**ORIGINAL PAPER**



# **Characterization of rheological properties of complex coacervates composed by whey protein isolate, chitosan and garlic essential oil**

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## **Abstract**

This work aims to study the efect of incorporation of garlic essential oil (GEO) with loading of 10% (GEO-10) and 20% (GEO-20) on the strength and stability of polyelectrolyte complex coacervate obtained by electrostatic interactions between chitosan (CH) and whey protein isolate (WPI) with positive and negative charges, respectively. Rheological studies were applied to investigate the viscosity and viscoelastic properties of complex coacervates. The viscoelastic properties were investigated by dynamic oscillatory tests and static tests (creep and recovery). The coacervates exhibited the shear-thinning behavior of non-Newtonian fuid, and the frequency sweep test revealed magnitude of elastic modulus (G′) higher than loss modulus (G″) at high frequency due to the formation of compact network structure with elastic dominant property (solid-like behavior). Arrhenius model was able to estimate the relationship between viscosity and temperature, and the high temperature caused molecular expansion and increase in intermolecular distances, leading to decrease on the viscosity. The energy of activation  $(E_a)$  was 25.24 and 20.74 kJ mol<sup>-1</sup> for WPI/GEO-10/CH and WPI/GEO-20/CH, respectively. The highest  $E_a$  value for WPI/GEO-10/CH indicated the formation of more strength and structured network matrices for GEO protection. Creep and recovery data were well fitted by Burger model and exponential decay function, respectively, and obtaining  $R^2$  higher than 0.98. The percentage recovery (%*R)* was 16.67% and 9.52% for WPI/GEO-10/CH and WPI/GEO-20/CH, respectively, indicating that WPI/GEO-10/CH had greater capacity for structural recovery and the most suitable to be applied in food product that industrially requires large stress, high temperature and long-time processes.

**Keywords** Garlic essential oil · Chitosan · Whey protein isolate · Complex coacervation

# **Introduction**

Garlic is an herbaceous plant that belongs to the genus *Allium* and botanic family of *Liliaceae*; It originated from Central Asia and cultivated in the tropical and subtropical countries worldwide  $[1, 2]$  $[1, 2]$  $[1, 2]$  $[1, 2]$  $[1, 2]$ . One of the most important products derived from garlic is garlic essential oil, and its mainly bioactive compounds are sulfdes derivatives, such as diallyl sulfide, diallyl disulfide, diallyl trisulfide and diallyl tetrasulfde [\[3,](#page-10-2) [4](#page-10-3)]. These compounds have diverse biological activities, including antiviral, antimutagenic, anticarcinogenic, antioxidant, antimicrobial, and efects on cholesterol levels [[5\]](#page-10-4). However, essential oils contain unstable compounds capable of decomposition, volatilization and oxidation when subjected to harsh environmental conditions, namely high temperature, as well as the presence of oxygen and light [[1](#page-10-0), [6](#page-10-5)]. In addition, garlic essential oil have strong favor and organoleptic characteristics that can alter the sensorial characteristic of product, afecting its application in some food products [[1](#page-10-0)]. In this sense, diferent encapsulation methods have been employed in the protection of GEO against adverse environmental conditions. Complex coacervation is one of the encapsulation methods widely used in the protection of volatile compounds. This method consists of hydrogen bonding and electrostatic interactions between two oppositely charged colloidal species, which leads to the formation of two distinct and incompatible phases: a polymer-rich phase (coacervate) in equilibrium with a diluted solvent phase [\[2](#page-10-1), [7\]](#page-10-6). The coacervate obtained from the complex coacervation process contains a high amount of solvent, which needs to be evaporated from the product and turned

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into powder using dehydration methods such as spray drying and freeze drying [[8](#page-10-7)]. However, before drying process, the study of rheological properties is essential to understand the structural characteristics of the coacervate. Rheology is the science that studies the fow and deformation of fuids, and also describes how the materials react to applied stress or strain [\[9](#page-10-8), [10](#page-10-9)]. Rheological analyses provide useful information about molecular interactions between polymers and consequent formation of network structure between them, allowing to assess details about specifc molecular mechanism of encapsulation process that can be used to predict the fnal properties of microparticles [[1,](#page-10-0) [11](#page-10-10)]. The determination of rheological properties of food products can provide useful scientifc knowledge for food researchers during the phase of ingredient selection, proving important information for selecting and optimizing production techniques and implementation of suitable storage strategies [\[12](#page-10-11)]. The rheological measurements include the viscosity and viscoelastic properties of the samples. The viscoelastic fuid can be investigated using dynamic oscillatory tests and static tests (creep or recovery) [\[9](#page-10-8), [10\]](#page-10-9). The ability to understand viscoelastic behavior of food products is crucial in the design and evaluation of its stability [\[13](#page-10-12)].

In the present study, chitosan (CH) and whey protein isolate (WPI) were used as wall materials in the encapsulation of GEO by complex coacervation method resulting from hydrogen bonding and electrostatic interactions between positively charged CH (pKa around 6.3) and WPI with a negative charge (isoelectric point about 5.2) [[14,](#page-10-13) [15](#page-10-14)]. The conjugation between polysaccharide and protein has been demonstrated to be a promising way to enhance the emulsifying properties of polymers [[16](#page-10-15)]. Yang et al. [\[17](#page-10-16)] reported concentration of 10% of GEO (on a total solid basis of wall material) to be optimum for encapsulation efficiency  $(80\%)$ using polyethylene glycol as wall materials. However, different other studies have been reported oil loading of 20% (on a total solid basis of wall material) in the encapsulation of essential oils [\[18](#page-10-17)[–21\]](#page-10-18). Tavares et al. [[2\]](#page-10-1), microencapsulated GEO with concentration of 10% (w/w) using two types of wall materials, namely soy protein isolate/chitosan and β-cyclodextrin, obtaining entrapment yield varying from 71.74 to 82.03%. However, studies about incorporation of GEO-10 (10%) and GEO-20 (20%) into the matrices of biopolymers and determination of rheological properties of coacervate composed by WPI/GEO/CH have not yet been carried out. Furthermore, the importance of this research is centered on evaluating the efect of incorporation of two diferent concentrations of GEO (10 and 20% on a total solid basis) on the network structure of WPI/CH coacervate by examining the rheological properties of the produced coacervates. Therefore, the objective of this study was to study the efect of (GEO) incorporation on the strength, stability and structure of polyelectrolyte complex coacervate phases ((WPI/GEO-10/CH and WPI/GEO-20/CH) according to rheological measurements of steady shear (viscosity), dynamic oscillatory (stress, frequency, temperature and time sweeps) and static (creep and recovery).

# **Materials and methods**

Garlic essential oil (GEO), containing mainly 14.6% of allyl methyl sulfde, 26.3% of diallyl disulfde, 25.2% diallyl trisulfde, 5.5% of allyl methyl trisulfde, 12.9% of diallyl tetrasulfde, was acquired from Lazlo (Belo Horizonte, Brazil). Whey protein isolate and chitosan (CH) with deacetylation degree (DD) of 96% were generously provided by Arla Foods Ingredients (São Paulo, Brazil) and Primex (Siglufordur, Iceland), respectively. Sodium acetate trihydrate and glacial acetic acid were purchased from CAQ – Casa da Química, and the hydrochloric acid (HCl) and sodium hydroxide (NaOH), both with analytical grade, were obtained from Sigma-Aldrich.

# **Encapsulation of garlic essential oil by complex coacervation**

The dispersions of WPI and CH were prepared at 3% (w/w) in acetate buffer (100 mM) at pH 6 and pH 5.5, respectively, according to zeta potential analyses reported by Tavares and Noreña [[22](#page-10-19)]. A magnetic stirrer was used to agitate both dispersions for 4 h and then allowed to rest for 24 h at  $-4^{\circ}$ C to ensure complete hydration. After that, GEO at concentration of 10% (GEO-10) and 20% (GEO-20) were slowly mixed with dispersion of WPI and then homogenized for 5 min at 6000 rpm in a high-speed homogenizer (Ultra-Turrax IKA, T18). Then, the dispersion of CH 3% (w/w) was gradually transferred to a fask with WPI/GEO-10 or WPI/ GEO-10, resulting in dispersions of WPI/GEO-10/CH and WPI/GEO-20/CH, respectively. The dispersions were stirred with a magnetic stirrer (Fisaton, Model 752A) for 30 min. The result was the formation of two phases: a supernatantrich phase (solvent) and a precipitated biopolymer-rich phase denominated by coacervate. The supernatants were discarded and each of precipitated coacervate was recovered for rheological characterization.

#### **Rheological measurements**

The rheological properties of WPI/GEO-10/CH and WPI/ GEO-20/CH coacervates were carried out using straincontrolled rheometer (Thermo Scientifc, HAAKE MARS 40/60, Karlsruhe, Germany) ftted with parallel plate geometries (35 mm in diameter) and gap of 1 mm. The viscosity and viscoelastic properties of the coacervate were determined according to the following studies.

## **Viscosity**

The apparent viscosity was measured at  $25^{\circ}$ C as a function of shear rate ( $\dot{y}$ ) that ranged from 0.1 to 100 s<sup>-1</sup>. The efect of temperature on the apparent viscosity of the coacervates was evaluated using the Arrhenius model (Eq. [1\)](#page-2-0) [[23\]](#page-10-20), at a constant shear rate of 0.1 s<sup>-1</sup> and varying temperature from 20 to 80 °C.

$$
\eta_a = A \, \exp\left(\frac{E_a}{RT}\right) \tag{1}
$$

where  $\eta_a$  is the apparent viscosity (Pa s), *A* is a constant, *T* is the absolute temperature and  $R$  is the universal gas constant (8.3144621 J K<sup>-1</sup> mol<sup>-1</sup>),  $E_a$  is the energy of activation for flow curve  $(KJ \text{ mol}^{-1})$ . In order to estimate the parameters,  $E_a$  and A for each coacervate at a specific temperature, Eq. [\(1](#page-2-0)) was transformed to (Eq. [2](#page-2-1)), and the values of  $E_a$  and *A* were determined as the slope and intercept, respectively, of a straight line of ln of  $\eta_a$  versus the reciprocal of absolute temperature (1/T):

$$
\operatorname{Ln} \eta_a = \operatorname{Ln} A + \frac{E_a}{RT} \tag{2}
$$

#### **Viscoelastic properties**

The viscoelastic properties of the coacervates were determined using the following two methods: dynamic oscillatory and static (creep or relaxation) tests.

**Dynamic oscillatory test** The dynamic oscillatory tests were investigated according with two procedures: large amplitude oscillatory shear tests (LAOS) and small amplitude oscillatory shear tests (SAOS). For LAOS tests, the stress sweep was evaluated to make certain that the amplitude oscillatory shear (SAOS) tests were made within the linear viscoelastic region (LVR). Stress sweep tests were investigated from 0.1 to 150 Pa at a fixed frequency of 1 Hz and 20 °C. Thereafter, a constant stress of 1 Pa (within the LVR) was selected for the following SAOS tests: (a) frequency sweep tests were performed from 0.01 to 100 Hz at 20  $^{\circ}$ C; (b) temperature sweep tests the samples were heated from 20 to 90 °C at a fxed frequency of 1 Hz; and (c) time sweep tests were performed during 1 h at fxed temperature of 20 °C and frequency of 1 Hz. The generated values of storage or elastic modulus (G′) and loss or viscous modulus (G″) were plotted as a function of stress, frequency, temperature, or time on a logarithmic scale. For the frequency sweep tests, the parameters of complex modulus  $(G^*)$  and complex viscosity  $(\eta^*)$  were evaluated according to Eqs. [3](#page-2-2) and [4,](#page-2-3) respectively:

<span id="page-2-2"></span>
$$
|G^*| = \sqrt{(G')^2 + (G'')^2}
$$
 (3)

<span id="page-2-3"></span>
$$
\eta^* = \frac{G^*}{\omega} \tag{4}
$$

The Carreau–Yasuda model (Eq. [5\)](#page-2-4) was used to study the dependency of complex viscosity on angular frequency (ω in rad/s) [\[24](#page-10-21)].

<span id="page-2-4"></span><span id="page-2-0"></span>
$$
\eta^*(\omega) = \eta_0^* \left[ 1 + \left( \frac{\eta_0^*}{\tau^*} \times \omega \right)^a \right]^\frac{n-1}{a} \tag{5}
$$

where  $\eta_0^*$  is zero complex viscosity, *n* is the power-law index, *a* indicates the width of the transition region between Newtonian and non-Newtonian behavior and *τ\** is the shear stress at the transition between Newtonian and non-Newtonian region, and the relaxation time (*λ*) was calculated according to Eq. [6](#page-2-5) [\[25\]](#page-10-22).

<span id="page-2-5"></span>
$$
\lambda = \frac{\eta_0^*}{\tau^*} \tag{6}
$$

<span id="page-2-1"></span>**Creep recovery tests** In creep experiments, a small constant stress (1 Pa and within LVR) was applied over medium to long time periods, obtaining elastic or viscous deformation [ $26$ ]. The results are expressed in terms of compliance  $J(t)$ against time, that expresses the relation between the generated deformation and applied stress [\[13](#page-10-12)].

The results are expressed in terms of compliance function against time are expressed according to Eq. [7](#page-2-6) [[15\]](#page-10-14):

<span id="page-2-6"></span>
$$
J_t = \frac{\gamma(t)}{\tau_0} \tag{7}
$$

where  $\tau_0$  is the constant stress applied (Pa) and  $\gamma_{(t)}$  is the resulting dependent strain time during the test. Creep compliance was defined as  $J_c$  over the creep time (from 0 to 180 s) by applying a constant stress  $(\tau_0)$  of 1 Pa (within the LVR), and the recovery compliance was defined as  $J_R$  for the recovery time (from 180 to 360 s) after removal of stress (constant stress equal to 0). The Burger model was used to describe the creep  $(J_C)$  compliance (Eq. [8](#page-2-7)) (representing the Maxwell and Kelvin–Voigt models placed in series), and recovery  $(J_R)$  compliance was described by an exponential decay function (Eq. [9\)](#page-3-0) [[27,](#page-10-24) [28\]](#page-10-25).

<span id="page-2-7"></span>
$$
J_c = \frac{1}{G_0} + \frac{1}{G_1} \times \left[1 - \exp\left(\frac{-tG_1}{\eta_1}\right) + \frac{t}{\eta_0}\right]
$$
(8)

where  $G_0$  and  $\eta_0$  represent the mechanical Maxwell model of instantaneous shear modulus and residual viscosity (dashpot contribution), respectively, and  $G_1$  and  $\eta_1$  represent the mechanical Kelvin–Voigt model of shear modulus

(representing the retarded elastic region) and internal viscosity (dashpot contribution), respectively.

$$
J_R = J_{\infty} + J_{1R} \exp\left(-Bt^C\right) \tag{9}
$$

where  $J_{\infty}$  and  $J_{1R}$  represent the recovery compliance of the Maxwell dashpot and Kelvin–Voigt element, respectively, and B and C are parameters that defne the recovery speed of the system.

The samples' capacity to recover was calculated according to Eq. [10:](#page-3-1)

$$
\%R = \frac{J_{\text{max}} - J_{\infty}}{J_{\text{max}}}
$$
\n(10)

where %R is the total percentage recovery, and  $J_{max}$  and  $J_{\infty}$ represent the maximum compliance verifed and the recovery compliance of the Maxwell dashpot, respectively.

#### **Statistical analysis**

Statistical analysis was performed using SAS software (v. 9.3). Generated data were exposed to Analysis of Variance (ANOVA), and mean comparison of diferent treatments was evaluated using Tukey's test ( $p < 0.05$ ). The Burger model parameters and the parameters of exponential decay function were evaluated according to the Levenberg–Marquardt algorithm in the MATLAB® curve-ftting toolbox.

# **Results and discussion**

#### **Viscosity**

Viscosity of the fuid can be described as a system's resistance provided by the adjacent layers to one another during the fow of the fuid [[29\]](#page-10-26). The viscosity of the WPI/GEO-10/ CH and WPI/GEO-20/CH coacervates are shown in Fig. [1.](#page-3-2) The coacervates exhibited typical pseudoplastic fuid with shear-thinning behavior of non-Newtonian behavior, where the apparent viscosity decreases with increased shear rate [[9,](#page-10-8) [10](#page-10-9)]. Shear thinning occurs primarily as a result of network strength caused by underlying electrostatic forces between biopolymers, leading to a structural change in the coacervates [[30](#page-10-27)]. According to the results, two distinct regions can be identified: (a) from 0.1 to 40  $s^{-1}$  where the apparent viscosity  $(\eta)$  decrease as the shear rate increased, and  $(b)$ from 40 to 100 s<sup> $-1$ </sup> identified as Newtonian region where the apparent viscosity was constant with changing shear rates. From the shear rate higher than  $40 s^{-1}$ , the disruption of entanglements polymers chain results in rearrangement in the conformation of the polysaccharides molecules and entanglement density; therefore, a horizontal Newtonian plateau is obtained without reduction in the viscosity since

<span id="page-3-0"></span>

<span id="page-3-2"></span><span id="page-3-1"></span>**Fig. 1** Apparent viscosity as a function of shear rate between 0.1 to 100 s −1 for WPI/GEO-10/CH (flled square) and WPI/GEO-20/CH (flled circle) coacervates

all the chains are disentangled  $[31-33]$  $[31-33]$  $[31-33]$ . According to You et al. [[34\]](#page-10-30), the network structure of coacervate at greater shear rates is not stable, resulting in the breaking of physical bonds and structure disintegration. This phenomenon is associated with polymeric polysaccharide solutions with a high macromolecular weight [\[35\]](#page-10-31). The highest GEO concentration interfered in the chain entanglement and the network structure of the coacervate by reducing the resistance of the polymer chains mobility. According to Bordón et al. [[36\]](#page-10-32), presence of oil droplets disturbs the flow of the fluid, increasing the energy dissipation. It's possible to conclude that the disentanglement of coacervate macromolecular chains was less accentuated for WPI/GEO-10/CH, obtaining a fow curve behavior with higher viscosity at higher shear rate.

#### **Efect of temperature on apparent viscosity**

The effect of temperature on the apparent viscosity of the coacervates was examined from the temperature of 20 to 90 °C at a fixed shear rate  $(\dot{\gamma})$  of 0.1 s<sup>-1</sup>, corresponding to the  $\dot{\gamma}$  value where the network structure of the coacervate is less afected by the applied stress (high viscosity) (Fig. [2\)](#page-4-0).

The viscosity of both coacervates decreased with increased temperature until 70 °C, and then is verified an increase in the viscosity until the end of the test. The decrease in viscosity can be attributed to the disruption of the chain entanglement and increases in the intermolecular spaces caused the thermal expansion, leading to the reduction of intermolecular forces and consequently decrease in the viscosity of the sample [[31,](#page-10-28) [37,](#page-10-33) [38\]](#page-11-0).



<span id="page-4-0"></span>**Fig. 2** Apparent viscosity versus temperature from 20 to 80 °C for WPI/GEO-10/CH (flled square) and WPI/GEO-20/CH (flled circle) coacervates

According to Zhang et al. [\[39](#page-11-1)], higher temperatures cause molecular expansion and an increase in intermolecular distances, leading to decrease on the apparent viscosity. The results suggesting that WPI/GEO-20/CH coacervate has more fexible molecular conformation as compared with the WPI/GEO-10/CH, and the temperature rise caused higher disruption of its chain entanglement and network structure.

The emulsifcation process had an important role during the encapsulation process by complex coacervation method, since it is used as starting point of this method. Therefore, since the emulsion formation involves shearing, it is necessary to comprehend concepts such as activation energy, which is defned as barrier, induced by the resistance of the surrounding building units, to overcome to allow molecules to move during the viscosity measurements [[31\]](#page-10-28). The effect of temperature (30–60  $^{\circ}$ C) on the apparent viscosity of the coacervates at a fixed shear rate  $(0.1 \text{ s}^{-1})$  is shown in Fig. [3,](#page-4-1) using the Arrhenius model (Eq. [1\)](#page-2-0) to estimate the relationship of apparent viscosity and temperature.

The temperature ranges of 30 to 60 °C corresponds to the region where the Arrhenius model was able to estimate the relationship of viscosity and temperature, obtaining values of *R*<sup>2</sup> of 0.9874 and 0.9911 for WPI/GEO-10/CH and WPI/ GEO-20/CH, respectively (Fig. [3](#page-4-1)). From the adjusted data, the regression analysis of ln  $\eta_a$  versus 1/T (Fig. [3](#page-4-1)) allowed to estimate the magnitudes of  $E_a$  from the slope of linear regression analysis multiplied by the universal gas constant  $(8.3144621 \text{ J K}^{-1} \text{ mol}^{-1})$  (Eq. [2\)](#page-2-1).

The values of  $E_a$  were 25.24 and 20.74 kJ mol<sup>-1</sup>, whereas the values of constant *A* were 0.01 and 0.05 for WPI/GEO-10/CH and WPI/GEO-20/CH, respectively. The WPI/GEO-10/CH coacervate showed higher value of  $E_a$  than WPI/



<span id="page-4-1"></span>**Fig. 3** Arrhenius plots of apparent viscosity  $(\eta_a)$  versus the inverse of absolute temperature (T) for WPI/GEO-10/CH (flled square) and WPI/GEO-20/CH (flled circle) coacervates

GEO-20/CH, indicating that the viscosity of WPI/GEO-10/ CH coacervate was more sensitive to temperature change. The high value of  $E_a$  also indicate formation of a dense and structured matrix around the active compounds capable to protect them against thermal stress [\[31](#page-10-28), [40\]](#page-11-2). Chaharlang and Samavati [[41](#page-11-3)] reported that the high value of  $E_a$  is related to the decrease in the chain fexibility during the fow process. Therefore, the GEO compounds present in the WPI/ GEO-10/CH coacervate are more protected against thermal stress than GEO compounds of WPI/GEO-20/CH coacervate. This result also suggest that molecular chain entanglement was stronger than disentanglement, resulting in more energy in molecular motion [\[39](#page-11-1)]. This result indicates that WPI/GEO-10/CH complex is more suitable to be applied in food products that require high-temperature heating, and also products susceptible to high temperature changes during the processing, handling and storage.

## **Dynamic oscillatory test**

#### **Stress sweep**

The dependence of storage modulus (G′) and loss modulus (G″) on the stress for are represented in Fig. [4.](#page-5-0) The storage modulus G′ represents the magnitude of the energy that is stored in the material or recoverable per cycle of deformation, whereas G″ is a measure of the energy which is lost as viscous dissipation per cycle of deformation, and the magnitudes of both parameters are infuenced by stress, frequency, temperature, and time [[9\]](#page-10-8). Stress sweeps are used to estimate the linear viscoelasticity region (LVR) in which a system may withstand maximal deformation



<span id="page-5-0"></span>**Fig. 4** Stress sweep test for WPI/GEO-10/CH (square) and WPI/ GEO-20/CH (circle) coacervates. Filled and empty symbols represent storage modulus (G′) and loss modulus (G″), respectively

(critical strain) without causing permanent structural damage [[2](#page-10-1)]. According to Fig. [4](#page-5-0), with increasing stress, two diferent regions were obtained: an LVR where G′ and G″ were almost constant, and non-linear viscoelastic region (non-LVR) in which G′ and G″ started to decrease until the end of the test. The WPI/GEO-10/CH coacervate showed higher values of G' and G" than WPI/GEO-20/CH coacervates, indicating that the increase in the concentration of GEO from 10 to 20% resulted in a decrease in the magnitudes of both G′ and G″ moduli. This result indicates that the incorporation of GEO into the network matrices of the coacervate promote alteration in their structural strength, leading to the formation of coacervate with less compact and rigidity structure. Similar results were reported by Tavares and Noreña [[15\]](#page-10-14) in the encapsulation of ginger essential oil by complex coacervation using WPI/gum Arabic (GA) and CH/GA as complex wall materials.

The results of stress sweep test, corresponding to the LAOS experiment, indicated that the increase of stress causes damage on the network structure of both complexes. This fnding can be useful to predict the coacervate behavior during handing, processing and storage conditions, and can be used to understand how complex materials behave under high conditions of stress, which is fundamental for optimization and design purposes since a wide variety of industrial processes involve large stress. This fnding can be useful to predict the coacervate behavior during handing, processing and storage conditions, and can be used to understand how complex materials behave under high conditions of stress, which is fundamental for



<span id="page-5-1"></span>**Fig. 5** Frequency sweep test for WPI/GEO-10/CH (square) and WPI/ GEO-20/CH (circle) coacervates determined at constant temperature of 20 °C and fxed stress of 1 Pa. Filled and empty symbols represent storage modulus (G′) and loss modulus (G″), respectively

optimization and design purposes since a wide variety of industrial processes involve large stress [\[2\]](#page-10-1).

Therefore, the stress of 1 Pa, within the linear viscoelastic region, was used in the SAOS tests (frequency, temperature and time sweeps), avoiding any modifcation of the molecular structure caused by stress, since in this region the network structure of coacervate was not damaged by the stress imposed during the stress sweep measurements**.**

#### **Frequency sweep test**

The frequency sweep measurements were employed to study the effect of GEO concentration on the network structure of coacervates (Fig. [5\)](#page-5-1).

The magnitude of G′ and G″ increased with increased values of frequency for both coacervates. The coacervates showed magnitudes of G″ higher than the G′ at frequency below 10 Hz, and then occur the crossover point  $(G''=G')$ and the magnitudes of G′ became higher than G″.

According to Zhang et al. [[39](#page-11-1)], at low frequencies, the molecular chains had enough time to disentangle and reorder, whereas at high frequencies the molecular chains had less time to disentangle, and the entanglement points contributed to a temporary cross-linking junction zone.

This result indicates greater frmness of the coacervates and formation of a compact network and stronger network structure. According to Yang et al. [[42\]](#page-11-4), material with compact structure has more elastic behavior since the movement of the molecular chains are more difficult. At low frequency, the coacervate behaved similarly to a weak gel with liquidlike behavior  $(G'' > G')$ , while at higher frequencies (2.5 Hz)

the coacervate behaved similarly to a strong gel with solidlike behavior ( $G'' < G'$ ). According to Steffe [\[10](#page-10-9)], the crossover lines between G′ and G″ at centered frequency range indicates concentrated solutions with solid-like behavior at higher frequencies. In this sense, it is possible to conclude that the high values of frequency coacervate induced the formation of stronger network structure with solid-like behavior. Samples with magnitude of G′ higher than G″ indicate the formation of stronger network structure  $[43]$  $[43]$ . Yuan et al. [\[44](#page-11-6)] investigated the rheological behavior of complex coacervate composed by soy protein isolate/algal oil/chitosan, and they reported the formation of highly linked network structures with values of G′ higher than G″.

The WPI/GEO-10/CH and WPI/GEO-20/CH coacervates revealed similar viscoelasticity properties, and the efect of incorporation of 10 and 20% of GEO on the biopolymers matrices is not clear using the frequency sweep test. Therefore, the analyses of the parameter's complex modulus  $(G^*)$ and complex viscosity were evaluated to investigate possible diferences between the structure of the WPI/GEO-10/CH and WPI/GEO-10/CH coacervates (Fig. [6](#page-6-0)).

The complex viscosity (η\*) decreased linearly with increase in frequency, indicating that the coacervates had



<span id="page-6-0"></span>**Fig. 6** Complex viscosity (η\*) (flled) and complex modulus (G\*) (empty) as a function of frequency (Hz) for WPI/GEO-10/CH (square) and WPI/GEO-20/CH (circle) coacervates

non-Newtonian behavior of shear-thinning fuid. The high frequency causes permanent molecular misalignment or disentanglement of long chain polymers, and a decrease in complex viscosity [[45](#page-11-7)]. The shear-thinning behavior for higher frequency is in accordance with the results of apparent viscosity reported in Fig. [1](#page-3-2). The magnitudes of G\* increased with frequency, indicating that the high frequency induced the formation of a compact, strong and stable network structure, preventing the molecular chains movement in both coacervates. The strengthening of the gel-network is mainly due to the enhancement of attractive forces of van der Waals interactions and hydrogen bonding between hydrocolloid particles, resulting in the formation of gel structure with higher degree of cross-linking and/or entanglement [[46\]](#page-11-8). According to Zare et al. [[47\]](#page-11-9), at low frequencies, the polymer chains have enough time for relaxation, obtaining lower values of  $G^*$ , and at high frequencies (short-range deformation) the polymer chains cannot relax and hardly deform increase the values of G\*. The WPI/GEO-10/CH and WPI/GEO-20/CH coacervates showed curves with similar behavior, which are in concordance with the results of frequency sweep test represented in Fig. [5.](#page-5-1) In this sense, the Carreau–Yasuda model was used to ft the experimental complex viscosity data in order to verify possible diferences between the structure of the WPI/GEO-10/CH and WPI/GEO-10/CH coacervates. This model can be applied to complex viscosity data to study the shear thinning behavior and the Newtonian and non-Newtonian regions of the samples. The values of Carreau–Yasuda model parameters are presented in Table [1.](#page-6-1)

The Carreau-Yasuda model was suitable to ft the experimental complex viscosity data, obtaining values of  $R^2$ higher than 0.99 for both coacervates. The WPI/GEO-10/ CH showed higher values of  $\eta_0^*$  and  $\tau^*$  than WPI/GEO-20/ CH coacervate, confrming its stronger and compact network structure. The high values of relaxation time  $(\lambda)$  obtained for WPI/GEO-10/CH indicate stronger interfacial interaction between polymer chains, and also lower mobility of polymer chain [[25](#page-10-22)]. Moreover, WPI/GEO-20/CH showed lower values of parameters *n*, indicating more shear thinning behavior. The parameter *a*, which represents the width of the transition region between Newtonian and non-Newtonian

<span id="page-6-1"></span>**Table 1** The estimated values of Carreau–Yasuda model parameters for the WPI/GEO-10/CH and WPI/GEO-20/CH coacervates



\*\*Different letters (a and b) in the same column indicate values that are significantly different ( $p < 0.05$ ) based on Tukey's multiple comparison test.  $\eta_0^*$  is the zero complex viscosity; *n* is the power-law index; *a* indicates the width of the transition region between Newtonian and non-Newtonian behavior; *τ\** is the shear stress at the transition between Newtonian and non-Newtonian region; *λ* is the relaxation time

regions, was higher for WPI/GEO-20/CH due to its weaker network structure and high width of the transition between the Newtonian to non-Newtonian regions.

#### **Temperature sweep test**

The temperature sweep curves with variation G′ and G″ moduli upon heating from 20 to 90 °C at a fxed frequency (1 Hz) and stress (1 Pa) are shown in Fig. [7](#page-7-0).

The coacervate showed a storage modulus (G′) higher than the loss modulus  $(G'')$ , in the entire range of investigated temperatures. There was no crossover point for G′ and G″, which indicates that the coacervate structure was predominantly elastic and remains in the solid-like behavior during the whole range of investigated temperatures. The values of G″ and G′ decrease with increased temperature until 70 °C and 75 °C for WPI/GEO-10/CH and WPI/ GEO-20/CH, respectively, and then was verifed abruptly increased of both moduli for both coacervates. The initial decrease in G′ and G″ can be related to the increase in fuidity with increasing temperature, which can be attributed to the energy dissipation movement of the molecules and decrease in intermolecular interactions [\[48\]](#page-11-10). The initial decrease in G′ and G″ can be related to the increase in fuidity with increasing temperature, which can be attributed to the energy dissipation movement of the molecules and decrease in intermolecular interactions [\[48](#page-11-10)].

The temperature in the region between 70 and 75 °C indicate the point where the whey proteins present in coacervate start to denature and the elastic modulus starts to invert the decreasing trend, and the elastic module fts the standard



<span id="page-7-0"></span>**Fig. 7** Temperature sweep test for WPI/GEO-10/CH (flled square) and WPI/GEO-20/CH (flled circle) coacervates determined at constant frequency of 1 Hz and fxed stress of 1 Pa. Filled and empty symbols represent storage modulus (G') and loss modulus (G''), respectively

heat-set whey protein gelation behavior [[49](#page-11-11)]. Similar result was reported by Yang et al. [[42\]](#page-11-4), indicating that the changes in G′ and G″ with temperature result from protein unfolding due to the denaturation of the protein myosin present in surimi. For the temperature above 70 °C and 75 °C for WPI/GEO-10/CH and WPI/GEO-20/CH, respectively, the results suggest reorganization of the network structure of the coacervate, causing the strengthening of the structures mainly due to formation of three-dimensional network structure with a strong gel-like behavior. The G′ was always greater than G″ throughout the temperature range covered. This result indicates the formation of a strong gel-like network structures with increased temperature [\[43\]](#page-11-5). In addition, the coacervates can show a solid-like behavior even at high temperatures and their structures get stronger for the temperature above 65 and 80 °C for WPI/GEO-10/CH and WPI/GEO-20/CH, respectively. The magnitudes of G′ and G″ were higher for WPI/GEO-10/CH than WPI/GEO-20/CH complex at two temperature range: 20 to 40 °C, and 70 to 90 °C and WPI/GEO-20/CH. This result confrms a stronger network structure for WPI/GEO-10/CH coacervate, which was less afected by increasing temperature. Samples with strong network structure and improved mechanical strength, hardness, gumminess, and stifness are desirable in the context of industrial application [[43](#page-11-5)].

#### **Time sweep test**

Oscillatory time sweeps are important in the rheological measurements of dispersions, and polymers that may undergo macro-or micro-structural rearrangement with time [[50\]](#page-11-12). This concept is applied for the complex coacervation method, where is required time to rearrangement and formation of the entanglement network structure. The temperature sweep curves with changes in G' and G" as a function of time for 1 h at fxed frequency of 1 Hz and temperature of 20 °C for WPI/GEO-10/CH and WPI/GEO-20/CH coacervates are illustrated in Fig. [8.](#page-8-0)

For both coacervates, the values of G′ were higher than G′ for the entire aging time, indicating that elastic component predominated over the viscous component G″. The G′ and G″ values were not remarkably changed during 30 min. After that, the magnitudes of G′ and G″ increased sharply, representing a reinforcement of the polymer networks structure of the complex of WPI/CH coacervate. The values of G′ were higher than G″, indicating that the elastic behavior of the structure of coacervate predominated over its viscous behavior during over tested time. The G′ and G″ values for WPI/GEO-10/CH was higher than obtained for WPI/GEO-20/CH throughout the entire tested time. This result indicates that WPI/GEO-20/CH exhibited weaker elastic character as compared with WPI/GEO-10/CH coacervate, and the incorporation of high concentration of GEO in the polymeric





<span id="page-8-0"></span>**Fig. 8** Time sweep test for WPI/GEO-10/CH (square) and WPI/GEO-20/CH (circle) coacervates determined at constant frequency of 1 Hz, fxed stress of 1 Pa and temperature of 20 °C. Filled and empty symbols represent storage modulus (G′) and loss modulus (G″), respectively

matrices of the wall materials resulted in the formation of lesser compact network structure. Coacervate with strong, compact and stable network structure are desirable during the production of microparticles, since strong, stable and compact network structure of colloidal material sufer less changes when subjected to high shear stress during industrial application [[2\]](#page-10-1).

The viscoelastic properties of the WPI/GEO-10/CH and WPI/GEO-20/CH coacervates determined by the SAOS test suggest that the presence of high concentration of GEO decreases the rigidity and entanglement of the network structure of the coacervates. The internal network structure of both coacervates is greatly afected by the high values of temperature, frequency and time employed at end of the tests, causing some structural alteration and molecular rearrangement (Figs.  $2, 5, 7$  $2, 5, 7$  $2, 5, 7$  $2, 5, 7$  and [8](#page-8-0)).

## **Creep and recovery**

Creep and recovery tests were performed to determine the values of compliance  $(J(t))$ , which represent the deformation of samples caused by the application of shear stress [\[13\]](#page-10-12). The creep and recovery tests have been employed to study the internal structure of a material, and its structural changes associated with the introduction of some alteration on the initial composition [[51](#page-11-13)]. In the creep-recovery test, samples with stronger, compact and stable structures have lower  $J_t$  values, while samples with weaker network structure have higher  $J_t$  values [[52\]](#page-11-14). Creep-recovery tests were performed to determine the infuence of GEO incorporation on the matrices of biopolymers and the results of  $J_t$  for the



<span id="page-8-1"></span>**Fig. 9** Compliance  $(J_t)$  versus time in creep phase (from 0 to 180 s) and recovery phase (from 180 to 360 s) for WPI/GEO-10/CH (black) and WPI/GEO-20/CH (red) coacervates

complex coacervates with and without GEO the creep and recovery phases are showing in Fig. [9](#page-8-1).

For the creep phase, constant stress of 1 Pa was applied to samples for 180 s, and the increase of creep compliance  $(J_c)$ corresponds to the deformation of the coacervate structure caused by the applied stress within the LVR. The WPI/GEO-10/CH showed lower magnitudes of  $J_c$ , indicating the formation of a stronger structure. The higher values of  $J_c$  obtained for WPI/GEO-20/CH indicates coacervate with weaker network structure. These results confrmed that the incorporation of GEO on the matrices of biopolymers caused a reduction on the rigidity of coacervate, leading to the formation of a less compact structure, confrming the results obtained for viscosity (Fig. [1](#page-3-2)) and temperature and time sweep tests represented in the Figs. [7](#page-7-0) and [8,](#page-8-0) respectively. The formation of a stronger network structure results in lower creep compliance values [[15\]](#page-10-14). Tavares and Noreña [[22](#page-10-19)] reported similar results for the encapsulation of ginger essential oil by complex coacervation using complex of whey protein isolate/gum Arabic and gum Arabic/chitosan as wall materials, suggesting alterations in the structural characteristic of the coacervates.

Burger model was applied in order to study the creep phase behavior, and this model result by the association of the Maxwell and Kelvin–Voigt models in series, and the determination of its four parameters  $(G_0, G_1, \eta_0)$  and  $\eta_1$ ) allow to compare the internal structure of diferent systems [\[51](#page-11-13)]. The Burger model parameters are presented in Table [2](#page-9-0).

In both cases, the coefficients of determination  $(R^2)$ were higher than 0.98, indicating that the creep phase was well fitted by the Burger model. The  $G_0$  provides results of magnitude intensity of the elastic strength on the molecular

<span id="page-9-0"></span>**Table 2** The ftting parameters of Burger model for WPI/GEO-10/CH and WPI/GEO-20/CH coacervates



\*\*Different letters in the same column indicate values that are significantly different ( $p < 0.05$ ) based on Tukey's multiple comparison test.  $G_0$  is the instantaneous shear modulus of the Maxwell unit;  $G_1$  is the shear modulus of Kelvin–Voigt;  $\eta_0$  is the residual viscosity (dashpot contribution) of the Maxwell element;  $\eta_1$  is the internal viscosity (dashpot contribution) of Kelvin–Voigt unit

bonds present in the interfacial network structure [\[52\]](#page-11-14). In this sense, the highest value of  $G_0$  obtaining for WPI/CH refect its greater elasticity with a stronger and compact network structure formed by entanglement of the biopolymer's chains. In contrast, the WPI/GEO-20/CH coacervate with high GEO concentration showed the lowest  $G_0$ , which was mainly due to its characteristic of the weaker gel with less compact network structure. The parameter  $G_1$  reflects the magnitude of the retarded elastic deformation and the resistance to deformation caused by the three-dimensional network structure [[53\]](#page-11-15). The highest  $G_1$  value indicated the formation of a more complex network structure rich in zone junctions, whereas the lowest  $G_1$  value indicated the formation of a simpler network structure with lower junction's zones [\[53](#page-11-15), [54\]](#page-11-16). The highest  $G_1$  value obtaining WPI/GEO-20/CH confrms that the GEO interfered in the structure of WPI/CH complex. The viscosity parameters  $\eta_0$  (associated with the Maxwell dashpot) and  $\eta_1$  (associated with Kelvin–Voigt dashpot) also decreased when the amount of GEO incorporated in the network structure of WPI/CH increases, causing the gel fow more easily due to the decrease of the resistance to the fow.

In any food system, the decrease in values of Burger model parameters is mainly due to its weakened network structure, which allows for decreases in shear moduli and viscosity [[27](#page-10-24)]. Samples with a compact, stale and robust network structure have greater viscoelastic properties and less deformations in their internal structure during the creep–recovery measurements [\[15](#page-10-14)].

The results of obtained for the four Burger model parameters indicate that there is a relationship between the viscoelastic properties determined by the oscillatory

dynamic test and the static test (creep phase). According to Parot and Duperray [[55\]](#page-11-17), for a linear viscoelastic material, there is a relationship between the complex modulus, the creep function and the relaxation modulus.

The recovery phenomenon was monitored in the end of the creep period during 180 s, where the constant stress applied was zero. Parameters estimated of  $J_{\infty}$ ,  $J_{IR}$ ,  $C$ ,  $B$ , *Jmax*, and fnal percentage recovery of samples (*%R*) are shown in Table [3](#page-9-1). Both coacervates showed  $R^2$  higher than 0.99, confrming that the exponential decay function (Eq. [4](#page-2-3)) ftted well the recovery phase data. The WPI/ GEO-20/CH showed significantly ( $p < 0.05$ ) higher values of *J*∞ and *Jmax* than WPI/GEO-10/CH, indicating that the high GEO concentration induce the formation of a weaker and softer network structure, whereas WPI/GEO-10/CH showed the lowest values of  $J_{\infty}$  and  $J_{max}$  due to its more rigidity, stable, compact internal network structure. These results are in accordance with the obtained in the creep phase and dynamic oscillatory frequency sweep test. The WPI/GEO-20/CH coacervate showed superior values of parameter *C* (related to the curvature shape) and inferior values for *B* parameter (showing less phase magnitude in compliance decay). The WPI/GEO-10/CH showed higher percentage recovery (*%R)* values due to its higher capacity for structural recovery, suggesting stronger interaction between the polymer chain as compared with WPI/GEO-20/CH [\[15\]](#page-10-14). The high value of *%R* for WPI/GEO-20/CH indicates the formation of structure with more viscous behavior. The total recovery shape and degree of material deformation are afected by the length of the test, the amount of stress applied, and the temperature of the sample [[56](#page-11-18)].

<span id="page-9-1"></span>**Table 3** The ftting parameters of empirical model for WPI/GEO-10/CH and WPI/GEO-20/CH coacervates

Complex	$J_{\infty}$ (Pa <sup>-1</sup> )	$J_{max}$ (Pa <sup>-1</sup> )	$J_{1p}$ (Pa <sup>-1</sup> )	$B \times 10^{-3}$		$%R$ $(%$	$R^2$
WPI/GEO-10/CH	$0.35 + 0.03^{b**}$	$0.42 + 0.01^b$	$0.83 + 0.05^{\circ}$	$6.20 + 0.44$ <sup>a</sup>	$1.20 + 0.06^{\circ}$	16.67	0.9843
WPI/GEO-20/CH	$0.76 + 0.04^a$	$0.84 + 0.01^a$	$1.67 + 0.10^a$	$2.90 + 0.24^b$	$1.37 + 0.11^a$	9.52	0.9902

\*\*Different letters in the same column indicate values that are significantly different ( $p < 0.05$ ) based on Tukey's multiple comparison test. J<sub>max</sub> is the maximum compliance;  $J_{\infty}$  is the compliance of the Maxwell dashpot;  $J_{IR}$  is the Kelvin–Voigt element; %R is the final percentage recovery; B and C are the constant parameters of systems

# **Conclusion**

The viscosity and viscoelastic properties determined by oscillatory measurements (stress, frequency, temperature and time sweeps) and static test (creep and recovery) revealed suitable to obtain information about internal network structure, stability and strength of produced complex coacervates. This study demonstrated that the incorporation of garlic essential oil in the biopolymers matrices with loading of 20% (on a total solid basis of wall material) result in coacervate with less compact and rigidity structure as compared with loading of 10%. The coacervate with GEO of 10% (WPI/GEO-10/CH) showed higher viscosity than coacervate with GEO of 20% (WPI/GEO-20/CH). The WPI/ GEO-10/CH coacervate showed higher value of energy of activation (25.24 kJ mol<sup>-1</sup>) than that obtained for WPI/GEO-10/CH (20.74 kJ mol−1), indicating that WPI/GEO-10/CH had more compact and structured matrix to protect GEO compounds. The stress, time and temperature sweep tests indicated that WPI/GEO-10/CH tended to form the more stable viscoelastic solutions compared to WPI/GEO-20/ CH. Therefore, WPI/GEO-10/CH coacervate revealed most suitable for industrial applications that involve large stress, long time and high temperature. The potential application of complex coacervate as active ingredients in the elaboration of food products should be evaluated in future studies. In addition, further research should be conducted to study the textural properties, particle size, morphology, glass transition temperature, thermal properties, and sensory evaluation in order to assess the relationship with rheological analyses.

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## **References**

- <span id="page-10-0"></span>1. L. Tavares, L. Santos, C.P. Zapata Noreña, Trends Food Sci. Technol. **114**, 232 (2021)
- <span id="page-10-1"></span>2. L. Tavares, L. Santos, C.P.Z. Noreña, Powder Technol. **390**, 103 (2021)
- <span id="page-10-2"></span>3. C.T. Ho, J. Li, M.C. Kuo, in *Flavor Chemistry of Ethnic Foods*. ed. by F. Shahidi, C.T. Ho (Springer, Boston, 1999), pp. 55–76
- <span id="page-10-3"></span>4. S.G. Santhosha, P. Jamuna, S.N. Prabhavathi, Food Biosci. **3**, 59 (2013)
- <span id="page-10-4"></span>5. M. Corzo-Martínez, N. Corzo, M. Villamiel, Trends Food Sci. Technol. **18**, 609 (2007)
- <span id="page-10-5"></span>6. N. Ozdemir, A. Bayrak, T. Tat, F. Altay, M. Kiralan, A. Kurt, J. Food Meas. Charact. **15**, 1865–1876 (2021)
- <span id="page-10-6"></span>7. S. Rojas-Moreno, F. Cárdenas-Bailón, G. Osorio-Revilla, T. Gallardo-Velázquez, J. Proal-Nájera, J. Food Meas. Charact. **12**, 650–660 (2018)
- <span id="page-10-7"></span>8. M. Lengyel, N. Kállai-Szabó, V. Antal, A.J. Laki, I. Antal, Sci. Pharm. **87**, 20 (2019)
- <span id="page-10-8"></span>9. M.A. Rao, in *Rheology of Fluid, Semisolid, and Solid Foods: Principles and Applications*. ed. by M.A. Rao (Springer, Boston, 2014), pp. 27–61
- <span id="page-10-9"></span>10. J.F. Stefe, *Rheological Methods in Food Process Engineering* (Freeman Press, New York, 1996)
- <span id="page-10-10"></span>11. C. Wandrey, A. Bartkowiak, S.E. Harding, in *Encapsulation Technologies for Active Food Ingredients and Food Processing*. ed. by N.J. Zuidam, V. Nedovic (Springer, New York, 2010), pp. 31–100
- <span id="page-10-11"></span>12. H. Dogan, J.L. Kokini, *Batters and Breadings in Food Processing* (AACC International Press, Washington, 2011), pp. 263–299
- <span id="page-10-12"></span>13. A. Ibarz, G.V. Barbosa-Cánovas, *Unit Operations in Food Engineering* (CRC Press, Boca Raton, 2002)
- <span id="page-10-13"></span>14. L. Tavares, H.L.B. Barros, J.C.P. Vaghetti, C.P.Z. Noreña, Food Bioprocess Technol. **12**, 2093 (2019)
- <span id="page-10-14"></span>15. L. Tavares, C.P.Z. Noreña, Food Hydrocoll. **89**, 360 (2019)
- <span id="page-10-15"></span>16. L.H. Wang, X. Sun, G.Q. Huang, J.X. Xiao, J. Food Meas. Charact. **12**, 2718–2724 (2018)
- <span id="page-10-16"></span>17. F.L. Yang, X.-G. Li, F. Zhu, C.L. Lei, J. Agric. Food Chem. **57**, 10156 (2009)
- <span id="page-10-17"></span>18. C. Valcourt, P. Saulnier, A. Umerska, M.P. Zanelli, A. Montagu, E. Rossines, M.L. Joly-Guillou, Int. J. Pharm. **498**, 23 (2016)
- 19. N. Parris, P.H. Cooke, K.B. Hicks, Encapsulation of essential oils in zein nanospherical particles. J Agric Food Chem. **53**, 4788 (2005)
- 20. Y.I. Chang, J. Scire, B. Jacobs, *Flavor Encapsulation* (American Chemical Society, Washington, 1988), pp. 87–102
- <span id="page-10-18"></span>21. L.P. Fernandes, I.C.C. Turatti, N.P. Lopes, J.C. Ferreira, R.C. Candido, W.P. Oliveira, Dry. Technol. **26**, 1534 (2008)
- <span id="page-10-19"></span>22. L. Tavares, C.P.Z. Noreña, Food Bioprocess Technol. **13**, 1405 (2020)
- <span id="page-10-20"></span>23. J. Stefe, Introduction to rheology. Rheol. Methods Food Process. Eng. **2**, 1 (1996)
- <span id="page-10-21"></span>24. K. Yasuda, Massachusetts Institute of Technology, 1979.
- <span id="page-10-22"></span>25. Y. Zare, S.P. Park, K.Y. Rhee, Results Phys. **13**, 102245 (2019)
- <span id="page-10-23"></span>26. V.S. Kulkarni, C. Shaw, Rheological studies, in *Essential Chemistry for Formulators of Semisolid and Liquid Dosages*. ed. by V.S. Kulkarni, C. Shaw (Academic Press, Boston, 2016), pp. 145–182
- <span id="page-10-24"></span>27. S. Karaman, M.T. Yilmaz, H. Cankurt, A. Kayacier, O. Sagdic, Food Res. Int. **48**, 507 (2012)
- <span id="page-10-25"></span>28. M.T. Yilmaz, S. Karaman, M. Dogan, H. Yetim, A. Kayacier, J. Food Eng. **108**, 327 (2012)
- <span id="page-10-26"></span>29. A.K. Sharma, A.K. Tiwari, A.R. Dixit, Sust. Energ. Rev. **53**, 779 (2016)
- <span id="page-10-27"></span>30. Y. Liu, H.H. Winter, S.L. Perry, Adv. Colloid Interface Sci. **239**, 46–60 (2017)
- <span id="page-10-28"></span>31. W. Rosas-Flores, E.G. Ramos-Ramírez, J.A. Salazar-Montoya, Carbohydr. Polym. **98**, 1011 (2013)
- 32. H. Gong, M. Liu, J. Chen, F. Han, C. Gao, B. Zhang, Carbohydr. Polym. **88**, 1015 (2012)
- <span id="page-10-29"></span>33. Y. Wei, Y. Guo, R. Li, A. Ma, H. Zhang, Food Hydrocoll. **110**, 106198 (2021)
- <span id="page-10-30"></span>34. G. You, X.L. Liu, M.M. Zhao, Food Hydrocoll. **74**, 255–266 (2018)
- <span id="page-10-31"></span>35. M. Fathi, Z. Emam-Djomeh, A. Sadeghi-Varkani, Int. J. Biol. Macromol. **120**, 1265–1274 (2018)
- <span id="page-10-32"></span>36. M.G. Bordón, A.J. Paredes, N.M. Camacho, M.C. Penci, A. González, S.D. Palma, P.D. Ribotta, M.L. Martinez, Powder Technol. **391**, 479–493 (2021)
- <span id="page-10-33"></span>37. Q. Xiao, Q. Tong, L.T. Lim, Carbohydr. Polym. **87**, 1689 (2012)
- <span id="page-11-0"></span>38. H. Toǧrul, N. Arslan, Mathematical model for prediction of apparent viscosity of molasses. J. Food Eng. **62**, 281 (2004)
- <span id="page-11-1"></span>39. L. Zhang, Z. Liu, X. Han, Y. Sun, X. Wang, Int. J. Biol. Macromol. **134**, 807–814 (2019)
- <span id="page-11-2"></span>40. A.L. Muñoz-Celaya, M. Ortiz-García, E.J. Vernon-Carter, J. Jauregui-Rincón, E. Galindo, L. Serrano-Carreón, Carbohydr. Polym. **88**, 1141 (2012)
- <span id="page-11-3"></span>41. M. Chaharlang, V. Samavati, Int. J. Biol. Macromol. **79**, 56 (2015)
- <span id="page-11-4"></span>42. Y. Yang, X. Liu, Y. Xue, C. Xue, Y. Zhao, Food Hydrocoll. **98**, 105260 (2020)
- <span id="page-11-5"></span>43. L. Tavares, E.E. EsparzaFlores, R.C. Rodrigues, P.F. Hertz, C.P.Z. Noreña, Food Hydrocoll. **106**, 105876 (2020)
- <span id="page-11-6"></span>44. Y. Yuan, Z.Y. Kong, Y.E. Sun, Q.Z. Zeng, X.Q. Yang, LWT **75**, 171–179 (2017)
- <span id="page-11-7"></span>45. L. Wang, H.M. Liu, C.Y. Zhu, A.J. Xie, B.J. Ma, P.Z. Zhang, Carbohydr. Polym. **209**, 230 (2019)
- <span id="page-11-8"></span>46. A. Rafe, S.M.A. Razavi, Food Hydrocoll. **62**, 58–65 (2017)
- <span id="page-11-9"></span>47. Y. Zare, K.Y. Rhee, Compos. B **156**, 100 (2019)
- <span id="page-11-10"></span>48. M.A. Hesarinejad, A. Koocheki, S.M.A. Razavi, Food Hydrocoll. **35**, 583 (2014)
- <span id="page-11-11"></span>49. C.M.R. Rocha, H.K.S. Souza, N.F. Magalhães, C.T. Andrade, M.P. Gonçalves, Carbohydr. Polym. **110**, 345 (2014)
- <span id="page-11-13"></span><span id="page-11-12"></span>50. M.V. Chandra, B.A. Shamasundar, Food Hydrocoll. **48**, 47 (2015) 51. M. Dolz, M.J. Hernández, J. Delegido, Food Hydrocoll. **22**, 421
- (2008)
- <span id="page-11-14"></span>52. J. Huang, S. Zeng, S. Xiong, Q. Huang, Food Hydrocoll. **61**, 48 (2016)
- <span id="page-11-15"></span>53. M.G. de Alcântara, N. de FreitasOrtega, C.J.F. Souza, E.E. Garcia-Rojas, Food Struct. **24**, 100137 (2020)
- <span id="page-11-16"></span>54. Y.Y. Chang, D. Li, L.J. Wang, C.H. Bi, B. Adhikari, Carbohydr. Polym. **108**, 183 (2014)
- <span id="page-11-17"></span>55. J.M. Parot, B. Duperray, Mech. Mater. **40**, 575 (2008)
- <span id="page-11-18"></span>56. M. Cabuk, M. Yavuz, H.I. Unal, Colloids Surf. A **510**, 231–238 (2016)

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