



Roles of SiO₂ Additive on Preparation of Ferrotitanium from Ilmenite Concentrate by Electrochemical Reduction in CaCl₂ Molten Salt

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The effect of the content of an SiO₂ additive on the electrochemical reduction of ilmenite concentrate to prepare ferrotitanium is investigated in CaCl₂ molten salt. A thermodynamic analysis of the Ti-Fe system and possible reactions has been carried out, and it demonstrated that SiO₂ and FeTiO₃ can be readily reduced to Si and intermediates (Fe and CaTiO₃), respectively. The experimental results demonstrated that the optimal molar ratio of Ti:Fe:Si in the cathode mixtures is 1.2:1:0.2. The porous ferrotitanium with uniform particle sizes were successfully obtained by electrolysis at 1173 K with a cell voltage of 3.2 V for 2 h. The SiO₂ additive plays an important role during the formation process of ferrotitanium, which is first reduced to Si and then serves as a reductant to catalyze CaTiO₃ and Fe to form FeTi alloys.

INTRODUCTION

Ferrotitanium, one of the best ferroalloys, has been widely employed as hydrogen storage material or has served as a deoxidizer in the steel-making industry. Generally, ferrotitanium is produced either by aluminothermic reduction of ilmenite concentrate as well as from titanium slag, or by re-melting iron and titanium scraps together at high temperatures.^{1,2} However, these two methods have obvious disadvantages, such as high residual oxygen content, high impurities in products, and high energy consumption.^{3,4} In recent decades, many efforts have been made to modify the refinement process for the production of ferrotitanium.

The direct electrolysis of a solid oxide in molten salt, known as the Fray–Farthing–Chen Cambridge (FFC) process with the merits of short-flow course and lower energy consumption, has been applied widely since 1998.^{5,6} Numerous metals (e.g., Cr,⁷ Ti,⁸ Nb,⁹ Ta,¹⁰ Zr¹¹), and alloys (e.g., LaNi,¹² TiC/SiC,¹³ FeTi,¹⁴ and TiSi¹⁵) have been prepared from corresponding oxides via the FFC method. Panigrahi et al. reported the preparation of

ferrotitanium alloys from the direct electrolysis of TiO₂ and Fe₂O₃ mixtures in CaCl₂ molten salt.¹⁶ However, a relative slower deoxidization rate and higher energy consumption were observed on account of the difficult reduction of TiO₂ and the multi-intermediates formed, such as CaTiO₃ and TiO. It has become imperative to develop an effective way to promote the reduction process. A great number of endeavors, including lowering the cathode mold pressure, and improving the cathode sintering temperature and cathode porosity, have been put into practice.^{11,17} As a result, shorter electrolytic times and elevated electrolytic currents have been achieved. However, the intrinsic reduction routes have not been changed. Besides, our previous work suggests that the addition of CaO into CaCl₂-based molten salts can accelerate the transmission of O²⁻ and introduce the calciothermic reduction of cathodic oxides, leading to favorable cathodic reaction kinetics.¹⁸ The only fly in the ointment could be that the CaO additive will result in the easy formation of intermediate CaTiO₃, so that the subsequent reaction is difficult.¹⁹

Recently, an acid oxide, SiO₂, was introduced in our work to accelerate the reduction of ilmenite. Here, the influence of the content of the SiO₂

additive on the electrochemical reduction of ilmenite concentrate to prepare ferrotitanium was investigated. The thermodynamic analysis of the Ti-Fe system and possible reactions were performed by Outokumpu HSC Chemistry. A variety of techniques, including XRD, SEM, and EDS, were utilized to characterize the samples. The roles of the SiO₂ additive in the reduction process have also been proposed.

EXPERIMENTAL

Chemicals

The chemicals of analytical grade used in present work were purchased commercially from Aisinal-addin-e.com, Shanghai, China. The x-ray diffraction (XRD) pattern of the ilmenite concentrate sample in this experiment is shown in Fig. 1a, and the main phases are FeTiO₃ and TiO₂. The chemical composition of the ilmenite concentrate is also given in the inset. The molar ratio of the main elements in ilmenite concentrate is Ti:Fe:Si = 1.2:1:0.076.

Preparation of Cathode

Before electrolysis, the crushed ilmenite concentrate with an average particle size of ~ 50 μm was blended with the SiO₂ at different molar ratios of Ti:Fe:Si (1.2:1:0.076, 1.2:1:0.1, 1.2:1:0.2, 1.2:1:0.3, and 1.2:1:0.4). Then, the powders (1.5 g) were mixed with 10 wt.% polyvinyl alcohol and 25 wt.% NH₄HCO₃, and pressed into a cylindrical pellet (13 mm in diameter and 2.0 mm in thickness) under a pressure of 15 MPa. Finally, the pellets were sintered in an argon inert atmosphere at 1373 K for 4 h to obtain sufficient strength and the desired porosity.

Electrolysis Experiments

The electrolytic experiments were operated in a crucible furnace. A schematic of the experimental

apparatus is shown in Fig. 1b. Before electrolysis, the sintered pellet was assembled by a molybdenum rod (99.95% in purity, 3 mm in diameter and 200 mm in length) to serve as the cathode. The graphite rod (99.9% in purity, 6 mm in diameter and 100 mm in length) tied by a molybdenum rod served as the anode. The electrolytic experiment was performed at 1173 K for 0.5–2.0 h in an Al₂O₃ crucible (Φ70 mm × 70 mm, 99.9% in purity) and a constant cell voltage of 3.2 V was supplied by a DPS-305BF DC voltage-stabilized power source (Zhejiang Yueqing Yizhan Electronics, China). As the furnace was heated to 1173 K, the electrodes were immersed in the CaCl₂ molten salt under an inert atmosphere. After the electrolysis, the cathode pellet was cooled to room temperature in the molten salt, then washed with distilled water to remove excessive molten salt, and dried in vacuum.

Characterization Analysis

The phases of sample were analyzed by XRD (Version D/Max-2200pc model with Cu-Kα radiation) at a scan rate of 8°/min in the range of 10°–90°. The morphology and element constituents of samples were characterized by SEM equipped with EDS (LEO-FEGSEM model).

RESULTS AND DISCUSSION

Thermodynamic Analysis

According to existing reports,^{18,19} the electrochemical reduction of ilmenite concentrate is a complex process which involves the formation of intermediates, such as Fe, CaTiO₃, TiO, et al. It can be seen from the Ti-Fe binary phase diagram (Fig. 2a) that ferrotitanium alloys (Fe₂Ti and FeTi) exist in this system.²⁰ As a result, Fe₂Ti and FeTi can be formed during the electrolysis of FeTiO₃. When SiO₂ is added into the system, the reduction process will be more complicated. Here, possible

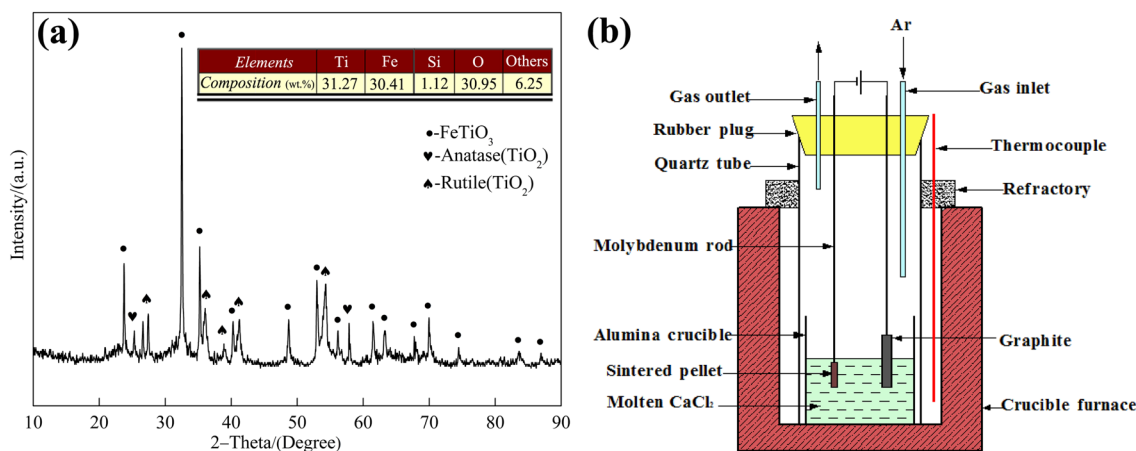


Fig. 1. (a) XRD pattern of ilmenite concentrate, (b) schematic of the electrolytic apparatus. Inset chemical composition of the ilmenite concentrate (wt.%).

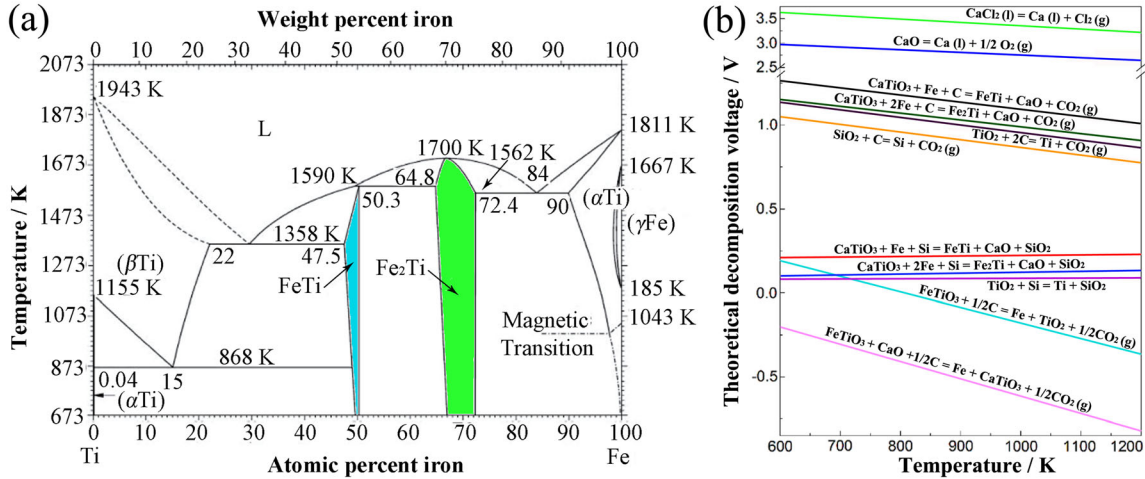


Fig. 2. (a) Ti-Fe binary phase diagram, (b) relationships between the theoretical decomposition voltage and temperature.

Table I. Possible reactions and relationships between Gibbs free energy, decomposition potentials and temperature

No.	Reaction	$\Delta G_T^0 - T$	$\frac{\Delta G_T^0}{(T=1173\text{ K})} / \text{kJ}$	$\frac{E^0}{(T=1173\text{ K})} / \text{V}$
(1)	$\text{CaCl}_2(\text{l}) = \text{Ca}(\text{l}) + \text{Cl}_2(\text{g})$	$772.98 - 0.09T$	667.41	3.46
(2)	$\text{CaO} = \text{Ca}(\text{l}) + 1/2\text{O}_2(\text{g})$	$648.23 - 0.138T$	486.36	2.52
(3)	$\text{FeTiO}_3 + 1/2\text{C} = \text{Fe} + \text{TiO}_2 + 1/2\text{CO}_2(\text{g})$	$145.36 - 0.180T$	- 65.78	-
(4)	$\text{FeTiO}_3 + \text{CaO} + 1/2\text{C} = \text{Fe} + \text{CaTiO}_3 + 1/2\text{CO}_2(\text{g})$	$82.36 - 0.201T$	- 153.41	-
(5)	$\text{SiO}_2 + \text{C} = \text{Si} + \text{CO}_2(\text{g})$	$511.81 - 0.177T$	304.28	0.79
(6)	$\text{TiO}_2 + \text{C} = \text{Ti} + \text{CO}_2(\text{g})$	$545.64 - 0.178T$	336.09	0.87
(7)	$\text{TiO}_2 + \text{Si} = \text{Ti} + \text{SiO}_2$	$33.44 - 0.0014T$	31.80	0.08
(8)	$\text{CaTiO}_3 + 2\text{Fe} + \text{C} = \text{Fe}_2\text{Ti} + \text{CaO} + \text{CO}_2(\text{g})$	$538.93 - 0.157T$	354.76	0.92
(9)	$\text{CaTiO}_3 + 2\text{Fe} + \text{Si} = \text{Fe}_2\text{Ti} + \text{CaO} + \text{SiO}_2$	$24.64 + 0.022T$	50.45	0.13
(10)	$\text{CaTiO}_3 + \text{Fe} + \text{C} = \text{FeTi} + \text{CaO} + \text{CO}_2(\text{g})$	$587.44 - 0.166T$	392.72	1.02
(11)	$\text{CaTiO}_3 + \text{Fe} + \text{Si} = \text{FeTi} + \text{CaO} + \text{SiO}_2$	$72.02 + 0.014T$	88.44	0.23

reactions during the electrochemical reduction of FeTiO_3 and TiO_2 are illustrated in Table I. The relationships between the standard Gibbs free energy, ΔG_T^0 , the theoretical decomposition voltage, E^0 , and temperature, T , have been calculated by HSC Chemistry 6.0, as presented in Fig. 2b. Based on the calculation, this demonstrates that the theoretical decomposition voltage, E^0 , of CaCl_2 (3.46 V at 1173 K) is the highest, implying that all the oxides can be reduced before the decomposition of the electrolyte. The Gibbs free energy values, ΔG_T^0 , of reactions (3) and (4) are negative at 1173 K, and thus FeTiO_3 can be easily reduced to Fe and TiO_2 or CaTiO_3 . However, the Gibbs free energy change of reaction (4) is more negative than that of reaction (3), suggesting that FeTiO_3 can be easily reduced to Fe and CaTiO_3 via reaction (4).

From the calculation results, the decomposition voltage E^0 of reaction (5) is 0.79 V, indicating that SiO_2 can be readily reduced to Si. Moreover, the value of the theoretical decomposition voltage, E^0 , of

reaction (5) is much lower than that of reactions (8) and (10), which implies that Si is preferentially formed before the reduction of CaTiO_3 . Looking further at the thermodynamic calculations, comparing reactions (8–11), CaTiO_3 can be reduced to ferrotitanium alloys via reactions (9) and (11) due to their low theoretical decomposition voltages, E^0 . In addition, the theoretical decomposition voltage, E^0 , of reaction (7) is much lower than that of reaction (6), which means that the reduction of TiO_2 is significantly promoted by the formation of Si. Therefore, the participant of SiO_2 is thermodynamically favorable for the formation of ferrotitanium from ilmenite concentrate.

Time-Current Curves

The current as a function of time was recorded during the electrolysis of ilmenite concentrate with different SiO_2 contents, as shown in Fig. 3. All the values of the current decrease remarkably in the initial 30 min and then decay slightly later. The

decline of the current value reflects the change of the reaction rate. At the beginning of electrolysis, the rapid reduction rate is put down to the large three-phase reaction interface between the cathodic oxide reactant, the metallic product, and the molten salt. As the reaction is performed inside the pellet, the reduction rate becomes slow because of the lessened three-phase interface.

In addition, from Fig. 3, it can be seen that the increase of SiO₂ content has a significant effect on the current values. In the initial 10 min, the current value decreases remarkably when the SiO₂ content is high. For example, the current value at 10 min decreases from 1.8 A to 1.76 A, 1.7 A, 1.55 A, and 1.45 A as the Ti:Fe:Si molar ratio varies from 1.2:1:0.076 to 1.2:1:0.1, 1.2:1:0.2, 1.2:1:0.3, and 1.2:1:0.4, respectively. However, in the subsequent electrolysis from 20 min to 120 min, the current values reduce slightly at high SiO₂ content. For instance, the current values at 60 min increase from 0.63 A to 0.75 A, 1.0 A, 1.13 A, and 1.83 A, respectively. According to thermodynamic analysis mentioned above, FeTiO₃ will be preferentially reduced to Fe and CaTiO₃ via reaction (4), and the intermediate CaTiO₃ will be deoxidized via reactions (8–11). Thus, the electrochemical reduction of ilmenite concentrate is suggested to be divided into two steps. FeTiO₃ is first reduced in the initial period and then CaTiO₃ is deoxidized. Moreover, it should be pointed out that the addition of SiO₂ into the cathode pellet might reduce the effective interface area of FeTiO₃ as the cathode weight is a constant, and the electrolysis of SiO₂ will consume more electricity. As a result, the reduction rate of FeTiO₃ decreases with an increase in the SiO₂ content of the cathode in the initial period. In contrast, with the participation of SiO₂, the further reduction of CaTiO₃ can be enhanced in thermodynamics, leading to the increase of the current value.

Phase Characterization

The ilmenite concentrate with different SiO₂ contents was electrochemically reduced at 3.2 V and 1173 K for 0.5 h, 1 h, and 2 h, respectively. The XRD patterns of the products are illustrated in Fig. 4 and the observed phases are listed in Table II.

As shown in Fig. 4 and Table II, when the samples are electrolyzed for 0.5 h, the FeTiO₃ can be completely reduced to form the dominant phases, Fe-Ti-O and CaTiO₃, and the minor phases, FeTi, Fe₂Ti, and SiO₂. This result reveals that FeTiO₃ can be preferentially reduced to intermediates Fe-Ti-O and CaTiO₃ in the initial period of 0.5 h. Looking further at the results in Fig. 4a and Table II, a small amount of SiO₂ can be detected, except in the sample with the Ti:Fe:Si molar ratio of 1.2:1:0.076, indicating that the SiO₂ is stable. Therefore, this suggests that the addition of SiO₂ has little impact on the initial electrochemical conversion of FeTiO₃

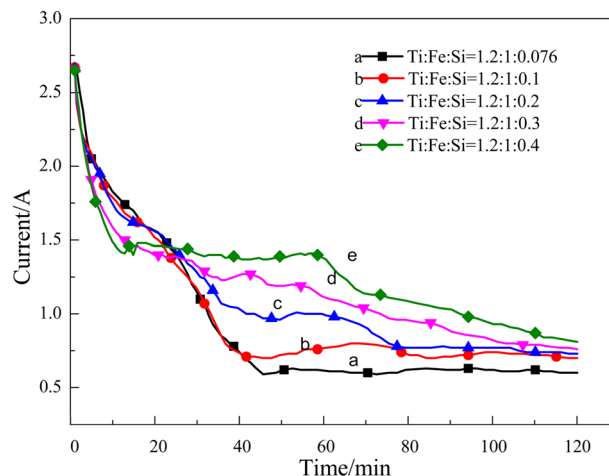


Fig. 3. Time–current curves during the electrolysis of samples with different SiO₂ contents.

to CaTiO₃ and Fe via reaction (4). After 1 h (Fig. 4b), Si is observed in the product, which implies that SiO₂ can be reduced to Si at the middle stage from 0.5 h to 1 h. Meanwhile, the relative intensity of CaTiO₃ decreases with the increase of SiO₂ content. When the molar ratio of Si is higher than 0.3, CaTiO₃ is completely electrolyzed because the dominant phase is Fe-Ti-O, and the minor phases include FeTi, Fe₂Ti, and Si. This result shows that the further reduction process of CaTiO₃ can be accelerated by the addition of SiO₂, which is in good agreement with the thermodynamic analysis in “Thermodynamic Analysis” section.

When the electrolytic time is prolonged to 2 h (Fig. 4c), a small amount of CaTiO₃ is detected in the sample with the Ti:Fe:Si molar ratio of 1.2:1:0.076. However, the residual CaTiO₃ has been completely deoxidized to produce the dominant FeTi phase and other minor phases such as Fe₂Ti, Fe-Ti-O, TiSi, Ti₅Si₃, and TiSi₂ as the SiO₂ content increased. This means that the addition of SiO₂ can enhance the reduction process of CaTiO₃ and so plays a positive role in the electrolysis process. In addition, a small number of Ti-Si (TiSi, Ti₅Si₃, and TiSi₂) by-products are also formed with the addition of SiO₂. This may lead to a higher content of silicon impurities in the ferrotitanium. Thus, it is necessary to optimize the addition of SiO₂ content. Based on present research, the optimal Ti:Fe:Si molar ratio in the samples is 1.2:1:0.2, because ilmenite can be completely reduced to ferrotitanium alloys (FeTi, Fe₂Ti) for 2 h, as shown in Table II.

Micrograph of Products

The SEM images of the ilmenite concentrate and the products obtained after electrolysis of the samples with different SiO₂ contents under constant cell voltage of 3.2 V at 1173 K for 2 h are shown in Fig. 5. The ilmenite concentrate powders are of dense blocky-shaped particles with inhomogeneous

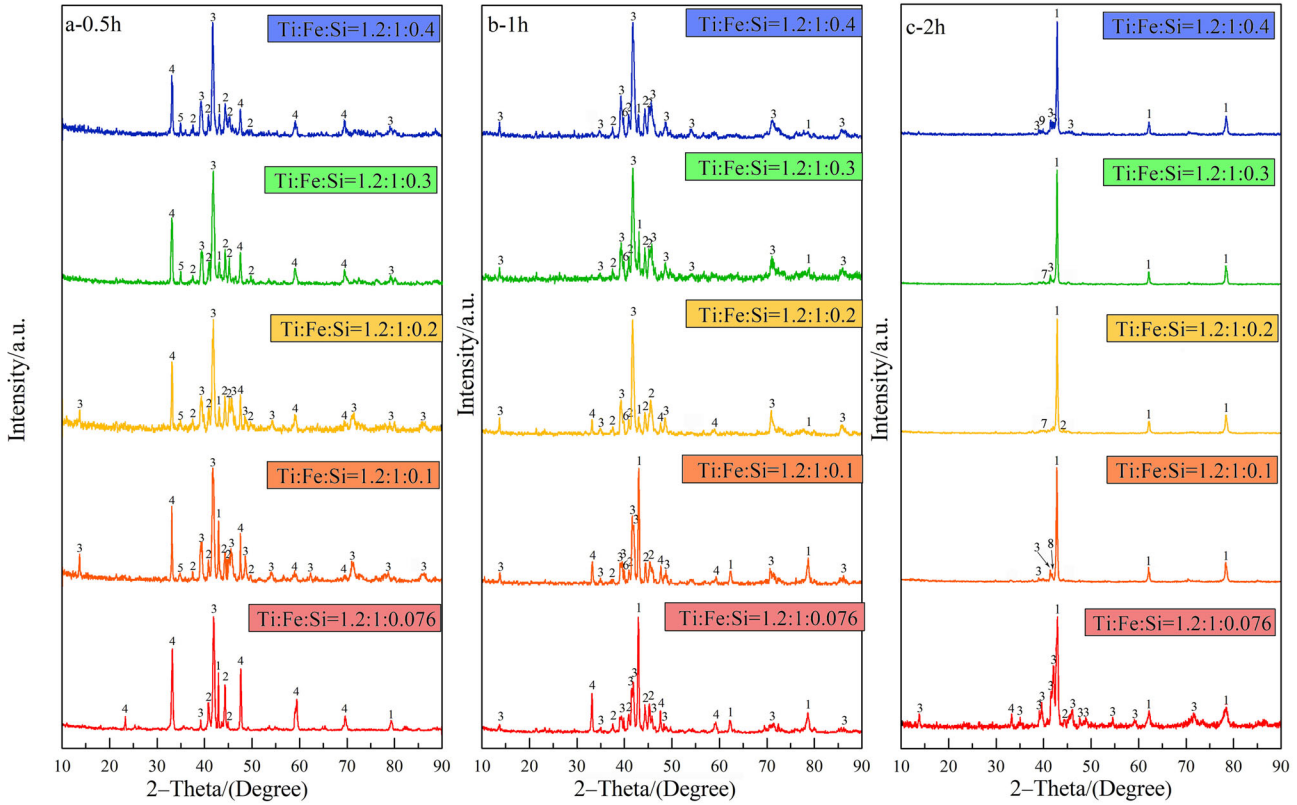


Fig. 4. XRD patterns of the products obtained after electrolysis of samples with different SiO_2 contents under 3.2 V at 1173 K for different times (a) 0.5 h, (b) 1 h, (c) 2 h. (1 FeTi, 2 Fe_2Ti , 3 Fe-Ti-O, 4 CaTiO_3 , 5 SiO_2 , 6 Si, 7 Ti_5Si_3 , 8 TiSi, 9 TiSi_2).

Table II. Phase observationd after electrolysis of the samples with different SiO_2 contents for various periods

Stoichiometric ratio	Time (h)					
	0.5		1		2	
	Dominant phase	Minority phase	Dominant phase	Minority phase	Dominant phase	Minority phase
Ti:Fe:Si = 1.2:1:0.076	Fe-Ti-O CaTiO_3	FeTi, Fe_2Ti	FeTi, Fe-Ti-O	Fe_2Ti , CaTiO_3	FeTi, Fe-Ti-O	Fe_2Ti , CaTiO_3
Ti:Fe:Si = 1.2:1:0.1	Fe-Ti-O CaTiO_3	FeTi, Fe_2Ti , SiO_2	FeTi, Fe-Ti-O	Fe_2Ti , CaTiO_3 , Si	FeTi	Fe-Ti-O, TiSi
Ti:Fe:Si = 1.2:1:0.2	Fe-Ti-O CaTiO_3	FeTi, Fe_2Ti , SiO_2	Fe-Ti-O	Fe_2Ti , FeTi, CaTiO_3 , Si	FeTi	Fe_2Ti , Ti_5Si_3
Ti:Fe:Si = 1.2:1:0.3	Fe-Ti-O CaTiO_3	FeTi, Fe_2Ti , SiO_2	Fe-Ti-O	FeTi, Fe_2Ti , Si	FeTi	Fe-Ti-O, Ti_5Si_3
Ti:Fe:Si = 1.2:1:0.4	Fe-Ti-O CaTiO_3	FeTi, Fe_2Ti , SiO_2	Fe-Ti-O	Fe_2Ti , FeTi, Si	FeTi	Fe-Ti-O, TiSi ₂

structures in a size of about 2–10 μm (Fig. 5a). After electrolysis, products with a porous structure are obtained, as illustrated in Fig. 5b–f. In addition, it can be seen that the size of the newly formed particles decreases with the increase of SiO_2 content. Therefore, with the addition of SiO_2 into the sample, the ilmenite concentrate can be constantly

electrolyzed to produce ferrotitanium powder with a smaller particle size. In addition, the products obtained after electrolysis of the sample with the Ti:Fe:Si molar ratio of 1.2:1:0.2 was further analyzed by EDS, as shown in Fig. 5g. It can be seen that the obtained particles are composed of the enriched elements, Fe and Ti, and that the Si

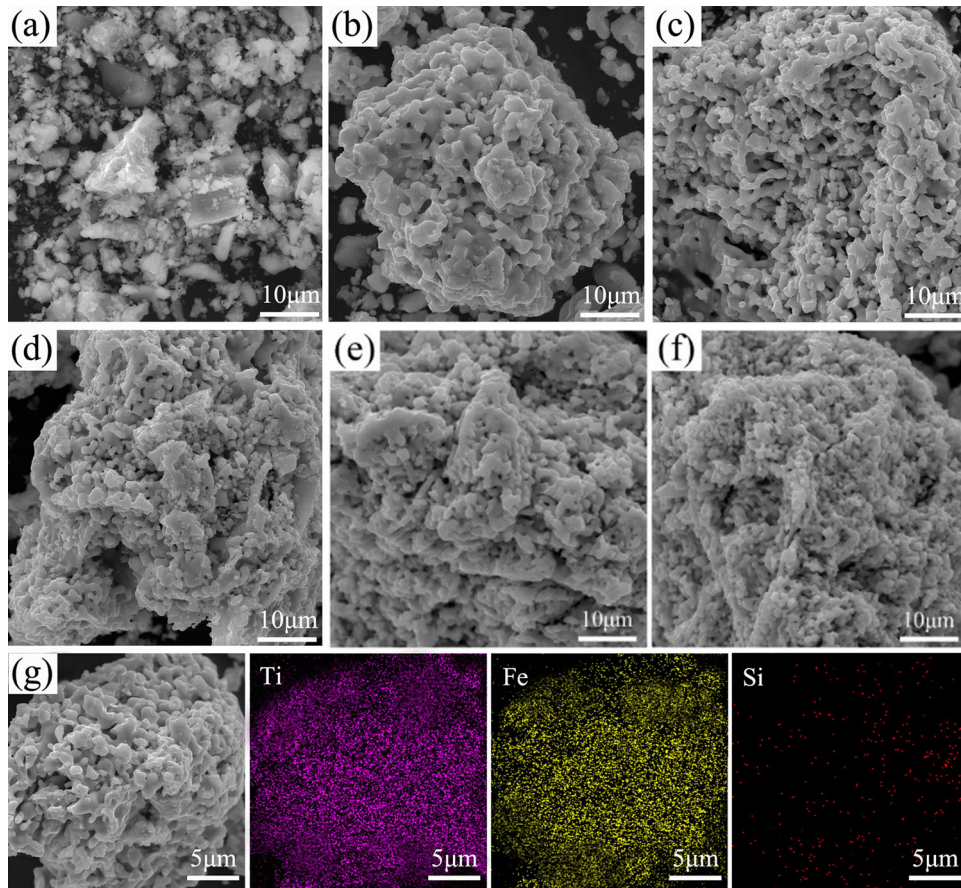


Fig. 5. (a–f) SEM images and (g) EDS analysis of the electrolytic products with different SiO₂ additions. (a) Ilmenite concentrate, (b) Ti:Fe:Si = 1.2:1:0.076, (c) Ti:Fe:Si = 1.2:1:0.1, (d, g) Ti:Fe:Si = 1.2:1:0.2, (e) Ti:Fe:Si = 1.2:1:0.3, (f) Ti:Fe:Si = 1.2:1:0.4.

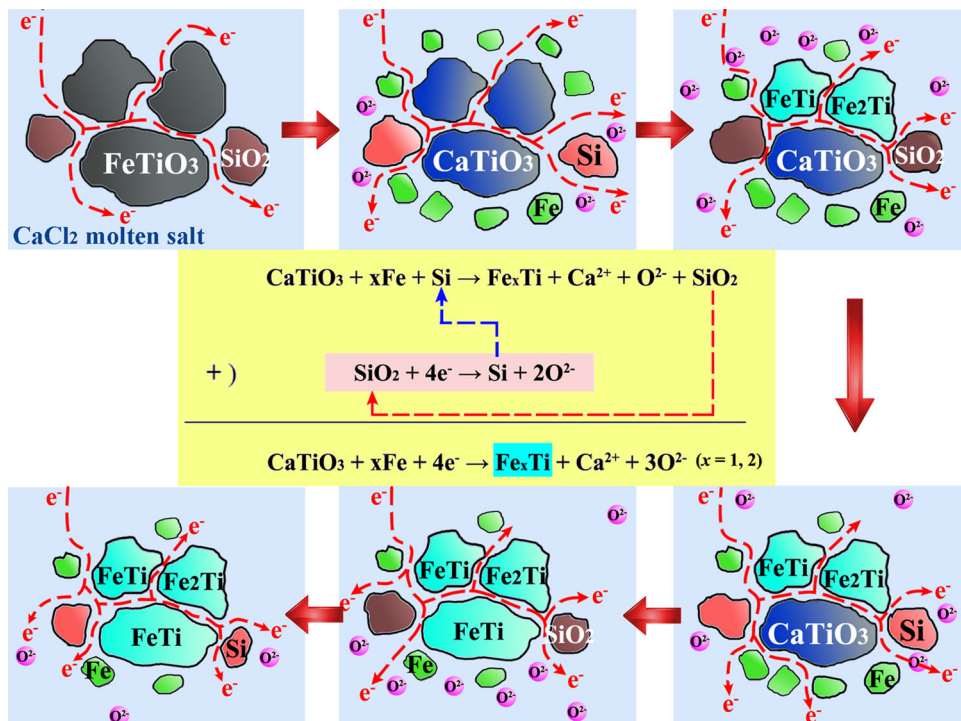


Fig. 6. Schematic of the roles of SiO₂ during the electrochemical reduction of ilmenite concentrate in CaCl₂ molten salt.

content is much lower. Moreover, the Si is dispersed throughout these particles, which mainly include FeTi.

Role of SiO₂ Additive

Based on the above analysis, the preparation of FeTi from ilmenite concentrate by electrochemical reduction in CaCl₂ molten salt is a complex multi-step process. First, FeTiO₃ is preferentially reduced to intermediates Fe and CaTiO₃ via reaction (4). In the second step, the intermediate CaTiO₃ is further reduced to ferrotitanium alloys through reactions (8) and (10). The further reduction of CaTiO₃ can be accelerated via reactions (9) and (11) with the addition of SiO₂, which demonstrates that the addition of SiO₂ into the sample during the electrochemical process can significantly promote the reduction of the intermediate CaTiO₃. The detailed roles of SiO₂ in the electrochemical reduction process can be proposed, as shown in Fig. 6. SiO₂ is first electrolyzed to produce Si, and the newly formed Si will act as the reductant to reduce CaTiO₃. Finally, the reduced Ti and Fe form FeTi alloys.

CONCLUSION

Ferrotitanium alloys were successfully prepared from ilmenite concentrate by electrochemical reduction with the addition of SiO₂ in CaCl₂ molten salt. SiO₂ plays an important role during the reduction process, and the optimal molar ratio in the cathode mixtures is Ti:Fe:Si = 1.2:1:0.2. Thermodynamic analysis of the Ti-Fe system and possible reactions indicate that SiO₂ can be readily reduced to Si, and that FeTiO₃ can be first transformed into intermediates, such as Fe and CaTiO₃. Electrolysis experiments demonstrated that SiO₂ is first reduced to Si and then serves as the reductant to participate in the reduction of CaTiO₃ and Fe to form FeTi alloys. The further reduction process of CaTiO₃ is promoted by the increase of SiO₂ content. The micromorphology of the ferrotitanium exhibits a porous structure and uniform particle size with the addition of SiO₂ into the ilmenite concentrate.

ACKNOWLEDGEMENT

The authors acknowledge the financial support of the National Natural Science Foundation of China (Project Nos. 51604136, 51274108).

REFERENCES

1. M. Panigrahi, R.K. Paramguru, R.C. Gupta, E. Shibata, and T. Nakamura, *High Temp. Mater. Processes* 29, 495 (2010).
2. M. Panigrahi, A. Iizuka, E. Shibata, and T. Nakamura, *J. Alloys Compd.* 550, 545 (2013).
3. B. Wang, X. Lan, X. Zhao, and X. Wu, *Chin. J. Rare Met.* 30, 671 (2006).
4. G. Shenghui, P. Jinhui, Z. Shiming, F. Xingxiang, and Z. Libo, *Light Met.* 11, 51 (2002).
5. G.Z. Chen, D.J. Fray, and T.W. Farthing, *Nature* 407, 361 (2000).
6. G.Z. Chen, D.J. Fray, and T.W. Farthing, *Metall. Mater. Trans. B* 32, 1041 (2001).
7. Z.W. Liu, H.L. Zhang, L.L. Pei, Y.L. Shi, Z.H. Cai, H.-B. Xu, and Y. Zhang, *Trans. Nonferrous Met. Soc. China* 28, 376 (2018).
8. P. Lai, T. Ma, and M. Hu, *JOM* 71, 1033 (2019).
9. Q. Song, X. Qian, J. Meng, T. Lou, Z. Ning, Q. Yang, and Y. Kai, *J. Alloys Compd.* 647, 245 (2015).
10. Q. Song, Q. Xu, X. Kang, J. Du, and Z. Xi, *J. Alloys Compd.* 490, 241 (2010).
11. K.S. Mohandas and D.J. Fray, *Metall. Mater. Trans. B* 40, 685 (2009).
12. Z. Yong, D. Wang, M. Meng, X. Hu, X. Jin, and G.Z. Chen, *Chem. Commun.* 24, 2515 (2007).
13. K. Chen, Y. Hua, C. Xu, Q. Zhang, C. Qi, and Y. Jie, *Ceram. Int.* 41, 11428 (2015).
14. C. Qi, Y. Hua, K. Chen, Y. Jie, Z. Zhou, J. Ru, L. Xiong, and K. Gong, *JOM* 68, 668 (2016).
15. K. Zheng, X. Zou, X. Xie, C. Lu, C. Chen, Q. Xu, and X. Lu, *JOM* 70, 138 (2018).
16. M. Panigrahi, E. Shibata, A. Iizuka, and T. Nakamura, *Electrochim. Acta* 93, 143 (2013).
17. J. Du, Z. Xi, Q. Li, Q. Xu, Y. Tang, and Z. Li, *Trans. Nonferrous Met. Soc. China* 17, s514 (2007).
18. L. Xiong, Y. Hua, C. Xu, J. Li, Y. Li, Q. Zhang, Z. Zhou, Y. Zhang, and J. Ru, *J. Alloys Compd.* 676, 383 (2016).
19. X. Lu, X. Zou, C. Li, Q. Zhong, W. Ding, and Z. Zhou, *Metall. Mater. Trans. B* 43, 503 (2012).
20. Z. Zhou, Y. Zhang, Y. Hua, C. Xu, P. Dong, Q. Zhang, and D. Wang, *JOM* 70, 575 (2018).

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