



Thermodynamic Descriptions of the Co–Zr and Co–Fe–Zr Systems

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Abstract The Co–Fe–Zr system and its Co–Zr subsystem were optimized using the CALculation of PHase Diagram (CALPHAD) approach. The substitutional solution model was used for describing the phases liquid, fcc_A1, bcc_A2 and hcp_A3. Two Laves phases were modeled as $(\text{Co,Fe,Zr})_2(\text{Co,Fe,Zr})_1$, and the phases CoFe and CoZr with the bcc_B2 crystal structure were described as the ordered one of bcc_A2 in the formula $(\text{Co,Fe,Va,Zr})_{0.5}(\text{Co,Fe,Va,Zr})_{0.5}\text{Va}_3$. With limited solubility ranges, all other phases were treated as the line compounds $(\text{Co,Fe})_m\text{Zr}_n$. An excellent agreement between the reported and calculated results was reached. The reliable thermodynamic parameters of the Co–Fe–Zr system were acquired, which can be well applied to various thermodynamic calculations and materials design.

Keywords Co–Zr system · Co–Fe–Zr system · CALPHAD · phase diagram

1 Introduction

The Co–Fe–Zr system is a basic and key system in hydrogen storage materials, amorphous alloys, high-entropy alloys, and magnetic materials.

In the international thermonuclear experimental reactor (ITER) project, the intermetallic compound ZrCo is

intended to replace uranium for the storage and delivery of tritium.^[1] Fe substitution for Co can enhance the durability against the hydrogen-induced disproportionation, which makes it more favorable to store tritium.^[2] And cobalt, iron and zirconium are the principal elements in amorphous alloys^[3–6] and high-entropy alloys.^[7–9] Furthermore, Hoque et al.^[10] have reported a two-phase magnetic $\text{Co}_{11}\text{Zr}_2\text{Co}_{23}\text{Zr}_6$ system and the addition of Fe can improve its magnetic and mechanical properties.

The further development of such novel materials is largely dependent on the accurate phase equilibria information and detailed thermodynamic description of the Co–Fe–Zr system. Recently, the Co–Fe–Zr isothermal sections between 1273 and 1573 K have been experimentally studied by Wang et al.^[11], and the Co–Fe, Co–Zr and Fe–Zr subsystems have been thermodynamically assessed by several researchers.^[12–14] Whereas the Co–Zr thermodynamic parameters^[13] still need to be adjusted because of the inappropriate thermodynamic model of CoZr and low-temperature decomposition of CoZr_3 . As a result, the current study is aimed to develop reasonable thermodynamic descriptions and obtain a self-consistent set of thermodynamic parameters for the Co–Zr and Co–Fe–Zr systems using the CALPHAD approach.

2 Literature Review

2.1 Co–Fe System

Guillemet,^[15] Ohnuma et al.^[16] and Turchanin et al.^[17] carried out the thermodynamic studies of the Co–Fe system, but their calculated magnetic properties did not completely reproduce the experimental data.^[18–20] Wang et al.^[12] conducted the first-principles calculations and heat

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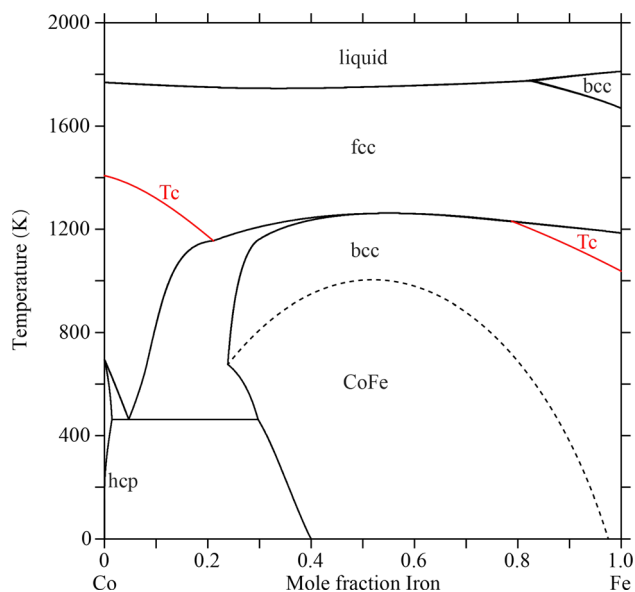


Fig. 1 Co–Fe phase diagram assessed by Wang et al.^[12]

capacity measurements and performed a detailed thermodynamic assessment of the Co–Fe system. Their thermodynamic parameters^[12] are directly adopted in the current work. Fig. 1 presents the Co–Fe phase diagram assessed by Wang et al.^[12]

2.2 Co–Zr System

Chart and Putland,^[21] Saunders and Miodownik^[22] and Bratberg and Jansson^[23] performed the early thermodynamic optimizations of the Co–Zr system, but the thermochemical data were not considered in their work. Liu et al.^[24] carried out the detailed experimental determination and proper thermodynamic assessment of the Co–Zr system; however, the reported mixing enthalpies of liquid phase^[25–27] were still not taken into consideration. Durga and Kumar^[28] first coupled bcc_A2 and CoZr using an order-disorder model and improved the Co–Zr thermodynamic description. Kosorukova et al.^[29] and Semenova et al.^[30] performed the experimental investigations on the controversial part of the Co–Zr phase diagram including the phase transition and phase stability of CoZr₃. Given the available phase equilibria and thermochemical information^[24–37], Agraval et al.^[13] conducted a novel Co–Zr thermodynamic assessment. Nevertheless, the thermodynamic parameters of CoZr and CoZr₃^[13] still required to be revised to match the common model of the order-disorder transition and avoid the low-temperature decomposition of CoZr₃. As a result, the Co–Zr thermodynamic modeling is updated in this work.

The Co–Zr phase diagram was first studied by Pechin et al.,^[31] who identified the five compounds Co₁₁Zr₂, Co₄Zr (also called as Co₂₃Zr₆), λ₂, CoZr and CoZr₂. Bataleva et al.^[32] used metallography, EPMA, XRD and DTA to carry out the experimental study on the Co–Zr phase diagram, especially the liquidus temperatures. The reported phase diagrams^[31, 32] were contradictory in the Zr-rich part owing to the presence of CoZr₃^[32]. Liu et al.^[24] adopted the same method as Bataleva et al.^[32] to measure the phase equilibria of the Co–Zr system in the complete composition ranges above 1073 K. CoZr₃ was found to form peritectically from liquid + bcc_A2 at 1253 K,^[32] but peritectoidally from CoZr₂ + bcc_A2 at 1254 K.^[24] Kosorukova et al.^[29] also reported the temperatures of four invariant reactions using metallography, XRD and DTA. Semenova et al.^[30] determined the CoZr₂–Zr region of the Co–Zr phase diagram using the same methods as Kosorukova et al.,^[29] and their experimental results supported the conclusion^[24] that CoZr₃ formed by the peritectoid reaction CoZr₂ + bcc_A2 → CoZr₃ at 1254 K. For the development of the present description, all phase equilibria data^[24, 29–32] are considered.

The enthalpies of formation of the Co–Zr compounds were studied by several researchers using direct synthesis reaction calorimetry^[33, 34], differential calorimetry,^[35] solution calorimetry^[36] and first-principles calculations^[37]. In the update process, the reported thermochemical data related to CoZr, CoZr₂ and CoZr₃ are taken into consideration.

2.3 Fe–Zr System

The early thermodynamic studies of the Fe–Zr system were performed by Servant et al.^[38] and Jiang et al.^[39] The Fe–Zr phase diagram was measured using metallography, EPMA, XRD and DTA by Stein et al.,^[40] who suggested that Fe₂₃Zr₆ should be a metastable phase and its existence in the Fe–Zr system was mainly due to the stabilization of oxygen. Guo et al.^[41] accepted their experimental results^[40] and then performed a new thermodynamic assessment of the Fe–Zr system. But Yang et al.^[42] and Lu et al.^[43] thought Fe₂₃Zr₆ as a stable phase and re-modeled the Fe–Zr system. Saenko et al.^[14] considered the experimental and theoretical thermochemical properties,^[44–46] determined the heat capacity of FeZr₂ from 220 to 450 K, agreed with Stein et al.^[40] that Fe₂₃Zr₆ was not an equilibrium phase, and carried out the thermodynamic remodeling of the Fe–Zr system. Their calculated results reproduced the experimental data better, hence the thermodynamic parameters of Saenko et al.^[14] are directly

adopted in this work. Fig. 2 is the Fe–Zr phase diagram assessed by Saenko et al.^[14]

2.4 Co–Fe–Zr System

The isothermal section of the Co–Fe–Zr system at 1273 K was reported by Panteleimonov et al.,^[47] Two continuous solid solutions (Co,Fe)Zr₂ and λ₂ and three three-phase regions (Co,Fe)Zr₂ + λ₂ + CoZr, λ₂ + Co₄Zr + Fe₃Zr and Co₄Zr + Fe₃Zr + fcc(Co,Fe) were identified, but the stability of FeZr₂ was inconsistent with that in the Fe–Zr system^[40]. Mishenina et al.^[48] investigated some equilibrated alloys to determine the Co–Fe–Zr isothermal section

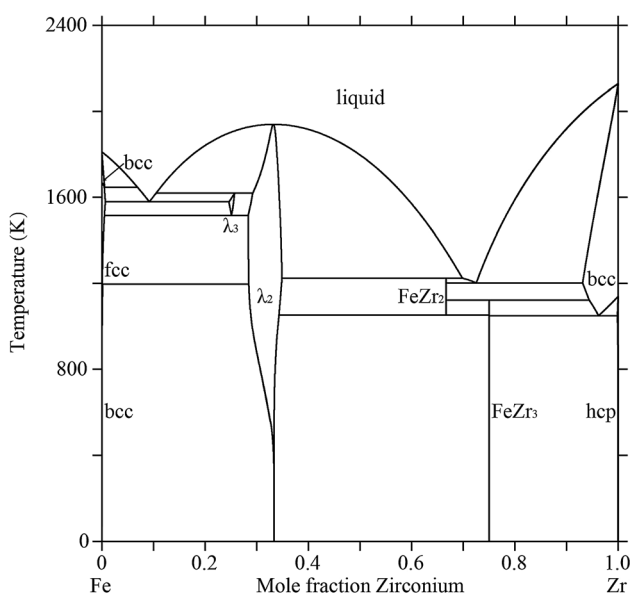


Fig. 2 Fe–Zr phase diagram assessed by Saenko et al.^[14]

at 770 K, but the FeZr₂ stability was also in discrepancy with that in the Fe–Zr system^[40]. In addition, Mishenina et al.^[48] did not report the bcc_A2/CoFe phase boundaries from the Co–Fe system and the occurrence of Co₁₁Zr₂ and CoZr₃. Wang et al.^[11] measured four isothermal sections in the entire composition ranges at 1273, 1373, 1473 and 1573 K utilizing metallography, EPMA, XRD and DSC, in which liquid and λ₂ formed the continuous solid solutions between 1273 and 1573 K from the Co–Zr to Fe–Zr corner. Four reported isothermal sections^[11] are in good accordance with the corresponding subsystems and thus accepted in the optimization process.

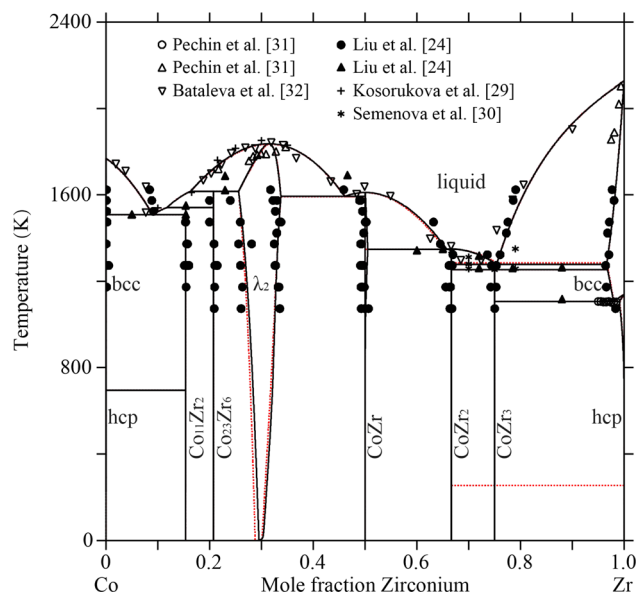


Fig. 3 Calculated Co–Zr phase diagram (solid line) compared with the previous work^[13] (dotted line) and experimental data.^[21, 26–29]

Table 1 The crystal structures and thermodynamic models of each phase in the Co–Fe–Zr system

Phase	Strukturbericht designation	Pearson symbol	Space group	Prototype	Thermodynamic model
Liquid	(Co,Fe,Zr) ₁
fcc(Co,Fe)	A1	cF4	Fm $\bar{3}m$	Cu	(Co,Fe,Zr) ₁ Va ₁
hcp(Co,Zr)	A3	hP2	P63/mmc	Mg	(Co,Fe,Zr) ₁ Va _{0.5}
bcc(Fe,Zr)	A2	cI2	Im $\bar{3}m$	W	(Co,Fe,Va,Zr) ₁ Va ₃
CoFe/CoZr	B2	cP2	Pm $\bar{3}m$	CsCl	(Co,Fe,Va,Zr) _{0.5} (Co,Fe,Va,Zr) _{0.5} Va ₃
Co ₁₁ Zr ₂	(Co,Fe) ₁₁ Zr ₂
(Co,Fe) ₂₃ Zr ₆	D8 _a	cF116	Fm $\bar{3}m$	Mn ₂₃ Th ₆	(Co,Fe) ₂₃ Zr ₆
λ ₂	C15	cF24	Fd $\bar{3}m$	MgCu ₂	(Co,Fe,Zr) ₂ (Co,Fe,Zr) ₁
(Co,Fe) ₁ Zr ₂	C16	tI12	I4/mcm	Al ₂ Cu	(Co,Fe) ₁ Zr ₂
(Co,Fe) ₁ Zr ₃	E1 _a	oC16	Cmcm	Re ₃ B	(Co,Fe) ₁ Zr ₃
λ ₃	C36	hP24	P63/mmc	MgNi ₂	(Co,Fe,Zr) ₂ (Co,Fe,Zr) ₁

Table 2 The invariant reactions in the Co–Zr system

Invariant reaction	T_i (K)	Compositions (at.%Zr)			References
		Phase 1	Phase 2	Phase 3	
liq. \rightarrow fcc(Co) + Co ₁₁ Zr ₂	1507	9.0	0.01	15.4	This work 13
	1503	9.5	31
	1513	9.0	32
	1503	24
liq. + Co ₂₃ Zr ₆ \rightarrow Co ₁₁ Zr ₂	1540	11.8	20.7	15.4	This work 13
	1543	31
	1543	32
	1544	24
	1553	29
liq. + λ_2 \rightarrow Co ₂₃ Zr ₆	1615	16.3	25.6	20.7	This work 31
	1723	32
	1623	24
	1616	13
liq. \rightarrow λ_2	1615	16.3	25.6	20.7	This work 32
	1836	31.5	31.5	...	13
	1833	31
liq. \rightarrow λ_2 + CoZr	1835	31.5	31.5	...	This work 32
	1592	46.1	33.8	50.0	13
	1583	46.6	This work 31
	1533	46.0	32
liq. \rightarrow CoZr	1586	24
	1591	46.1	33.8	50.0	13
	1610	50.0	50.0	...	This work 32
	1643	13
liq. \rightarrow CoZr + CoZr ₂	1610	50.0	50.0	–	This work 31
	1348	65.8	50.5	66.7	32
	1333	65.0	24
	1313	64.0	13
	1337	This work 31
liq. \rightarrow CoZr ₂	1348	65.5	50.0	66.7	32
	1349	66.7	66.7	...	13
	1363	This work 30
	1343	31
liq. \rightarrow CoZr ₂ + bcc(Zr)	1349	66.7	66.7	...	13
	1279	75.4	66.7	96.6	This work 31
	1253	78.5	24
	1258	29
	1303	75.4	30
	1259	78.0	13
fcc(Co) + Co ₁₁ Zr ₂ \rightarrow hcp(Co)	1284	75.5	66.7	96.7	This work 13
	695	0.01	15.4	0.01	31
CoZr ₂ + bcc(Zr) \rightarrow CoZr ₃	1279	75.4	66.7	96.6	This work 31
	1254	66.7	96.8	75.0	24
	1254	29
	1251	30
	1254	13
bcc(Zr) \rightarrow CoZr ₃ + hcp(Zr)	1254	66.7	96.9	75.0	This work 32
	1106	97.9	75.0	99.0	24
	1103	29
	1111	13
	1103	31
	1106	98.0	75.0	99.1	13

Table 3 The enthalpies of formation of the Co–Zr compounds

Phase	T, K	Enthalpies of formation (J/mol of atoms)	References
Co ₁₁ Zr ₂	298	−23944	13, This work
Co ₂₃ Zr ₆	1596	−29800 ± 1500	33
λ ₂	0	−21900	37
	298	−28642	13, This work
	1708	−41000 ± 1600	33
	298	−37667 ± 3667	36
	298	−35800 ± 600	34
	0	−31680	37
	298	−31920	13
	1708	−37261	This work
	298	−31775	This work
	CoZr	1512	−42200 ± 1000
1030		−43050 ± 3900	35
298		−35800 ± 700	34
0		−28830	37
298		−35326	13
1512		−40267	This work
298		−35694	This work
298		−35694	This work
CoZr ₂	1290	−33000 ± 2000	33
	298	−26400 ± 1000	34
	0	−26300	37
	298	−30745	13
	1290	−32547	This work
	298	−28946	This work
CoZr ₃	0	−22440	37
	298	−23010	13, This work

3 Thermodynamic Models

3.1 Unary Phases

The lattice stability parameters of Co, Fe and Zr were taken from the SGTE Pure 5.1 Database.^[49]

3.2 Solution Phases

The substitutional solution model was adopted to describe the solution phases ϕ (ϕ = liquid, fcc_A1, bcc_A2 and hcp_A3):

$$G_m^\phi(T) = \sum_i x_i G_i^\phi(T) + RT \sum_i x_i \ln x_i + {}^E G_m^\phi + {}^{mag} G_m^\phi \tag{Eq 1}$$

where x_i represents the molar fraction of i (i = Co, Fe, Zr); means the excess Gibbs energy, generally expanded using a Redlich–Kister type polynomial;^[50] ${}^{mag} G_m^\phi$ presents the magnetic part of the Gibbs energy, expanded using a Hillert–Jarl type formalism.^[51]

$$\begin{aligned} {}^E G_m^\phi = & x_{Co} x_{Fe} \sum_j {}^j L_{Co,Fe}^\phi (x_{Co} - x_{Fe})^j \\ & + x_{Co} x_{Zr} \sum_j {}^j L_{Co,Zr}^\phi (x_{Co} - x_{Zr})^j \\ & + x_{Fe} x_{Zr} \sum_j {}^j L_{Fe,Zr}^\phi (x_{Fe} - x_{Zr})^j \\ & + x_{Co} x_{Fe} x_{Zr} (x_{Co} {}^0 L_{Co,Fe,Zr}^\phi \\ & + x_{Fe} {}^1 L_{Co,Fe,Zr}^\phi + x_{Zr} {}^2 L_{Co,Fe,Zr}^\phi) \end{aligned} \tag{Eq 2}$$

where the j th interaction parameters ${}^j L_{Co,Fe}^\phi$, ${}^j L_{Co,Zr}^\phi$, ${}^j L_{Fe,Zr}^\phi$, ${}^j L_{Co,Fe,Zr}^\phi$ are taken from Refs.^[12–14] or optimized in the present work.

3.3 Intermetallic Phases

Two Laves phases were described as (Co,Fe,Zr)₂-(Co,Fe,Zr)₁ using a usual two-sublattice model. Moreover, four intermetallic phases Co₁₁Zr₂, (Co,Fe)₂₃Zr₆, (Co,Fe)₁-Zr₂ and (Co,Fe)₁Zr₃ were modeled as the line compounds in the formula (Co,Fe) _{m} Zr _{n} due to their limited

Table 4 The thermodynamic parameters in the Co–Fe–Zr system

Phase	Thermodynamic parameters	References	
Liquid	${}^0L_{\text{Co,Fe}}^{\text{liq}} = -9939.0 + 3.2900T$	12	
	${}^1L_{\text{Co,Fe}}^{\text{liq}} = -1713.0 + 0.9100T$	12	
	${}^2L_{\text{Co,Fe}}^{\text{liq}} = +1271.0$	12	
	${}^0L_{\text{Co,Zr}}^{\text{liq}} = -145951.0 + 20.0000T$	13	
	${}^1L_{\text{Co,Zr}}^{\text{liq}} = -12061.8 - 5.3370T$	13	
	${}^2L_{\text{Co,Zr}}^{\text{liq}} = +5415.8$	13	
	${}^0L_{\text{Fe,Zr}}^{\text{liq}} = -85196.3 + 12.8300T$	14	
	${}^1L_{\text{Fe,Zr}}^{\text{liq}} = -1655.5$	14	
	${}^0L_{\text{Co,Fe,Zr}}^{\text{liq}} = -110919.3 + 83.1767T$	This work	
	${}^1L_{\text{Co,Fe,Zr}}^{\text{liq}} = -172919.3 + 83.1767T$	This work	
	${}^2L_{\text{Co,Fe,Zr}}^{\text{liq}} = -137419.3 + 83.1767T$	This work	
	fcc_A1	${}^0L_{\text{Co,Fe}}^{\text{fcc_A1}} = -9112.0 + 3.3000T$	12
${}^2L_{\text{Co,Fe}}^{\text{fcc_A1}} = +1667.0$		12	
${}^0T_{\text{cCo,Fe}}^{\text{fcc_A1}} = +283$		12	
${}^2T_{\text{cCo,Fe}}^{\text{fcc_A1}} = +879$		12	
${}^0\beta_{\text{Co,Fe}}^{\text{fcc_A1}} = +8.9$		12	
${}^2\beta_{\text{Co,Fe}}^{\text{fcc_A1}} = -3.9$		12	
${}^0L_{\text{Fe,Zr}}^{\text{fcc_A1}} = -16847.9 - 3.5600T$		14	
bcc_A2 (disordered part of B2)	$G_{\text{Va}}^{\text{bcc_A2}} = +30T$	12	
	${}^0L_{\text{Co,Va}}^{\text{bcc_A2}} = +126184.0$	12	
	${}^0L_{\text{Fe,Va}}^{\text{bcc_A2}} = +150000.0$	12	
	${}^0L_{\text{Zr,Va}}^{\text{bcc_A2}} = +150000.0$	This work	
	${}^0L_{\text{Co,Fe}}^{\text{bcc_A2}} = -20205.0 + 14.8000T + 0.9845T \times \ln T - 0.0076434T^2$	12	
	${}^2L_{\text{Co,Fe}}^{\text{bcc_A2}} = +1316.0$	12	
	${}^0T_{\text{cCo,Fe}}^{\text{bcc_A2}} = +590$	12	
	${}^0\beta_{\text{Co,Fe}}^{\text{bcc_A2}} = +1.5$	12	
	${}^2\beta_{\text{Co,Fe}}^{\text{bcc_A2}} = -0.6$	12	
	${}^0L_{\text{Co,Zr}}^{\text{bcc_A2}} = -79348.0 + 23.3360T$	13	
	${}^0L_{\text{Fe,Zr}}^{\text{bcc_A2}} = -33690.0 + 8.7700T$	14	
	${}^1L_{\text{Fe,Zr}}^{\text{bcc_A2}} = -11176.6 + 7.6300T$	14	
	bcc_B2	$G_{\text{Co,Fe}}^{\text{bcc_B2}} = G_{\text{Fe,Co}}^{\text{bcc_B2}} = -1245.0 - 1.8900T$	12
		${}^0L_{\text{Fe,Co,Fe}}^{\text{bcc_B2}} = {}^0L_{\text{Co,Fe,Fe}}^{\text{bcc_B2}} = -872.0$	12
$T_{\text{cCo,Fe}}^{\text{bcc_B2}} = T_{\text{cFe,Co}}^{\text{bcc_B2}} = +370$		12	
$\beta_{\text{Co,Fe}}^{\text{bcc_B2}} = \beta_{\text{Fe,Co}}^{\text{bcc_B2}} = +0.14$		12	
${}^0T_{\text{cCo,Co,Fe}}^{\text{bcc_B2}} = {}^0T_{\text{cCo,Fe,Co}}^{\text{bcc_B2}} = {}^0T_{\text{cFe,Co,Fe}}^{\text{bcc_B2}} = {}^0T_{\text{cCo,Fe,Fe}}^{\text{bcc_B2}} = -370$		12	
$G_{\text{Co,Zr}}^{\text{bcc_B2}} = G_{\text{Zr,Co}}^{\text{bcc_B2}} = -34937.0 - 3.7845T$		This work	
${}^0L_{\text{Zr,Co,Zr}}^{\text{bcc_B2}} = {}^0L_{\text{Co,Zr,Zr}}^{\text{bcc_B2}} = +20000.0$		This work	
$G_{\text{Fe,Zr}}^{\text{bcc_B2}} = G_{\text{Zr,Fe}}^{\text{bcc_B2}} = -29679.4 + 5.6578T$		This work	
${}^0L_{\text{Zr,Co,Fe}}^{\text{bcc_B2}} = {}^0L_{\text{Co,Fe,Zr}}^{\text{bcc_B2}} = -2816.9 - 6.9789T$		This work	
${}^1L_{\text{Zr,Co,Fe}}^{\text{bcc_B2}} = {}^1L_{\text{Co,Fe,Zr}}^{\text{bcc_B2}} = +4346.2 - 8.1181T$		This work	
${}^0T_{\text{cZr,Co,Fe}}^{\text{bcc_B2}} = {}^0T_{\text{cCo,Fe,Zr}}^{\text{bcc_B2}} = -370$	This work		

Table 4 continued

Phase	Thermodynamic parameters	References	
hcp_A3	${}^0L_{\text{Co,Fe}}^{\text{hcp_A3}} = -8500.0 + 7.0000T$	12	
	${}^1L_{\text{Co,Fe}}^{\text{hcp_A3}} = -800.0$	12	
	${}^0T_{\text{cCo,Fe}}^{\text{hcp_A3}} = -253$	12	
	${}^2T_{\text{cCo,Fe}}^{\text{hcp_A3}} = +1494$	12	
	${}^0\beta_{\text{Co,Fe}}^{\text{hcp_A3}} = -0.78$	12	
	${}^2\beta_{\text{Co,Fe}}^{\text{hcp_A3}} = +1.54$	12	
	${}^0L_{\text{Co,Zr}}^{\text{hcp_A3}} = -43000.0$	This work	
	${}^0L_{\text{Fe,Zr}}^{\text{hcp_A3}} = +5769.6$	14	
	$\text{Co}_{11}\text{Zr}_2$	$G_{\text{Co:Zr}}^{\text{Co}_{11}\text{Zr}_2} = +11\text{GHSER}_{\text{Co}} + 2\text{GHSER}_{\text{Zr}} - 405002.0 + 89.7390T$	13
		$G_{\text{Fe:Zr}}^{\text{Co}_{11}\text{Zr}_2} = +11\text{GHSER}_{\text{Fe}} + 2\text{GHSER}_{\text{Zr}} - 240011.8 + 55.2912T$	This work
${}^0L_{\text{Co,Fe:Zr}}^{\text{Co}_{11}\text{Zr}_2} = +526887.8 - 378.7426T$		This work	
$(\text{Co,Fe})_{23}\text{Zr}_6$	$G_{\text{Co:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} = +23\text{GHSER}_{\text{Co}} + 6\text{GHSER}_{\text{Zr}} - 1026600 + 162.4000T$	13	
	$G_{\text{Fe:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} = +23\text{GHSER}_{\text{Fe}} + 6\text{GHSER}_{\text{Zr}} - 680411.0 + 123.3419T$	This work	
	${}^0L_{\text{Co,Fe:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} = -69757.7 - 92.4928T$	This work	
	${}^1L_{\text{Co,Fe:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} = +338832.1 - 167.8839T$	This work	
	${}^2L_{\text{Co,Fe:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} = -49983.2$	This work	
λ_2	$G_{\text{Co:Co}}^{\lambda_2} = +3\text{GHSER}_{\text{Co}} + 15000.0$	13	
	$G_{\text{Co:Zr}}^{\lambda_2} = +2\text{GHSER}_{\text{Co}} + \text{GHSER}_{\text{Zr}} - 112008.0 + 2.9100T$	13	
	$G_{\text{Zr:Co}}^{\lambda_2} = +G_{\text{Co:Co}}^{\lambda_2} + G_{\text{Zr:Zr}}^{\lambda_2} - G_{\text{Co:Zr}}^{\lambda_2}$	13	
	$G_{\text{Zr:Zr}}^{\lambda_2} = +3\text{GHSER}_{\text{Zr}} + 15000.0$	13	
	${}^0L_{\text{Co:Co,Zr}}^{\lambda_2} = -111925.0 + 58.0000T$	This work	
	${}^1L_{\text{Co:Co,Zr}}^{\lambda_2} = +45000.0$	13	
	$G_{\text{Fe:Fe}}^{\lambda_2} = +3\text{GHSER}_{\text{Fe}} + 15000.0$	14	
	$G_{\text{Co:Fe}}^{\lambda_2} = +2\text{GHSER}_{\text{Co}} + \text{GHSER}_{\text{Fe}} + 15000.0$	This work	
	$G_{\text{Fe:Co}}^{\lambda_2} = +G_{\text{Co:Co}}^{\lambda_2} + G_{\text{Fe:Fe}}^{\lambda_2} - G_{\text{Co:Fe}}^{\lambda_2}$	This work	
	$G_{\text{Fe:Zr}}^{\lambda_2} = -112156.0 + 438.6000T - 79.1130T \times \ln T - 0.0068T^2 + 330106T^{-1}$	14	
	$G_{\text{Zr:Fe}}^{\lambda_2} = -G_{\text{Fe:Zr}}^{\lambda_2} + 30000.0$	14	
	${}^0L_{\text{Fe:Fe,Zr}}^{\lambda_2} = -23000.0 + 22.5000T$	14	
	${}^0L_{\text{Fe,Zr:Zr}}^{\lambda_2} = +56000.0$	14	
	$T_{\text{cFe:Zr}}^{\lambda_2} = +585$	14	
	$\beta_{\text{Fe:Zr}}^{\lambda_2} = +1.4$	14	
	${}^0L_{\text{Co,Fe:Zr}}^{\lambda_2} = -92413.7 + 33.3198T$	This work	
	${}^1L_{\text{Co,Fe:Zr}}^{\lambda_2} = -36207.3 + 16.6599T$	This work	
$(\text{Co,Fe})_1\text{Zr}_2$	$G_{\text{Co:Zr}}^{(\text{Co,Fe})_1\text{Zr}_2} = +\text{GHSER}_{\text{Co}} + 2\text{GHSER}_{\text{Zr}} - 95360.2 + 10.4660T$	This work	
	$G_{\text{Fe:Zr}}^{(\text{Co,Fe})_1\text{Zr}_2} = +\text{GHSER}_{\text{Fe}} + 2\text{GHSER}_{\text{Zr}} - 44258.8 - 2.7322T$	14	
	${}^0L_{\text{Co,Fe:Zr}}^{(\text{Co,Fe})_1\text{Zr}_2} = +86785.1 - 73.2012T$	This work	
	${}^1L_{\text{Co,Fe:Zr}}^{(\text{Co,Fe})_1\text{Zr}_2} = +4496.8$	This work	

Table 4 continued

Phase	Thermodynamic parameters	References
(Co,Fe) ₁ Zr ₃	$G_{\text{Co:Zr}}^{(\text{Co,Fe})_1\text{Zr}_3} = +\text{GHSER}_{\text{Co}} + 3\text{GHSER}_{\text{Zr}} - 100563.2 + 13.9980T$	This work
	$G_{\text{Fe:Zr}}^{(\text{Co,Fe})_1\text{Zr}_3} = -80910.0 + 519.9000T - 97.8640T \times \ln T - 0.0141T^2 + 144141T^{-1}$	14
λ_3	$G_{\text{Fe:Fe}}^{\lambda_3} = +3\text{GHSER}_{\text{Fe}} + 15000.0$	14
	$G_{\text{Fe:Zr}}^{\lambda_3} = -113009.0 + 440.2000T - 79.1130T \times \ln T - 0.0068T^2 + 330106T^{-1}$	14
	$G_{\text{Zr:Fe}}^{\lambda_3} = -G_{\text{Fe:Zr}}^{\lambda_3} + 30000.0$	14
	$G_{\text{Zr:Zr}}^{\lambda_3} = +3\text{GHSER}_{\text{Zr}} + 15000.0$	14
	${}^0L_{\text{Fe:Fe:Zr}}^{\lambda_3} = -1533.1 + 3.0950T$	14
	${}^0L_{\text{Fe:Zr:Zr}}^{\lambda_3} = +56000.0$	14
	$G_{\text{Co:Co}}^{\lambda_3} = +3\text{GHSER}_{\text{Co}} + 15000.0$	This work
	$G_{\text{Co:Fe}}^{\lambda_3} = +2\text{GHSER}_{\text{Co}} + \text{GHSER}_{\text{Fe}} + 15000.0$	This work
	$G_{\text{Fe:Co}}^{\lambda_3} = +G_{\text{Co:Co}}^{\lambda_3} + G_{\text{Fe:Fe}}^{\lambda_3} - G_{\text{Co:Fe}}^{\lambda_3}$	This work
	$G_{\text{Co:Zr}}^{\lambda_3} = +2\text{GHSER}_{\text{Co}} + \text{GHSER}_{\text{Zr}} - 97008.0 + 2.9100T$	This work
	$G_{\text{Zr:Co}}^{\lambda_3} = +G_{\text{Co:Co}}^{\lambda_3} + G_{\text{Zr:Zr}}^{\lambda_3} - G_{\text{Co:Zr}}^{\lambda_3}$	This work

homogeneity ranges.^[11] Taking the Laves phase λ_2 as an example, its Gibbs energy is given as follows:

$$G_m^{\lambda_2} = \sum_r y'_r \sum_s y''_s G_{r:s}^{\lambda_2} + RT(2 \sum_r y'_r \ln y'_r + \sum_s y''_s \ln y''_s) + {}^E G_m^{\lambda_2} \quad (\text{Eq 3})$$

$${}^E G_m^{\lambda_2} = \sum_u \sum_v y'_u y'_v \sum_w \sum_j y''_w {}^j L_{u:v:w}^{\lambda_2} (y'_u - y'_v)^j + \sum_u \sum_v y''_u y''_v \sum_w \sum_j y'_w {}^j L_{w:u,v}^{\lambda_2} (y''_u - y''_v)^j \quad (\text{Eq 4})$$

where y'_* and y''_* are the site fractions of * (* = Co, Fe and Zr); $G_{r:s}^{\lambda_2}$ represent the Gibbs energy in its SER state, hcp_A3 for Co, bcc_A2 for Fe or hcp_A3 for Zr; ${}^j L_{u:v:w}^{\lambda_2}$ and ${}^j L_{w:u,v}^{\lambda_2}$ are the assessed j th interaction parameters in this work.

The triple-defect mechanism is important for bcc_B2 when considering its site ordering.^[52] In order to combine with bcc_B2, the vacancies should occupy sites on each sublattice in bcc_A2. Two intermetallic phases CoFe and CoZr had the ordered bcc_B2 crystal structure and a single Gibbs energy function derived by Ansara et al.^[53] was proposed to describe the disordered bcc_A2 and ordered bcc_B2 simultaneously:

$$G_m^{\text{bcc}} = G_m^{\text{bcc_A2}}(x_i) + \Delta G_m^{\text{bcc_B2}}(y'_i, y_i) = G_m^{\text{bcc_A2}}(x_i) + G_m^{\text{bcc_B2}}(y'_i, y_i) - G_m^{\text{bcc_B2}}(x_i) \quad (\text{Eq 5})$$

where $G_m^{\text{bcc_A2}}(x_i)$ means the Gibbs energy of bcc_A2; $G_m^{\text{bcc_B2}}(y'_i, y_i)$ and $G_m^{\text{bcc_B2}}(x_i)$ are the contribution of bcc_B2 and the one from bcc_A2 to bcc_B2, respectively. When $x_i = y'_i = y_i$ ($i = \text{Co, Fe, Va and Zr}$), the phase is bcc_A2, otherwise it would be bcc_B2.

4 Result and Discussion

In the present work, the Thermo-Calc software package^[54] is used for optimizing the Co–Zr and Co–Fe–Zr systems. The crystal structures and thermodynamic models of each phase are presented in Table 1.

In the optimization process, $\text{Fe}_{23}\text{Zr}_6$ is treated as a metastable phase in the Fe–Zr system according to the detailed experimental results^[40]. And the value a of $G_{\text{Fe:Zr}}^{(\text{Co,Fe})_{23}\text{Zr}_6} (=a + bT)$ is set to -680411.0 based on the reported enthalpy of formation from the ab-initio calculations^[43], and the value b is set to a suitable one to satisfy the metastable state in the Fe–Zr system.

Figure 3 and Table 2 present the calculated phase diagram and invariant reactions of the Co–Zr system superimposed with the previous work^[13] and experimental

Fig. 4 Calculated isothermal section at 1273 K of the Co–Fe–Zr system compared with the experimental data^[11].

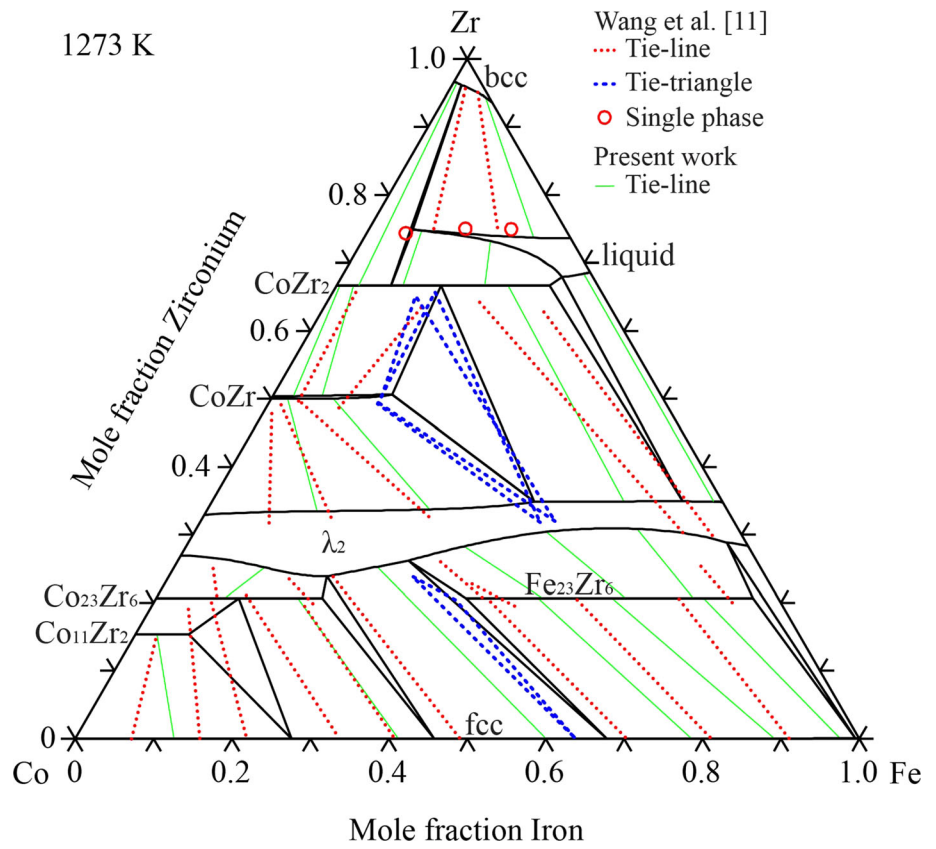


Fig. 5 Calculated isothermal section at 1373 K of the Co–Fe–Zr system compared with the experimental data^[11].

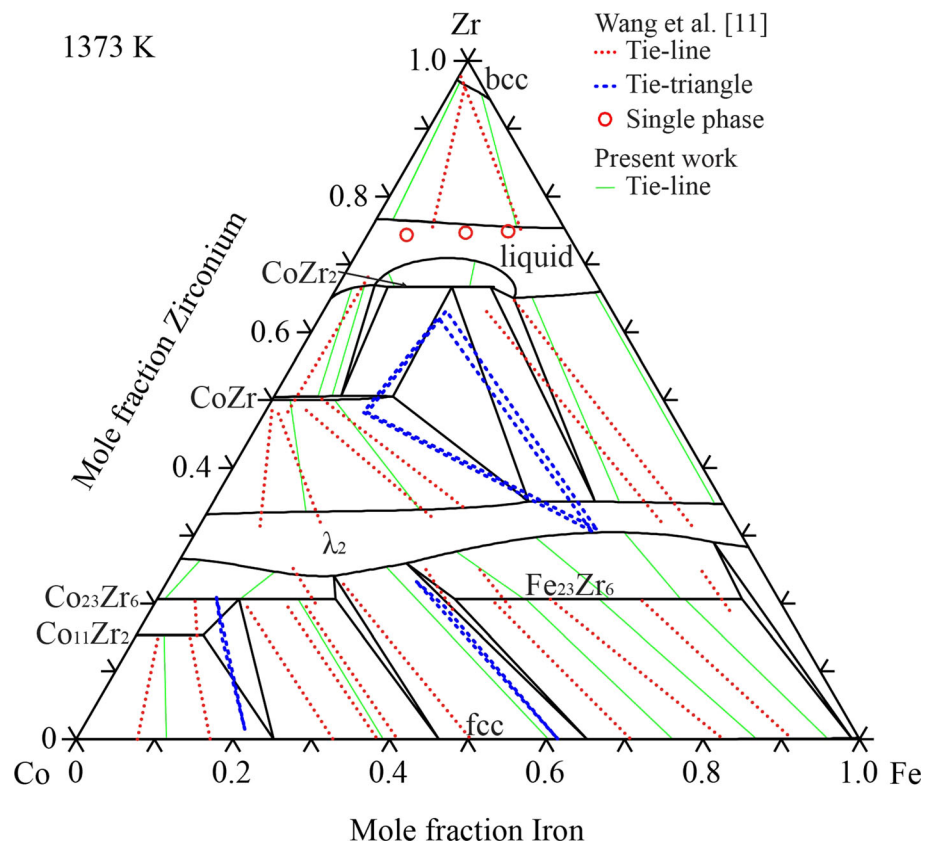


Fig. 6 Calculated isothermal section at 1473 K of the Co–Fe–Zr system compared with the experimental data^[11].

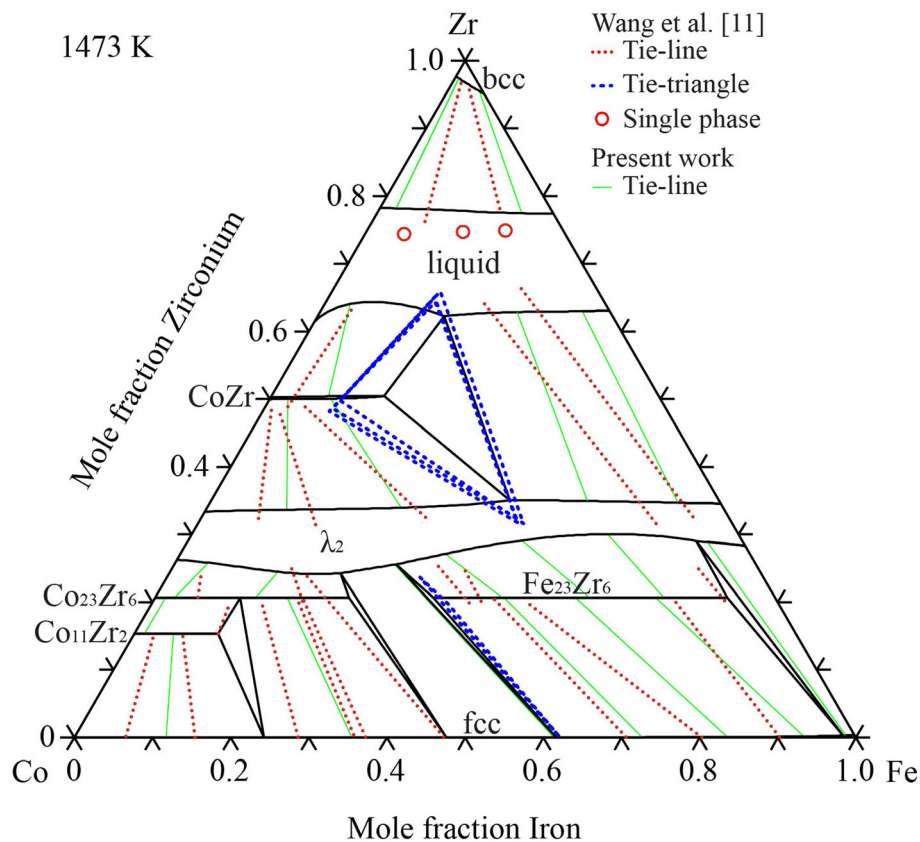


Fig. 7 Calculated isothermal section at 1573 K of the Co–Fe–Zr system compared with the experimental data^[11].

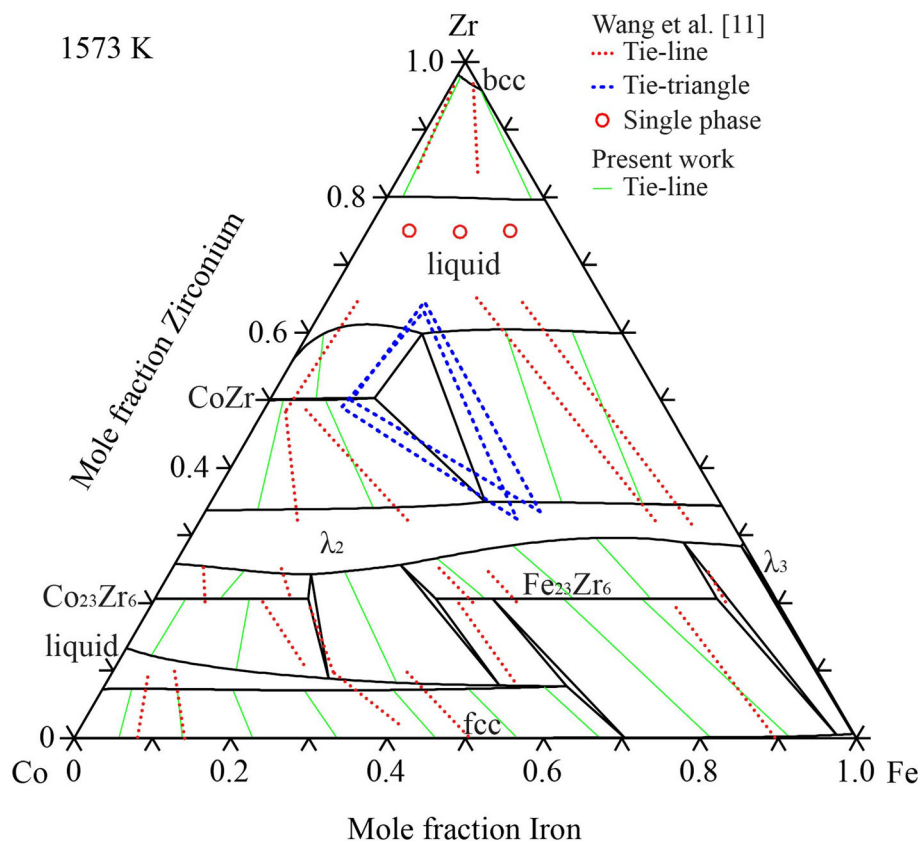


Fig. 8 Calculated liquidus surface projection of the Co–Fe–Zr system.

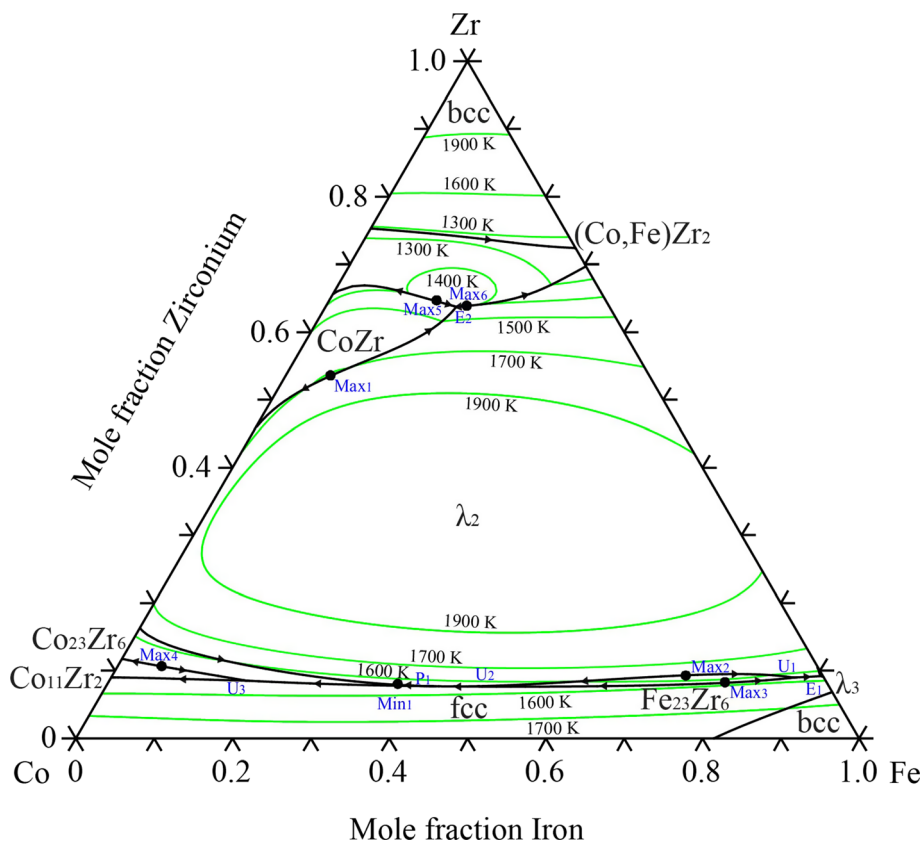


Table 5 Predicted invariant reactions involving liquid phase in the Co–Fe–Zr system

Reaction	Type	T,K	Liquid compositions at.%		
			Co	Fe	Zr
liq. + λ ₂ ↔ CoZr	p ₁ , Max ₁	1705	0.407	0.057	0.536
liq. + λ ₂ ↔ Fe ₂₃ Zr ₆	p ₂ , Max ₂	1627	0.175	0.732	0.093
liq. ↔ Fe ₂₃ Zr ₆ + fcc(Co,Fe)	e ₁ , Max ₃	1587	0.130	0.787	0.083
liq. ↔ λ ₂ + Co ₂₃ Zr ₆	e ₂ , Min ₁	1556	0.522	0.400	0.078
liq. ↔ Co ₂₃ Zr ₆ + Co ₁₁ Zr ₂	e ₃ , Max ₄	1543	0.837	0.056	0.107
liq. + CoZr ↔ (Co,Fe)Zr ₂	p ₃ , Max ₅	1408	0.217	0.137	0.646
liq. + λ ₂ ↔ (Co,Fe)Zr ₂	p ₄ , Max ₆	1402	0.184	0.177	0.639
liq. + Fe ₂₃ Zr ₆ ↔ λ ₂ + fcc(Co,Fe)	U ₁	1579	0.038	0.872	0.090
liq. ↔ λ ₂ + λ ₃ + fcc(Co,Fe)	E ₁	1577	0.003	0.905	0.092
liq. + Fe ₂₃ Zr ₆ ↔ λ ₂ + fcc(Co,Fe)	U ₂	1559	0.479	0.444	0.077
liq. + λ ₂ + fcc(Co,Fe) ↔ Co ₂₃ Zr ₆	P ₁	1557	0.506	0.417	0.077
liq. + Co ₂₃ Zr ₆ ↔ Co ₁₁ Zr ₂ + fcc(Co,Fe)	U ₃	1525	0.740	0.174	0.086
liq. ↔ (Co,Fe)Zr ₂ + CoZr + λ ₂	E ₂	1401	0.195	0.166	0.639

data.^[24, 29–32] In comparison with the former work,^[13] the low-temperature decomposition of CoZr₃ has been solved. The calculated enthalpies of formation of the Co–Zr compounds at 298 K in comparison with the previous work^[13] and experimental data^[33–37] are presented in Table 3. Nearly all the reported enthalpies of formation are well reproduced. The calculated enthalpy of formation of

CoZr₂ is more positive than the reported one^[13] to avoid the low-temperature decomposition of CoZr₃.

The Co–Fe–Zr thermodynamic parameters are summarized in Table 4. Figure. 4, 5, 6, 7 show the four calculated Co–Fe–Zr isothermal sections at 1273, 1373, 1473, and 1573 K together with the experimental data.^[11] Most of the experimental information is well reproducible, but there

still exist a few acceptable discrepancies. The calculated phase boundaries of the liquid phase at 1573 K show large inconsistency with the experimental data^[11] probably because of the experimental uncertainty at a very high temperature. With the stability limit of CoZr_2 at 1473 K, the two-phase region $\text{CoZr}_2 + \lambda_2$ at 1373 K is impossible to fully meet the experimental data.^[11] The three-phase regions $\text{Co}_{23}\text{Zr}_6 + \text{Co}_{11}\text{Zr}_2 + \text{fcc}(\text{Co,Fe})$ at 1273 and 1373 K disagree with the experimental information.^[11] Although great efforts were made, the value b of ${}^0L_{\text{Co,Fe:Zr}}^{\text{Co}_{11}\text{Zr}_2}$ ($=a + bT$) would need to be $-60 \text{ J}/(\text{mol K})$ to fit this three-phase region. This value leads to the occurrence of $\text{Co}_{11}\text{Zr}_2$ at 1573 K and cannot be accepted in this work. Therefore, further studies are recommended to determine the phase relations about $\text{Co}_{11}\text{Zr}_2$ below 1373 K. Additionally, the tie-lines $\lambda_2 + \text{Co}_{23}\text{Zr}_6$ at 1273, 1373, 1473, and 1573 K have some differences from the experimental data,^[11] which is due to the experimental homogeneity range and corresponding Gibbs energy of λ_2 .

The calculated liquidus surface projection and corresponding invariant reactions of the Co–Fe–Zr system are also shown in Fig. 8 and Table 5.

5 Conclusion

In the current study, the thermodynamic descriptions of the Co–Zr and Co–Fe–Zr systems have been carried out using the CALPHAD approach in accordance with the experimental phase equilibria and thermochemical information. There is a satisfactory agreement between the experimental and calculated results. The reliable Co–Fe–Zr thermodynamic parameters are first acquired, which can be used as a cost-effective tool for materials design and processing.

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