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Recovery of Astaxanthin from Shrimp Cooking Wastewater: Optimization of Astaxanthin Extraction by Response Surface Methodology and Kinetic Studies

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Abstract A protein and astaxanthin-concentrated fraction $(R_{\rm f})$ can be recovered from shrimp cooking wastewater by ultrafiltration at 300 kDa, indicating that astaxanthin is somehow associated to membrane-retained proteins. Response surface analysis showed that astaxanthin can be extracted from $R_{\rm f}$ using sunflower oil (3:1 v/v) under milder conditions (T< 40 °C) than directly from shrimp exoskeleton. Modeling astaxanthin extraction kinetics at 30 °C revealed that the process is a consequence of both mass transfer and hydrogen bonding between astaxanthin and oil. The freeze-dried concentrate (FR_f) showed two-phase extraction profiles with a much faster pigment recovery observed at 30 °C compared to the liquid form (R_f) . The best yields of astaxanthin extraction were not further improved after hydrolysis with alcalase at 45 °C for 30 min (HR_t), although higher yields were obtained when both $R_{\rm f}$ and $LR_{\rm f}$ were extracted in the presence of 200 mg/L butylated hydroxyanisole or ethoxyquin. Astaxanthin from this shrimp by-product has low thermal stability in oil at high temperatures (60 and 70 °C), suggesting the carotenoid is mainly free as a result of the cooking process and not bounded to proteins or lipids as it occurs in its natural form.

Keywords Astaxanthin · Sunflower oil · Shrimp by-products · Extraction kinetics · Mathematical modeling · Surface response methodology

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Introduction

The fish processing industry generates several wastewater effluents (washing, thawing, rinsing, and cooking), which involve serious problems of pollution and environmental health. Among these effluents, cooking juice (more than 40 % of the total) contains a high saline content and organic load (Cros et al. 2006). To reduce their pollutant content, cooking wastewaters need to be treated, increasing the cost of the manufacturing process. So, an alternative to reduce wastewater processing costs would be the recovery of products with high added value such as proteins, aromas, and flavors (Vandajon et al. 2002).

During the last years, the application of membrane technology as the main method of separation, concentration, and purification of these valuable compounds from fish processing residual materials has been highly developed (Afonso et al. 2004; Murado et al. 2009, 2010). But also, given the carotenoprotein character of the pigmented by-product from crustacean process wastewaters (Cano-López et al. 1987; Simpson and Haard 1985), these effluents can be a possible source of carotenoids.

Astaxanthin (3,3-dihydroxy- β , β -carotene-4,4 dione) is a ketocarotene widely used in aquaculture as feed additive for the pigmentation of salmonid meat and shrimp and lobster shells. The majority of commercial astaxanthin for aquaculture is industrially produced by chemical synthesis (Rodríguez-Sáiz et al. 2010), although its increasing interest, due to novel applications as nutraceutical in the food, pharmaceutical, and cosmetic industries (Del Campo et al. 2007), has led to the search for new natural sources of astaxanthin. In this way, many studies describe the recovery of astaxanthin from shrimp by-products such as head and body skeleton (Armenta-López et al. 2002; Bi et al. 2010; Sachindra and Mahendrakar 2005). De Holanda and Netto (2006) also reported obtaining astaxanthin as a valuable subproduct of the

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chitin production from shrimp processing waste. Different extraction methods are applied for the recovery of astaxanthin from shrimp solid by-products such as enzymatic hydrolysis (De Holanda and Netto 2006), fermentative process (Sachindra and Bhaskar 2008), organic solvents (Sachindra et al. 2006), and vegetable oils (Chen and Meyers 1982; Handayani et al. 2008; Sachindra and Mahendrakar 2005).

The optimization of these extraction processes is usually conducted using one-factor-at-a-time approach; however, the use of response surface methodology (RSM) allows predicting optimal extraction conditions and interactions between variables. In fact, using this methodology to optimize alkali (Liu et al. 2012), solid-phase (Zhu and Row 2013), and supercritical CO₂ (Yang et al. 2013), astaxanthin extraction from shrimp by-products has been recently reported. Also, factorial design methodologies have been successfully applied to the optimization of astaxanthin extraction using vegetable oils (Sachindra and Mahendrakar 2005) and organic solvents (Sachindra et al. 2006).

Astaxanthin in crustacean shells is mainly esterified or complexed with proteins (Matsuno 2001), increasing pigment stability. However, when extracted from natural sources, astaxanthin is unstable due to its sensitivity to various environmental factors such as light, oxygen, acidity, and heat (Mezzomo et al. 2011), causing the loss of its bioactivity. Lactic acid fermentation (Armenta-López et al. 2002) and the addition of antioxidants (Armenta-López et al. 2002; Chen and Meyers 1982) have improved the stability of astaxanthin, thereby leading to increase astaxanthin yield after extraction with different solvents.

In the present study, we describe a feasible process using membrane technology for the recovery of astaxanthin from shrimp cooking wastewater. This methodology allows obtaining a protein and astaxanthinconcentrated fraction that can be used as additive in the animal feed industry, while reducing the costs of wastewater treatment. This study also reports the optimized conditions (temperature, time, oil/waste ratio, and use of antioxidants) for carotenoid extraction using sunflower oil and proposes kinetic models that would be helpful for the further scale-up of the process.

The company Bajamar Séptima, Pescanova Group (A

Coruña, Galicia, Spain) kindly provided the cooking

wastewater from the industrial manufacturing of shrimp

Materials and Methods

Materials

(*Penaeus vannamei*). Shrimp cooking juice was sampled and immediately stored at -18 °C until further use.

Analytical Determinations

Protein, total nitrogen, total sugar, and reducing sugar contents were determined from the samples taken before storage. Total nitrogen was determined by the method of Havilah et al. (1977). Soluble proteins were determined using the method of Lowry et al. (1951); total sugar content by the phenol-sulfuric acid method (Dubois et al. 1956), according to Strickland and Parsons (1968); and reducing sugars were quantified by means of a 3,5-dinitrosalicylic reaction (Bernfeld 1951).

Recovery of Astaxanthin by Ultrafiltration of Shrimp Wastewater

The concentration of astaxanthin from shrimp cooking juice consisted of ultrafiltration-diafiltration using a spiral polyethersulfone membrane (Millipore Prepscale) of 0.56 m² with molecular weight cut-off (MWCO) of 300 kDa. The operation mode was as follows: an initial phase of ultrafiltration (UF) with total recycling of retentate, immediately followed by diafiltration (DF). During UF, the inlet pressure remained constant to determine the drops of flow rate due to the increased concentration of the retentate and to possible membrane adhesions. The final retentate (after DF) was divided into two batches: one was directly stored at -18 °C $(R_{\rm f})$ and the other freeze-dried $(FR_{\rm f})$ and stored at 4 °C for further analysis. Both permeates in the UF and DF phase were discarded after analysis. The kinetics of UF and DF of the effluent were defined by the protein levels as determined by two procedures: the method of Lowry and total nitrogen multiplied by 6.25.

Enzymatic Hydrolysis Process

The enzymatic hydrolysis of the concentrated fraction was performed using a commercial protease, alcalase 2.4 L from Novo Co. (Novozyme Nordisk, Bagsvaerd, Denmark) at a ratio of 0.01:1 (Anson units per milliliter, AU/mL) enzyme/ substrate. One AU is the amount of enzyme that, under standard conditions, digests hemoglobin at an initial rate that produces an amount of trichloroacetic acid-soluble product that gives the same color with the Folin reagent as one milliequivalent of tyrosine released per minute. The pH of the retentate was adjusted to pH 9.0 using 5 mM Britton-Robinson buffer, and proteolysis was carried out in a water bath with soft agitation at 45 °C for 30 min. The hydrolysate (*HR_f*) was stored at -18 °C until further use.

Combined Effect of Temperature, Heating Time, and Oil/Waste Ratio on Astaxanthin Extraction

A second-order rotatable design, based on three variables at five levels (Akhnazarova and Kafarov 1982; Box et al. 2005), was used to study the combined effect of temperature (T), time (t), and oil/waste ratio (R) on the yield of recovered astaxanthin from shrimp process wastewater. The joint effect of the three variables was studied in the $R_{\rm f}$ fraction.

The experimental domains of each variable were 40– 100 °C for *T*, 30–300 min for *t*, and 1.0–3.0 (ν/ν) for *R*. The design consisted of 20 experiments with four (2²) factorial points, four axial points to form a central composite design with α =1.682, and six center points for replication. The experimental domain and codification of the variables are shown in Table 1. Experimental data were fitted to the following empirical model with the yield of astaxanthin as dependent variable:

$$A_{\rm e} = b_0 + \sum_{i=1}^3 b_i x_i + \sum_{i=1}^3 b_{ii} x_i^2 + \sum_{i=1}^2 \sum_{j=i+1}^3 b_{ij} x_i x_j \tag{1}$$

Statistical significance of the coefficients was evaluated by Student's *t* test (α =0.05). Consistency of the model was tested by Fisher's *F* test (α =0.05), using the following mean squares ratios:

	The model is acceptable if
F_1 =Model/Total error	$F_1 \ge F_{den}^{num}$
$F_2 = (Model + Lack of fitting)/Model$	$F_2 \leq F_{den}^{num}$
F_3 =Total error/Experimental error	$F_3 \leq F_{den}^{num}$
F_4 =Lack of fitting/Experimental error	$F_4 \leq F_{den}^{num}$

Data fitting, parametric estimation performed by minimization of the sum of quadratic differences between experimental and model-predicted values, and significance tests both for

 Table 1
 Experimental domain and codification of independent variables in the factorial design

Coded values	Natural values				
	<i>T</i> (°C)	t (min)	R (L:L or L:S)		
-1.68 (-α)	40.0	30	1.0		
-1	52.2	85	1.4		
0	70.0	165	2.0		
+1	87.8	245	2.6		
+1.68 (+ <i>α</i>)	100.0	300	3.0		

Codification: $V_{\rm c} = (V_{\rm n} - V_0) / \Delta V_{\rm n}$

Decodification: $V_{\rm n} = V_0 + (\Delta V_n \times V_{\rm c})$

 $V_{\rm n}{=}{\rm natural}$ value in the center of the domain, $\Delta V_{\rm n}{=}{\rm increment}$ of $V_{\rm n}$ for unit of $V_{\rm c}$

parameters and model were performed with the *Microsoft Excel* spreadsheet.

Extraction of Astaxanthin Using Sunflower Oil

The extraction of astaxanthin in sunflower oil was carried out from the final retentate (R_f), but also two other pretreated samples were studied as astaxanthin sources. For this purpose, R_f was hydrolyzed using alcalase (HR_f) or freeze-dried (FR_f) in order to test if the carotenoid was more available to sunflower oil in any of these forms.

Extraction from both R_f and HR_f was performed using the optimized conditions defined by a second-order rotatable design, as previously described. In case of FR_{f_2} the oil/waste ratio was increased to 100:1, an adequate relation due to the increased concentration of the carotenoid as a consequence of the freeze-drying process. In the latter fraction, the extraction was studied at different temperatures: 30, 40, 50, and 60 °C. Extractions were carried out in stirred 250 mL flasks and appropriate R_f or HR_f volumes or FR_f masses were added to sunflower oil preheated at the appropriate temperature. Duplicate samples were removed after different incubation times. Then samples were filtered through washed glass wool and centrifuged at 5,000g for 15 min, and the pigmented oil layer from the supernatant was recovered. The astaxanthin concentration was measured spectrophotometrically at λ_{max} (487 nm: A_{487}), and the carotenoid yield as astaxanthin, for liquid ($\mu g/mL$) or solid ($\mu g/g$) samples, was determined using the following equation (Sachindra and Mahendrakar 2005):

$$Y = \frac{A_{487} \times V_{\text{oil}} \times 10^6}{100 \times V_{\text{w}} \times E} \tag{2}$$

where *Y* is the astaxanthin yield per volume of bulk liquid ($\mu g/mL$) or per shrimp waste mass ($\mu g/g$), V_{oil} is the volume of recovered pigmented oil, V_w is the volume of waste (for R_f and HR_f samples) or the weight of freeze-dried powder (for FR_f samples), and *E* is the specific extinction coefficient.

Finally, the effect of the addition of butylated hydroxyanisole (BHA) or ethoxyquin (ETQ) at 200 mg/L on the astaxanthin extraction was also studied in both $R_{\rm f}$ and FR_{f} .

Mathematical Modeling of Extraction Kinetics

The dynamics of astaxanthin extraction were modeled using a mass transfer kinetic model (Handayani et al. 2008):

$$Y = Y_{e}[1 - \exp(-k_{L}at)]$$
(3)

where *Y* and *Y_e* are the astaxanthin yield in bulk liquid and at equilibrium per volume (μ g/mL) or per mass of shrimp waste (μ g/g), respectively; *t* is the time of the extraction

process (min); and $k_{\rm L}a$ is a volumetric mass transfer coefficient (min⁻¹).

We also used a pseudo-second-order model that accounts for the esterification between hydroxyl groups in free astaxanthin and fatty acids in sunflower oil (Handayani et al. 2008). Considering that the concentration of astaxanthin at the beginning of the extraction process is zero and rewriting the equation in terms of yield:

$$Y \frac{Y_{\rm e}^2 k_{\rm A} t}{(1+Y_{\rm e} k_{\rm A} t)} \tag{4}$$

where *Y* and *Y*_e are the astaxanthin yield in bulk liquid and at equilibrium per volume (μ g/mL) or per mass of shrimp waste (μ g/g), respectively; *t* is the time of the extraction process (min); and *k*_A is a reaction constant (min⁻¹).

Finally, when a two-phase extraction profile was observed, data were modeled using the sum of two mass transfer kinetic models (biphasic model) with different volumetric mass transfer coefficients and yields at equilibrium (Y_{e1} and Y_{e2}):

$$Y = Y_{e1}[1 - \exp(-k_{L1}at)] + Y_{e2}[1 - \exp(-k_{L2}at)]$$
(5)

where Y_{e1} and Y_{e2} are the astaxanthin yields per mass of shrimp waste (µg/g) of the first and second phase, respectively; *t* is the time of the extraction process (min); $k_{L1}a$ and $k_{L2}a$ are the volumetric mass transfer coefficients of the first and second phase, respectively (min⁻¹).

Considering that the sum of both Y_{e1} and Y_{e2} is the maximum yield of extraction achieved (Y_{m}), and rewriting Eq. 5 in terms of a global process with a single yield at equilibrium (Y_{e}), we have:

$$Y = Y_{e}[1 - \exp(-k_{L1}at)] + (Y_{m} - Y_{e})[(1 - \exp(-k_{L2}at))]$$
(6)

For comparative purposes, data were normalized by dividing astaxanthin yields (μ g/mL or μ g/g) by the highest yield (μ g/mL or μ g/g) of astaxanthin extracted from each fraction (R_{f} , HR_{f} , or FR_{f}) regardless of the experimental conditions assayed in each case.

Numerical and Statistical Methods

Fitting procedures and parametric estimates from the experimental results were performed by minimization of the sum of quadratic differences between observed and model-predicted values, using the nonlinear least-squares (quasi-Newton) method provided by the macro *Solver* of *Microsoft Excel XP* spreadsheet. Then, confidence intervals from the parametric estimates (Student's *t* test) and consistence of mathematical models (Fisher's *F* test), both with α =0.05, were determined using *SolverAid* macro, which is freely available from de

Levie's Excellaneous website: http://www.bowdoin.edu/ ~rdelevie/excellaneous/.

Results and Discussion

Ultrafiltration of Shrimp Wastewater

The shrimp cooking wastewater utilized in this work had a pH of 6.07 ± 0.04 , a protein content of 1.92 ± 0.08 g/L, and a total soluble sugar concentration of 0.21 ± 0.02 g/L. In the diafiltration with constant volume (filtration flow=water intake flow), the concentration (or the total amount) of a permeable solute in the retentate follows a first-order kinetics (Amado et al. 2013; Murado et al. 2010):

$$C = C_{\rm f} + C_0 \exp[-(1-s)D_{\rm r}]$$
(7)

where *C* is the concentration of the permeable solute in the retentate, with C_0 as the initial value. C_f is the final asymptotic value if only a part of a polydisperse solute is permeable. When using normalized values (%): $C_0+C_f=100$, with $C_f=0$ when the solute is completely permeable. The parameter *s* is the solute-specific retention, which varies between 0 (the solute is filtered as the solvent) and 1 (the solute is totally retained). D_r is the relative diavolume or the ratio volume of added water/constant retentate volume.

This equation satisfactorily described the kinetics of protein diafiltration process with a molecular cut-off at 300 kDa (Fig. 1). The values of the coefficients were $C_f=75.9$ % and s=0.381, which means a rather high retention of the protein and also a specific retention that would demand a relative diavolume of 5.7 to eliminate 99 % of permeable protein. In a common diafiltration, with an initial volume of 2 L of concentrated shrimp wastewater and working with a relative diavolume of 5, at 50-55 °C and 2 atm (~30 psi), the protein concentration in the retentate can be maintained around 15-20 g/L, with a filtrate flow that decays 40-45 % during the process and maintains an average value of 325 mL min⁻¹ m⁻² (data not shown). Under these experimental conditions, the values of protein calculated by the Lowry method or total nitrogen×6.25 were almost indistinguishable (Fig. 1). These results indicate a high retention of peptidic material after ultrafiltration of shrimp cooking wastewater despite the heat treatment during shrimp processing.

The ultrafiltration-diafiltration process with a molecular cut-off at 300 kDa showed a high retention of astaxanthin despite the low molecular weight (597 Da) of this pigment. During the ultrafiltration phase, the initial permeates showed slight yellowish coloration, completely disappearing after diafiltration and leading to an intense colored retentate. In fact, a concentration factor of 13 is achieved after 300 kDa



Fig. 1 Ultrafiltration-diafiltration kinetics of shrimp (*Penaeus vannamei*) cooking wastewater using a polyethersulfone membrane with MWCO at 300 kDa. *Left*: concentration of retained protein in linear relation with the factor of volumetric concentration (fc) showing experimental data (*points*) and theoretical profiles (*discontinuous line*). *Right*: progress of

UF-DF of shrimp cooking wastewater, reaching average astaxanthin concentrations between 10 and 13 $\mu g \ mL^{-1}$ in the retentate extracted with sunflower oil.

These results suggest that aggregation phenomena are occurring due to the hydrophobic properties of astaxanthin. It is known that astaxanthin from the shell matrix of crustaceans is mainly found esterified or complexed with proteins (Matsuno 2001). Therefore, astaxanthin in the retentate must be forming polymeric aggregates (Velu et al. 2003) and/or bound to macromolecules, mainly proteins, that are retained during ultrafiltration using the reported cut-off membrane.

Accordingly, the 300 kDa concentrated fraction could be used as a supplement for animal diets due to its high astaxanthin and protein content. In the same way, Pérez-Santín et al. (2013) obtained a concentrate rich in lipids and proteins with crustacean aroma, attractive orange coloring, and antioxidant and ACE-inhibitory capacities making it attractive for the formulation of feeds or functional foods.

Enzymatic Hydrolysis

The use of proteolytic enzymes has been widely reported to disrupt the protein-carotenoid complex and increase astaxanthin extraction from solid shrimp by-products (De Holanda and Netto 2006; Sowmya et al. 2011). With this purpose, in a preliminary experiment, the hydrolysis conditions using alcalase were optimized to maximize the astaxanthin recovery without compromising its stability. Different temperatures (35, 45, and 55 °C) and times (30, 60, 90, and 120 min) of hydrolysis were assayed, maintaining a constant ratio of 0.01:1 (AU/mL) enzyme/substrate. After each incubation time, samples were withdrawn and quickly cooled down in an ice-water bath for 5 min to inactivate the protease. Then astaxanthin was extracted in sunflower oil at 70 °C, according to the optimal conditions reported in the



protein (*empty circle*) and nitrogen (*filled circle*) retention with the increase of diavolume from DF process (D). For clarity, confidence intervals (in all cases, less than 5 % of the experimental mean value; α =0.05; n=2) were omitted

literature for the extraction of carotenoids from shrimp waste using vegetable oils (Sachindra and Mahendrakar 2005), for 30 min.

Results are shown in Fig. 2 where the yields of astaxanthin recovery were calculated according to Eq. (2). The highest recovery of astaxanthin under these conditions (70 °C, 30 min) is obtained at 45 °C, falling a 70 % on average when the temperature of hydrolysis is 35 or 55 °C. Moreover, astaxanthin yields decreased correlatively with the incubation time at all temperatures tested. At the optimum temperature, the recovery of astaxanthin decreased about 36 % when the reaction time increased from 30 to 120 min. Taking into account these results, the hydrolysis conditions selected were as follows: 30 min at 45 °C using a ratio of 0.01:1 (AU/mL) alcalase/substrate.



Fig. 2 Recovery of astaxanthin in sunflower oil from hydrolysates of the 300 kDa concentrated fraction (R_{t}). Hydrolysis was performed at different temperatures: 35 (*empty triangle*), 45 (*empty circle*), and 55 °C (*filled circle*)

Combined Effect of Temperature, Heating Time, and Oil/Waste Ratio on the Extraction of Astaxanthin

The effects of temperature, heating time, and oil/waste ratio on the yield of astaxanthin recovery are important factors that must be considered for a further scale-up of the process. Although the combined effect of these variables can be studied using a one-factor-at-a-time approach, this methodology cannot predict the optimal reaction conditions, ignores interactions, and may lead to misleading conclusions. In this regard, experimental design methodologies (Box et al. 2005) are more efficient than the one-factor-at-a-time approach. Response surface methodology uses statistical and mathematical techniques to evaluate the combined effect of factors instead of single factors at different times.

In this work, a second-order rotatable design, based on three variables at five levels (Akhnazarova and Kafarov 1982; Box et al. 2005), was used to study the combined effect of temperature (*T*), time (*t*), and ratio oil/waste ration (*R*) on the yield of astaxanthin recovery. The experimental domain is shown in Table 1, with temperatures and oil/waste ratios selected according to previous reported conditions for the extraction of astaxanthin using vegetable oils (Sachindra and Mahendrakar 2005). Applying the significance criteria specified in the "Materials and Methods" section, the empirical model obtained for the theoretical yield of extracted astaxanthin (A_e) as a function of the three processing variables was:

$$A_{\rm e} = 8.23 - 1.53T + 0.69R - 1.15tT + 1.11tR$$
$$+ 0.53tTR - 0.43T^2 \tag{8}$$

The response surfaces obtained varying two independent variables, when the third variable is kept at a constant value, are depicted in Fig. 3, and the complete statistical analysis is shown in Table 2. The analysis of variance indicates that the model is significant (α =0.05) and the adjusted R^2 value shows

Fig. 3 Response surfaces of the combined effect of temperature (T) and ratio oil/waste (R) (*left*) and temperature (T) and time of extraction (t) (*right*) on the predicted yield of extracted astaxanthin (Y) according to Eq. (8)

a good correlation with the experimental data. Besides, according to the statistical analysis, all the parameters in Eq. (8) were significant.

The response surface for astaxanthin yield as a function of temperature and oil/waste ratio (Fig. 3, left) indicates that the extraction yield increases linearly with the oil/waste ratio. At high temperatures, the response increases notably (96 % within the experimental domain) with the proportion of extracting agent. By contrast, at low extraction temperatures, the differences on the astaxanthin yield by varying the phase relationship are much lower (20 %). It should also be noted that at high temperatures and low phase relationships, a degradation of the pigment is observed resulting in practically null values of recovered astaxanthin. Figure 3 (right) further confirms these results since it shows that the increase in the extraction time has an effect on astaxanthin recovery only at low temperatures. This result also agrees with that reported by Pu et al. (2010), who found that shrimp astaxanthin degradation in flaxseed oil was significantly influenced by temperature, with increased degradation rates at 50 and 60 °C compared to 30 and 40 °C using a 1:1 (w/v) phase relationship.

Although an absolute maximum response was not achieved within the experimental domain, maximal yields can be obtained at low temperature (<40 °C), high oil/waste ratio (3:1 v/v), and high incubation time (>4 h). Our results also suggest that the extraction could be performed at lower temperatures (25–30 °C) without appreciable loss in astaxanthin yield and even improving pigment recovery.

Interestingly, our results reveal that astaxanthin can be recovered from shrimp cooking wastewaters using milder conditions than the usual high temperatures (Sachindra and Mahendrakar 2005) and organic solvents (Sachindra et al. 2006) utilized for the extraction of astaxanthin from crustacean shells. The fact that astaxanthin is more easily extracted from the liquid effluent than from solid by-products is likely to be due to the cooking process. In fact, several authors suggest that cooking can break the carotenoid-protein complex, releasing the carotenoid compounds and facilitating its



Table 2 Results of the factorial design of the combined effect of temperature (T), time (t), and oil/waste ratio (R) on the yield of recovered astaxanthin from shrimp process wastewater with sunflower oil according to Eq. (1) and analysis of significance of the proposed model

Т	t	R	A	A _e	Coefficients	Student's t	Model
-1	-1	-1	8.16	8.09	8.23	35.92	8.23
1	-1	-1	6.96	8.38	-1.53	10.08	-1.53 <i>T</i>
-1	1	-1	9.61	9.22	0.06	0.41	t (NS)
1	1	-1	1.69	2.79	0.69	4.53	0.69 <i>R</i>
-1	-1	1	7.81	8.28	-1.15	5.81	-1.15 <i>Tt</i>
1	-1	1	5.97	6.48	0.37	1.84	TR (NS)
-1	1	1	11.61	11.77	1.11	5.61	1.11 <i>tR</i>
1	1	1	7.26	7.45	0.53	2.64	0.53 <i>TtR</i>
-1.682	0	0	8.95	9.61	-0.43	2.88	$-0.43T^{2}$
1.682	0	0	5.59	4.45	-0.07	0.44	t^2 (NS)
0	-1.682	0	8.41	8.23	-0.19	1.26	R^2 (NS)
0	1.682	0	8.17	8.23			
0	0	-1.682	7.07	7.07			
0	0	1.682	8.90	9.39	Average value	7.77	
0	0	0	7.22	8.23	Expected average value	8.22	
0	0	0	8.08	8.23	$Var(E_e)$	0.316	
0	0	0	8.31	8.23	<i>t</i> (α<0.05; <i>ν</i> =6)	2.447	
0	0	0	8.79	8.23			
0	0	0	8.22	8.23			
0	0	0	8.69	8.23			
	SS	ν	ν	QM	Mean square ratios		
Model (M)	64.62	_	6	10.770	$QM_M/QME=18.6$	$F_{13}^6(\alpha = 0.05)$	= 2.915
Error (E)	7.53	-	13	0.579	$QM(_{M+LF})/QM_{M}=0.504$	$F_6^{13}(\alpha = 0.05)$	= 3.976
Exp. error (E_e)	1.578	6	-	0.263	QM_E/QM_{Ee} =2.201	$F_6^{13}(\alpha = 0.05)$	= 3.976
Lack of fit (LF)	5.95	7	-	0.850	QM_{LF}/QM_{Ee} =3.231	$F_{6}^{7}(\alpha = 0.05)$	= 4.207
Total	72.15		19		$R^2 = 0.896$ Adjusted $R^2 = 0.847$	~ ·	

Independent variables according to Table 1

A experimental astaxanthin concentration (μ g/mL), A_e expected astaxanthin concentration (μ g/mL), NS nonsignificant coefficient, SS sum of squares, ν degrees of freedom, QM quadratic means of model (M), E total error, E_e experimental error, LF lack of fit



Fig. 4 Astaxanthin extraction kinetics (30 °C) from R_f (*filled circle*) and HR_f (*filled triangle*) fractions, using increasing oil/waste ratios: 1:1 (**a**); 2:1 (**b**), and 3:1 (**c**). Experimental data (*points*) and fittings to Eqs. (3) (*broken line*) and (4) (*solid line*) are shown

Model	Parameters	$R_{ m f}$			HR_{f}		
		1:1	2:1	3:1	1:1	2:1	3:1
Eq. (3)	Y _e	0.72±0.04	0.87±0.02	0.97±0.04	0.94±0.06	0.97±0.04	0.94±0.05
	$k_{\rm L}a$	$0.0057 {\pm} 0.0015$	$0.0103 {\pm} 0.0013$	$0.0072 {\pm} 0.0013$	$0.0083 {\pm} 0.0027$	$0.0118 {\pm} 0.0031$	0.0080 ± 0.0022
	R^2	0.985	0.996	0.990	0.970	0.984	0.978
Eq. (4)	Ye	$0.79 {\pm} 0.03$	$0.91 {\pm} 0.04$	$1.00 {\pm} 0.04$	$1.00 {\pm} 0.03$	$1.00 {\pm} 0.02$	$1.00 {\pm} 0.03$
	k _A	0.0116 ± 0.0029	$0.0212 {\pm} 0.0013$	$0.0131 {\pm} 0.0035$	$0.0132{\pm}0.0031$	$0.0235 {\pm} 0.038$	$0.0130 {\pm} 0.0032$
	R^2	0.994	0.988	0.997	0.995	0.999	0.994

Table 3 Parametric estimations and determination coefficients of Eqs. (3) and (4) applied to the extraction of astaxanthin from the retentate obtained by UF-DF of shrimp cooking wastewaters, before (R_f) and after

hydrolysis with alcalase 2.4 L (HR_{f}). Extractions were carried out at 30 °C using different oil/waste ratios (1:1, 2:1, and 3:1 ν/ν)

 Y_e normalized astaxanthin yield at equilibrium (dimensionless), $k_L a$ volumetric mass transfer coefficient (min⁻¹), k_A reaction constant (min⁻¹)

extraction (Hornero-Méndez and Mínguez-Mosquera 2007; Mezzomo et al. 2011).

Mathematical Modeling of Astaxanthin Extraction Kinetics

Optimal values from the factorial design were applied to further improve astaxanthin yield, and so extraction kinetics were performed at low temperature (30 °C) and increasing extraction times. Extraction kinetics from R_f and HR_f at different oil/waste ratios and their predicted profiles using Eqs. (3) and (4) are shown in Fig. 4. All parameters were statistically significant (Student's *t* test, α =0.05), and the predictive ability of both equations was high with a goodness of fit of not less than 0.970 (Table 3).

Nevertheless, the pseudo-second-order model (Eq. (4)) showed better correlations (R^2) than the mass transfer kinetic model (Eq. (3)) in all oil/waste ratios. Handayani et al. (2008)



Fig. 5 Kinetics of astaxanthin extraction from the 300 kDa freeze-dried retentate (*FR_f*) from shrimp cooking wastewater at different temperatures: 30 (*filled circle*), 40 (*filled square*), 50 (*filled diamond*), and 60 °C (*filled triangle*). Experimental data (*points*) and fittings to Eqs. (4) (*broken line*) and (6) (*solid line*)

also observed better adjustment of Eq. (4) to the extraction kinetics of shrimp waste in palm oil, which they attributed to the reaction between the hydroxyl groups in astaxanthin with fatty acids. According to these authors, the extraction process is a consequence of both mass transfer and hydrogen bonding between astaxanthin and oil.

Higher astaxanthin yield at equilibrium (Y_e) was found for R_f fraction with the increase of oil/waste ratio, whereas identical Y_e values were obtained for HR_f at the three assayed oil/waste ratios (Table 3). According to these results, the lowest oil/waste ratio might be insufficient to allocate globular proteins in R_f which would tend to be more retained in the oilwater interphase. Astaxanthin can then be partially partitioned between the oil and water interphase. Owing to the excluded volume interactions (Mazzola et al. 2008) between the carotenoid and these proteins, lower astaxanthin concentrations can be recovered in the oily phase. On the contrary, peptides in HR_f are easier to order and tend to go into the aqueous phase and so astaxanthin could be more easily separated after filtration and centrifugation.

On the other hand, kinetic constants from Eqs. (3) and (4) $(k_{\rm L}a, \min^{-1} \text{ and } k_{\rm A}, \min^{-1})$ were greater when a 2:1 (ν/ν) ratio was used for oil extraction (Table 3), suggesting that this phase relationship is optimal for mass transfer and reaction between astaxanthin and fatty acids in both $R_{\rm f}$ and HR_{f} .

The effect of increasing temperatures on the pigment extraction kinetics from FR_f was also studied. Experimental trends showed the existence of two phases along extraction time, that is, two mass transfer phenomena with different rates (Fig. 5). Such behavior could be due to astaxanthin existing in different forms dependent on the affinity, degree or strength of pigment-protein interactions, and also to the presence of free astaxanthin (Pérez-Santín et al. 2013). These profiles made it necessary to use a biphasic equation as Eq. (6) to more adequately adjust the experimental data than Eq. (4), as can be seen according to determination coefficients (Table 5). The normalized maximum yield of extraction (Y_m) or the asymptotic value on the plateau phase (Fig. 5, continuous line) was

Table 4 Parametric estimations and determination coefficients of Eqs. (4) and (5) applied to the extraction of astaxanthin from the freeze-dried retentate (FR_{f}) obtained by UF-DF of shrimp cooking wastewaters. Extractions were performed at different temperatures using a 100:1 oil/waste ratio

Model	Parameters	Temperature (°C)				
		30	40	50	60	
Eq. (4)	Ye	0.87±0.06	$0.59 {\pm} 0.08$	0.43 ± 0.08	0.29±0.01	
	k _A	$0.38 {\pm} 0.17$	$0.28 {\pm} 0.26$	$0.48 {\pm} 0.43$	$1.98 {\pm} 0.58$	
	R^2	0.963	0.800	0.681	0.978	
Eq. (5)	$Y_{\rm m}$	0.89 ± 0.13	$0.77 {\pm} 0.04$	$0.61 {\pm} 0.04$	$0.29 {\pm} 0.01$	
	Ye	$0.44{\pm}0.10$	$0.37 {\pm} 0.02$	$0.26 {\pm} 0.02$	$0.18 {\pm} 0.049$	
	$k_{L1}a$	1.23 ± 0.17	$0.46 {\pm} 0.12$	$0.91 {\pm} 0.29$	$0.96 {\pm} 0.58$	
	$k_{L2}a$	$0.0373 {\pm} 0.0051$	$0.0015 {\pm} 0.0005$	$0.0013 {\pm} 0.0004$	0.0571 ± 0.0420	
	R^2	0.975	0.993	0.993	0.988	

 Y_e normalized astaxanthin yield at equilibrium (dimensionless), k_A reaction constant (min⁻¹), Y_m normalized maximum yield of extraction (dimensionless), $k_{LI}a$ and $k_{L2}a$ are the volumetric mass transfer coefficients of the first and second extraction phase, respectively (min⁻¹)

calculated by parametric estimation, minimizing the sum of quadratic differences between the observed and model (Eq. (6)) predicted values. Y_m was dependent with temperature, and so lower $Y_{\rm m}$ values were obtained with temperature increase. This result is in concordance with those using the response surface approach where maximal yields were achieved at low temperatures (<40 °C). According to the literature, astaxanthin in its free form is unstable and extremely sensitive to factors such as light, oxygen, acidity, and heat (Mezzomo et al. 2011), so these results also support the hypothesis that cooking can break the carotenoid-protein complex and that astaxanthin from cooking wastewater could be mainly in its free form. Indeed, a recent study conducted to investigate the compositional properties and bioactive potential of shrimp cooking juice (Pérez-Santín et al. 2013) identified free astaxanthin (cis and trans isomers) and derived monoesters or diesters in the organic phase extracted from the liquid supernatant of this waste material.

Moreover, extraction at 30 °C was much faster from FR_f than from either R_f or HR_f , as can be seen in view of the

kinetic constants from Eq. (4) (Tables 3 and 4). The effect of freeze-drying on the improvement of astaxanthin recovery is in accordance with the results of Mezzomo et al. (2011), who observed that cooking, drying, and milling improved the total carotenoid content recovered from shrimp residues, for instance, the head, carapace, and tail, after extraction using different solvents.

Finally, extraction kinetics in the presence of synthetic antioxidants were performed in order to study the effect these compounds had on astaxanthin recovery. A concentration of 200 mg/L was selected according to previous dosages applied for astaxanthin extraction in oil (Chen and Meyers 1982) and to the maximum concentrations approved by the EU (Regulation 1831/2003) for animal feeds (150 mg/kg). According to our results (Fig. 6 and Table 5), the addition of either BHA or ETQ improved astaxanthin extraction in sunflower oil. Although different behaviors were observed whether astaxanthin was extracted from R_f (Fig. 6a) or FR_f (Fig. 6b). The addition of BHA or ETQ significantly (p<0.05) increased astaxanthin extraction compared to the control when

Fig. 6 Kinetics of astaxanthin extraction from the R_f (**a**) and FR_f (**b**) fractions, without (*filled circle*) and with 200 mg/L of BHA (*filled square*) or ethoxyquin (*filled triangle*). Experimental data (*points*) and fittings (*lines*) to Eqs. (4) (**a**) and (6) (**b**)



Table 5 Parametric estimations and determination coefficients of Eqs. (4) and (5) applied to the extraction of astaxanthin from the retentate obtained by UF-DF of shrimp cooking wastewaters before (R_t) and after freeze-drying (FR_f), respectively. Extractions were performed at 30 °C in the presence of two antioxidants (BHA and ETQ) and without (control), with the other extraction conditions described in the text

Sample	Parameters	Treatment			
		Control	BHA	ETQ	
$R_{\rm f}$	Y _e	0.61±0.06	$1.00{\pm}0.07$	1.32±0.30	
	k _A	$0.0117 {\pm} 0.0072$	$0.0035 {\pm} 0.0013$	$0.0009 {\pm} 0.0007$	
	R^2	0.963	0.989	0.976	
LR_{f}	$Y_{\rm max}$	$0.85 {\pm} 0.08$	0.99 ± 0.12	$0.94{\pm}0.08$	
2	$Y_{\rm e}$	0.37±0.13	0.52 ± 0.12	$0.48 {\pm} 0.08$	
	$k_{L1}a$	$0.0110 {\pm} 0.0083$	$0.0012 {\pm} 0.0007$	$0.0016 {\pm} 0.0008$	
	$k_{L2}a$	$0.59 {\pm} 0.37$	0.72 ± 0.34	$0.78 {\pm} 0.34$	
	R^2	0.958	0.974	0.981	

 Y_e normalized astaxanthin yield at equilibrium (dimensionless), k_A reaction constant (min⁻¹), Y_m normalized maximum yield of extraction (dimensionless), $k_{LI}a$ and $k_{L2}a$ are the volumetric mass transfer coefficients of the first and second extraction phase, respectively (min⁻¹)



Fig. 7 Flowchart highlighting the recovery of astaxanthin from shrimp cooking wastewater in sunflower oil. The extraction from a protein and astaxanthin-concentrated fraction (R_t) and from its hydrolysate (HR_f) and freeze-dried (FR_f) forms is shown

the pigment was extracted from $R_{\rm f}$, although these differences were not significant (p>0.05) in FR_{f} . However, a slower extraction is also observed when performed in the presence of either two antioxidants (Table 5), suggesting that they have a stabilizing effect on astaxanthin that in turn explains the improved extraction observed in the water-oil system. The stabilizing effect of antioxidants such as ethoxyquin has been reported to increase astaxanthin extraction from crawfish waste using soy oil (Chen and Meyers 1982). Also, the inoculation of shrimp wastes with a *Lactobacillus* culture isolated from tropical shrimp stabilized astaxanthin structure, increasing its extraction yields using different organic solvents (Armenta-López et al. 2002).

In the present study, the normalized maximum yields of extraction ($Y_{\rm m}$) for $R_{\rm f}$, HR_{f} , and FR_{f} correspond, under the best conditions determined for each of these fractions, to astaxanthin concentrations of 12.9, 11.2 µg/mL, and 210 µg/g, respectively. The addition of BHA increased astaxanthin recovery to 17.3 µg/mL in $R_{\rm f}$ and 299 µg/g in FR_{f} , while ETQ led to concentrations of 22.6 µg/mL and 282 µg/g for the liquid and solid shrimp concentrates, respectively.

Conclusions

Our results show that a protein and astaxanthin-concentrated fraction (R_f) can easily be recovered from shrimp processing wastewaters by UF at 300 kDa. Response surface methodology was successfully applied to optimize extraction conditions from $R_{\rm f}$ showing an optimal temperature lower (<40 °C) than that utilized for astaxanthin recovery from solid shrimp wastes. Further analysis of extraction kinetics at 30 °C showed that astaxanthin recovery is a consequence of both mass transfer and hydrogen bonding between astaxanthin and oil. The freeze-dried concentrate wastewater (FR_f) showed a twophase extraction and, at 30 °C, was much faster than from the liquid form. No improvement in astaxanthin yields was observed after hydrolysis with alcalase at 45 °C for 30 min (HR_{f}), but higher recoveries were obtained when both $R_{\rm f}$ and LR_{f} were extracted in the presence of 200 mg/L BHA or ETO. Astaxanthin from this shrimp by-product showed low thermal stability in oil at high temperatures (60 and 70 °C), suggesting that the carotenoid is mainly free as a result of the cooking process and not bounded to proteins or lipids as it occurs in its natural form (Fig. 7).

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