



# Phase Equilibria of the Mg-Sn-Pr Ternary System at 500 °C

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**Abstract** The phase equilibria of the Mg-Sn-Pr ternary system at 500 °C were investigated by x-ray power diffraction (XRD), scanning electron microscope equipped with energy dispersive spectrometer (SEM-EDS). Seven ternary phases were observed. The crystal structure for the phases:  $\tau_1$  (MgSnPr, *I4/mmm*, *tI12*) and  $\tau_2$  (MgSn<sub>2</sub>Pr, *I42m*, *tI32*) were confirmed to exist at this temperature. Five new ternary compounds  $\tau_3$  to  $\tau_7$  are stable at 500 °C. Their compositions have been determined, but their crystal structures are still under investigation. The solubility of Mg in PrSn<sub>3</sub>,  $\alpha$ Pr<sub>3</sub>Sn<sub>5</sub> and PrSn<sub>3</sub> is about 2, 2 and 11 at.% Mg, respectively. The MgPr shows a solubility of 5.7 at.% Sn.

**Keywords** experimental phase equilibria · Mg-Sn-Pr ternary system · Mg-Sn-Rare earth alloy

## 1 Introduction

Magnesium alloys are considered promising alternatives to conventional metal alloys (Al alloys, Ti alloys and steel, etc.) for automotive and aerospace applications due to their low density ( $\sim 1.7 \text{ g/cm}^3$ ), high specific strength, good castability and availability.<sup>[1–3]</sup> However, the relatively low creep resistance at elevated temperature of Mg alloys is regarded as the key challenge limiting their wider application in automotive and aerospace industries since some

critical components are used at temperatures above 175 °C.<sup>[4]</sup> Adding alloying elements is an effective way to strengthen Mg alloys. Sn is a promising age-hardening element for Mg since its solid solubility in Mg matrix varies greatly with temperature and Mg<sub>2</sub>Sn is a thermally stable phase.<sup>[5]</sup> Nevertheless, the Mg<sub>2</sub>Sn particles that form in Mg matrix are larger, thus reducing the age-hardening response of the alloys.<sup>[6]</sup> Rare earth (RE) metals are another important alloying element of Mg alloys. Studies have found that Mg alloys with RE elements have good corrosion resistance, high strength, excellent creep resistance and better deformability.<sup>[7–9]</sup> Lim et al. reported that a small amount of Sn can enhance the ductility in Mg-rich Mg-MM (misch-metal) alloys.<sup>[10]</sup> In order to find a new creep-resistant Mg alloys, the knowledge of phase equilibria in Mg-Sn-RE systems is of fundamental importance. Up to now, the phase equilibria of the Mg-Sn-Pr ternary system have not been reported yet. The purpose of present work is to experimentally investigate the phase equilibria of the Mg-Sn-Pr system at 500 °C in equilibrated alloys using x-ray diffraction (XRD) and scanning electron microscope equipped with energy dispersive spectrometer (SEM/EDS). The obtained phase diagram is expected to provide useful information for novel Mg alloy design.

## 2 Literature Review

The Mg-Sn and Mg-Pr binary phase diagrams were adopted from the book of Massalski,<sup>[11]</sup> which was based on the evaluated diagrams by Nayeb-Hashemi and Clark.<sup>[5,12]</sup> There is only one binary compound Mg<sub>2</sub>Sn in the Mg-Sn system, and it is congruently formed from liquid at 770 °C. The Mg-Pr system has five binary compounds: Mg<sub>12</sub>Pr, Mg<sub>41</sub>Pr<sub>5</sub>, Mg<sub>3</sub>Pr, Mg<sub>2</sub>Pr and MgPr. Mg<sub>2</sub>Pr is stable at high

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temperature and decomposes at 670 °C. The Pr-Sn binary system is complex due to the high oxidizability of Pr-Sn alloys. The Pr-Sn phase diagram reported by Eremenko et al. [13] and reproduced by Massalski [11] contains eight compounds: Pr<sub>3</sub>Sn, αPr<sub>5</sub>Sn<sub>3</sub>, βPr<sub>5</sub>Sn<sub>3</sub>, Pr<sub>5</sub>Sn<sub>4</sub>, PrSn, αPr<sub>3</sub>Sn<sub>5</sub>, βPr<sub>3</sub>Sn<sub>5</sub> and PrSn<sub>3</sub>. Subsequently, the PrSn<sub>2</sub>, Pr<sub>3</sub>Sn<sub>7</sub>, Pr<sub>2</sub>Sn<sub>5</sub> and Pr<sub>2</sub>Sn<sub>3</sub> phases were reported by several researchers.[14–16] The phase diagram of the Pr-Sn binary system was assessed by Kim et al. using the Calphad method.[17] It contains 13 binary compounds and was adopted in the present work. In the Mg-Sn-Pr ternary system, two ternary phases, i.e., τ<sub>1</sub>-MgSnPr and τ<sub>2</sub>-MgSn<sub>2</sub>Pr, were reported.[18,19] The three binary boundary phase diagrams and the two ternary compounds are shown in Fig. 1 and the crystallographic data for all unary and

binary solid phases in the Mg-Sn-Pr system are listed in Table 1.

### 3 Experimental Procedure

High-purity metal nuggets: Mg 99.5, Sn 99.5 and Pr 99.5 wt. % were used as starting materials. More than 30 ternary alloys were synthesized in the ternary system. Several steps were taken in the preparation procedure. First, small pieces of the starting materials were weighed and put into tantalum tubes. Then these Ta tubes were sealed in an enclosed chamber filled with argon. Subsequently, the sealed Ta tubes were sealed into evacuated quartz tubes. Finally, these double-sealed samples were

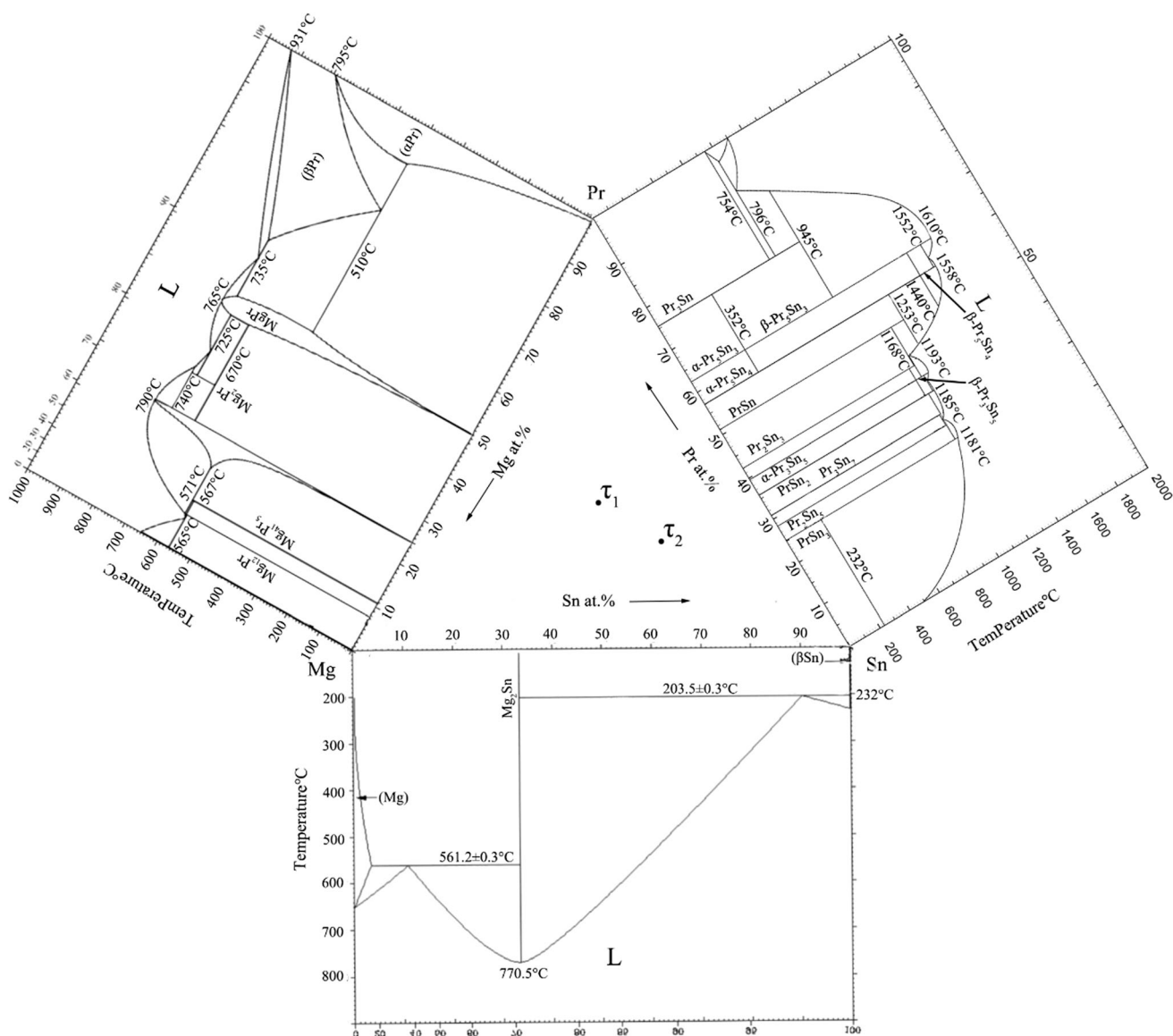


Fig. 1 Binary phase diagrams constituting the Mg-Sn-Pr ternary system

**Table 1** Crystallographic data for the unary and binary phases in the Mg-Sn-Pr system

Phase	Pearson symbol	Space group	Prototype	Strukturbericht type	Ref
(Mg)	<i>hP2</i>	<i>P6<sub>3</sub>/mmc</i>	Mg	A3	5
(βSn)	<i>tI4</i>	<i>I4<sub>1</sub>/amd</i>	βSn	A5	5
(αSn)	<i>cF8</i>	<i>Fd-3 m</i>	C (diamond)	A4	5
Mg <sub>2</sub> Sn	<i>cF12</i>	<i>Fm3m</i>	CaF <sub>2</sub>	C1	5
(αPr)	<i>hP4</i>	<i>P6<sub>3</sub>/mmc</i>	αLa	A3'	12
(βPr)	<i>cI2</i>	<i>Im-3 m</i>	W	A2	12
Mg <sub>12</sub> Pr	<i>tI26</i>	<i>I4/mmm</i>	Mn <sub>12</sub> Th	D2 <sub>b</sub>	12
Mg <sub>41</sub> Pr <sub>5</sub>	<i>tI92</i>	<i>I4/m</i>	Mg <sub>41</sub> Ce <sub>5</sub>	...	12
Mg <sub>3</sub> Pr	<i>cF16</i>	<i>Fm-3 m</i>	BiF <sub>3</sub>	D0 <sub>3</sub>	12
Mg <sub>2</sub> Pr	<i>cF24</i>	<i>Fd-3 m</i>	Cu <sub>2</sub> Mg	C15	12
MgPr	<i>cP2</i>	<i>Pm-3 m</i>	CsCl	B2	12
Pr <sub>3</sub> Sn	<i>cP4</i>	<i>Pm-3 m</i>	AuCu <sub>3</sub>	L1 <sub>2</sub>	11
Pr <sub>2</sub> Sn <sub>5</sub>	<i>oC28</i>	<i>Cmmm</i>	Ce <sub>2</sub> Sn <sub>5</sub>	...	16
Pr <sub>3</sub> Sn <sub>7</sub>	<i>oC20</i>	<i>Cmmm</i>	Ce <sub>3</sub> Sn <sub>7</sub>	...	16
PrSn <sub>2</sub>	<i>oC12</i>	<i>Cmmm</i>	ZrGa <sub>2</sub>	...	16
Pr <sub>2</sub> Sn <sub>3</sub>	...	...	...	...	16
Pr <sub>11</sub> Sn <sub>10</sub>	...	...	...	...	16
βPr <sub>5</sub> Sn <sub>3</sub>	<i>hP16</i>	<i>P6<sub>3</sub>/mcm</i>	Mn <sub>5</sub> Si <sub>3</sub>	D8 <sub>8</sub>	11
αPr <sub>5</sub> Sn <sub>3</sub>	<i>tI32</i>	<i>I4/mcm</i>	W <sub>5</sub> Si <sub>3</sub>	D8 <sub>m</sub>	11
Pr <sub>5</sub> Sn <sub>4</sub>	<i>oP36</i>	<i>Pnma</i>	Sm <sub>5</sub> Ge <sub>4</sub>	...	11
PrSn	<i>oP8</i>	<i>Pnma</i>	FeB	B27	11
βPr <sub>3</sub> Sn <sub>5</sub>	...	...	...	...	11
αPr <sub>3</sub> Sn <sub>5</sub>	...	...	...	...	11
PrSn <sub>3</sub>	<i>cP4</i>	<i>Pm-3 m</i>	AuCu <sub>3</sub>	L1 <sub>2</sub>	11

melted in a resistance furnace through the following process: the resistance furnace was heated to 600 °C and held for one hour, then the temperature was increased to 750 °C and held for two hours, and finally the temperature was raised to 820 °C and held for two days. At 820 °C, the sealed tubes with the samples were turned upside-down every few hours in order to homogenize the samples. After being melted, these samples were annealed at 500 °C for 45 days, followed by ice water quenching.

Phase identification was done by x-ray diffraction (XRD) with Cu-K $\alpha$  radiation at 40 kV and a current of 40 mA (D8 Discover X, BRUKER, Germany). It should be mentioned that a small amount of paraffin was added to prevent the oxidation of the samples when the samples were ground into powder and characterized/analyzed by XRD. Phase compositions were determined by energy dispersive spectroscopy (EDS) analyzer (Oxford X-MAX80 Britain) attached to a field-emission scanning electron microscope (HitachiSU-8000 Japan). The compositions of each phase were obtained from the average value of 5-10 measured EDS data. It should be noted that the metallographic samples were ground with anhydrous alcohol initially and with anhydrous polishing agent at end to avoid any possible reaction of Mg and Pr with water.

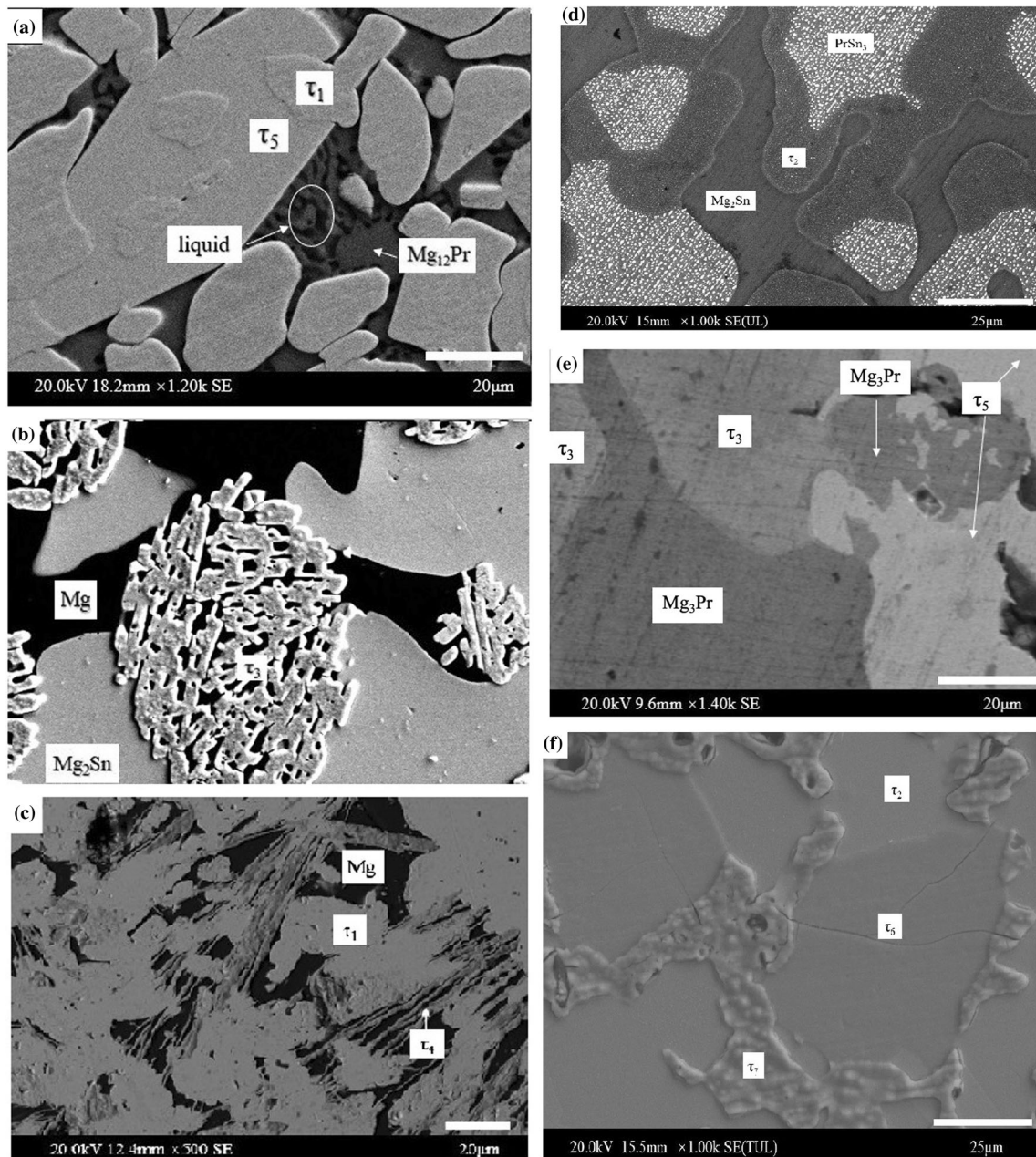
The prepared metallographic samples were first stored in anhydrous alcohol, and then taken to a vacuum glove box, where they were removed from the alcohol, after being dried out and sealed in a vacuum plastic bag waiting microscopic inspection.

## 4 Results and Discussion

### 4.1 Microstructure and Phase Equilibria

In the present work, the compositions of the phases in equilibrated alloys at 500 °C were measured by EDS, and their crystal structures were analyzed by XRD. The chemical compositions are given in atomic ratio (at.%). The microstructure of selected samples are shown on Fig. 2(a-f) and two XRD patterns containing ternary compounds  $\tau_2$  and  $\tau_3$  are presented in Fig. 3(a-b).

The SEM picture of 1# alloy (Mg<sub>74.9</sub>Sn<sub>10.6</sub>Pr<sub>14.5</sub>) provides key experimental evidence that  $\tau_5$  (Mg<sub>44.6</sub>Sn<sub>24.2</sub>Pr<sub>31.2</sub>) is a different phase compared to  $\tau_1$  (Mg<sub>35.7</sub>Sn<sub>33.2</sub>Pr<sub>31.1</sub>). The colors of the two phases are so close that they cannot be easily distinguished from each other. However, a phase boundary can be observed at the

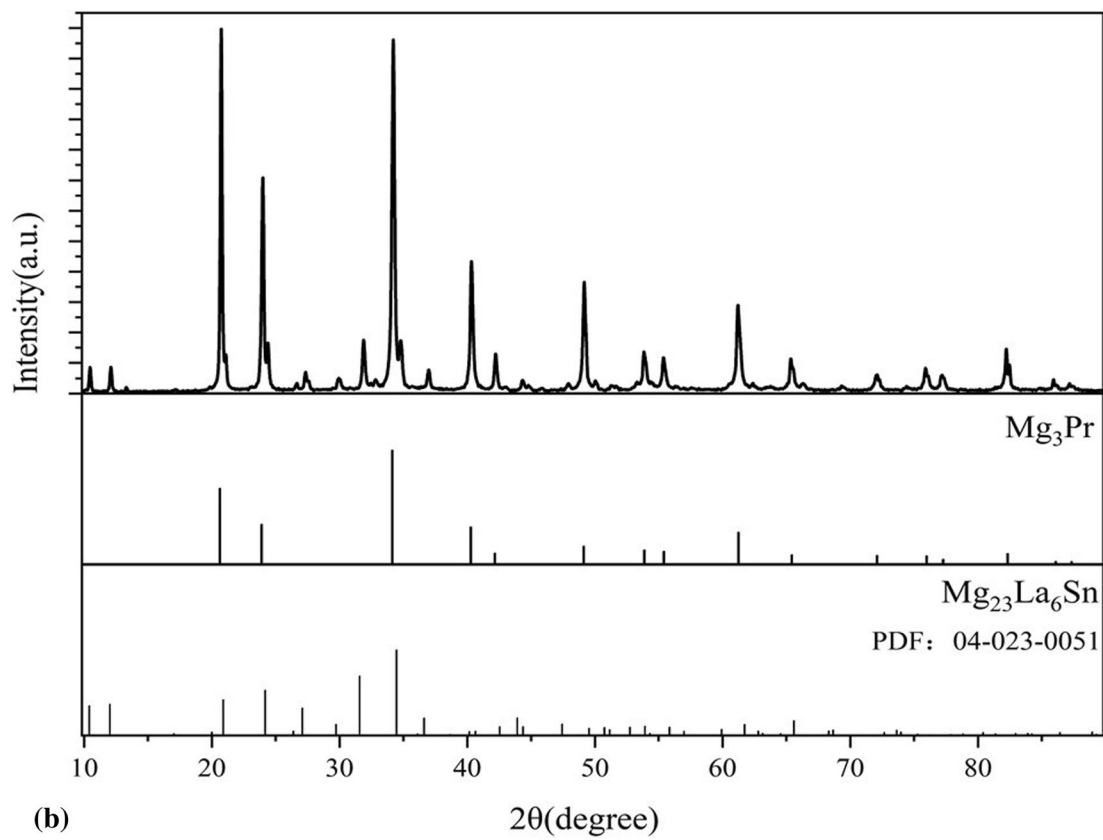
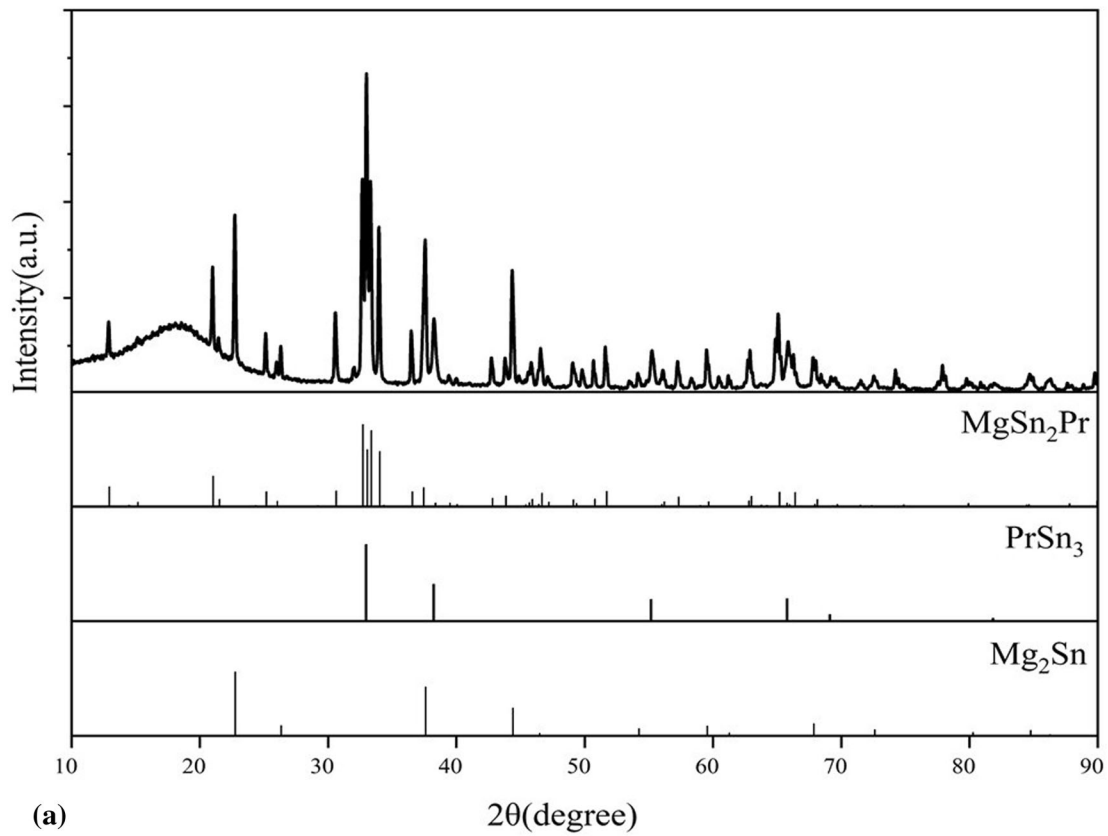


**Fig. 2** Typical SEM images obtained from equilibrium alloys annealed at 500 °C for 45 days: (a) 1# alloy ( $Mg_{74.9}Sn_{10.6}Pr_{14.5}$ ) showing coexistence of  $\tau_1$  (grey,  $Mg_{35.7}Sn_{33.2}Pr_{31.1}$ ) +  $\tau_5$  (grey,  $Mg_{44.6}Sn_{24.2}Pr_{31.2}$ ) + Liq ( $Mg_{12}Pr$  + (Mg) eutectic structure); (b) 2# alloy ( $Mg_{67.5}Sn_{27}Pr_{5.5}$ ) showing coexistence of (Mg) (dark) +  $\tau_4$  (mesh,  $Mg_{55.5}Sn_{27.5}Pr_{17}$ ) +  $Mg_2Sn$  (light grey); (c) 3# alloy ( $Mg_{75.4}Sn_{12.6}Pr_{12}$ ) showing coexistence of  $\tau_1$  (blocky grey,  $Mg_{33.3}Sn_{33.3}Pr_{33.4}$ ) + (Mg) (black) +  $\tau_4$  (needle-like grey,  $Mg_{59}Sn_{24}Pr_{17}$ ); (d) 4#

alloy ( $Mg_{20.1}Sn_{58.6}Pr_{21.3}$ ) showing coexistence of  $Mg_2Sn$  (black) +  $\tau_2$  (grey,  $Mg_{26.2}Sn_{52.7}Pr_{21.1}$ ) +  $PrSn_3$  (light grey,  $Mg_{11.1}Sn_{65.2}Pr_{23.7}$ ); (e) 5# alloy ( $Mg_{65.2}Sn_{8.1}Pr_{26.7}$ ) showing coexistence of  $\tau_5$  (light grey,  $Mg_{41.3}Sn_{23.1}Pr_{35.6}$ ) +  $\tau_3$  (grey,  $Mg_{75.2}Sn_{2.3}Pr_{22.5}$ ) +  $Mg_3Pr$  (deep grey,  $Mg_{74.2}Sn_{0.1}Pr_{25.7}$ ); (f) 22# alloy ( $Mg_{30}Sn_{41.7}Pr_{28.3}$ ) showing coexistence three phases,  $\tau_2$  (light grey,  $Mg_{21}Sn_{51.1}Pr_{26.9}$ ) +  $\tau_6$  (grey,  $Mg_{38}Sn_{37}Pr_{25}$ ) +  $\tau_7$  grey phase with a rough surface,  $Mg_{20}Sn_{45}Pr_{35}$ )

junction of the two phases. It is necessary to state that the 1# alloy is not a fully equilibrated alloy since the (Mg) +  $Mg_{12}Pr$  eutectic structure still exists in the alloy. In Fig. 2(b, a) three-phase microstructure of (Mg) +  $\tau_4$  +  $Mg_2Sn$  is observed for 2# alloy ( $Mg_{67.5}Sn_{27}Pr_{5.5}$ ). The grey phase is  $Mg_2Sn$ , and the black phase is (Mg). The

composition of the grey network is  $Mg_{55.5}Sn_{27.5}Pr_{17}$ , which we as assumed to be a new ternary compound and named it  $\tau_4$ . Figure 2c shows a three phases field of  $\tau_1$  +  $\tau_4$  + (Mg) in 3# alloy ( $Mg_{75.4}Sn_{12.6}Pr_{12}$ ). The large blocky grey phase is  $\tau_1$  and the black phase is (Mg). The composition of the acicular grey phase is  $Mg_{59}Sn_{24.0}Pr_{17}$ , which is like the  $\tau_4$





◀ **Fig. 3** X-ray diffraction patterns of (a) 4# alloy ( $\text{Mg}_{20.1}\text{Sn}_{58.6}\text{Pr}_{21.3}$ ) showing coexistence of three phase,  $\tau_2$ ,  $\text{Pr}_3\text{Sn}$  and  $\text{Mg}_2\text{Sn}$ ; (b) 14# alloy ( $\text{Mg}_{75.2}\text{Sn}_1\text{Pr}_{23.8}$ ) showing that it contains  $\text{Mg}_3\text{Pr}$  and a phase with the same structure as  $\text{Mg}_{23}\text{SnLa}_6$ . The vertical marks indicate the positions of possible Bragg reflections of each phase in the studied alloys

of 2# alloy (Fig. 2b). Currently, we believe that both phases are the same ternary compound  $\tau_4$ :  $\text{Mg}_{59-x}\text{Sn}_{24+x}\text{Pr}_{17}$  ( $x = 0 \sim 3.5$ ), and Mg and Sn have a certain mutual solubility due to the relatively close compositions of these two phases and the lack of key high-quality XRD patterns.

The 4# ( $\text{Mg}_{20.1}\text{Sn}_{58.6}\text{Pr}_{21.3}$ ) alloy shows three distinct phases in Fig. 2(d). Whilst the dark phase and large grey phase could be identified as  $\text{Mg}_2\text{Sn}$  and  $\tau_2$  ( $\text{Mg}_{26.2}\text{Sn}_{52.7}\text{Pr}_{21.1}$ ) by EDS analysis, the composition of large light grey is  $\text{Mg}_{11.1}\text{Sn}_{65.2}\text{Pr}_{23.7}$  is difficult to determine and whether this phase is a new ternary phase or a binary phase with a solid solubility. The XRD pattern of the alloys (Fig. 3a) reveals the answer, in it the  $\text{PrSn}_3$  phase can be identified as well as the characteristic peaks of  $\text{Mg}_2\text{Sn}$  and  $\tau_2$  phases. In other words,  $\text{PrSn}_3$  dissolves up to 11 at.% Mg. As mentioned in the experimental procedure, paraffin oil was added to the samples during grinding and XRD analysis to slow down the oxidation rate of samples. Therefore, an amorphous hump could be observed at the low angle region in XRD pattern of sample. In addition, the surface of  $\text{PrSn}_3$  was covered with some small particles which turns out to be Rare Earth Oxide (REO). They were produced from an air exposure within two minutes, which occurred while the alloy was transferred to the scanning electron microscopy equipment.

The microstructure of 5# alloy ( $\text{Mg}_{65.2}\text{Sn}_{8.1}\text{Pr}_{26.7}$ ) in Fig. 2(e) shows the coexistence of three phases, the light grey phase is  $\tau_5$  ( $\text{Mg}_{41.3}\text{Sn}_{23.1}\text{Pr}_{35.6}$ ) and the large dark grey phase is  $\text{Mg}_3\text{Pr}$ . The color of third phase is lighter than  $\text{Mg}_3\text{Pr}$  and darker than  $\tau_5$ . The composition of third phase is  $\text{Mg}_{75.2}\text{Sn}_{2.3}\text{Pr}_{22.5}$ , which is close to the composition of  $\text{Mg}_3\text{Pr}$  ( $\text{Mg}_{74.2}\text{Sn}_{0.1}\text{Pr}_{25.7}$ ). But obviously, it is a different phase from  $\text{Mg}_3\text{Pr}$  since  $\text{Mg}_3\text{Pr}$  hardly contains solid solubility of Sn, and we named it  $\tau_3$ . Figure 3(b) shows the XRD pattern of the 14# alloy located between  $\text{MgPr}_3$  and  $\tau_3$  matched well the characteristic peaks of  $\text{Mg}_{23}\text{SnLa}_6$  phase (ICDD, PDF 04–023–0051) and the peaks of  $\text{Mg}_3\text{Pr}$

phase. It seems that  $\tau_3$  is an isostructural with  $\text{Mg}_{23}\text{SnLa}_6$ . ( $\text{Zr}_6\text{Zn}_{23}\text{Si}$  prototype,  $cF120$  Pearson symbol)[20]. The microstructure of 22# alloy contains three distinct phases as shown in Fig. 2(f). The light grey phase is  $\tau_2$  ( $\text{Mg}_{21.1}\text{Sn}_{51.1}\text{Pr}_{26.9}$ ). The grey phase with a rough surface has a new composition as  $\text{Mg}_{20}\text{Sn}_{45}\text{Pr}_{35}$  and was named  $\tau_7$ . The grey phase in the middle layer with another new composition ( $\text{Mg}_{38}\text{Sn}_{37}\text{Pr}_{25}$ ) was named  $\tau_6$ .

## 4.2 Isothermal Section at 500 °C

Experimental data of EDS and XRD obtained from selected equilibrium alloys, which have been annealed at 500 °C for 45 days, are summarized in Table 2. The isothermal section at 500 °C constructed based on these data is shown in Fig. 4 with symbols indicating the alloy compositions. It should be noted that the 5 alloys (18#–22#) located in the regions ( $\beta\text{Pr}_5\text{Sn}_3$ – $\tau_1$ – $\tau_6$ – $\tau_2$ – $\text{PrSn}_3$ ) near the Pr–Sn boundary system were only examined by SEM/EDS and not by XRD, due to the high oxidizability of Pr–Sn alloys. The phase regions without experimental data, which were estimated from the surrounding phase relationship, are indicated with dashed lines.

The binary phases show different ranges of solubility with respect to the third element in the system. The solid solubilities of Mg in  $\text{Pr}_3\text{Sn}$ ,  $\beta\text{Pr}_5\text{Sn}_3$  and  $\text{PrSn}_3$  are 2, 2 and 11 at.%, respectively. The  $\text{MgPr}$  compound shows a solubility of 5.7 at.% Sn. Other Pr–Sn and Mg–Pr binary compounds show no appreciable Mg or Sn solubility. The solubilities of  $\alpha\text{Pr}_5\text{Sn}_4$ ,  $\text{PrSn}$ ,  $\text{PrSn}_2$  and  $\alpha\text{Pr}_3\text{Sn}_5$  are shown as the dashed lines since they are simply deduced from the EDS data from alloys near them.

Within the regions that have been studied, seven ternary compounds were observed at 500 °C. Their homogeneity ranges and crystal structures are listed in Table 3. Two known ternary compounds  $\tau_1$  ( $\text{MgSnPr}$ ,  $I4/mmm$ ,  $tI12$ ) and  $\tau_2$  ( $\text{MgSn}_2\text{Pr}$ ,  $I42m$ ,  $tI32$ ) were detected at 500 °C. Five new compounds were named as  $\tau_n$ , with n ranging from 3 to 7 with decreasing of Mg content. Figure 3b shows that  $\tau_3$  may have the same structure as  $\text{Mg}_{23}\text{SnLa}_6$ . ( $\text{Zr}_6\text{Zn}_{23}\text{Si}$  prototype,  $cF120$  Pearson's code)[20]. The evidence for the existence of the other four new ternary compounds is mainly based on SEM/EDS data. The crystal structures of  $\tau_4$  to  $\tau_7$  have not been determined yet, since high-quality XRD patterns of these new ternary compounds are still

**Table 2** Phase identification (by EDS and XRD) of equilibrated Mg-Sn-Pr alloys at 500 °C

Alloy	Alloy Composition (at.%)			Phase	Phase composition (at.%)			Figure
	Mg	Sn	Pr		Mg	Sn	Pr	
1(a)	74.9	10.6	14.5	( $\tau_5$ ) <sup>b</sup>	44.6	24.2	31.2	Figure 2(a)
	...	...	...	$\tau_1$	35.7	33.2	31.1	...
	...	...	...	(Mg) + Mg <sub>12</sub> Pr	93.4	1.4	5.2	...
2	67.5	27.0	5.5	Mg <sub>2</sub> Sn	63.6	36.4	0.0	Figure 2(b)
	...	...	...	( $\tau_4$ )	55.5	27.5	17	...
	...	...	...	Mg	97.3	2.6	0.1	...
3	75.4	12.6	12.0	Mg	99.7	0.2	0.1	Figure 2(c)
	...	...	...	$\tau_1$	33.3	33.3	33.4	...
	...	...	...	( $\tau_4$ )	59.0	24.0	17.0	...
4	20.1	58.6	21.3	PrSn <sub>3</sub>	11.1	65.2	23.7	Figure 2(d)
	...	...	...	$\tau_2$	26.2	52.7	21.1	Figure 3(a)
	...	...	...	Mg <sub>2</sub> Sn	62.6	35.5	1.9	...
5	65.2	8.1	26.7	( $\tau_5$ )	41.3	23.1	35.6	Figure 2(e)
	...	...	...	( $\tau_3$ )	75.2	2.3	22.5	...
	...	...	...	Mg <sub>3</sub> Pr	74.2	0.1	25.7	...
6	72.6	6.3	21.1	( $\tau_5$ )	42.6	23.4	34.0	...
	...	...	...	( $\tau_3$ )	75.0	4.0	21.0	...
	...	...	...	Mg <sub>41</sub> Pr <sub>5</sub>	88.3	0.1	11.6	...
7	92.8	3.9	3.3	$\tau_1$	35.4	32.2	32.4	...
	...	...	...	Mg	99.9	0.1	0	...
8	54.9	11.9	33.6	( $\tau_5$ )	41.2	22.5	36.3	...
	...	...	...	Mg <sub>3</sub> Pr	73.0	0.3	26.7	...
	...	...	...	$\beta$ Pr <sub>5</sub> Sn <sub>3</sub>	2.8	36.5	60.4	...
9	19.3	21.7	59.0	$\beta$ Pr <sub>5</sub> Sn <sub>3</sub>	0.8	36.1	63.1	...
	...	...	...	Pr <sub>3</sub> Sn	4.8	22.7	72.5	...
	...	...	...	MgPr	43.4	5.6	51.0	...
10	38.3	17.7	44	$\beta$ Pr <sub>5</sub> Sn <sub>3</sub>	1.9	36.6	61.5	...
	...	...	...	Mg <sub>3</sub> Pr	73.9	0.3	25.8	...
	...	...	...	MgPr	47.4	3.1	49.5	...
11	18.5	64.5	16.9	PrSn <sub>3</sub>	2.4	72.2	25.5	...
	...	...	...	Liq (Sn)	24.2	73.5	2.3	...
	...	...	...	Mg <sub>2</sub> Sn	65.1	34.3	0.6	...
12	38.8	47.9	11.3	PrSn <sub>3</sub>	11.7	63.3	25	...
	...	...	...	$\tau_2$	25.3	49.4	25.3	...
	...	...	...	Mg <sub>2</sub> Sn	63.7	36.2	0.1	...
13	32.9	27.1	40.0	$\beta$ Pr <sub>5</sub> Sn <sub>3</sub>	2.2	36.4	61.4	...
	...	...	...	( $\tau_5$ )	41.1	23.0	35.9	...
14	75.2	1	23.8	Mg <sub>3</sub> Pr	75.2	0.2	24.6	Figure 3(b)
	...	...	...	$\tau_3$	75.3	2.1	22.6	...
15	15.7	11.7	72.6	(Pr)	1.0	0.4	98.6	...
	...	...	...	Pr <sub>3</sub> Sn	1.8	23.4	74.8	...
	...	...	...	MgPr	46.6	1.0	52.3	...
16	82.3	7.0	10.7	( $\tau_5$ )	33.1	33.3	33.6	...
	...	...	...	Mg <sub>12</sub> Pr	91.5	0.0	8.5	...
	...	...	...	(Mg)	99.6	0.1	0.3	...

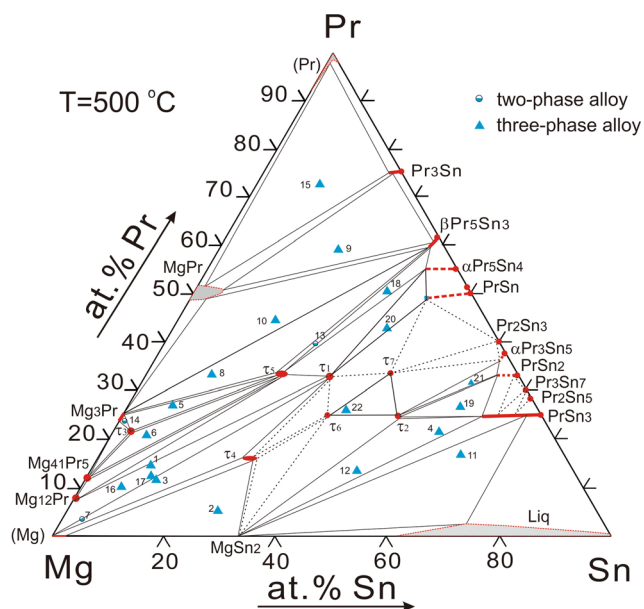
**Table 2** continued

Alloy	Alloy Composition (at.%)			Phase	Phase composition (at.%)			Figure
	Mg	Sn	Pr		Mg	Sn	Pr	
17	75.8	11.9	12.3	$\tau_1$	33.1	33.4	33.5	...
	...	...	...	Mg <sub>12</sub> Pr	91.5	0.11	8.32	...
	...	...	...	(Mg)	99.6	0.1	0.3	...
18*	15.3	34.8	49.9	( $\tau_5$ )	42	24	34	...
	...	...	...	Pr <sub>5</sub> Sn <sub>3</sub>	0.8	37.6	61.6	...
	...	...	...	Pr <sub>5</sub> Sn <sub>4</sub> ?	5.5	38.9	55.6	...
19*	13.2	59.2	27.6	$\tau_2$	24.1	50.1	25.8	...
	...	...	...	PrSn <sub>2</sub> ?	4.4	64.6	31.0	...
	...	...	...	PrSn <sub>3</sub>	11.4	63.2	25.4	...
20*	18.3	38.6	43.1	$\tau_1$	33.2	33.4	33.4	...
	...	...	...	PrSn ?	8	42.5	49.5	...
	...	...	...	Pr <sub>5</sub> Sn <sub>4</sub> ?	6	38.8	55.2	...
21*	9.3	59.5	31.2	$\tau_2$	24.2	50	25.8	...
	...	...	...	PrSn <sub>2</sub> ?	5.4	64.5	30.2	...
	...	...	...	Pr <sub>3</sub> Sn <sub>5</sub> ?	1.5	60.9	37.6	...
22*	30	41.7	28.3	( $\tau_2$ )	21	51.1	26.9	Figure 2(f)
	...	...	...	( $\tau_6$ )	38	37	25	...
	...	...	...	( $\tau_7$ )	20	45	35	...

(a) The 1# alloy is non-equilibrium since it contains eutectic structure of (Mg) + Mg<sub>12</sub>Pr.

(b) The  $\tau_4$ ,  $\tau_5$ ,  $\tau_6$  and  $\tau_7$  phases are enclosed in parenthesis since they were not identified by XRD.

\*: The samples marked with \* were only examined by SEM/EDS and not by XRD.



**Fig. 4** Experimental isothermal section of the Mg-Sn-Pr system at 500 °C

lacking. However, by comparing with the isothermal section of La-Mg-Sn system at 500 °C from the literature [20], we have found that except for  $\tau_4$  (Mg<sub>59-x</sub>Sn<sub>24+x</sub>Pr<sub>17</sub>, x = 0 ~ 4), the composition ratios of  $\tau_5$ (Mg<sub>40-44</sub>Sn<sub>26.5-22.5</sub>Pr<sub>33.5</sub>),  $\tau_6$ (Mg<sub>38</sub>Sn<sub>37</sub>Pr<sub>25</sub>) and  $\tau_7$ (Mg<sub>20</sub>Sn<sub>45</sub>Pr<sub>35</sub>) are like the ternary compounds (Mg<sub>4-x</sub>Sn<sub>2+x</sub>La<sub>3</sub> 0.12 < x ≤ 0.4, Mg<sub>35</sub>Sn<sub>40</sub>La<sub>25</sub> and Mg<sub>20</sub>Sn<sub>45</sub>La<sub>35</sub>) in the La-Mg-Sn system.

### 5 Conclusions

The 500 °C isothermal section of the Mg-Sn-Pr ternary system was determined by SEM with EDX and XRD. The main findings are as follow:

- (i) Within the investigated regions,  $\tau_1$  (MgSnPr) and  $\tau_2$  (MgSn<sub>2</sub>Pr), and five new ternary compounds ( $\tau_3$ ,  $\tau_4$ ,  $\tau_5$ ,  $\tau_6$  and  $\tau_7$ ) were observed in the section. Except for  $\tau_4$  phase, the  $\tau_3$ ,  $\tau_5$ ,  $\tau_6$  and  $\tau_7$  have same or similar composition ratios as four ternary compounds in La-Mg-Sn system.



**Table 3** Ternary compounds in the Mg–Sn–Pr system at 500 °C

Phase	Pearson symbol	Space group	Prototype	Ref	Comments
$\tau_1$ -MgSnPr	<i>tI12</i>	<i>I4/mmm</i>	MgSnCe	18	...
$\tau_2$ -MgSn <sub>2</sub> Pr	<i>tI32</i>	<i>I-42 m</i>	MgSn <sub>2</sub> La	19	...
$\tau_3 \sim \text{Mg}_{75}\text{Sn}_{2.5}\text{-}4\text{Pr}_{22.5\text{-}21}$	Unknown			TW	Its composition ratio and XRD pattern are similar to Mg <sub>23</sub> SnLa <sub>6</sub> [20]
$\tau_4 \sim \text{Mg}_{55.5\text{-}59}\text{Sn}_{27.5\text{-}24}\text{Pr}_{17}$	Unknown			TW	...
$\tau_5 \sim \text{Mg}_{40}\text{-}44\text{Sn}_{26.5\text{-}22.5}\text{Pr}_{33.5}$	Unknown			TW	Its composition ratio is similar to Mg <sub>4-x</sub> Sn <sub>2+x</sub> La <sub>3</sub> 0.12 < x ≤ 0.4 [20]
$\tau_6 \sim \text{Mg}_{38}\text{Sn}_{37}\text{Pr}_{25}$	Unknown			TW	Mg <sub>35</sub> Sn <sub>40</sub> La <sub>25</sub> [20]
$\tau_7 \sim \text{Mg}_{20}\text{Sn}_{45}\text{Pr}_{35}$	Unknown			TW	Mg <sub>20</sub> Sn <sub>45</sub> La <sub>35</sub> [20]

TW This work.

- (ii) At 500 °C, Pr<sub>3</sub>Sn, βPr<sub>5</sub>Sn<sub>3</sub> and PrSn<sub>3</sub> show a solubility of 2, 2 and 11 at.% Mg, respectively. The solubility of Sn in MgPr is 5.7 at.%.

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