–TiO₂/UFP, GO–Y₂O₃/UFP and GO–SiO₂/UFP samples

was confirmed that the $GO-TiO_2$ composite coating remarkably improved the corrosion resistance of the UFP coating.

The variation of the |Z|0.01 Hz values of the GOmetal oxide/UFP samples vs immersion time is shown in Fig. 14. The |Z|0.01 Hz values of the GO-TiO₂/UFP composite coating were higher than those of the two other samples during the immersion, indicating a better corrosion protection performance of the GO-TiO₂/ UFP composite coating due to the barrier effect of the GO-TiO₂ in the UFP polymer. The impedance values decreased for all UFP composite coatings with the increase of immersion time. It suggested that the corrosive electrolyte gradually diffused into the coating, thereby increasing the porosity and presence of electrolyte pathways.¹² Obviously, these results were in good accordance with the electrochemical tests.

According to Table 3, the GO–TiO₂/UFP coating had higher R_c than the other two samples. Indeed, the R_c values of the UFP composite coatings decreased with prolonged immersion time in the order of UFP < GO–SiO₂/UFP < GO–Y₂O₃/UFP < GO–TiO₂/UFP. The increase of the R_c value indicated the good dispersion of GO–TiO₂ in the coating, which improved its resistance against the uptake of corrosive species by decreasing its porosity.^{58,59}

Chemical resistance of the UFP composite coatings

To demonstrate the superior alkali resistance of the GO–SiO₂/UFP, GO–TiO₂/UFP and GO–Y₂O₃/UFP composite coatings, the chemical resistance of the coatings was examined by immersing coated samples in 10% NaOH, 30% H₂SO₄ and 3% NaCl for up to 14 days at room temperature, in conjunction with visual observations for cracking, blistering or other signs of solvent attack on the coatings surface. The results of the chemical resistance tests conducted on the com-

Table 3: Electrochemical parameters obtained from the EIS spactra of the UFP coatings containing different contents of $GO-TiO_2$, $GO-Y_2O_3$ and $GO-SiO_2$

Sample	Composite	$R_{\rm c}/{\rm K}\Omega/{\rm cm}^2$	CPE1	
			$Y_1/\mu\Omega^{-1}\mathrm{m}^{-2}S^n$	n ₁
1	GO-TiO ₂	1.27E+07	9.86E-04	0.96085
2	$GO-Y_2O_3$	4.14E+05	9.33E-04	0.96761
3	GO-SiO ₂	1.62E+05	1.09E-03	0.95254

posite coatings are listed in Table 4 as a reference for the electrochemical impedance spectroscopy (EIS) data. The GO–SiO₂/UFP showed a better alkali resistance than the other UFP composite coatings, with no damage after 14 days of immersion in a 10% NaOH solution, which indicated that the alkali resistance could be improved via the chemical reaction between GO–SiO₂ and UFP by decreasing the hydroxyl group content of pure UFP coating.¹

Corrosion protection mechanism

An explanation of the corrosion-resistance mechanisms of the GO–metal oxide/UFP composite coating was proposed according to the preceding observations and analysis.

Based on the coating capacitance [equations (3) and (5)]^{60–62} and the Brasher–Kingsbury equation [equation (4)], it was assumed that the transport of water through the polymer coating follows Fick's law:^{63,64}

$$C_c = \varepsilon \varepsilon_0 A / d \tag{3}$$

$$\phi_w = \frac{\log \frac{C_c}{C_0}}{\log \varepsilon_w} \tag{4}$$

$$C_c = (Y_0)^{\frac{1}{n}} \cdot \left(R_{\text{pore}}\right)^{\frac{1-n}{n}} \tag{5}$$

In equation (3), A is the active area, d is the coating thickness, ε is the relative dielectric constant of the UFP composite coating and ε_0 the permittivity of vacuum (8.85 × 10⁻¹⁴ F cm⁻¹). In equation (4), $\varepsilon_{\rm w}$ is the dielectric constant of water ($\varepsilon_w \approx 80$), C_c is the coating capacitance at immersion time t, and C_0 is the initial capacitance of the dry coating. The volume fraction of water uptake (φ_w) in the GO-TiO₂/UFP coatings can be calculated from their capacitance (C_c). In equation (5), the coating capacitance value was obtained using the EIS method including the admittance parameter (Y_0) and an exponent (n). The constant phase element consisting of the two parameters represented the deviation from ideal capacitive behavior. According to equation (4), this showed that the effect of an increase of the dielectric constant with

Sample	Composition		Chemical medium			
			30% H ₂ SO ₄	10% NaOH	3% NaCl	
1	GO-Y ₂ O ₃	UFP	+	+	+	
2	GO-TiO ₂	UFP	+	+	+	
3	$GO-SiO_2$	UFP	+	+	+	
4	UFP		-	-	-	

Table 4: Resistance of the GO–TiO₂/UFP, GO–Y₂O₃/UFP and GO–SiO₂/UFP composite coatings against chemical attack after immersion in 30% H_2SO_4 , 10% NaOH and 3% NaCl solution at room temperature

the permeation of water may increase the C_c value. That is, a change of the capacitance value indicates water uptake via the GO-metal oxide/UFP polymer film. In the case of the GO-TiO₂/UFP sample, corrosive electrolytes diffused into the coating increasing the amount of water uptake. Subsequently, crosslinking density of the UFP composite coating contributed to the significant decrease in the amount of water uptake with increasing immersion time. This indicated that silanols reacted with UFP by hydrolysis and condensation. It could be confirmed that the electrochemical corrosion resistance of the GO-TiO₂/UFP composite coating was superior to that of the other GO-metal oxide/UFP materials since GO-TiO₂ served as a barrier that blocked the diffusion paths of corrosive agents.

It is not difficult to see that the protection efficiency (P.E.) of the GO-TiO₂/UFP coatings increased remarkably by adding 3.0 wt% GO-TiO₂, which serves to demonstrate that the GO-TiO₂/UFP composite coating exhibited anticorrosive properties of metallic substrates by making the diffusion pathways of corro-sive agents in the UFP more tortuous.^{65,66} According to a few reports, the atomic/molecular situation of the interface of metal and organic coatings was assessed based on OM (quantum mechanics) approaches.⁶⁹ The OM computations also evidenced that with increasing the amino groups bound to GO surface, the interactions of UFP with modified GO surface strengthened, which could result in improved properties of prepared coatings of UFP and modified GO. Inclusion of GO- SiO_2 , GO-TiO₂ and GO-Y₂O₃ into the UFP coating improved its anticorrosion properties. The highest improvement of the polymer barrier performance was seen in the case of GO-TiO₂ composites. As a result, owing to stronger interfacial interactions, a metal substrate with higher OH coverage will be coated with a thicker cured-UFP layer, which leads to enhanced protection of carbon steel.^{67–70} Accordingly, a corrosion protection mechanism for GO-TiO₂/UFP composite coatings could be proposed as shown in Fig. 15.



Fig. 15: Schematic representation of the most likely mechanism of corrosion protection by the GO-metal oxide/UFP composite coatings on tinplate substrates

Conclusions

Metal oxide nanoparticle-decorated graphene oxide composites (GO–SiO₂, GO–TiO₂ and GO–Y₂O₃) were synthesized via a simple two-step solution approach. Their structure and morphology were characterized and they were incorporated into UFP-based coatings. The corrosion-resistance properties of the GO-metal oxide/UFP composite coatings were investigated by various techniques. The main findings are as follows: (1) Compared with the two other GO-metal oxide composites, the dispersion, compatibility, barrier properties and corrosion resistance of the GO-TiO₂/UFP composite coating were dramatically enhanced. (2) The addition of $GO-SiO_2$ appears to be an appropriate approach to evidently improve the alkali resistance of UFP at low doses. At 0.1 wt% and above, the addition of GO-SiO₂ drastically increased the alkali resistance of the resulting GO-SiO₂/UFP composite coating due to the chemical reaction between GO-SiO₂ and UFP, providing a more effective barrier against the ingress of corrosive ions.

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