# Solubility of carbon dioxide in ammonium-based ionic liquids: Butyltrimethylammonium bis(trifluoromethylsulfonyl)imide and methyltrioctylammonium bis(trifluoromethylsulfonyl)imide

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Abstract*−*Solubility results of carbon dioxide (CO2) in two ammonium-based ionic liquids, butyltrimethylammonium bis(trifluoromethylsulfonyl)imide ([N4,1,1,1][Tf<sub>2</sub>N]) and methyltrioctylammonium bis(trifluoromethylsulfonyl)imide  $(N1,8,8,8$ ][Tf<sub>2</sub>N]), are presented at pressures up to approximately 45 MPa and temperatures ranging from 303.15 K to 343.15 K. The solubility was determined by measuring bubble point pressures of mixtures of CO<sub>2</sub> and ionic liquid using a high-pressure equilibrium apparatus equipped with a variable-volume view cell. Sharp increase of equilibrium pressure was observed at high CO<sub>2</sub> compositions. The CO<sub>2</sub> solubility in ionic liquids increased with the increase of the total length of alkyl chains attached to the ammonium cation of the ionic liquids. The experimental data for the  $CO<sub>2</sub>$ +ionic liquid systems were correlated using the Peng-Robinson equation of state.

Key words: Solubility, Carbon Dioxide, Ionic Liquid, Ammonium, Correlation, Peng-Robinson Equation of State

## INTRODUCTION

Ionic liquids have shown excellent performance advancing existing technologies in a variety of chemical processes, resulting in explosive expansion of research and application. Currently, they are being used as catalysts and solvents in organic or inorganic reactions, electrolytes for fuel cells, solar cells and secondary batteries, and solvents for biomass processing [1-3]. Besides their use as potential new green solvents or reaction media, ionic liquids also can be used as separation media for various separation processes, especially as absorbents for capturing  $CO<sub>2</sub>$  from gas mixtures [4-10]. Studies on treatment of gases through the use of ionic liquids have drawn a great attention. The nonvolatility of ionic liquids would not contaminate a gas stream, which gives ionic liquids a strong advantage over conventional solvents used for absorbing gases. To select an efficient ionic liquid for use as a gas separation medium, it is necessary to know the solubility of the gas in the ionic liquid phase. A large number of publications on the solubility of  $CO<sub>2</sub>$  in pure ionic liquids have been released [11-22]. Many investigators have reported that the characteristic of  $CO<sub>2</sub>$  absorption of ionic liquids is very useful in separating  $CO<sub>2</sub>$  from natural and exhaust gases. As a result, the utilization of ionic liquids for  $CO<sub>2</sub>$  capture and separation has recently gained great interest in the issues of global warming and  $CO<sub>2</sub>$  emissions [23].

The current leading technology involves CO<sub>2</sub> absorption by aqueous amine solutions as chemical absorbents. Even though the aminebased methods are highly efficient for  $CO<sub>2</sub>$  capture, they have several concerns, including high volatility, thermal instability, high energy consumption for regeneration, corrosion, and degradation of amines. Many studies on the use of ionic liquids as an alternative  $CO<sub>2</sub>$  ab-

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sorbent, which are capable of overcoming those problems, have been conducted [8,24]. An ideal  $CO<sub>2</sub>$  absorbent needs to satisfy the following primary requirements: high  $CO<sub>2</sub>$  absorption capacity and selectivity, mild regeneration condition, thermal and chemical stability, low viscosity, and low price. As the ionic liquid consists of cation and anion, it is possible to change their characteristics by modifying the structures of cation and anion groups.

In this work, we used a high-pressure equilibrium apparatus with a variable-volume view cell to measure the CO<sub>2</sub> solubilities for two kinds of ammonium-based ionic liquids with the same anion: butyltrimethylammonium bis(trifluoromethylsulfonyl)imide ([N4,1,1,1] [Tf<sub>2</sub>N]) and methyltrioctylammonium bis(trifluoromethylsulfonyl) imide ( $[N1,8,8,8][Tf_2N]$ ). The solubility was determined on the basis of measuring phase boundaries, i.e., bubble point pressures, for a mixture of CO<sub>2</sub> and ionic liquid with a known composition at a fixed temperature. From the phase boundary data of the binary mixture, the CO<sub>2</sub> solubilities were obtained as a function of temperature and pressure. Moreover, the experimental data for the binary systems of  $CO<sub>2</sub>$ +ionic liquids were correlated using the Peng-Robinson equation of state with the two adjustable binary interaction parameters in its mixing rules.

### EXPERIMENTAL

#### 1. Materials

Two ionic liquids  $([N4,1,1,1][Tf_2N]$  and  $[N1,8,8,8][Tf_2N])$  used in this work were purchased from Sigma-Aldrich. For solubility measurements, the ionic liquid sample was placed in the equilibrium cell, followed by evacuation using a mechanical pump at room temperature during several days. The analysis of coulometric Karl Fischer titration (Metrohm model 684) was performed to measure the water content for the evacuated ionic liquid samples. The characteristic values of the ionic liquids studied in this work are given in

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Chemical name	Abbreviation	Chemical formula	CAS number	Molecular mass	Purity $(mass \%)$	Water content $(mass \%)$
Butyltrimethylammonium bis(trifluoromethylsulfonyl)imide	[N4,1,1,1][Tf,N]	$C_9H_{18}N_2S_2O_4F_6$	258273-75-5	396.37	98.5	0.40
Methyltrioctylammonium bis(trifluoromethylsulfonyl)imide	[N1,8,8,8][Tf,N]	$C_{27}H_{54}N_2S_2O_4F_6$ 375395-33-8		648.85	99	0.37

Table 1. Ionic liquids studied in this work



Fig. 1. Chemical structures of ionic liquids studied in this work: (a)  $[N4,1,1,1][Tf_2N]$ ; (b)  $[N1,8,8,8][Tf_2N]$ .

Table 1, and their chemical structures are shown in Fig. 1.  $CO<sub>2</sub>$  with 99.99% high purity to be used for measurements was purchased from Myung Sin General Gas Co. (Korea). No further purification was performed for use of the ionic liquids and  $CO<sub>2</sub>$ .

#### 2. Apparatus and Procedure

A high-pressure variable-volume view cell apparatus was set up for measuring the solubility of  $CO<sub>2</sub>$  in ionic liquids. A schematic diagram of the experimental apparatus and a detailed description of the experimental procedure are given in our previous publications [14,16,17]. The apparatus is composed of a view cell equipped with a sapphire window and a movable piston, a pressure generator (High Pressure Equipment Co. model 50-6-15), a borescope (Olympus model R080-044-000-50), a magnetic stirring system, and an air bath. The cylindrical view cell is 16 mm i.d. by 70 mm o.d., and its internal working volume is approximately 31 cm<sup>3</sup>. A high-precision pressure gauge (Dresser Heise model CC-12-G-A-02B, ±0.05 MPa accuracy, ±0.01 MPa resolution) was used to measure the system pressure. An RTD probe inserted into the cell was used in measurement of the system temperature within  $\pm 0.1$  K.

 $CO<sub>2</sub>$  solubilities in ionic liquid were determined through measuring bubble point pressures for  $CO<sub>2</sub>$ +ionic liquid mixtures with various compositions at known temperatures. A feature of using the variable-volume view cell apparatus is that the concentration of the system is maintained constant throughout the experiment. A brief description of the experimental procedure is as follows. An ionic liquid sample was injected into the cell by using a gas-tight syringe. A sensitive balance (AND model HM-30) measurable to  $\pm 0.1$  mg was used in determining the amount of the ionic liquid loaded. The cell was placed within the air bath after assembling a piston and a sapphire window. And then the cell was evacuated with a mechanical pump at room temperature during overnight to remove any entrapped air inside the cell and any dissolved gas and water in the ionic liquid.

 $CO<sub>2</sub>$  was delivered to the cell via a feed line by a small  $CO<sub>2</sub>$  cylinder after the vapor space of the cell was fully evacuated. The exact amount of CO<sub>2</sub> delivered to the cell was determined by measuring the weights of the CO<sub>2</sub> cylinder before and after delivery, in use of a balance (Precisa model 1,212 M) with an accuracy of  $\pm 1$  mg. Through dipping the CO<sub>2</sub> cylinder in a Dewar flask full of liquid nitrogen, CO<sub>2</sub> gas in the feed line was recovered back into the CO<sub>2</sub> cylinder. For ionic liquid and  $CO<sub>2</sub>$ , uncertainties in measuring their masses were 0.2 mg and 2 mg, respectively. For composition of each component, an uncertainty analysis was performed according to the ISO guideline [25].

For a  $CO<sub>2</sub>$ +ionic liquid mixture with a specified overall composition, the system pressure was changed until the phase change inside the cell was visually observed through the cell window. The fluid in the cell was compressed to dissolve CO<sub>2</sub> into the ionic liquid. The fluid was well stirred and simultaneously heated to the target temperature. The system temperature was controlled within an uncertainty of  $\pm 0.1$  K. At an elevated pressure, the fluid became a single homogeneous phase after dissolution of  $CO<sub>2</sub>$  into the ionic liquid phase. Then the pressure slowly decreased until tiny CO<sub>2</sub> bubbles started to form from the single phase solution. We defined the bubble point pressure of the solution at a given composition and temperature to be the initial pressure at which the first bubbles were observed. Every observation was repeated at least twice to ensure the reproducibility of experimental data. The uncertainty in measuring the bubble point pressure was 0.02 MPa. For a solution of very high  $CO<sub>2</sub>$  mole fractions, the cloud point behavior rather than the bubble point behavior was observed. Due to the phase transition from a single phase to a liquid+liquid phase, the solution became cloudy at the cloud point. The cloud pressure was defined as the pressure at which there was no more possibility of visually observing the stirring bar in the cell [26]. The precision for the measurement of cloud pressure was estimated to be about 0.1 MPa. Exactly the same way was repeated to measure the bubble or cloud point pressures at different temperatures and compositions.

#### **CORRELATION**

The solubility data for binary systems obtained in this work were correlated with a thermodynamic model which can be incorporated into a mathematical model for design calculation of absorption column. The correlation starts with a setup of phase equilibrium criterion for a binary system of  $CO<sub>2</sub>$  (component 1)+ionic liquid (component 2). Only pure  $CO<sub>2</sub>$  exists in the gas phase, because the ionic liquid is assumed to be non-volatile. Thus, the criterion for phase equilibrium at a constant temperature and pressure is satisfied when the fugacity of  $CO_2$  in gas phase  $(f_1^{gas})$  is equal to that of  $CO_2$  in ionic liquid phase  $(\hat{f}_1^{\mu})$ :

(1)  $f_1^{gas} = \hat{f}_1^{IL}$ 

The fugacity relationship with respect to temperature and pressure can be expressed by an equation of state. Among a variety of equations of state, the Peng-Robinson equation of state (PR-EoS), one of the most popular for practical applications, was used in this work.

The PR-EoS is written as follows [27]:

$$
P = \frac{RT}{V - b} - \frac{a(T)}{V(V + b) + b(V - b)}
$$
(2)

The following quadratic mixing rules were used to calculate the mixture parameters in ionic liquid phase:

$$
\mathbf{a} = \sum_{i} \sum_{j} \mathbf{x}_{i} \mathbf{x}_{j} \mathbf{a}_{ij} \tag{3}
$$

$$
a_{ij} = (a_{ii}a_{jj})^{1/2}(1-k_{ij})
$$
\n(4)

$$
b = \sum_{i} \sum_{j} x_{i} x_{j} b_{ij} \tag{5}
$$

$$
\mathbf{b}_{ij} = \left(\frac{\mathbf{b}_i + \mathbf{b}_j}{2}\right)(1 - l_{ij})\tag{6}
$$

In Eq. (5),  $b_{ii} = b_i$  and  $b_{jj} = b_j$ .  $k_{ij}$  and  $l_{ij}$  in Eq. (4) and Eq. (6) are the binary interaction parameters. The EoS parameters for pure component i  $(a_{ii}$  and  $b_i$ ) are the same as described in textbooks of classical thermodynamics  $[27]$ . The expressions for the fugacities of  $CO<sub>2</sub>$  in gas and ionic liquid phases using the PR-EoS can also be easily found from textbooks. Thus, it is not necessary to show the equations for calculating the pure component EoS parameters and the fugacities.

The utilization of the PR-EoS requires information on the critical properties and acentric factor for each component of the binary system. Those properties are readily available for  $CO<sub>2</sub>$ , while they are not available for ionic liquids. Therefore, those properties for ionic liquids should be estimated. We used the modified Lydersen-Joback-Reid group contribution method proposed by Valderrama and Rojas [28] to estimate the critical temperature and pressure and the acentric factor of the ionic liquids studied. The estimated values of the properties for the ionic liquids studied in this work are given in Table 2 along with those for  $CO<sub>2</sub>$ .

The phase equilibrium calculation for the  $CO<sub>2</sub>$ +ionic liquid system was performed in the following way. At a given temperature, equilibrium pressures (P) satisfying Eq. (1) were calculated as a function of  $CO<sub>2</sub>$  mole fraction  $(x<sub>1</sub>)$ . The volumetric properties of  $CO<sub>2</sub>$  and ionic liquid phases, which were required to calculate  $f<sub>1</sub><sup>gas</sup>$ and  $\hat{f}_1^{\mu}$ , were obtained by solving Eq. (2). A nonlinear least square method was used to perform this calculation. The same calculations were repeated at different temperatures.

A set of the optimum values of  $k_{12}$  and  $l_{12}$  at each temperature for a binary system was determined first before performing the above

Table 2. Critical properties and acentric factor estimated for ionic liquids

	Critical	Critical	Critical	Acentric
Ionic liquid			temperature, pressure, compressibility	factor,
	$T_{c}(K)$	$P_{c}$ (MPa)	factor, $Z_{\alpha}$	$\omega$
$[N4,1,1,1][Tf_2N]$	1038.7	2.59	0.286	0.333
$[N1, 8, 8, 8][Tf_2N]$	1376.1	1.06	0.184	0.996
CO <sub>2</sub>	304.2	7.38	0.274	0.224

phase equilibrium calculation. Those values were obtained by cor-Felating the experimental P−x<sub>1</sub> data with the PR-EoS and minimiz-<br>relating the experimental P−x<sub>1</sub> data with the PR-EoS and minimizing the following objective function:

$$
F = \sum_{m=1}^{N} \frac{\left| P_m^{calc} - P_m^{exp} \right|}{P_m^{exp}} \tag{7}
$$

where  $P_m^{exp}$  is the experimental value of equilibrium pressure for data point m,  $P_m^{\text{cancel}}$  is the equilibrium pressure calculated by the PR-EoS at the experimental value of  $x_1$  for the same data point, and N is the number of data points. An optimization routine, which solved a nonlinear least-squares problem, was used.

#### RESULTS AND DISCUSSION

## 1. CO*2* Solubility in Ionic Liquids

Solubility of gases including CO<sub>2</sub> in liquids tends to increase in proportion to pressure or decrease in inverse proportion to temperature. This tendency is universally applied to most ionic liquids reliant on physical absorption [11-22]. Even in chemical absorption with a strong  $CO<sub>2</sub>$  absorption capacity, dependence on physical absorption appears after absorption of a certain amount of  $CO<sub>2</sub>$ . Our study for ammonium-based ionic liquids confirmed this trend as well. Tables 3 and 4 show the experimental results of the phase boundaries for two binary systems:  $CO<sub>2</sub>+[N4,1,1,1][Tf<sub>2</sub>N]$  and  $CO<sub>2</sub>+[N1,8,8,8]$  $[Tf<sub>2</sub>N]$ , respectively. In those tables, the equilibrium pressure data observed at the bubble or cloud point of the  $CO<sub>2</sub>$  (component 1)+ ionic liquid (component 2) mixtures with different  $CO<sub>2</sub>$  mole fractions are given in the temperature range from about 303 K to about 343 K. The solubility data are provided in terms of the mole fraction

Table 3. Experimental bubble or cloud point data for various mole fractions of  $CO<sub>2</sub>$  in the  $CO<sub>2</sub>+[N4,1,1,1][Tf<sub>2</sub>N]$  system

Mole fraction of $CO_2$ , $X_1$	Uncertainty in $x_1$	Molality, $m_1$ (mol of $CO2/kg$ of ionic liquid)	T (K)	P (MPa)	Phase behavior observed
0.0776	0.0016	0.2122	303.2	0.10	$b^a$
			312.5	0.15	b
			322.5	0.20	b
			331.9	0.25	b
			342.3	0.35	b
0.1501	0.0029	0.4457	302.6	0.35	b
			312.4	0.45	b
			322.5	0.55	b
			332.7	0.75	b
			343.3	0.90	b
0.2554	0.0039	0.8655	302.7	0.95	b
			313.1	1.25	b
			322.9	1.50	b
			332.5	1.75	b
			342.8	2.10	b
0.3348	0.0048	1.2699	303.0	1.55	b
			312.0	1.85	b
			322.5	2.25	b
			332.9	2.65	b
			342.8	3.15	b

Table 3. Continued





of  $CO<sub>2</sub>(x<sub>1</sub>)$  in the ionic liquid phase. The uncertainty in the solubility measurement is also given for each point. The average uncertainty

Phase behavior observed

> $b^a$ b b b b

b b b b b

b b b b b

b b b b b

b b b b b

b b b b b

b b b b b

b b b b b

b b b b b

b b b b b

P (MPa)

> 0.35 0.50 0.60 0.75 0.85

> 1.10 1.25 1.45 1.65 1.90

1.55 1.90 2.20 2.45 2.85

2.10 2.50 2.90 3.35 3.75

2.60 3.10 3.65 4.15 4.75

2.80 3.35 3.80 4.40 4.95

3.45 4.15 4.85 5.50 6.30

4.10 4.95 5.85 6.65 7.55

4.65 5.75 6.65 7.70 8.80

5.15 6.30 7.40 8.70 10.05

342.9

Table 4. Continued

Mole fraction of $CO_2$ , $X_1$	Uncertainty $\ln x_1$	Molality, $m_1$ (mol of $CO2/kg$ of ionic liquid)	$\mathbf T$ (K)	$\mathbf{P}$ (MPa)	Phase behavior observed
0.7770	0.0140	5.3704	303.0	5.75	b
			313.9	7.25	b
			323.5	8.70	b
			333.1	10.30	b
			342.8	11.95	b
0.8074	0.0134	6.4588	302.7	6.40	b
			313.1	8.25	b
			323.4	10.45	b
			333.4	12.75	b
			342.4	14.75	b
0.8389	0.0124	8.0273	305.1	10.65	$c^b$
			314.8	13.50	$\mathbf c$
			323.4	15.70	$\ddot{c}$
			332.9	18.10	$\ddot{\textbf{c}}$
			343.0	20.60	$\mathbf c$
0.8539	0.0122	9.0098	303.2	14.45	$\ddot{\textbf{c}}$
			312.8	16.60	$\ddot{c}$
			322.6	18.90	$\ddot{c}$
			332.6	21.40	$\ddot{c}$
			342.6	23.80	$\ddot{c}$
0.8667	0.0120	10.0218	303.2	19.00	$\ddot{c}$
			313.9	20.90	$\ddot{c}$
			323.4	22.85	$\ddot{c}$
			333.6	25.15	$\ddot{c}$
			342.6	27.10	c
0.8809	0.0115	11.3982	303.1	28.85	$\ddot{\textbf{c}}$
			314.3	28.90	$\mathbf c$
			324.0	29.90	$\ddot{c}$
			333.2	31.45	$\ddot{\textbf{c}}$
			342.6	33.05	c

a Bubble point behavior observed

b Cloud point behavior observed

value in  $x_1$  was estimated to be 0.0054 for the CO<sub>2</sub>+[N4,1,1,1][Tf<sub>2</sub>N] system and  $0.0115$  for the CO<sub>2</sub>+[N1,8,8,8][Tf<sub>2</sub>N] system.

For each data point, information on the phase change behavior observed during measurement, i.e., bubble or cloud point behavior, is also given in Tables 3 and 4. As indicated in the tables, the cloud point behavior rather than the bubble point behavior was observed for solutions of quite high  $CO<sub>2</sub>$  mole fractions: more than about 0.73 for the  $CO_2+[N4,1,1,1][Tf_2N]$  system and 0.84 for the  $CO_2+[N1,8,8,8]$ [Tf<sub>2</sub>N] system. This phenomenon can be explained in the following manner, as already discussed in our previous publication [15]. When the  $CO<sub>2</sub>$  solubility in ionic liquid is measured in our experiments, the pressure is slowly reduced until phase separation occurs from the single-phase solution where  $CO<sub>2</sub>$  is dissolved in the ionic liquid phase. When the CO<sub>2</sub> mole fraction in the solution is small and the equilibrium pressure is low,  $CO<sub>2</sub>$  behaves like a gas, and thus the tiny bubbles come out of the solution with the pressure decrease even at temperatures above the critical point of  $CO<sub>2</sub>$ . How-



Fig. 2. P–T isopleths of phase boundaries for the  $CO<sub>2</sub>+[N4,1,1,1]$ [Tf<sub>2</sub>N] mixtures with various CO<sub>2</sub> mole fractions  $(x_1)$ .

ever, at higher  $CO<sub>2</sub>$  mole fractions and higher pressure,  $CO<sub>2</sub>$  behaves like a liquid, and the cloud pressure behavior is observed with a decrease of the equilibrium pressure. It is acknowledged that the high density of the  $CO<sub>2</sub>$  phase makes the demixing appear closer to liquid-liquid equilibrium behavior than to vapor-liquid equilibrium behavior. Due to the phase transition from a single phase to a liquid+ liquid phase, the solution becomes cloudy at the cloud point. The cloud point behavior was observed when the sharp increase of equilibrium pressure with the increase of  $CO<sub>2</sub>$  solubility occurred.

As an example of the graphical presentation of the experimental data, the P−T isopleths for the  $CO<sub>2</sub>+[N4,1,1,1][Tf<sub>2</sub>N]$  system are shown in Fig. 2. As the temperature increased at a given  $CO<sub>2</sub>$  mole fraction, the equilibrium pressure increased. The change of the equilibrium pressure with respect to temperature increased with the increase of the  $CO_2$  mole fraction. The equilibrium pressure increased significantly whe librium pressure with respect to temperature increased with the increase of the CO<sub>2</sub> mole fraction. The equilibrium pressure increased significantly when the  $CO<sub>2</sub>$  mole fraction increased isothermally. therm generated by plotting P as a function of  $x_1$  at various temcrease of the  $CO_2$  mole fraction. The equilibrium pressure increased<br>significantly when the  $CO_2$  mole fraction increased isothermally.<br>This phenomenon can be more distinctly observed from a P−x<sub>1</sub> iso-<br>therm generated b fitted with polynomial equations (second- or third-order) to obtain<br>the curve fits. And then the equilibrium pressures equivalent to desired<br>temperatures were calculated from the curve fits. Finally, the equi-<br>librium pre the curve fits. And then the equilibrium pressures equivalent to desired temperatures were calculated from the curve fits. Finally, the equilibrium pressures (P) as a function of  $x_1$  at different temperatures data obtained from the curve fits are listed in Table 5 for two systemperatures were calculated from the curve fits. Finally, the equilibrium pressures (P) as a function of  $x_1$  at different temperatures were obtained for each system. The interpolated isothermal P− $x_1$  data obtained fr for the  $CO_2+[N1,8,8,8][Tf_2N]$  system. In Fig. 3, the solubilities of  $CO<sub>2</sub>$  in mole fraction for [N1,8,8,8][Tf<sub>2</sub>N] are shown as a function of pressure at several temperatures.

The equilibrium pressure was relatively low at lower  $CO<sub>2</sub>$  compositions, while it increased sharply at higher  $CO<sub>2</sub>$  compositions. For example, in case of the  $CO<sub>2</sub>+[N1,8,8,8][Tf<sub>2</sub>N]$  in Fig. 3, the equilibrium pressure gradually increased until the  $CO<sub>2</sub>$  mole fraction reached about 0.8. On the other hand, at the  $CO<sub>2</sub>$  mole fractions higher

Mole fraction	Molality, $m_1$ (mol of	P (MPa) at following temperature						
of $CO_2$ , $X_1$	$CO2/kg$ of ionic liquid)	303.2K	313.2K	323.2K	333.2K	343.2 K		
	Ionic liquid: $[N4,1,1,1][Tf_2N]$							
0.0776	0.2122	0.10	0.15	$0.20\,$	0.27	0.35		
0.1501	0.4457	0.35	0.46	0.58	0.73	0.91		
0.2554	0.8655	0.97	1.23	1.51	1.80	2.10		
0.3348	1.2699	1.56	1.89	2.27	2.69	3.16		
0.4015	1.6927	2.07	2.51	3.02	3.58	4.21		
0.4825	2.3521	2.83	3.48	4.20	4.99	5.85		
0.5410	2.9734	3.44	4.28	5.21	6.23	7.34		
0.5851	3.5580	4.16	5.15	6.28	7.56	8.98		
0.6338	4.3669	5.03	6.25	7.74	9.47	11.46		
0.6711	5.1469	5.77	7.37	9.41	11.88	14.79		
0.7298	6.8152	9.48	14.37	19.05	23.51	27.76		
0.7575	7.8806	18.89	24.29	29.35	34.07	38.44		
0.7802	8.9537	33.17	38.66	43.79	48.56	52.97		
		Ionic liquid: $[N1,8,8,8][Tf2N]$						
0.2066	0.4014	0.35	0.48	0.61	0.74	0.86		
0.3362	0.7806	1.07	1.24	1.44	1.66	1.91		
0.4309	1.1672	1.55	1.86	2.18	2.51	2.84		
0.4996	1.5390	2.06	2.47	2.90	3.34	3.79		
0.5535	1.9108	2.61	3.11	3.63	4.19	4.77		
0.5785	2.1152	2.79	3.30	3.83	4.40	5.00		
0.6413	2.7554	3.46	4.11	4.80	5.53	6.30		
0.6840	3.3365	4.12	4.91	5.76	6.67	7.64		
0.7174	3.9127	4.64	5.61	6.64	7.72	8.85		
0.7448	4.4987	5.16	6.25	7.44	8.72	10.10		
0.7770	5.3704	5.77	7.16	8.66	10.29	12.03		
0.8074	6.4588	6.45	8.35	10.41	12.62	14.99		
0.8389	8.0273	10.13	12.98	15.67	18.22	20.62		
0.8539	9.0098	14.43	16.72	19.07	21.49	23.98		
0.8667	10.0218	18.97	20.82	22.82	24.98	27.28		
0.8809	11.3982	28.78	29.00	29.82	31.25	33.29		

Table 5. Interpolated isothermal solubility data for  $CO<sub>2</sub>$  in ionic liquids



Fig. 3. P−x<sub>1</sub> diagrams of the CO<sub>2</sub>+[N1,8,8,8][Tf<sub>2</sub>N] mixtures at different temperatures.

than about 0.8, the equilibrium pressure increased very sharply even with a small increase of the CO<sub>2</sub> mole fraction. This tendency was also generally observed for other ionic liquids as well as [N4,1,1,1] [Tf<sub>2</sub>N], to a greater or lesser extent [11-14,16-21]. Consequently, as the ionic liquids subject to this study basically show the phenomenon of physical absorption with regard to  $CO<sub>2</sub>$ , they have limitations in that the equilibrium pressure rapidly increases at a certain  $CO<sub>2</sub>$  mole fraction or higher. The higher  $CO<sub>2</sub>$  absorption capacity the ionic liquids have, the higher  $CO<sub>2</sub>$  mole fraction where the rapid change in equilibrium pressure is observed. As seen in Fig. 3, the CO<sub>2</sub> solubility decreased with an isobaric increase in temperature. In addition, its larger temperature dependence was observed at higher CO<sub>2</sub> mole fractions.

Fig. 4 compares the  $CO<sub>2</sub>$  solubility data for two ionic liquids [N4,1,1,1][Tf<sub>2</sub>N] and [N1,8,8,8][Tf<sub>2</sub>N] at 323.15 K. The CO<sub>2</sub> solubilities in ionic liquid were compared with respect to both the mole fraction and the molality. It illustrates the effect of structural modification of ammonium in the cation on the  $CO<sub>2</sub>$  solubility for the  $[Tf<sub>2</sub>N]$  anion-based ionic liquids. Compared at the same temperature and pressure,  $[N1,8,8,8][Tf_2N]$  had a higher  $CO_2$  solubility than  $[N4,1,1,1]$ [Tf<sub>2</sub>N]. This phenomenon can be explained in the fol-



Fig. 4. Comparison of CO<sub>2</sub> solubility in ionic liquids  $[N4,1,1,1][Tf,N]$ and  $[N1,8,8,8][Tf,N]$  at 333.2 K: (a) solubility in mole fraction; (b) solubility in molality.

lowing manner. As seen in the chemical structures of two ionic liquids (Fig. 1), the total length of the side chains attached to the ammonium cation of  $[N1,8,8,8][Tf,N]$  is longer than that of  $[N4,1,1,1]$ [Tf<sub>2</sub>N]. It is assumed that the longer side chains can expand free volume and increase  $CO<sub>2</sub>$  absorbed in the space [12]. As for another factor, the longer alkyl chain, the more weakened combination between cation and anion and the stronger combination between cation and  $CO<sub>2</sub>$ , and it led to increase in  $CO<sub>2</sub>$  absorption [29]. Consequently, the  $CO<sub>2</sub>$  solubility in ionic liquids increased with increase of the total length of alkyl chains attached to the ammonium cation of the ionic liquids, and this increase became more apparent at higher pressures. In Fig. 4(b), the CO<sub>2</sub> solubility results in  $[N4,1,1,1][Tf_2N]$ and  $[N1,8,8,8][Tf_2N]$  are illustrated in terms of the molality instead of the mole fraction. Unlike the mole fraction data, the molality data showed a little different behavior. As shown in Fig. 4(a), [N1,8,8,8]  $[Tf_2N]$  always gave higher  $CO_2$  solubilities in the mole fraction than  $[N4,1,1,1][Tf_2N]$  in the whole range of pressure. On the other hand, until the pressure reached about  $8$  MPa, the molality values of  $CO<sub>2</sub>$ in  $[N4,1,1,1][Tf_2N]$  and  $[N1,8,8,8][Tf_2N]$  were almost the same. This can be attributed to the big difference in molecular masses of



Fig. 5. Comparison between experimental values and calculated results by the PR-EoS for  $CO<sub>2</sub>$  solubility in ionic liquids: (a)  $[N4,1,1,1][Tf_2N]$ ; (b)  $[N1,8,8,8][Tf_2N]$ .

two ionic liquids. At pressures higher than about 8 MPa, the molality of CO<sub>2</sub> in  $[N1,8,8,8][Tf,N]$  was larger than that in  $[N4,1,1,1]$ [Tf<sub>2</sub>N], and the difference between two values became much bigger as the pressure increased. The same trends were also found at other temperatures. Therefore, when comparing the solubility of a gas in ionic liquids, it is necessary to express the gas solubility in terms of the molality as well as the mole fraction. This is because there may be a big difference in the molecular masses of ionic liquids depending on the types of cation and anion constituting the ionic liquids. 2. Correlation Results

The PR-EoS using the quadratic mixing rules was used to correlate the experimental data of the solubility of  $CO<sub>2</sub>$  in the ionic liquids studied in this work. For each system of  $CO<sub>2</sub>$ +ionic liquid, the two binary interaction parameters  $(k_{12}$  and  $l_{12})$  in the mixing rules were optimized using the P−x1 data given in Table 5. Table 6 lists the optimum values of the  $k_{12}$  and  $l_{12}$  parameters at five different temperatures for each system. The calculated results are graphically presented in Fig. 5 along with the experimentally obtained data of Table 5. The correlation results are summarized in Table 6. The average absolute deviations in percentage (AAD%) between the calculated and ex-

Table 6. Binary interaction parameters and correlation results using the PR-EoS for the  $CO<sub>2</sub>$ +ionic liquid systems

Ionic liquid	T(K)	parameters	$AAD\%^a$	
		$k_{12}$	$l_{12}$	
$[N4,1,1,1][Tf_2N]$	303.2	0.10210	0.08261	11.3
	313.2	0.10357	0.07743	9.9
	323.2	0.10530	0.07554	9.5
	333.2	0.10605	0.07257	9.1
	343.2	0.10712	0.07009	8.6
$[N1, 8, 8, 8]$ [Tf,N]	303.2	0.03985	0.03222	4.8
	313.2	0.03778	0.03122	4.8
	323.2	0.03523	0.03109	5.8
	333.2	0.03242	0.03132	6.5
	343.2	0.02970	0.03190	6.9

<sup>a</sup> Average absolute deviation in percentage, which is defined as:

 $\text{AAD}\% = \frac{1}{N} \sum_{m=1}^{N} \frac{\left| \mathbf{P}_{m}^{calc} - \mathbf{P}_{m}^{exp} \right|}{\mathbf{P}_{m}^{exp}} \times 100$  (N: number of data)  $\sum_{m=1}^{N} \frac{|\mathbf{P}_{m} - \mathbf{P}_{m}|}{\mathbf{P}_{m}^{exp}} \times 100$ 

perimental equilibrium pressures were calculated at five temperatures for each system. The average value of AAD% for entire data points in the whole range of temperature was  $9.7\%$  for  $[N4,1,1,1]$ [Tf<sub>2</sub>N] and 5.8% for [N1,8,8,8][Tf<sub>2</sub>N], respectively. The  $CO<sub>2</sub>+[N1,8,8,8]$ [Tf2N] system gave a little better correlation result. Overall, it can be concluded that the PR-EoS can satisfactorily correlate the highpressure solubility of  $CO<sub>2</sub>$  in [N4,1,1,1][Tf<sub>2</sub>N] and [N1,8,8,8][Tf<sub>2</sub>N] with the AAD% less than 10% over a wide range of pressure up to the supercritical region of  $CO<sub>2</sub>$ .

# **CONCLUSIONS**

For the two types of ammonium-based ionic liquids with different lengths of side chains in their cation, their solubilities of  $CO<sub>2</sub>$ were determined by measuring the bubble or cloud point pressures of the binary mixtures of  $CO<sub>2</sub>$ +ionic liquid using a high-pressure equilibrium apparatus equipped with a variable-volume view cell. Very high solubilities were obtained in the ionic liquids at lower pressures, whereas a sharp increase in the equilibrium pressure was observed at higher  $CO<sub>2</sub>$  compositions. The variation of the length of alkyl chains attached to the ammonium cation had a considerable effect on the  $CO<sub>2</sub>$  solubility in ionic liquid. The  $CO<sub>2</sub>$  solubility increased with an increase in the length of total alkyl chains on the cation at low pressures, and this increase became more apparent at higher pressures. The solubility data of  $CO<sub>2</sub>$  in the ammonium-based ionic liquids could be successfully correlated by using the PR-EoS with the AAD% of less than 10% over a wide range of pressure up to the supercritical region of  $CO<sub>2</sub>$ .

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