

## Effect of hydrogen partial pressure on a polymer electrolyte fuel cell performance

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(Received 11 September 2009 • accepted 12 October 2009)

**Abstract**—We first investigated the effect of partial pressure of hydrogen ( $H_2$ ) on the performance of polymer electrolyte fuel cells (PEFCs) by controlling the ratio of hydrogen and nitrogen ( $N_2$ ). The cell performance with Pt/C anode was significantly decreased with reduction of the partial pressure of  $H_2$  in the presence of carbon monoxide (CO), while the performance variation was negligible in the absence of CO. Severe CO poisoning on Pt/C electrode at low partial pressure of  $H_2$  might be attributed to the hindering effect by  $N_2$  and CO. On the other hand, PtRu/C anode showed consistent power performance even at low partial pressure of  $H_2$ .

Key words: PEM Fuel Cells, Reforming Gas,  $H_2/N_2$  Ratio, CO, Recovery Test

### INTRODUCTION

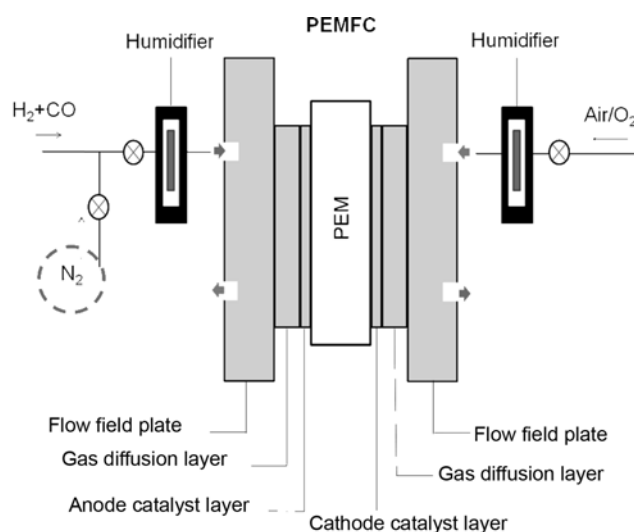
There have been several alternative portable energy systems of thin film battery, supercapacitors, solar cells and fuel cells for the operation of mobile devices such as cellular phones, lap-top computers, wheelchairs, robots and electric scooters [1-10]. Among the fuel cells, we could develop the following four types; 1) polymer electrolyte fuel cells with a micro reformer of hydrocarbons (micro-PEFCs), 2) PEFCs applying hydrogen from chemical hydride (e.g.,  $NaBH_4$ ), 3) direct liquid fuel cells (formic acid, L-ascorbic acid, methanol, ethanol), and 4) micro solid oxide and carbon fuel cells. In micro-PEFCs, hydrogen containing low concentrated CO produced *via* steam reforming or partial oxidation of methanol/methane or other hydrocarbons ( $C_nH_m$ ) requires noble metals and metal alloys as anode catalysts, since CO even below 10 ppm could cause severe energy dissipation and very low catalytic utilization [11-18]. Note that the product from micro reformer of hydrocarbons ( $C_nH_m$ ) is composed of CO,  $N_2$ ,  $H_2$ ,  $H_2O$  among others. As noted above, in addition to the presence of CO in the reformed product, another important factor would be the partial pressure of  $H_2$  and  $N_2$  in the gaseous mixture, as these may significantly affect the performance of the PEFCs. Also, we should consider another important factor of partial pressure of hydrogen and nitrogen in the presence of CO.

In this work, we describe the comparative power performance in relation to various  $H_2/N_2$  ratios in PEFCs experiments using both Pt/C and PtRu/C anode.

### EXPERIMENTAL

Two anodes of Pt/C and PtRu/C were prepared by spraying the catalyst slurry of  $0.3 \text{ mg/cm}^2$  (40% Pt/C, Tanaka),  $0.6 \text{ mg/cm}^2$  (40% PtRu/C, E-tek), respectively. Pt/C of  $0.3 \text{ mg/cm}^2$  (40% Pt/C, Tanaka)

was used as cathode. SGL 10BC was adopted as diffusion media of anode and cathode which have 5% Teflonized carbon microporous layer for easier access of oxygen and easy removal of produced water. Then, additional ionomer solution was sprayed onto the catalyst layer of each electrode in order to decrease the contact resistance with the polymer electrolyte membrane (Nafion 212, Dupont). Membrane-electrode assemblies (MEAs) of  $9 \text{ cm}^2$  were prepared by hot pressing with Nafion 212 at a temperature of  $140^\circ\text{C}$  and a pressure of  $30 \text{ kg/cm}^2$  for 5 min.



**Fig. 1.** Schematic of fuel cell setup with  $H_2/N_2$  ratio (0.35-1.0) and  $N_2$  gas supplied into the anode inlet. (a)  $H_2/N_2$  ratio=1.0, (b)  $H_2/N_2$  ratio=0.6, (c)  $H_2/N_2$  ratio=0.35. Cell temperature and relative humidity were at  $70^\circ\text{C}$  and RH 100%, respectively. The reaction gases were supplied through a humidifier and a mass flow controller from  $H_2/N_2$  mixture and air tanks. The reactant gases flowed in accordance with stoichiometry value (1.1-1.5 and 2.5 stoics for  $H_2/N_2$  and air).

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As shown in Fig. 1, hydrogen with nitrogen gas was supplied into the anode inlet by mass flow controller. Cell temperature and relative humidity were fixed at 70 °C and RH 100%, respectively. The reactant gases of H<sub>2</sub>/N<sub>2</sub> and air flowed in accordance with stoichiometry value of (1.2/2.5 stoics for H<sub>2</sub>/N<sub>2</sub> and air) loaded current.

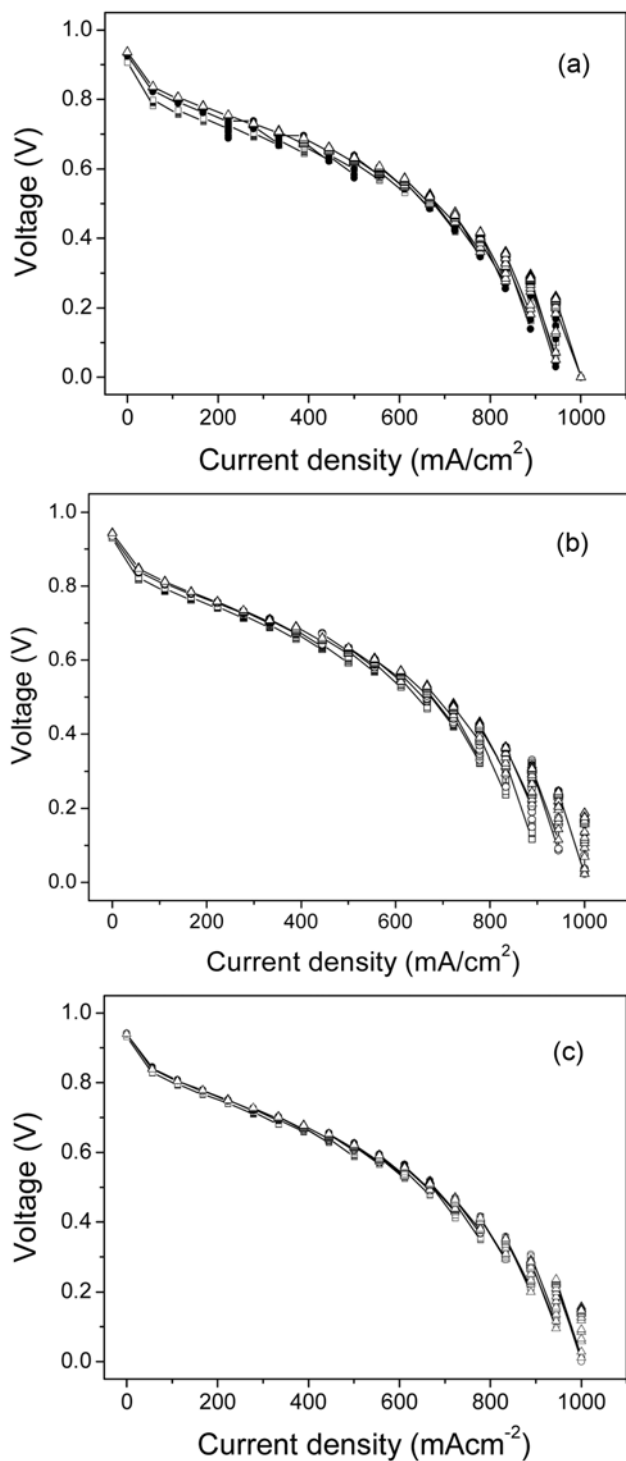


Fig. 2. Polarization curves of Pt/C of various H<sub>2</sub>/N<sub>2</sub> ratio with N<sub>2</sub> gas supplied into the anode inlet. (a) H<sub>2</sub>/N<sub>2</sub> ratio=1.0, (b) H<sub>2</sub>/N<sub>2</sub> ratio=0.6, (c) H<sub>2</sub>/N<sub>2</sub> ratio=0.35. Stoichiometry value of H<sub>2</sub>/N<sub>2</sub> (■)=1.1, (●)=1.2 and (▼)=1.5.

Current-voltage polarization curves were galvanostatically measured by using a fuel cell test station (Scitech Korea Inc). Both consecutive CO recovery test and durability test were performed and polarization curves were obtained at various H<sub>2</sub>/N<sub>2</sub> partial pressures.

## RESULTS AND DISCUSSION

Fig. 2 shows the polarization curves of Pt/C anode and Pt/C cathode under different H<sub>2</sub>/N<sub>2</sub> ratios and stoichiometric values (based on H<sub>2</sub>) in the absence of CO. The cell performance does not show any significant difference with changes in H<sub>2</sub>/N<sub>2</sub> ratio and stoichiometric values of hydrogen to 1.1 (■), 1.2 (●) and 1.5 (▼). This result indicates that the performance is not significantly affected by pure H<sub>2</sub>/N<sub>2</sub> ratio as well as stoichiometry value.

The effect of CO on the performance of Pt/C anode catalysts was tested with a gas mixture of H<sub>2</sub> and N<sub>2</sub> as shown in Fig. 3. The cell performance in Fig. 3(a) exhibited less activity than that of 10 ppm CO (see Fig. 3(b)) in all partial pressure of hydrogen, which might

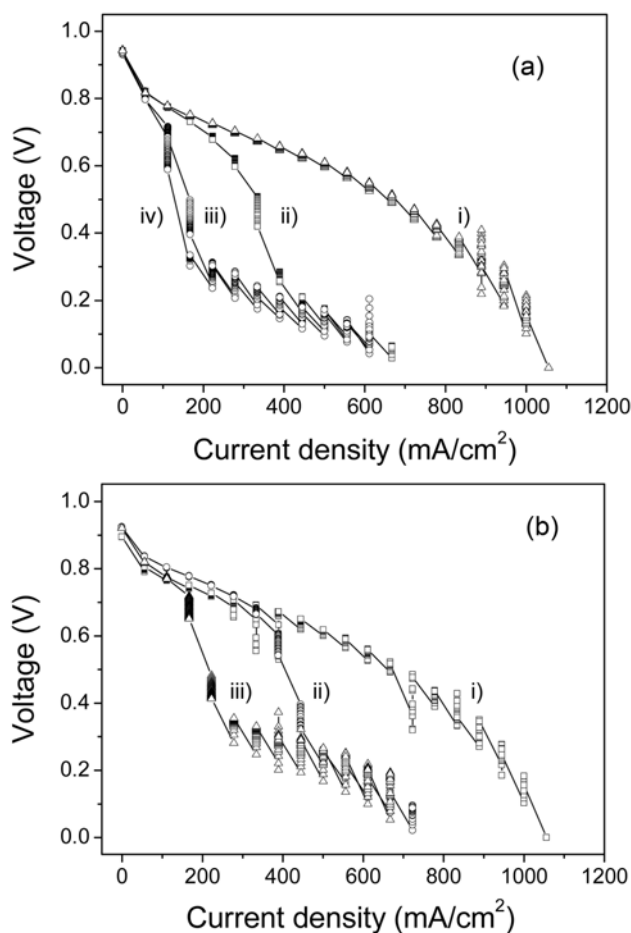
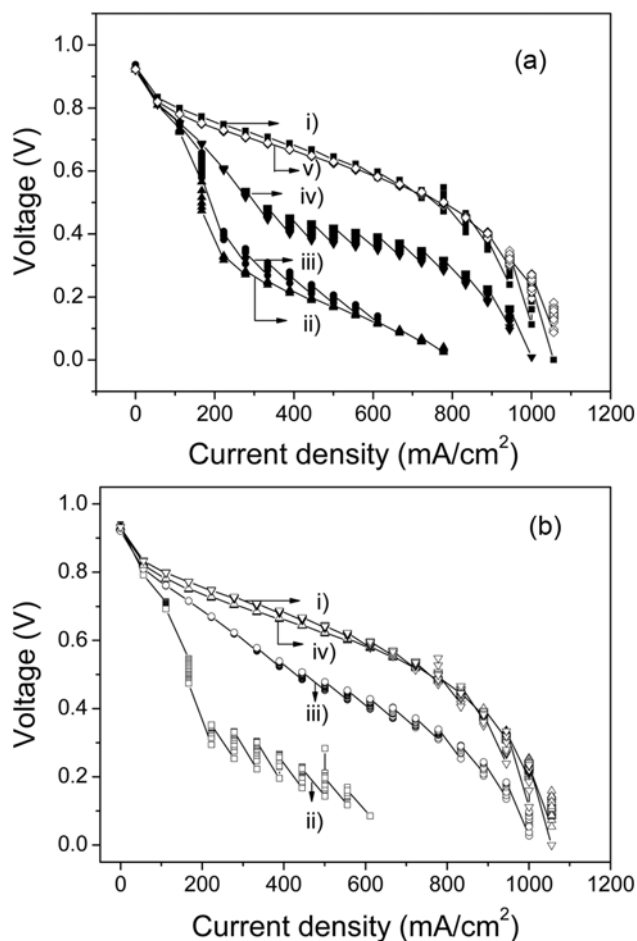


Fig. 3. Polarization curves of Pt/C various H<sub>2</sub>/N<sub>2</sub> ratio with (a) 100 ppm CO concentrations and (b) 10 ppm CO concentrations. (a) 100 ppm CO concentrations; i) H<sub>2</sub>/N<sub>2</sub> without CO concentration ii) H<sub>2</sub>/N<sub>2</sub>=1.0, iii) H<sub>2</sub>/N<sub>2</sub>=0.6, iv) H<sub>2</sub>/N<sub>2</sub>=0.35. (b) 10 ppm CO concentrations; i) H<sub>2</sub>/N<sub>2</sub>=1.0, ii) H<sub>2</sub>/N<sub>2</sub>=0.6, iii) H<sub>2</sub>/N<sub>2</sub>=0.35. The measurement is conducted at 70 °C. Both anode and cathode=100% humidification. Flow rate of H<sub>2</sub>/N<sub>2</sub>=1.2 and air=2.5, respectively (stoich).

have resulted from severe poisoning of Pt surface. The performance of a single cell was significantly decreased when  $H_2/N_2$  ratio was decreased in the presence of CO. As shown in Fig. 3(a), the power performance of the  $H_2/N_2$  ratio (iv) of 0.35 was lower than the  $H_2/N_2$  ratio (iii) of 0.6 at 0.4 V, and we observed similar results in Figs. 3(b)-(ii) and 3(b)-(iii), as also shown in Table 1. It indicates that this performance was more critically affected by CO poisoning itself

**Table 1. Current density of Pt/C with various  $H_2/N_2$  ratio with two concentrations of 10 ppm and 100 ppm CO at 0.4 V, which are reproduced from Fig. 3. The measurement is conducted at 70 °C. Both anode and cathode=100% humidification. Flow rate of  $H_2/N_2=1.2$  and air=2.5 (stoich)**

$H_2/N_2$ ratio	10 ppm CO	100 ppm CO
1.0	800 mA/cm <sup>2</sup>	333 mA/cm <sup>2</sup>
0.6	445 mA/cm <sup>2</sup>	167 mA/cm <sup>2</sup>
0.35	230 mA/cm <sup>2</sup>	160 mA/cm <sup>2</sup>



**Fig. 4. Polarization curves obtained for (a)  $H_2/N_2$  ratio=1.0 and (b)  $H_2/N_2$  ratio=0.35 after 100 ppm CO adsorption. The consecutive stripping tests were performed with different current steps. (a)  $H_2/N_2$  ratio=1.0; i)  $H_2$ , ii) CO 100 ppm, iii) 30 s, iv) 90 s and v) 180 s. (b)  $H_2/N_2$  ratio=0.35; i)  $H_2$ , ii) CO 100 ppm, iii) 90 s, iv) 180 s. The measurement is conducted at 70 °C. Both anode and cathode=100% humidification. Flow rate of  $H_2/N_2=1.2$  and air=2.5, respectively (stoich).**

at high saturated CO. Fig. 3(a)-(ii) shows that even if the ratio of 1.0 is applied, the energy dissipation is already 60% compared to the performance obtained by applying pure hydrogen gas. It indicates that the performance was more affected by blocking Pt active surface area unlike the results shown in Fig. 3(b), which was caused by  $N_2$  hindering effect at low saturated CO. An increase of moles of  $N_2$  plays a role in increasing its partial pressure according to the kinetic theory (1) [19].

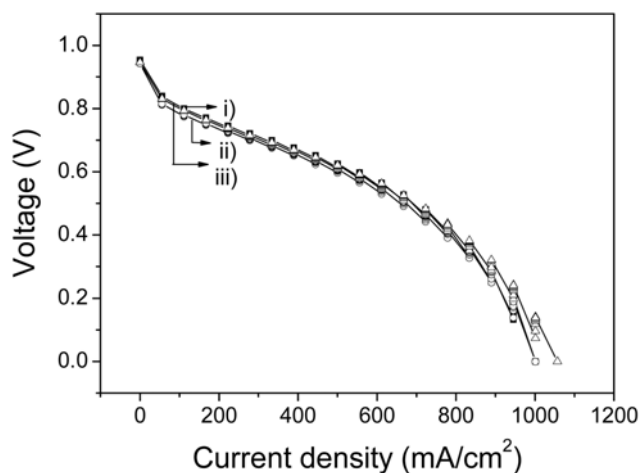
$$P=nMc^2/3V \quad (1)$$

where  $n$  is the mole,  $M$  is the molecular weight,  $c$  is the root mean square velocity and  $V$  is the volume.

The internal total pressure of a  $H_2/N_2$  ratio with 0.35 is relatively higher (Fig. 3(b)-(iii) than others (Fig. 3(b)-(i) and 3(b)-(ii)), which could result in more decreased cell performance. As expected, Fig. 3(b) shows that the current density was decreased with the reduced  $H_2/N_2$  ratio in the operating potential of 0.4V. This means the current density increased with the increase in the  $H_2/N_2$  ratios. In the operating potential of 0.4 V, a 71% and 51% reduction of current density was observed with a gas mixture of  $H_2/N_2$  ratio from 1.0 to 0.35 in the presence of CO concentration of 10 and 100 ppm, respectively.

Another interesting phenomenon, which is practically undesirable, is the saw-tooth shape behavior shown in all of the polarization curves. The oscillation seems to have something to do with inhomogeneous distribution of reactant through the catalyst layer, partially because it appears at lower cell voltage when we applied  $H_2/CO$  mixture or at high current density where we may be able to observe mass transfer limitation of reactant.

To support the evidence of  $N_2$  convection effect with  $H_2/N_2$  ratio, recovery experiments of Pt anode catalyst were performed after polarization measurements by applying 100 ppm of CO. Fig. 4 shows a series of CO recovery polarization curves in fuel cell operation in a way that repeated polarization measurements were carried out at a regular time interval. It was found that CO molecules become more strongly adsorbed on the surface of the catalyst as the  $H_2/N_2$  ratio becomes lower. In other words, the CO hindering effect markedly



**Fig. 5. Polarization curves of PtRu/C anode applying various  $H_2/N_2$  ratio with CO of 10 ppm. i)  $H_2/N_2=1.0$ , ii)  $H_2/N_2=0.6$ , iii)  $H_2/N_2=0.35$ . The measurement is conducted at 70 °C. Both anode and cathode=100% humidification. Flow rate of  $H_2/N_2=1.2$  and air=2.5, respectively (stoich).**

increased the CO poisoning on Pt surfaces as the ratio of  $H_2/N_2$  decreased. After consecutive current-voltage polarization measurements were conducted through a step-wise increment current for 30 s, 90 s and 180 s by applying pure hydrogen, both the  $H_2/N_2$  ratio of 1.0 and  $H_2/N_2$  ratio of 0.35 reach almost the initial value of current density. Interestingly, initial cell performance was lower with  $H_2/N_2$  ratio of 0.35 (see Fig. 4(b)) than that of 1.0 (see Fig. 4(a)), whereas the recovery of low  $H_2/N_2$  ratio shows a higher performance. It might be expected that the slightly larger performance of the  $H_2/N_2$  ratio of 0.35 than that of 1.0 was due to the forced convection effect of  $N_2$  gas.

Based on above experimental observations, it is likely that Pt/C anode is not efficient for CO tolerance, especially with lower hydrogen partial pressure. Fig. 5 shows the current-voltage curves of PtRu/C with different partial pressure of  $H_2$  and  $N_2$  gas. As shown in Fig. 5, the cell performance was not decreased with the 10 ppm CO. The PtRu/C anode had better performance than that of Pt/C catalyst as expected. The better activity would be explained as that CO

is weakly adsorbed on the PtRu/C surface and the  $CO_{ads}$  can be easily removed at lower potential than that of the Pt/C by way of bifunctional mechanism. The Pt-Ru alloy catalyst with a 50% Ru atomic composition has been a well-known electrocatalyst with CO-tolerance [20,21].

We also investigated the effects of  $N_2$  gas with two anode catalysts of Pt/C and PtRu/C via a durability test by measuring the voltage variation as a function of time with respect to the  $H_2/N_2$  ratios from 1.0, 0.6 and 0.35. As shown in Fig. 6, it was observed that the voltage drop increased with a decrease of  $H_2/N_2$  ratio. In addition, the voltage profile was stabilized and slightly dropped for three times longer in the use of PtRu/C anode, especially in 1.0 of  $H_2/N_2$  ratio. The cell voltage drop rates for the Pt/C with a gas mixture of  $H_2/N_2$  ratio from 1.0 to 0.35 showed 0.13 mV/s, 0.27 mV/s and 0.42 mV/s, respectively, while the cell voltage drop rates for the PtRu/C of the same partial pressures were 0.046 mV/s, 0.14 mV/s and 0.12 mV/s, respectively. These results clearly support that PtRu/C and/or Pt-alloy/C anode catalyst in PEFCs are still clearly inevitable in terms of the performance and durability if one insists on using a reformat gas as a fuel.

## CONCLUSIONS

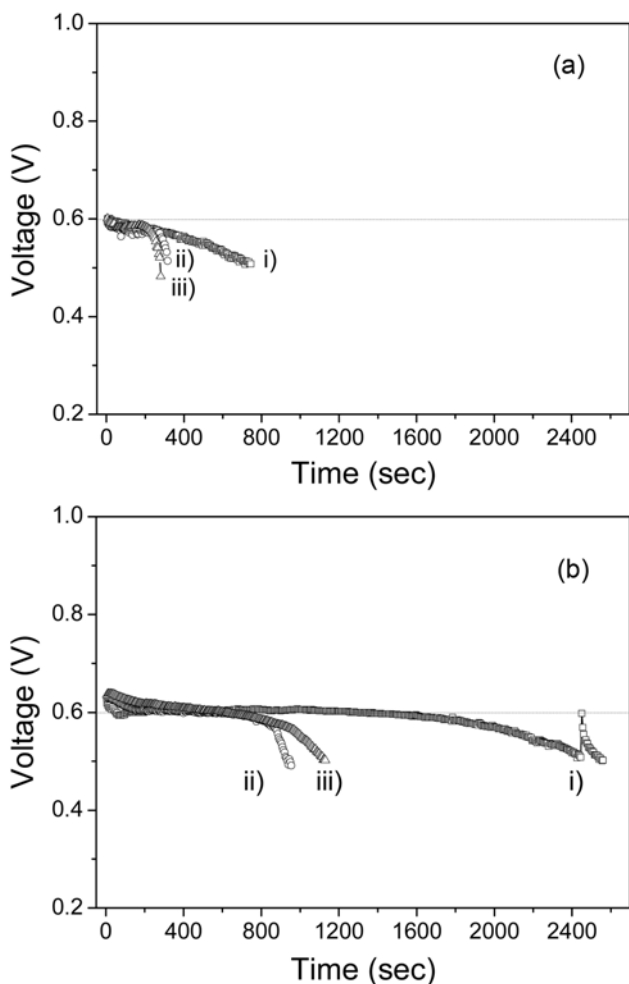
The cell performance was significantly affected by the ratio of the  $H_2/N_2$  in the presence of carbon monoxide (CO). The CO poisoning in addition to the blanket effect of  $N_2$  as a carrier gas impedes the favorable access of hydrogen fuel into the active surface area of the catalyst. In the operating potential of 0.4 V with Pt/C, a 71% and 51% reduction of current density was observed with a gas mixture of  $H_2/N_2$  ratio from 1.0 to 0.35 in the presence of CO concentration of 10 and 100 ppm, respectively. For a more practical application of the reformat system to fuel cell unit, in-depth research regarding the effect of impurity in a fuel should be accompanied with the development of robust anode catalyst possessing high selectivity and tolerance.

## ACKNOWLEDGMENTS

This work was financially supported by the Korea Institute of Machinery and Materials, and by Ministry of Commerce Industry and Energy (10017159-2007-31).

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**Fig. 6.** Durability results in presence of 100 ppm CO applying 555 mA/cm<sup>2</sup>. (a) 55 wt% Pt/C i)  $H_2/N_2$  ratio=1.0 ii)  $H_2/N_2$  ratio=0.6 iii)  $H_2/N_2$  ratio=0.35. (b) 40 wt% PtRu/C i)  $H_2/N_2$  ratio=1.0 ii)  $H_2/N_2$  ratio=0.6 iii)  $H_2/N_2$  ratio=0.35. The measurement is conducted at 70 °C. Both anode and cathode=100% humidification. Flow rate of  $H_2/N_2=1.2$  and air=2.5, respectively (stoich).

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