# Simplified synthesis of K<sub>2</sub>CO<sub>3</sub>-promoted hydrotalcite based on hydroxide-form precursors: Effect of Mg/Al/K<sub>2</sub>CO<sub>3</sub> ratio on high-temperature CO<sub>2</sub> sorption capacity

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**Abstract**–Hydrotalcite was synthesized from hydroxide-form precursors to prepare a novel high-temperature  $CO_2$  sorbent, and the effect of Mg/Al ratio on  $CO_2$  sorption was studied. To enhance the  $CO_2$  sorption capacity of the sorbent,  $K_2CO_3$  was coprecipitated during the synthetic reaction. X-ray diffraction analysis indicated that the prepared samples had a well-defined crystalline hydrotalcite structure, and confirmed that  $K_2CO_3$  was successfully coprecipitated in the samples. The morphology of the hydrotalcite was confirmed by scanning electron microscopy, and  $N_2$  adsorption analysis was used to estimate its surface area and pore volume. In addition, thermogravimetric analysis was used to measure its  $CO_2$  sorption capacity, and the results revealed that the Mg : Al :  $K_2CO_3$  ratio used in the preparation has an optimum value for maximum  $CO_2$  sorption capacity.

Keywords: Hydrotalcite, Sorption, CO2 Sorbent, K2CO3 Promotion, Hydrothermal Synthesis

## INTRODUCTION

The threat of global warming necessitates the development of technologies for the reduction of greenhouse gases. CO<sub>2</sub> is the main anthropogenic greenhouse gas, and its concentration in the atmosphere continues to increase because fossil fuels, which emit CO<sub>2</sub> through combustion, are still used in many industries [1]. Therefore, the capture of CO<sub>2</sub> from power plant flue gases is an important strategy to reduce industrial CO<sub>2</sub> emissions. Technologies for the direct capture of CO2 at high temperature are required to efficiently and economically capture CO<sub>2</sub> from high-temperature flue gases. Calcium oxide, lithium zirconate, and hydrotalcite have been widely considered as sorbents for high-temperature CO<sub>2</sub> capture. Both calcium oxide and lithium zirconate have high CO<sub>2</sub> sorption capacities at high temperature, but the sorption capacity of calcium oxide continuously deteriorates over repeated sorption and desorption cycles, and lithium zirconate exhibits relatively slow CO2 sorption kinetics. Moreover, both materials require very high temperatures of more than 800 °C for regeneration [2,3]. However, hydrotalcite has relatively fast CO<sub>2</sub> sorption kinetics, good thermal stability, and a moderate regeneration temperature.

Hydrotalcite, also known as layered double hydroxide (LDH), is composed of positively charged brucite-like layers in which some of the divalent cations are substituted with trivalent cations. The excess positive charge in the hydrotalcite layers is compensated by interlayer anions and H<sub>2</sub>O molecules [4]. Hydrotalcite has the general formula  $[M^{2+}_{1-x}M^{3+}_{x}(OH)_{2}][A^{n-}_{x/n}]\cdot mH_{2}O$ , where  $M^{2+}$  is a divalent cation such as  $Mg^{2+}$ ,  $Zn^{2+}$ ,  $Co^{2+}$ ,  $Cu^{2+}$ , or  $Ni^{2+}$ ,  $M^{3+}$  is a trivalent cation such as  $Al^{3+}$ ,  $Cr^{3+}$ ,  $Ga^{3+}$ , or  $Mn^{3+}$ ,  $A^{n-}$  is an interlayer anion such as  $CO_3^{2-}$ ,  $NO_3^{-}$ , or  $SO_4^{2-}$ , m is the amount of H<sub>2</sub>O present in the interlayer, and x is the substitution degree of the trivalent cations [5,6]. Hydrotalcite materials have received considerable attention as catalysts, anion-exchangers, pharmaceuticals, and sorbents [7-9]. Recently, to develop and improve hydrotalcites as high-temperature CO<sub>2</sub>-capturing sorbents, many studies have focused on the effects of different divalent and trivalent cations, synthetic pH, and promotion with alkali metals [10-13]. Of these strategies, alkali metal-promoted hydrotalcite has shown particularly improved CO<sub>2</sub> sorption capacity, but its current synthesis method is time-consuming and inconvenient, because the hydrotalcite synthesis and alkali metal impregnation steps are performed separately [14].

Conventional hydrotalcite is easily synthesized by a co-precipitation method from water-soluble nitrate precursors, but the product crystallinity is relatively low. Moreover, the product must be repeatedly washed to remove remaining nitrate ions that originate from the metal nitrate precursors, and the large amounts of KOH or NaOH that are used to control the solution pH. Repeated washing steps generate wastewater and cause environmental problems.

In this study, we synthesized hydrotalcites with different Mg/Al molar ratios from hydroxide-form precursors to investigate the effect of the Mg/Al ratio on the  $CO_2$  sorption capacity of the hydrotalcite. The purpose of this study is the development of a high-performance  $CO_2$  sorbent using a simple and eco-friendly synthesis method. Hydroxide precursors such as Mg(OH)<sub>2</sub> and Al(OH)<sub>2</sub>, and K<sub>2</sub>CO<sub>3</sub> were used to supply divalent and trivalent cations, and interlayer anions, respectively, as follows [15]:

 $\begin{aligned} (1-x)Mg(OH)_2+xAl(OH)_3+(x/2)K_2CO_3+mH_2O\\ \rightarrow [Mg_{1-x}Al_x(OH)_2][CO_3]_{x/2}\cdot mH_2O+xKOH \end{aligned}$ 

The Mg/Al molar ratio was varied to 1, 2, 3, and 5 to assess the effect of Mg/Al ratio on  $CO_2$  sorption, and the  $K_2CO_3/Al$  ratio was

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$Mg(OH)_2$ : $Al(OH)_3$ : $K_2CO_3$ molar ratio in feed	Initial pH	Final pH	BET surface area (m <sup>2</sup> /g)	Pore volume $(cm^3/g)$
1:1:0.5	11.1	11.2	179	0.239
2:1:0.5		12.5	166	0.208
3:1:0.5		13.2	148	0.205
5:1:0.5		13.0	137	0.192
1:1:3	11.3	11.6	47.9	0.121
2:1:3		13.4	34.3	0.0813
3:1:3		13.5	29.8	0.0896
5:1:3		13.5	46.0	0.124

Table 1. Synthetic conditions and physical properties of hydrotalcites

also varied for the  $K_2CO_3$ -promoted hydrotalcites. The stoichiometric  $K_2CO_3/Al$  molar ratio required to supply sufficient  $CO_3^{2-}$ anions is 0.5, but we added 1-6 times the stoichiometric amount of  $K_2CO_3$  for comparison. With excess  $K_2CO_3$  in the preparation, the remaining  $K_2CO_3$  is co-precipitated during the hydrotalcite synthesis. In this preparation method, a washing step is not needed because the only remaining byproduct is KOH, which can be easily separated during the filtering step. Using this simple and novel method, we have synthesized  $K_2CO_3$ -promoted hydrotalcites with different Mg/Al ratios for use as high-temperature  $CO_2$  sorbents.

#### **EXPERIMENTAL SECTION**

#### 1. Materials

All precursors, including magnesium hydroxide (Mg(OH)<sub>2</sub>,  $\geq$ 95%), aluminum hydroxide (Al(OH)<sub>3</sub>, reagent grade), and potassium carbonate (K<sub>2</sub>CO<sub>3</sub>,  $\geq$ 99%), were purchased from Sigma-Aldrich (USA). All reagents were used without further purification. Distilled water was used as a solvent in the synthesis procedure.

## 2. Preparation of Samples

The hydrotalcites were prepared by the hydrothermal method because  $Mg(OH)_2$  and  $Al(OH)_3$  have very small solubility product constants (K<sub>sp</sub>) at room temperature. First, predetermined amounts of  $Mg(OH)_2$ ,  $Al(OH)_3$ , and  $K_2CO_3$  were mixed with 30 mL of distilled water, and the initial pH of the mixture was measured. The mixture was then transferred to 40 mL Teflon-lined stainless steel autoclave and hydrothermally reacted at 160 °C for 24 h. The solution was then quickly cooled, and the final pH of the mother liquor was measured. The aged suspension was filtered, and the filter cake was dried at 110 °C. Finally, the resulting white powder was calcined at 500 °C for 3 h under a N<sub>2</sub> atmosphere.

#### 3. Characterization

The pH of the reaction solution was measured before and after the reaction using a pH meter (Thermo scientific, Orion 4 star). The Brunauer-Emmett-Teller (BET) surface area and Barret-Joyner-Halenda (BJH) desorption pore volume were calculated from the  $N_2$ adsorption isotherm at 77 K, as obtained by using an ASAP2020 analyzer (Micromeritics). The morphology of the samples was observed by field emission scanning electron microscopy (FESEM, Hitachi S-4300). Before the measurement, samples were coated with Pt using ion sputtering because visualization of structural details in FESEM requires optimal conductivity. The X-ray diffraction (XRD) patterns of the samples were measured with a Rigaku D/Max2500V X-ray diffractometer with Cu K $\alpha$  radiation ( $\lambda$ =0.15418 nm) and a power of 40 kV×40 mA. The 2 $\theta$  scan range was from 5° to 70° at a scanning rate of 4°/min. The crystalline phases were identified by comparison of the XRD patterns with the JCPDS database. **4. CO<sub>2</sub> Sorption Measurement** 

The CO<sub>2</sub> sorption capacities of the hydrotalcites were measured through thermogravimetric analysis (TGA, TA Instruments Q50). Before CO<sub>2</sub> sorption measurement, samples were pretreated at 500 °C for 3 h under an N<sub>2</sub> atmosphere to remove any moisture and CO<sub>2</sub>. After pretreatment, the temperature was decreased to the sorption temperature of 240 °C, and the sample weight was stabilized before the N<sub>2</sub> gas was switched to pure CO<sub>2</sub> gas. The sorption capacity was determined from the weight change during the CO<sub>2</sub> sorption at 240 °C and 1 atm CO<sub>2</sub> over 5 h.

### **RESULTS AND DISCUSSION**

After the synthetic reaction, the pH value of all solutions was increased, as shown in Table 1, because KOH was generated as a byproduct. Moreover, when the  $K_2CO_3/AI$  ratio was increased from 0.5 to 3, pH values of both the initial and final solution increased. Table 1 also shows the BET surface areas and BJH desorption pore volumes. When only the stoichiometric amount of  $K_2CO_3$  was used, the BET surface area and pore volume were higher than when an excess of  $K_2CO_3$  ( $K_2CO_3/AI=3$ ) was used. This implies that the remaining  $K_2CO_3$  that did not participate in the synthetic reaction was successfully co-precipitated during the reaction, and filled and blocked the hydrotalcite pores.

The FESEM images of hydrotalcites with different Mg/Al molar ratios are shown in Fig. 1. For Mg/Al ratios of 1 or 2, there are irregular small particles on the plate-like structures. When the Mg/Al ratio increases to 3, no irregular small particles are observed. It is notable that hydrotalcite adopts its typical hexagonal plate-like morphology when the Mg/Al ratio is 3 or 5. In addition, when only stoichiometric  $K_2CO_3$  is used, hexagonal plates do not fully develop because the amount of  $CO_3^{2-}$  is insufficient to facilitate the formation of the hexagonal plate-like morphology of hydrotalcite. The morphology does not change during calcination at 500 °C for 3 h under an N<sub>2</sub> atmosphere.

Fig. 2 shows the XRD patterns of the synthesized hydrotalcites with different Mg/Al and K<sub>2</sub>CO<sub>3</sub>/Al ratios. All the samples present characteristic hydrotalcite peaks and well-defined layered structures, although some samples present peaks for unreacted Mg(OH)<sub>2</sub>. For



Fig. 1. SEM images of hydrotalcites synthesized with different Mg:Al: K<sub>2</sub>CO<sub>3</sub> ratios: (a) 1:1:0.5, (b) 2:1:0.5, (c) 3:1:0.5, (d) 5:1:0.5, (e) 1:1:3, (f) 2:1:3, (g) 3:1:3, and (h) 5:1:3.



Fig. 2. XRD patterns of hydrotalcites synthesized with different Mg : Al :  $K_2CO_3$  ratios: (a) 1 : 1 : 0.5, (b) 2 : 1 : 0.5, (c) 3 : 1 : 0.5, (d) 5 : 1 : 0.5, (e) 1 : 1 : 3, (f) 2 : 1 : 3, (g) 3 : 1 : 3, and (h) 5 : 1 : 3. Left: before calcination; right: after calcination.

the hydrotalcites prepared with Mg/Al ratios of 1 or 2, the characteristic  $Mg(OH)_2$  peaks are not significant. When the Mg/Al ratio increases from 2 to 3 or 5, the  $Mg(OH)_2$  peak intensity increases. This indicates that  $Mg(OH)_2$  conversion decreases with increasing Mg/Al ratio. This result also implies that only a limited amount of  $Mg(OH)_2$  participates in the synthetic reaction and is incorporated into the hydrotalcite structure. A plausible explanation for this is that as the Mg/Al ratio increases, a relatively large number of Mg ions cannot substitute with Al ions to develop the hydrotalcite structure because the number of Al ions is relatively small.

When only a stoichiometric amount of K2CO3 is used, no K2CO3

peaks appear because almost all the  $K_2CO_3$  participates in the synthetic reaction and supplies the  $CO_3^{2-}$  anions to form the hydrotalcite structure. However,  $K_2CO_3$  peaks are clearly detected when excess amounts of  $K_2CO_3$  are used. This indicates that  $K_2CO_3$  is co-precipitated during the synthesis step. Thus, by using excess  $K_2CO_3$ as a precursor material,  $K_2CO_3$ -promoted hydrotalcite is successfully synthesized.

The degree of transformation was calculated from the Mg(OH)<sub>2</sub> and hydrotalcite peak intensity ratios in the XRD patterns at their characteristic peak angles of  $38.0^{\circ}$  and  $11.5^{\circ}$  (2 $\theta$ ), respectively [16]. The relative contents of Mg(OH)<sub>2</sub> and hydrotalcite are shown in

Mg: Al: K molar ratio in feed	$I_{Mg(OH)_2}/I_{hydrotalcite}$ (%)
1:1:0.5	11.3
2:1:0.5	15.3
3:1:0.5	40.9
5:1:0.5	120
1:1:3	9.2
2:1:3	11.1
3:1:3	38.4
5:1:3	108

Table 2. Relative content of  $Mg(OH)_2$  in the synthesized hydrotalcites based on XRD patterns

Table 2. When the Mg/Al ratio is 1 or 2, a relatively small amount of unreacted Mg(OH)<sub>2</sub> remains, but as the Mg/Al ratio increases to 3 or 5, a relatively large amount of unreacted Mg(OH)<sub>2</sub> remains in the sample. Moreover, when only a stoichiometric amount of  $K_2CO_3$  is used, the relative amount of unreacted Mg(OH)<sub>2</sub> in the sample is higher than that when an excess amount of  $K_2CO_3$  is used. This is because a stoichiometric amount of  $K_2CO_3$  is not enough to efficiently supply the interlayer anions. However, the  $K_2CO_3/Al$ ratio does not significantly influence the synthesis conversion. A relatively small increase in the reaction conversion is observed even when six-times the stoichiometric amount of  $K_2CO_3$  is used.

In general, hydrotalcite itself is not directly applied as a CO<sub>2</sub> sorbent, but is thermally treated before use. During thermal treatment, the hydrotalcite loses its interlayer water and anions, and then dehydroxylation and decarbonation occur. During the thermal treatment, the hydrotalcite structure is transformed into an amorphous mixed oxide [17]. The thermally treated hydrotalcite has a higher surface area and pore volume than pristine hydrotalcite [18,19], and this enhances its CO<sub>2</sub> sorption capacity. Therefore, in this study, all hydrotalcites were calcined before CO<sub>2</sub> sorption tests. Fig. 2 also shows the XRD patterns of hydrotalcites after calcination at 500 °C for 3 h under a N<sub>2</sub> atmosphere. After calcination, all the hydrotalcite and Mg(OH)<sub>2</sub> phases are transformed to mixed oxides. How-



Fig. 3. CO<sub>2</sub> sorption capacities at 240 °C and 1 atm CO<sub>2</sub> for hydrotalcites prepared with different Mg/Al and K<sub>2</sub>CO<sub>3</sub>/Al ratios.

Fig. 3 compares the CO<sub>2</sub> sorption capacities at 240 °C and 1 atm CO<sub>2</sub> for the hydrotalcites prepared with different Mg/Al and K<sub>2</sub>CO<sub>3</sub>/ Al ratios. In the hydrotalcites prepared with a stoichiometric amount of K<sub>2</sub>CO<sub>3</sub> (Al: K=1:0.5), the Mg/Al ratio has no significant effect on CO<sub>2</sub> sorption capacity. Upon increasing the Mg/Al ratio from 1 to 5, the  $CO_2$  sorption capacity shows a slight increase, but it is not significant. However, when excess K<sub>2</sub>CO<sub>3</sub> is used (Al: K=1:3), the effect of the Mg/Al ratio on CO2 sorption capacity is significant. The hydrotalcite prepared with a Mg/Al ratio of 3 shows significantly increased CO2 sorption capacity because the co-precipitated K<sub>2</sub>CO<sub>3</sub> enhances the CO<sub>2</sub> sorption. Its CO<sub>2</sub> sorption capacity is much higher than that of conventional hydrotalcites [12,20,21]. Conversely, the other hydrotalcite samples exhibit similar CO<sub>2</sub> sorption capacities, even those prepared with K<sub>2</sub>CO<sub>3</sub> co-precipitation. It was reported that the effect of K2CO3 amount on the CO2 sorption capacity of hydrotalcite can vary depending on the Mg/Al ratio [11]. Also, the K<sub>2</sub>CO<sub>3</sub> is thought to have two conflicting effects on the CO<sub>2</sub> sorption capacity of hydrotalcite. The increasing amount of K<sub>2</sub>CO<sub>3</sub> enhances the basicity of the hydrotalcite, which is beneficial for the sorption of weakly acidic CO2. However, co-precipitated K<sub>2</sub>CO<sub>3</sub> also can block and fill the pores of hydrotalcite, resulting in the decreased number of sorption sites and finally reduced physisorption of CO<sub>2</sub>. Therefore, the amount of co-precipitated K<sub>2</sub>CO<sub>3</sub> has an optimum value for maximum CO<sub>2</sub> sorption capacity of hydrotalcite.

#### CONCLUSIONS

Hydrotalcites were synthesized from hydroxide-form precursors to assess the effect of Mg/Al ratio on CO<sub>2</sub> sorption capacity. When only a stoichiometric amount K2CO3 was used in the preparation, the Mg/Al ratio did not significantly affect the CO<sub>2</sub> sorption capacity of the hydrotalcite. When excess K<sub>2</sub>CO<sub>3</sub> was used, K<sub>2</sub>CO<sub>3</sub>-promoted hydrotalcite was successfully synthesized and the resultant K<sub>2</sub>CO<sub>3</sub>-promoted hydrotalcite exhibited improved CO<sub>2</sub> sorption capacity. This new method is simple and eco-friendly because the synthetic reaction and K<sub>2</sub>CO<sub>3</sub> co-precipitation occur simultaneously, thus avoiding wasteful and time-consuming washing steps. The hydrotalcite prepared with a Mg/Al ratio of 3 showed significantly increased CO<sub>2</sub> sorption capacity, implying that an optimum K<sub>2</sub>CO<sub>3</sub>/Al/Mg ratio for CO<sub>2</sub> sorption exists. In this study, the optimum Mg: Al:  $K_2CO_3$  ratio for CO<sub>2</sub> sorption was 3:1:3, and the CO<sub>2</sub> sorption capacity of the resultant hydrotalcite was much higher than that of conventional hydrotalcites.

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## REFERENCES

- D. J. Hofmann, J. H. Butler, E. J. Dlugokencky, J. W. Elkins, K. Masarie, S. A. Montzka and P. Tans, *Tellus B*, 58, 614 (2006).
- 2. J. Ida and Y. S. Lin, Environ. Sci. Technol., 37, 1999 (2003).
- W. Q. Liu, H. An, C. L. Qin, J. J. Yin, G. X. Wang, B. Feng and M. H. Xu, *Energy Fuel*, 26, 2751 (2012).
- 4. A. Garcia-Gallastegui, D. Iruretagoyena, M. Mokhtar, A. M. Asiri, S. N. Basahel, S. A. Al-Thabaiti, A. O. Alyoubi, D. Chadwick and M. S. P. Shaffer, *J. Mater. Chem.*, **22**, 13932 (2012).
- 5. F. Li, X. R. Jiang, D. G. Evans and X. Duan, *J. Porous Mater.*, **12**, 55 (2005).
- M. K. R. Reddy, Z. P. Xu, G. Q. Lu and J. C. D. Da Costa, *Ind. Eng. Chem. Res.*, 45, 7504 (2006).
- 7. L. Feng and X. Duan, Struct. Bond., 119, 193 (2006).
- N. Barakos, S. Pasias and N. Papayannakos, *Bioresour. Technol.*, 99, 5037 (2008).
- 9. D. P. Debecker, E. M. Gaigneaux and G. Busca, *Chem-Eur. J.*, 15, 3920 (2009).
- C. T. Yavuz, B. D. Shinall, A. V. Iretskii, M. G. White, T. Golden, M. Atilhan, P. C. Ford and G. D. Stucky, *Chem. Mater.*, 21, 3473 (2009).

- J. M. Lee, Y. J. Min, K. B. Lee, S. G. Jeon, J. G. Na and H. J. Ryu, *Lang-muir*, 26, 18788 (2010).
- Q. A. Wang, H. H. Tay, D. J. W. Ng, L. W. Chen, Y. Liu, J. Chang, Z. Y. Zhong, J. Z. Luo and A. Borgna, *ChemSusChem*, 3, 965 (2010).
- Q. Wang, H. H. Tay, Z. H. Guo, L. W. Chen, Y. Liu, J. Chang, Z. Y. Zhong, J. Z. Luo and A. Borgna, *Appl. Clay Sci.*, 55, 18 (2012).
- S. Walspurger, L. Boels, P. D. Cobden, G. D. Elzinga, W. G. Haije and R. W. van den Brink, *ChemSusChem*, 1, 643 (2008).
- H. J. Jang, C. H. Lee, S. Kim, S. H. Kim and K. B. Lee, ACS Appl. Mater. Interfaces, 6, 6914 (2014).
- 16. Z. Zhang, G. M. Chen and K. L. Xu, Appl. Clay Sci., 72, 206 (2013).
- 17. W. S. Yang, Y. Kim, P. K. T. Liu, M. Sahimi and T. T. Tsotsis, *Chem. Eng. Sci.*, **57**, 2945 (2002).
- F. Rey, V. Fornes and J. M. Rojo, J. Chem. Soc. Faraday T., 88, 2233 (1992).
- 19. Y. J. Min, S.-M. Hong, S. H. Kim, K. B. Lee and S. G. Jeon, *Korean J. Chem. Eng.*, **31**, 1668 (2014).
- 20. J. I. Yang and J. N. Kim, Korean J. Chem. Eng., 23, 77 (2006).
- 21. Z. Yong, V. Mata and A. E. Rodriguez, *Ind. Eng. Chem. Res.*, **40**, 204 (2001).