Sulfur Dioxide: A Versatile Reagent for the Processing of Cobaltic Oxide **Minerals**

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Cobaltic oxide minerals are readily dissolved in mildly acidic sulfuric solutions provided a reducing agent is also present. Sulfur dioxide is the most common reductant recommended for this purpose, but its addition during the leaching step could lead to significant environmental problems and could affect the recovery of copper if present in large amounts. This paper presents a novel approach whereby the reductant used during the leach is ferrous sulfate and sulfur dioxide is added at a later stage in a controlled manner to regenerate the reductant after any copper present has been recovered. Sulfur dioxide can also be used during purification of the cobalt bleed, where, blended with oxygen, it constitutes a powerful oxidant capable of selectively oxidizing and precipitating manganese away from the cobalt. This paper will present several applications of the use of sulfur dioxide as a primary reductant, a regenerant for ferrous sulfate, and a selective oxidant for manganese.

INTRODUCTION

Historically, primary cobalt has been mostly recovered as a by-product of the copper and nickel industries. For many decades, a significant portion of the world's primary cobalt originated from the Central Africa Copper Belt, more particularly from the Democratic Republic of Congo (DRC, formerly known as Zaire).

In the DRC Gecamines plants, cobalt sulfide (mostly carrollite $CuCo_{2}S_{4}$) was recovered by flotation. In its oxide form, cobalt is present as cobaltous (mostly sphaerocobaltite CoCO₂), but mostly as cobaltic mineral. The most abundant cobaltic mineral is heterogenite, named stainierite $Co_2O_2 \cdot H_2O$ in its fully crystallized form, more generally CoO·2Co₂O₂·6H₂O in its amorphous form. Cobaltic minerals also frequently occur as a cobaltiferous wad ("asbolite") in a mixture with manganese and iron oxides. Similar associations are also encountered in manganiferous sea and land nodules,1 and in nickel laterites.2-6

Cobaltic oxide minerals are fairly refractory in mildly acidic solutions, as are manganic oxide minerals. As manganic oxides, they require a reducing environment to undergo dissolution.

Sulfur dioxide is a very common reductant produced in large quantities during the roasting and smelting of sulfides. It has been suggested for use as a primary reductant for manganic oxide minerals and therefore for cobaltic oxide minerals. However, sulfur

How would you... ...describe the overall significance of this paper? This paper documents several improvements/modifications to the hydrometallurgy of cobalt by the diverse application of a common chemical, sulfur dioxide. ۶-... describe this work to a materials science and engineering professional with no experience in your technical specialty? ٤1 It shows that the same common chemical (sulfur dioxide) can be used in various applications during goals and optimize the process. ... describe this work to a layperson? and a sound knowledge of basic chemistry gives the metallurgist flexibility to optimize the metallurgy of cobalt by using the same common

the same process to achieve different

This work shows that some creativity chemical (sulfur dioxide) in various areas of the process.

dioxide is a fairly versatile reagent that can find several applications during the treatment of cobaltic minerals: it can be used also as secondary reductant after the leach and as an oxidant (in a gas mixture) for the selective precipitation of iron and manganese during the purification of cobalt solutions.

This paper presents various uses of sulfur dioxide during the treatment of cobaltic oxide minerals, the underlying chemistry, and examples of applications.

COBALTIC OXIDE ORE SAMPLES TESTED

Ore samples of various types and origins have been investigated during this study. Table I presents their chemical analyses. Samples A, B, and C originated from Central Africa and represent sedimentary copper-cobalt siliceous ores with copper mainly as malachite. Sample D originated from Central America while sample E, originating from West Africa, represented a nickel-cobalt lateritic ore.

All these samples contained the cobalt in the cobaltic form, with usually less than 20% of the cobalt soluble in mildly acidic solutions. As an example, Figure 1 presents the results of an agitation leach carried out on sample A ground to a P₈₀ of 80 µm.

Copper dissolution in acid solutions was excellent (95% in 45 minutes), as expected from malachite. Cobalt dissolution was limited to less than 10% due to the refractory nature of cobalt (III) under those conditions.

SULFUR DIOXIDE AS A PRIMARY REDUCTANT

It has long been known that sulfur dioxide could be used effectively as a reductant during acid dissolution of py-

rolusite MnO₂ ores.⁷ By analogy, sulfur dioxide has also been suggested as a primary reductant during acid dissolution of cobaltic ores.8 It is suggested9 that the reductive dissolution of heterogenite occurs as per the reaction:

$$2 \operatorname{CoOOH} + \operatorname{SO}_2 + \operatorname{H}_2 \operatorname{SO}_4 \\ \rightarrow 2 \operatorname{CoSO}_4 + 2 \operatorname{H}_2 \operatorname{O}$$
(1)

)

Figure 2 confirms the dissolution of cobalt (and manganese) when adding sulfur dioxide during the column leach of sample E. Sulfur dioxide was added as sodium metabisulfite to the leach solution. Similarly, when gas SO₂ was added (80 kg SO_2/t) to sample A under otherwise the same conditions as those presented in Figure 1, cobalt extractions



Table I. Chemical Analyses of Cobalt Ores/Concentrates used in the Study (%)					
	Α	В	С	D	Е
Cu	9.9	4.8	5.1	0.43	<0.01
Co	1.8	0.43	0.43	0.07	0.75
Fe	1.8	1.8	1.8	7.94	36.0
Mn	<0.05	<0.05	<0.05	4.49	1.62
Ni	_	< 0.003	< 0.003	0.01	0.80

increased to 94.7% in 2 hours. These results confirmed the effectiveness of sulfur dioxide as a primary reductant for cobaltic oxides.

However, the use of SO₂ presents several major drawbacks. The most obvious relates to the environmental and health risks associated with gaseous SO₂ emissions and almost precludes its use in heap or vat operations.

Another drawback is metallurgical, as illustrated in Figure 3. The results in that figure confirm the positive effect of sulfur dioxide additions on cobalt extraction but also a significant drop of copper extraction at higher SO₂ additions, likely due to the precipitation of Le Chevreult's salt, as per the reaction:

$$3 \operatorname{CuSO}_{4} + \operatorname{SO}_{2} + 6\operatorname{H}_{2}O$$

$$\rightarrow \operatorname{CuSO}_{3} \cdot \operatorname{Cu}_{2}\operatorname{SO}_{3} \cdot 2\operatorname{H}_{2}O$$

$$+ 4 \operatorname{H}_{2}\operatorname{SO}_{4} \qquad (2)$$

This potential side precipitation of a copper sulfite salt represents a significant danger of losing metal values.

SULFUR DIOXIDE AS A SECONDARY REDUCTANT

As an alternative to using SO_2 as a reductant during the leaching stage of cobalt oxide ores, it has been suggested to add ferrous sulfate in the leach solution.9,10 By analogy with manganese ores,11-14 it is assumed that the chemistry of the reductive leach follows Reaction 3:

$$2 \operatorname{CoOOH} + 2\operatorname{FeSO}_4 + 3\operatorname{H}_2\operatorname{SO}_4 \rightarrow 2 \operatorname{CoSO}_4 + \operatorname{Fe}_2(\operatorname{SO}_4)_3 + 4\operatorname{H}_2\operatorname{O}$$
(3)

Confirmation of the concept is presented in Figure 4 for the same ore type A as used in Figures 1 and 3. Results in Figure 4 confirm the suitability of using ferrous sulfate instead of sulfur dioxide at the leach stage; it also demonstrates that excess reductant does not have a negative impact on copper recovery since the conditions for copper sulfite precipitation do not exist.

The reductant being already dissolved, the efficiency of the reduction does not depend on a gas phase mass transfer and the kinetics of cobalt reductive dissolution are fairly rapid, as shown in Figure 5.

The dosage of ferrous sulfate needed in solution will depend on various factors, and under the proper conditions, cobalt extractions higher than 90% could be obtained in 4 hours. As expected, and as was the case when using SO₂ (see Figure 2), any manganic oxides in the ore would also be reductively leached with ferrous sulfate, as shown in Figure 6. Under the conditions of the leach, without a reductant, about 44% of the manganese and 58% of the cobalt are acid soluble. The addition of ferrous sulfate brings manganese recovery practically to completion (97.5%), while that of cobalt is increased by 20%.

It is usually desirable to regenerate the reductant, not only to lower the operating costs, but also to minimize the concentration of iron in the cobalt leach solution prior to the subsequent cobalt recovery/purification circuit.

A convenient method would be to reduce the ferric sulfate (resulting from Reaction 3), as per the well-known Reaction 4, using sulfur dioxide as a secondary reductant:

$$Fe_2(SO_4)_3 + SO_2 + 2H_2O \rightarrow 2FeSO_4 + 2H_2SO_4$$
(4)

The extent of the reduction is conveniently monitored by measuring the solution oxidation reduction potential (ORP). Examples of application are presented in Figure 7 for various SO_2 flow rates and a 1L solution containing 12 g/L Co, 1.5 g/L Cu, 26 g/L H_2SO_4 , and 6.8 g/L Fe^{3+} .

The reduction of ferric sulfate with SO_2 gas was rapid and completed in less than 1 hour at the higher flowrate. The reduction of the ferric ion is more efficient if carried out from a solution instead of a pulp. One of the major advantages of using ferrous sulfate as a primary reductant during the leach, and sulfur dioxide as a secondary reductant to regenerate the ferrous sulfate at a later stage, is the opportunity of applying this process to heap and vat leaching.

In those situations, the leach solution





Figure 10. A conceptual process to oxidize/precipitate Fe, Mn during Al, Si hydrolysis using SO₂/O₂ mixtures.



Figure 11. The selective removal of manganese from a cobalt leach solution using SO_2 /air mixtures. Temperature: 60° C; 2% SO_2 in air.



Figure 12. The potential uses of sulfur dioxide during the treatment of cobaltic ores.

containing ferrous sulfate as the primary reductant can be percolated through the vat/heap, and, when needed, ferrous sulfate can be regenerated using SO_2 gas sparged in an agitated reactor. An example of application is presented in Figure 8 for sample C.

In that test, 0.635 cm ore was agglomerated with 2.2 kg H_2SO_4/t of ore, and cured for 24 hours before being placed in a 15 cm column and percolation leached (374 L/h/m²) upflow with a solution containing 30 g/L H_2SO_4 and 5 g/L Fe²⁺. After 8 days, the extraction was 90.4% and 87.4% for copper and cobalt, respectively, and was still continuing, with 2 g/L Fe²⁺ present.

The same concept can easily be applied to an agitated leach process, as illustrated in Figure 9. About 20 tonnes of sample C were pilot tested in 1997 at SGS Lakefield Research using this concept: the ore ground to a P_{80} of 80 µm was processed through the flowsheet illustrated in Figure 9 at a flow-rate of 60 kg/h, and leach recoveries of 98.1% copper, 91.8% cobalt were demonstrated.

USE OF SULFUR DIOXIDE MIXTURES TO PURIFY COBALT SOLUTIONS

Reductive leaches of cobaltic ores will also dissolve significant amounts of manganese, as shown earlier. The cobalt leach solution will therefore also contain manganese, iron (from the ferrous sulfate added as reductant), and other impurities (aluminum, silicon, copper, etc.). Such a solution needs to be purified and concentrated (for example, using solvent extraction with Cyanex 272) to produce electrowon cobalt. Typically, hydrolysis to a pH of around 4.5 will eliminate aluminum, silica, and ferric (but not ferrous and manganous ions) without significant cobalt losses. Cobalt-manganese separation from such solutions is not easy but feasible. One method would be to chemically oxidize ferrous and manganous ions prior to hydrolyze them together with aluminum and silica. A simple and fairly inexpensive procedure to oxidize/precipitate manganese from cobalt solutions would be to use SO₂/O₂ mixtures, as per the concept presented in Figure 10.

It has long been known that SO_2/O_2

mixtures, under proper conditions, can act as powerful oxidants for various ions such as iron, cyanide (Inco's process), and manganese,¹⁵ and it can be applied to Co-Mn and Zn-Mn separations. A typical example is presented in Figure 11.

In this application, the leach solution assayed about 7 g/L cobalt and 600 mg/ L manganese. That solution was produced during the pilot plant operation described in Figure 9. The results indicated that, as soon as the SO₂/air mixtures were sparged through the cobalt solution (1 vessel volume per minute), the ORP of the pulp rose significantly to >1,200 mV and the manganese precipitated. In less than 2 hours, manganese was reduced to less than 10 mg/L. The process was demonstrated in 1997 at a pilot plant scale (60 L/h of cobalt solution). The manganese precipitate contained less than 0.5% of the cobalt initially present in the leach solution, and the leach solution, after additional purification for copper, was directed to a solvent extraction (Cyanex 272)-electrowinning (SX-EW) circuit, producing good quality cobalt cathodes.

CONCLUSIONS

Despite its negative reputation due to past abuses and deleterious impacts on the environment when not handled properly, sulfur dioxide represents for the metallurgical industries a very useful reagent that is plentiful, effective, and relatively inexpensive. Besides its traditional main use to manufacture sulfuric acid, it could find several applications in the processing of cobaltic ores, as illustrated in Figure 12 for a typical sedimentary copper-cobalt ore.

References

1. J.H. Canterford, "Cobalt Extraction and Concentration from Manganese WAD by Leaching and Precipitation," *Hydrometallurgy*, 12 (1984), pp. 335–354.

2. P. Burger, *Implication of Geological and Mineralogical Aspects of Laterite Deposits for Metallurgical Plant Design* (Perth, Australia: Alta, 1998).

3. E. Krause, B.C. Blakey, and V.G. Papangelakis, *Pressure Acid Leaching of Nickeliferrous Laterite Ores* (Perth, Australia: Alta, 1998).

4. P. Mason, *Ramu Nickel Process Piloting* (Perth, Australia: Alta, 1998).

5. P.L. Hellman, *Mineralogical and Geochemical Studies—Key Elements in Evaluating Nickel Laterites* (Perth, Australia: Alta, 2001).

6. M. Fleischer and J.A. Mandarino, "Glossary of

Mineral Species–1991," *The Mineralogical Record* (Tucson, AZ: The Mineralogical Record, Inc., 1991).

7. C. Abruzzese, "Aqueous SO₂ Processing of Manganese Ores," *Separation Processes in Hydrometallurgy*, ed. G.A. Davies (Chichester, U.K.: Ellis Horwood Publishers, 1987), pp. 77–87.

8. J.P. Allen, L.J. Froisland, and MR. Shirts, "Chemical Processing of Cobalt-Manganese Crusts," TMS-AIME Paper No. A87-15 (1987).

 C.J. Ferron, "Iron Control in Hydrometallurgy: The Positive Side of the Coin," *Iron Control Technologies*, ed. J.E. Dutrizac and P.A. Riveros (Montreal, Canada: METSOC, 2006), pp. 25–43.

10. C.J. Ferron and P. Henry, "The Use of Ferrous Sulphate to Enhance the Dissolution of Cobaltic Minerals" (Presentation at Hydrometallurgy 2008, Phoenix, AZ, 17–20 August 2008).

11. S.C. Das, P. Sahoo, and P. Rao, "Extraction of Manganese from Low-Grade Ores by FeSO₄ Leaching," *Hydrometallurgy*, 8 (1982), pp. 35–47.

12. H.P. LeVan, E.G. Davis, and L.S. Smith, USBM Report of Investigation RI 6452 (1964).

13. H.P. LeVan, E.G. Davis, and F.E. Brantley, "Extraction of Manganese from Georgia Umber Ore by a Sulphuric Acid-Ferrous Sulphate Process," USBM Report of Investigations 6692 (1965).

14. L.A. Teixeira and L.Y. Tavares, "Precipitation of Jarosite from Manganese Sulphate Solutions," *Iron Control in Hydrometallurgy*, ed. J.E. Dutrizac and A.J. Monhemius (Westergate, W. Sussex, U.K.: Ellis Horwood, 1986), pp. 431–453.

15. C.J. Ferron, *The Control of Manganese in Acidic Leach Liquors, with Special Emphasis to Laterite Leach Liquors* (Perth, Australia: ALTA, 2002).

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